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A FEM APPROACH TO PREDICT ACOUSTIC RESONANCE IN MULTISTAGE CENTRIFUGAL PUMP

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Presenter/Author Bios

Francesco Annese- Engineering Manager

Team manager of a group dedicated to Centrifugal Pump hydraulic design and technical support to commercial operation for Baker Hughes. He joined GE in 2007 after 2 years' experience as design engineer for gas metering systems. Mr. Annese holds a M.S degree (mechanical engineering) from the Politecnico di Bari.

Rita Brizzi – Lead Hydraulic Design Engineer

Lead hydraulic design engineer in the Engineering team for Baker Hughes. She joined GE in 2011 after a 3 years' experience as Static Equipment and Heaters design engineer. Ms. Brizzi holds a M.S degree (mechanical engineering) from the Politecnico di Bari. Simone Bruno– Lead Customer Application Engineer Lead Customer AE in ITO team for Baker Hughes. He joined GE in 2011 after a 4 years' experienceas structural design engineer. For 8 years he worked as Lead Hydraulic Engineer in R&D and OTR Eng team. Dr. Bruno holds a M.S. degree (mechanical engineering) in 2002 and a PhD (mechanical engineering) in 2006 from the Politecnico di Bari.



CONCLUSIONS

VALIDATION OF NEW METHOD OF ANALYSIS

CASE STUDY 2

FEM ANALYSIS OF CASE STUDY 1

CASE STUDY 1

INTRODUCTION

CASE STUDY 1 FEM ANALYSIS OF CASE STUDY 1 CASE STUDY 2 VALIDATION OF NEW METHOD OF ANALYSIS CONCLUSIONS

INTRODUCTION

INTRODUCTION

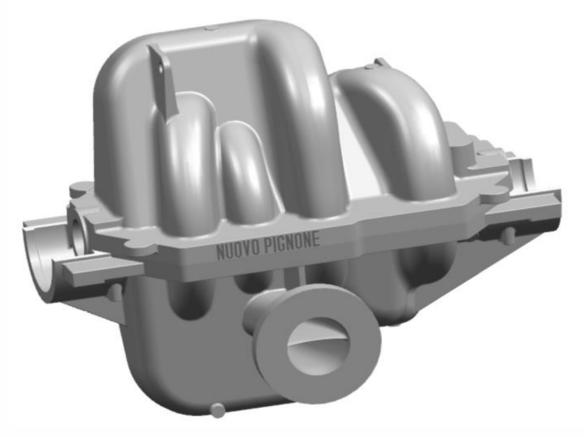
- In the past, minimal consideration of pressure pulsation
- Experimental estimation of active length and correlation
- Wider range of velocity increased the possibility to match the natural frequencies of the system
- Low accuracy of prediction related to the uncertainties of the fluid characteristics and active length
- Small change in the working conditions can produce a significant effect



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For an Ammonia project:

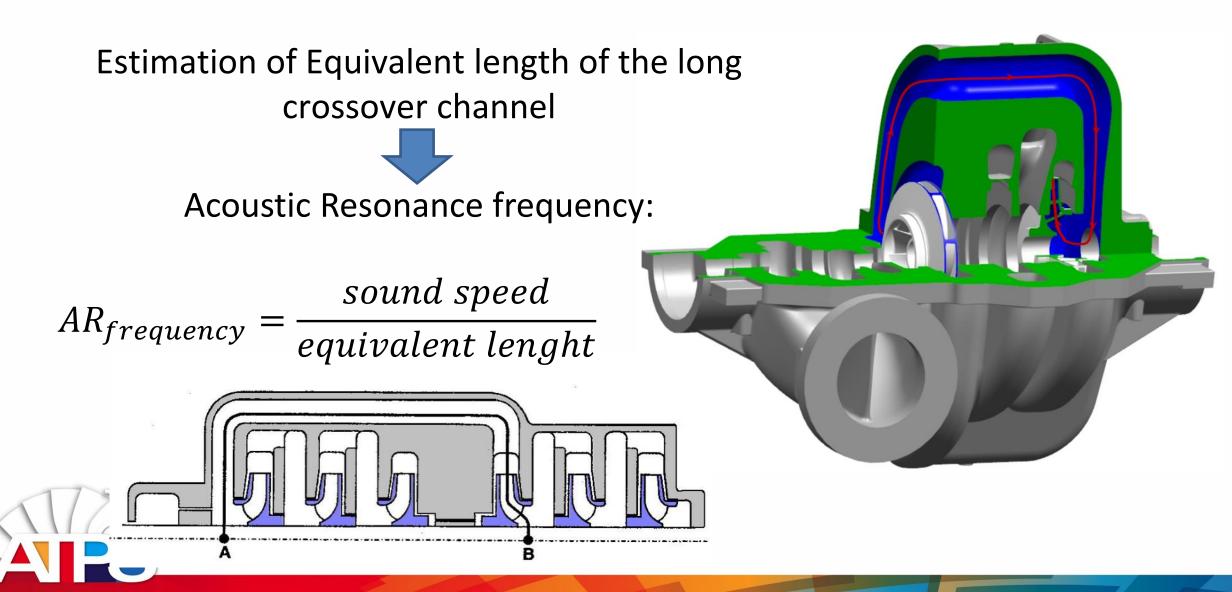
- 8x13 BB3 (Axially split, multistage, between bearing)
- double suction
- 3 stages
- 3000 rpm





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FEM APPROACH TO PREDICT ACOUSTIC RESONANCE IN MULTISTAGE CENTRIFUGAL PUMP



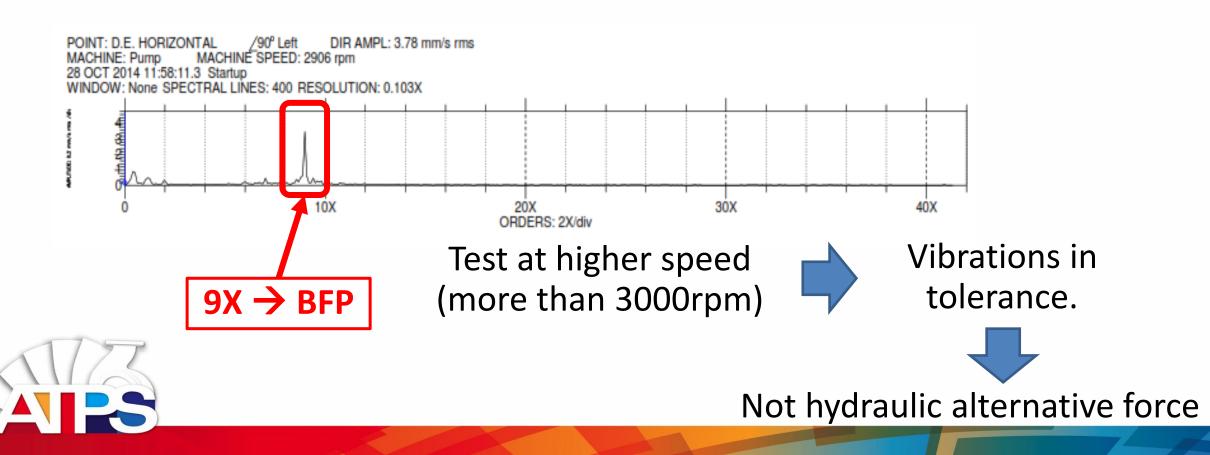
HOUSTON we have a problem

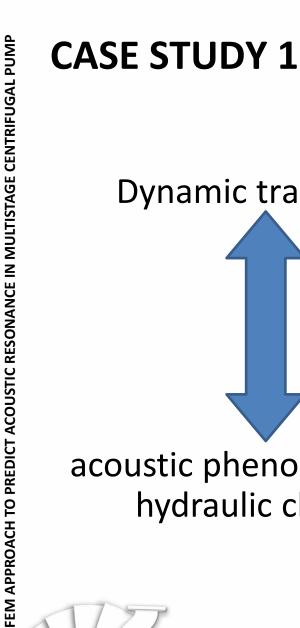


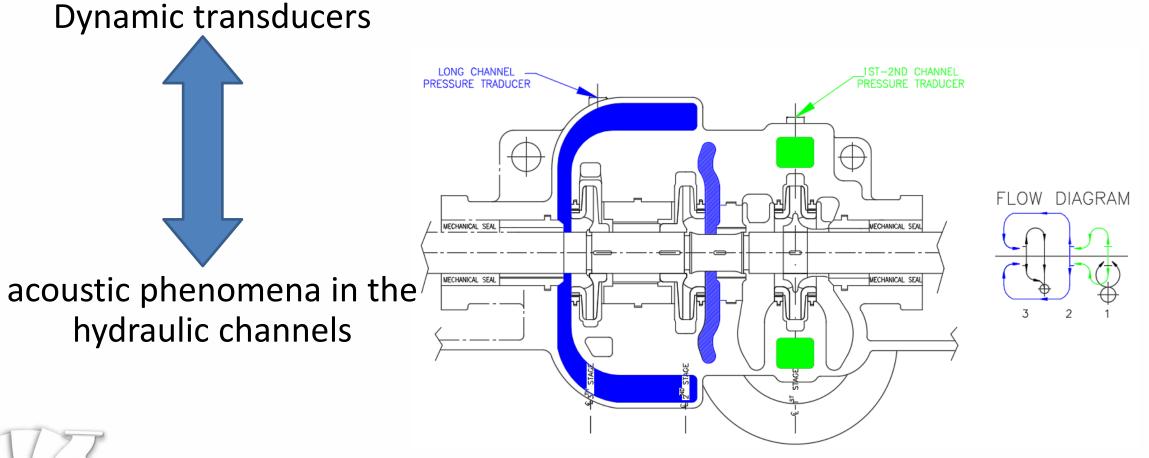


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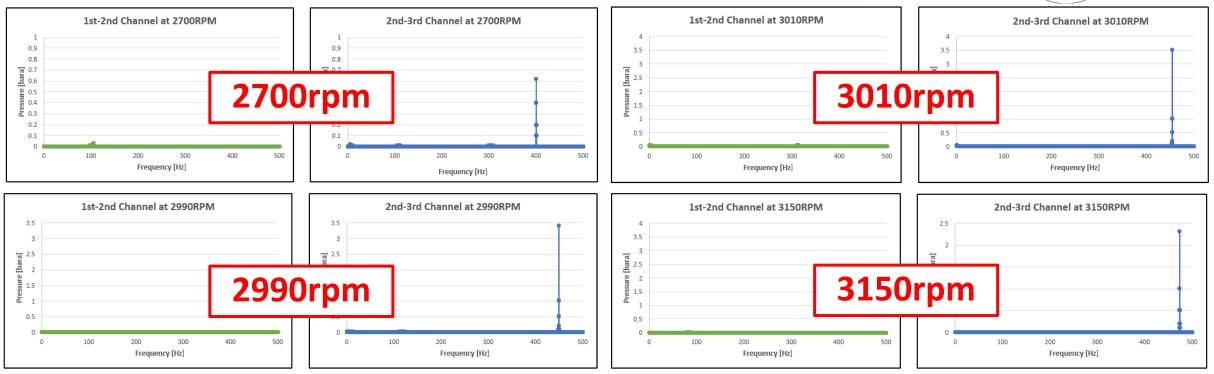
High values of the overall direct amplitude at the vertical DE at 3000 rpm.

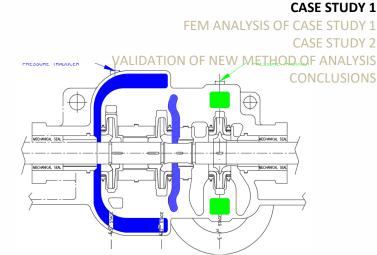






Peak in the long crossover channel (blue diagrams) **No peak** in the first-second channel (green diagrams).





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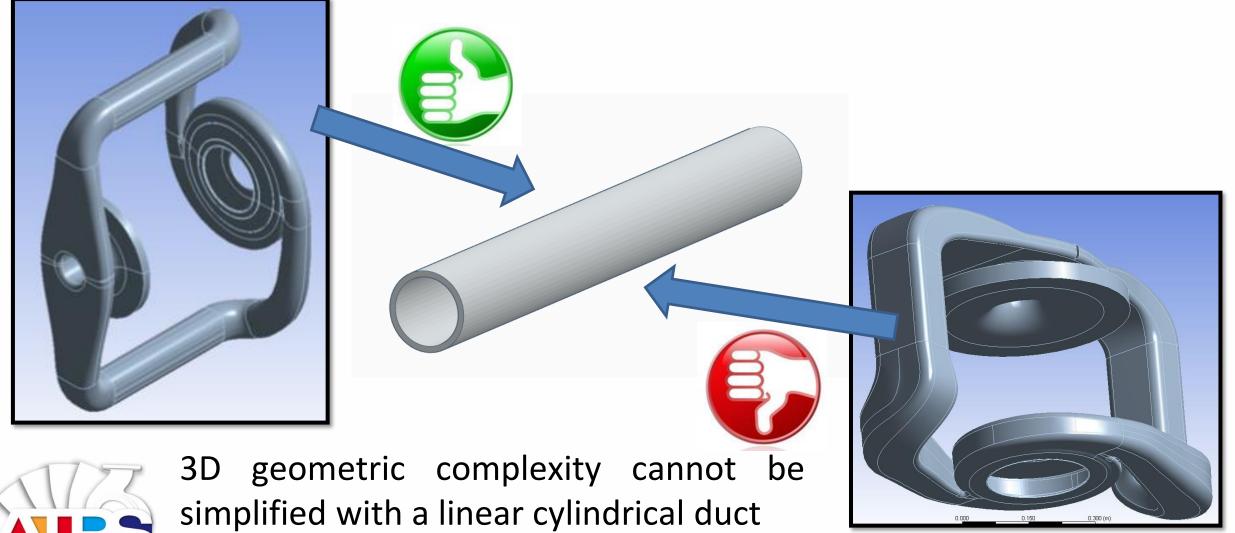
Speed close to the nominal speed \rightarrow greater amplitude of pressure peak

The AR frequency of the channel is close to the nominal speed.

	BPF	Pressure		
Speed	(2 nd stage Impeller)	Peak-to-peak		
[RPM]	[Hz]	[bara]		
2700	405	0.6		
2990	449	3.4		
3010	452	3.5		
3150	473	2.3		

FEM ANALYSIS OF CASE STUDY 1

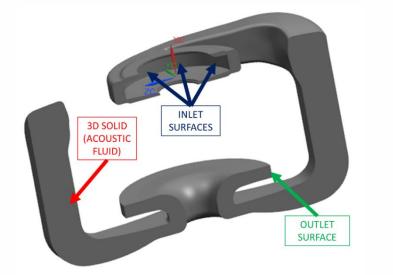
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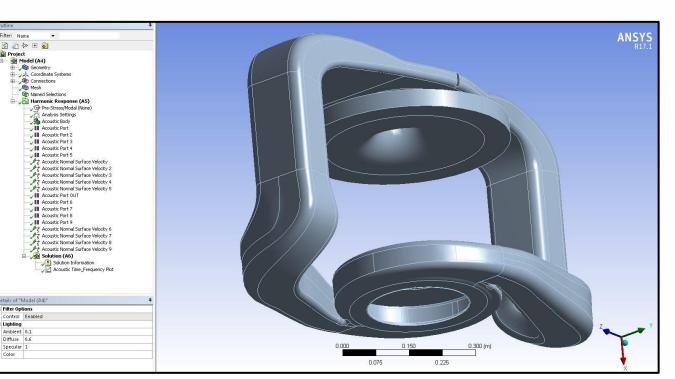
FEM ANALYSIS OF CASE STUDY 1

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3D modeling + FEM analysis + Ansys[®] acoustic model



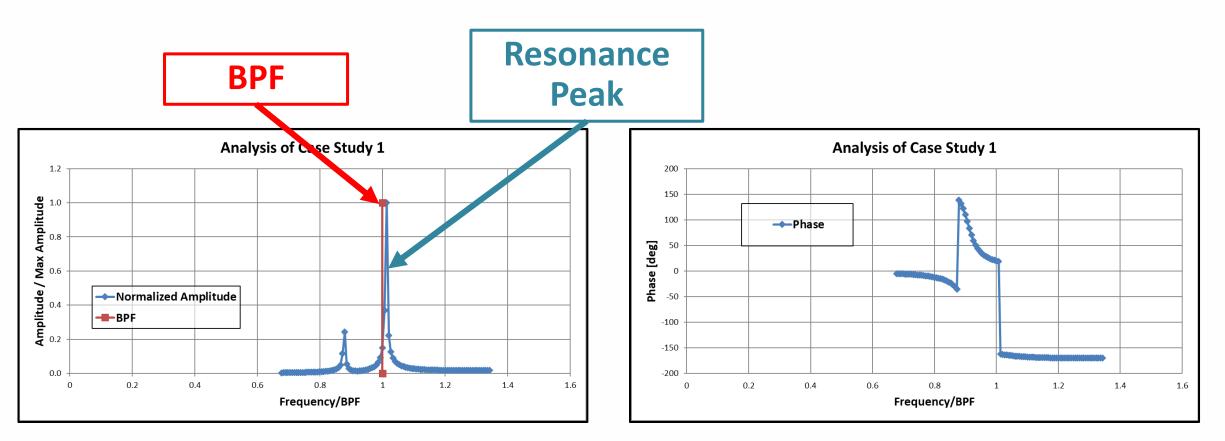
- small pressure changes respect to mean pressure
- rigid wall boundary



FEM ANALYSIS OF CASE STUDY 1

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Resonance peak of resonance very close to the BPF





New pumps to be tested $\leftarrow \rightarrow$ Provide the set of the se

Procedure validation

AR close to the BPF for a new BB5 4x11/7 stages

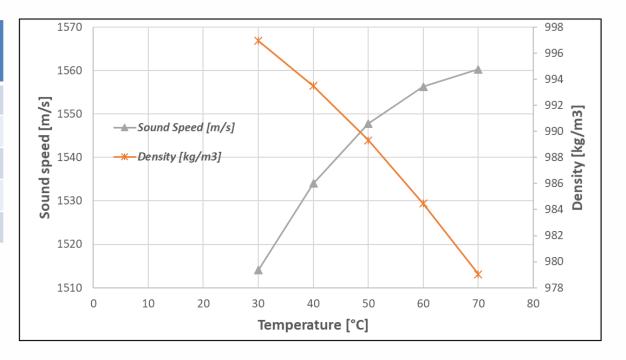
Test with interception between BPF AR in two ways:

- 1. varying the rotation speed;
- 2. varying the resonance frequency by the fluid sound speed.



The fluid (water) sound speed is function of the temperature:

Temperature	Pressure	Density	Sound Speed
[°C]	[bar]	[kg/m3]	[m/s]
30	30	996.94	1514.1
40	30	993.48	1534
50	30	989.3	1547.8
60	30	984.46	1556.3
70	30	979.04	1560.3





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Normalized Amplitude

1.1

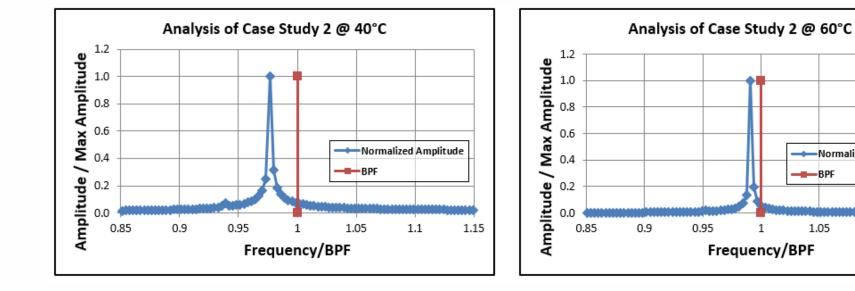
1.15

1.05

FEM Analysis \rightarrow AR frequency in long channel approaches to the BPF

No pressure transducers on channel but only vibration probes on the

bearings.



The resonance was highlighted with the variation of the vibration levels.

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VALIDAT



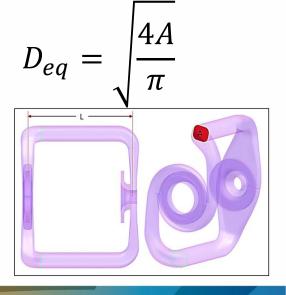
Analysis of older tests pumps from database

VALIDATION OF NEW METHOD

	Testing issue	Analysis issue	API Pump	Peak Frequency / BPF	Speed [rpm]	Nr of blades	L3/L2 %	L/Deq
Test 3	NO	YES	BB3/7 Stages	1.035	2915	7	6.0	61
Test 4	NO	NO	BB3/4 Stages	1.427	1490	7	14.0	27
Test 5	NO	NO	BB3/10 Stages	0.861	5700	6	0.1	110
Test 6	YES	YES	BB3/6 Stages	0.972	2980	7	12.0	34
Test 7	NO	NO	BB3/6Stages	0.893	2985	7	7.0	50
Test 8	NO	NO	BB3/4 Stages	1.273	1490	8	12.0	30

Deq: diameter of a circular section with area A calculated as

- L2: equivalent length calculated using the 1-D method
- L3: equivalent length calculated using the 3-D method
- L: interstage channel length



CENTRIFUGAL

OF ANALYSIS

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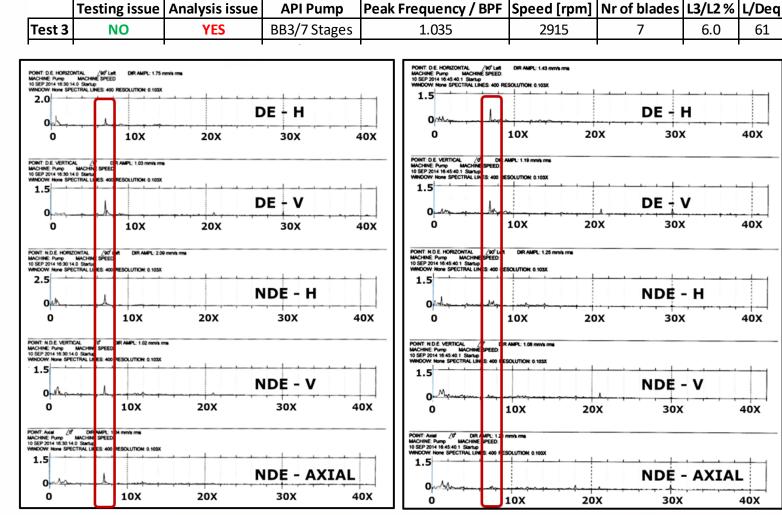
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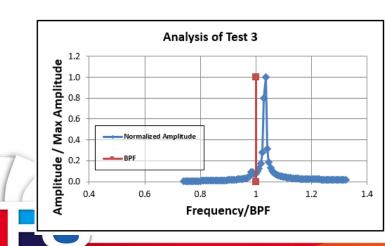
FEM Analysis:

acoustic resonance for the Test 3

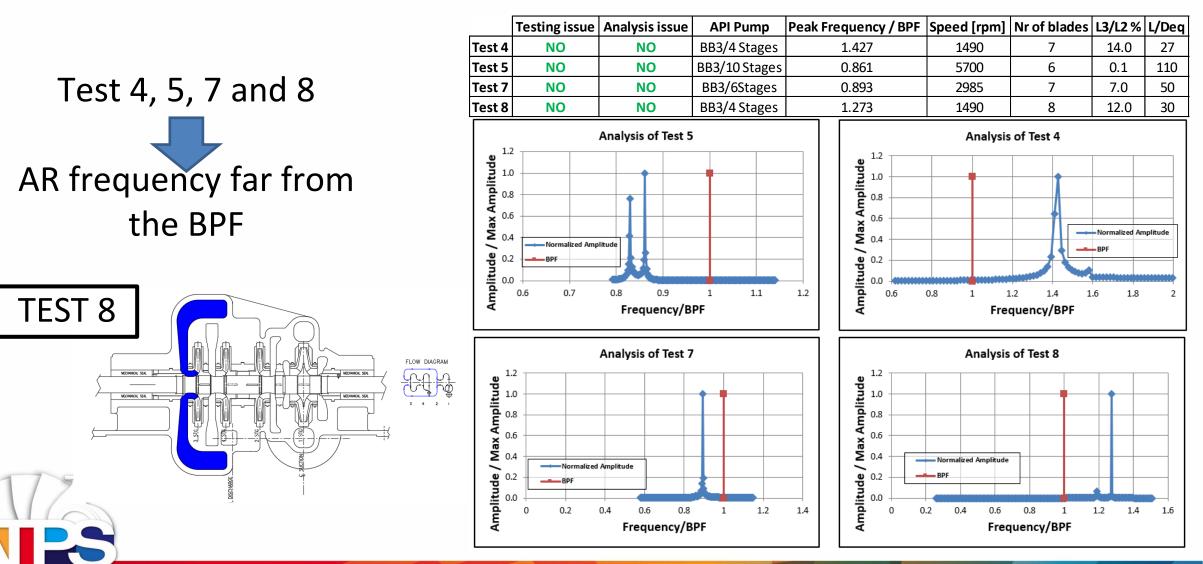
Tests:

vibrations below the limits(damping effect)





VALIDATION OF NEW METHOD OF ANALYSIS





VALIDATION OF NEW METHOD OF ANALYSIS

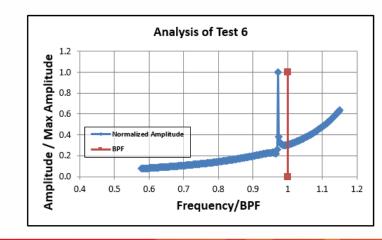
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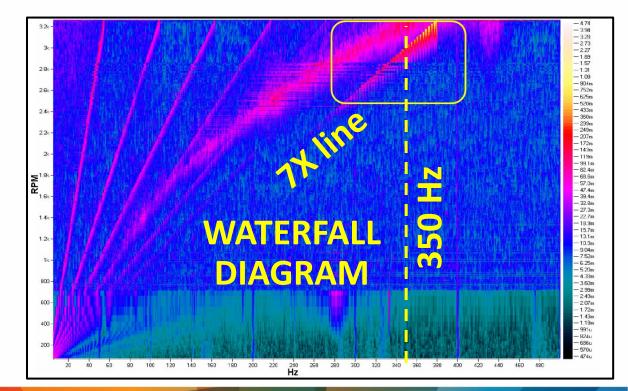
FEM Analysis Waterfall diagram

 $n \rightarrow$

peak of AR for **Test 6** peak on line 7X close to 350Hz (7 x 50Hz)

Rotation speed = 2985 rpm (~50Hz) Nr of blades = 7





CONCLUSIONS

- Necessity of improve the design procedure for a possible issue on field
- New method for AR prediction in complex 3D geometries
- New procedure validation with tests and simulations
- The error in length calculation is related to the ratio L/Deq
- Computational capacity
- Updating of design procedure after new method validation



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