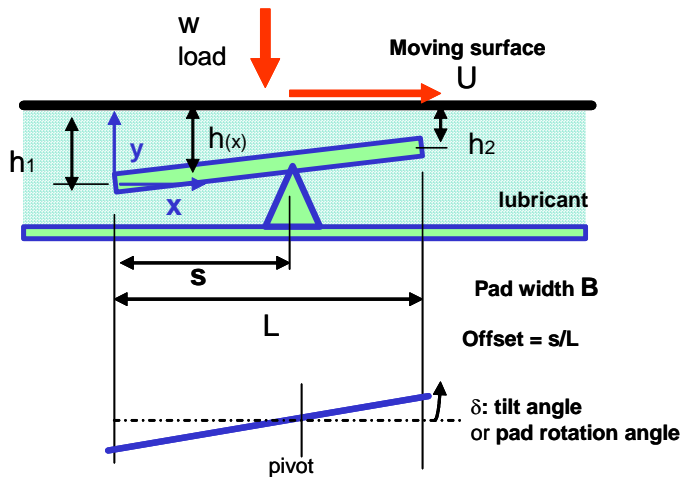


Performance of 1D-Tilting Pad Bearing

Luis San Andres (c) 2006, 2009



film thickness expression

$$h(x) := h_2 \cdot \left[\alpha + (1 - \alpha) \cdot \frac{x}{L} \right]^2 \quad \alpha := \frac{h_1}{h_2}$$

$$\delta = \frac{(h_1 - h_2)}{L}$$

U: surface speed - varies

Bearing geometry:

$L_w := 0.06$ m length and width of bearing

$B := 0.180$

offset := 0.59 pad pivot location s/L

Fluid properties $\mu_{in} := 0.0597$ Pa-sec $\rho := 878$ kg/m³ $c_p := 1880$ J/kg-degC

$\alpha_v := 0.0414$ 1/degC viscosity temperature coefficient

Operating conditions:

$T_{inlet} := 40$ degC - inlet temperature

$W := 40000$ N external load

$\kappa_T := 0.80$ thermal convection parameter
=0 isothermal

visc-Temperature relationship

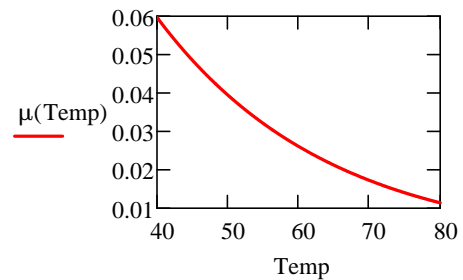
$$\mu(T) := \mu_{in} \cdot e^{-\alpha_v (T - T_{inlet})}$$

Convergence params in load (N), moment (Nm) & temp (degC):

$W_{eps} := 0.001$ (ratio)

$$M_{eps} := W \cdot \frac{\text{offset} \cdot L}{100000}$$

$T_{eps} := 0.01$ $M_{eps} = 0.01$



visc-Temperature relationship

Calculated performance (Vary runner surface speed)

$U_{min} := 2$ $U_{max} := 15$ [m/s]

Number of cases: $N_{cases} := 6$

EXPAND regions below to display code

▣ pad bearing parameters

$$\begin{aligned}
\text{Find_pars}(h_2, \alpha, U, T_{\text{out}}) := & \begin{cases} T_{\text{eff}} \leftarrow 0.5 \cdot (T_{\text{inlet}} + T_{\text{out}}) \\ \mu_{\text{eff}} \leftarrow \mu(T_{\text{eff}}) \\ q \leftarrow \frac{\alpha}{1 + \alpha} \\ p_{\text{max}} \leftarrow \frac{1}{4} \cdot \frac{(\alpha - 1)}{\alpha \cdot (1 + \alpha)} \\ w \leftarrow \frac{1}{(1 - \alpha)^2} \cdot \left[\ln(\alpha) + 2 \cdot \frac{(1 - \alpha)}{(1 + \alpha)} \right] \\ f \leftarrow -1 \cdot \left(\frac{6}{1 + \alpha} + 4 \cdot \frac{\ln(\alpha)}{1 - \alpha} \right) \\ t \leftarrow \frac{f}{q} \\ M_{\text{pad}} \leftarrow -6 \cdot \frac{[(1 - \alpha) \cdot (1 + 5 \cdot \alpha) + 2 \cdot \alpha \cdot (2 + \alpha) \cdot \ln(\alpha)]}{2 \cdot (1 - \alpha)^2 \cdot (1 - \alpha^2)} - \text{offset} \cdot 6 \cdot w \\ C_{\text{pre}} \leftarrow \mu_{\text{eff}} \cdot U \cdot \frac{L}{h_2^2} \\ \text{Force} \leftarrow 6 \cdot C_{\text{pre}} \cdot B \cdot L \cdot w \\ Q \leftarrow q \cdot U \cdot h_2 \cdot B \\ \text{ShearF} \leftarrow f \cdot C_{\text{pre}} \cdot B \cdot h_2 \\ \Delta T \leftarrow t \cdot \kappa_T \cdot \frac{C_{\text{pre}}}{(\rho \cdot c_p)} \\ T_{\text{out}} \leftarrow T_{\text{inlet}} + \Delta T \\ P_{\text{max}} \leftarrow p_{\text{max}} \cdot C_{\text{pre}} \cdot 6 \\ M_{\text{pad}} \leftarrow M_{\text{pad}} \cdot C_{\text{pre}} \cdot B \cdot L^2 \\ (h_2 \quad T_{\text{eff}} \quad \text{Force} \quad \text{ShearF} \quad Q \cdot 60000 \quad T_{\text{out}} \quad \mu_{\text{eff}} \quad P_{\text{max}} \quad M_{\text{pad}}) \end{cases}
\end{aligned}$$

From:

$$w(\alpha) := \frac{1}{(1 - \alpha)^2} \cdot \left[\ln(\alpha) + 2 \cdot \frac{(1 - \alpha)}{(1 + \alpha)} \right]$$

or

$$M_{\text{pad}}(\alpha) := -6 \cdot \frac{[(1 - \alpha) \cdot (1 + 5 \cdot \alpha) + 2 \cdot \alpha \cdot (2 + \alpha) \cdot \ln(\alpha)]}{2 \cdot (1 - \alpha)^2 \cdot (1 - \alpha^2)} - \text{offset} \cdot 6 \cdot w$$

For Pad moment to be null

$$6 \cdot \frac{[(1 - \alpha) \cdot (1 + 5 \cdot \alpha) + 2 \cdot \alpha \cdot (2 + \alpha) \cdot \ln(\alpha)]}{2 \cdot (1 - \alpha)^2 \cdot (1 - \alpha^2)} := -(\text{offset} \cdot 6 \cdot w) \quad \blacksquare$$

$$\text{Offset}(\alpha) := \frac{-[(1-\alpha) \cdot (1+5 \cdot \alpha) + 2 \cdot \alpha \cdot (2+\alpha) \cdot \ln(\alpha)]}{2 \cdot (1-\alpha)^2 \cdot (1-\alpha^2)}$$

$$\left[\frac{1}{(1-\alpha)^2} \cdot \left[\ln(\alpha) + 2 \cdot \frac{(1-\alpha)}{(1+\alpha)} \right] \right]$$

pad bearing parameters

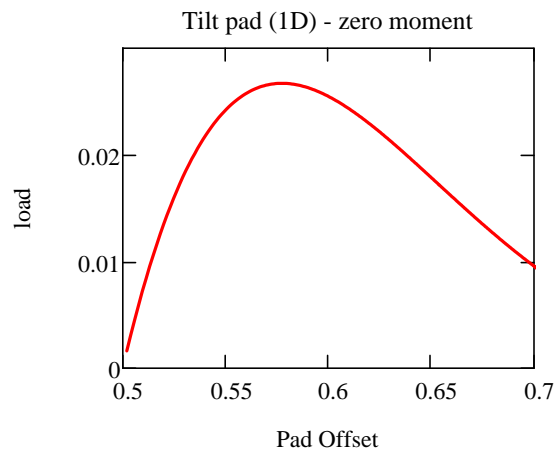
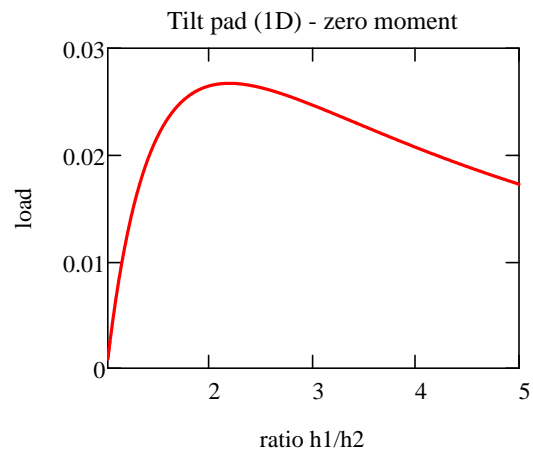
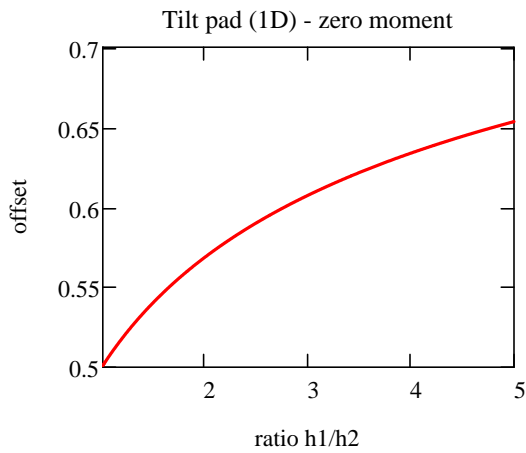


The following graphs show dimensionless parameters: load and offset needed for null moment versus film inlet/outlet ratio

Each pad offset determines a fixed α ratio satisfying the pad moment = 0.

Note that there is a certain offset given the optimum load, i.e.

(offset = 0.59) approximately



iterative loop

Guess values $i_{\max} := 199$ Max number of steps for convergence

$h_2 := 20 \cdot 10^{-6}$

$h_1 := 3 \cdot h_2$

$T_{\text{out}} := 50$

based on experience

GRAPHS of Tilting Pad Bearing Performance versus runner speed.

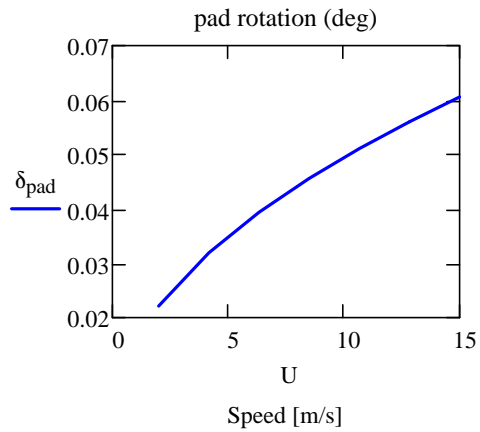
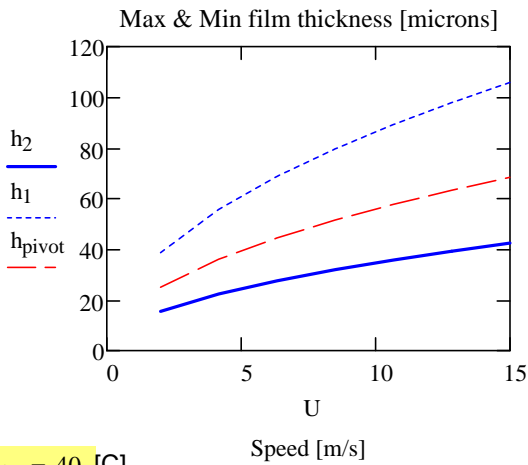
$W = 4 \times 10^4$ [N]

offset = 0.59

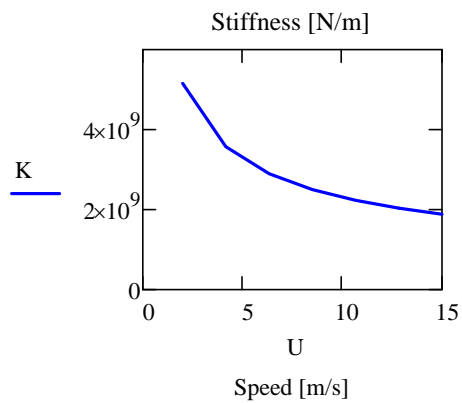
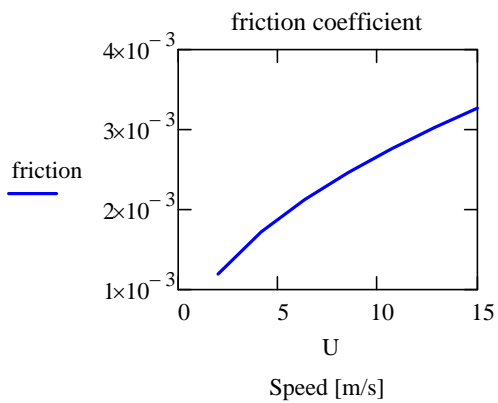
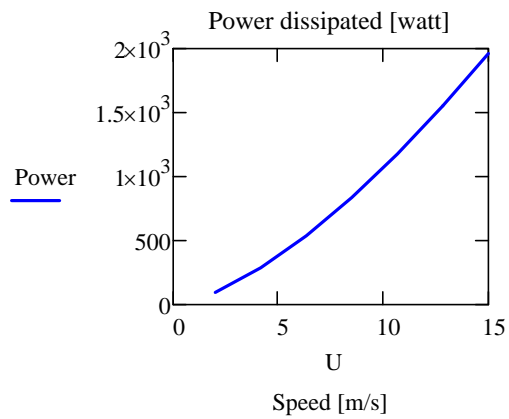
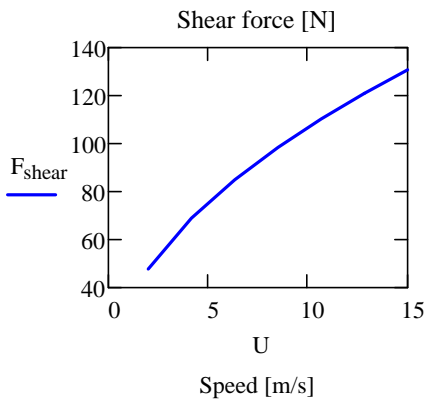
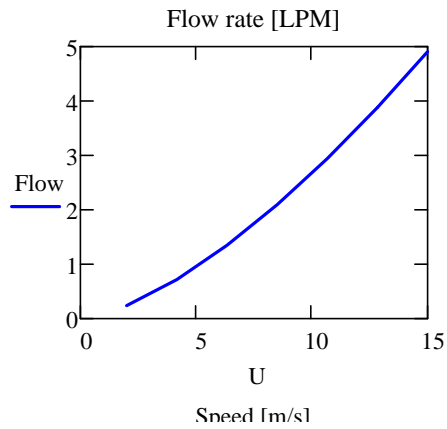
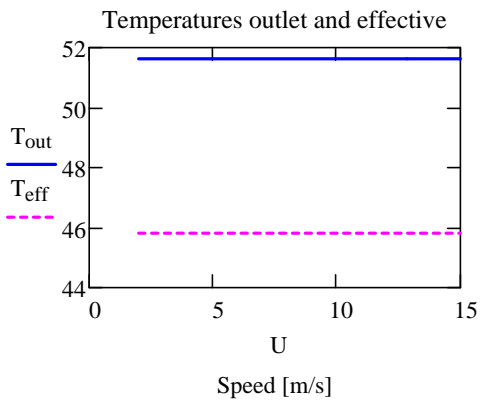
$\alpha_1 = 2.49$

$\max(h_2) = 42.42$

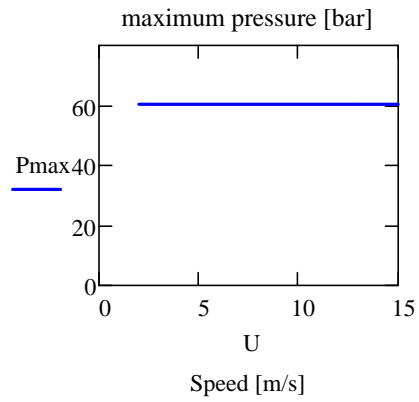
$\min(h_2) = 15.49$



$T_{inlet} = 40$ [C]



$P_{\text{spec}} = 37.04$ [bar] specific pressure = load/area



$i_{\text{max}} = 199$

