## **Supplementary files:**

Appendix A: Reactive solute transport in a filled single fracture-matrix system under the unilateral flow.

The governing equations of reactive solute transport in the mobile and immobile domains of filled fracture and rock matrix in Eqs.2.1-2.3 should be transformed in dimensionless formats. The dimensionless variables used in the study of the unilateral flow model are as follows:

$$C_{mD} = \frac{c_m}{c_0}; \quad C_{imD} = \frac{c_{im}}{c_0}; \quad C_{kD} = \frac{c_k}{c_0}; \quad x_D = \frac{x}{b}; \quad z_D = \frac{z}{b}\sqrt{\frac{R_3D_m}{R_1D_d}}; \quad t_D = \frac{D_m}{R_1b^2}t; \quad Pe = \frac{v_mb}{D_m}$$
$$\theta_1 = \theta_{im}/\theta_m; \quad \theta_2 = \theta_k/\theta_m; \quad \alpha = \frac{R_1b^2}{D_m}; \quad \alpha_1 = \theta_2\sqrt{\frac{R_3D_d}{R_1D_m}}; \quad M'_{fmD} = \frac{M'_{fm}}{c_0b^2\sqrt{\frac{R_1D_d}{R_3D_m}}}; \quad M'_{fimD} = \frac{M'_{fm}}{c_0b^2\sqrt{\frac{R_1D_d}{R_3D_m}}};$$

In the unilateral flow model, the non-dimensional governing equations (Eqs. (2.1)-(2.3)) now are transformed to their dimensionless formats of Eqs. (A1)-(A3):

$$\frac{\partial C_{mD}}{\partial t_D} + \frac{\theta_1 R_2}{R_1} \frac{\partial C_{imD}}{\partial t_D} = \frac{\partial^2 C_{mD}}{\partial x_D^2} - Pe \frac{\partial C_{mD}}{\partial x_D} - \lambda_1 \alpha C_{mD} - \lambda_2 \theta_1 \alpha \frac{R_2}{R_1} C_{im} + \alpha_1 \frac{\partial C_{kD}}{\partial z_D} \bigg|_{z_D = \sqrt{\frac{R_3 D_m}{R_1 D_d}}}, \quad (A.1)$$

$$\frac{\partial C_{imD}}{\partial t_D} = \frac{\omega \alpha}{\theta_{im} R_2} \left( C_{mD} - C_{imD} \right) - \lambda_2 \alpha C_{imD}, \qquad (A.2)$$

$$\frac{\partial C_{kD}}{\partial t_D} = \frac{\partial^2 C_{kD}}{\partial z_D^2} - \lambda_3 \alpha C_{kD} \,. \tag{A.3}$$

Applying Laplace transform to Eqs. (A.1)-(A.3) would lead to the following equations:

$$p\overline{C_{mD}} + p\frac{\theta_1 R_2}{R_1}\overline{C_{imD}} = \frac{d^2\overline{C_{mD}}}{dx_D^2} - Pe\frac{d\overline{C_{mD}}}{dx_D} - \lambda_1\alpha\overline{C_{mD}} - \lambda_2\theta_1\alpha\frac{R_2}{R_1}\overline{C_{imD}} + \alpha_1\frac{d\overline{C_{kD}}}{dz_D}\bigg|_{z_D = \sqrt{\frac{R_3D_m}{R_1D_d}}},$$

$$p\overline{C_{imD}} = \frac{\omega\alpha}{\theta_{im}R_2} \left(\overline{C_{mD}} - \overline{C_{imD}}\right) - \lambda_2 \alpha \overline{C_{imD}}, \qquad (A.5)$$

$$p\overline{C_{kD}} = \frac{d^2 \overline{C_{kD}}}{dz_D^2} - \lambda_3 \alpha \overline{C_{kD}} , \qquad (A.6)$$

where p is the Laplace transform parameter in respect to the dimensionless time,  $t_D$  and overbar means the term in Laplace domain. From Eq. (A.6), one has

$$\frac{d^2 \overline{C_{kD}}}{dz_D^2} = (\lambda_3 \alpha + p) \overline{C_{kD}} \quad , \tag{A.7}$$

The general solution of Eq. (A7) is

$$\overline{C_{kD}} = Ae^{wz_D} + Be^{-wz_D}, \qquad (A.8)$$

where  $w = \sqrt{\lambda_3 \alpha + p}$ .

Recalling boundary condition of rock matrix at infinity (Eq. (2.11)), Eq. (A.8) can be simplified as:

$$\overline{C_{kD}} = Be^{-wz_D} \quad . \tag{A.9}$$

Substituting Eq. (A.9) to Eq. (A.6), one can get the following relation:

$$\overline{C_{mD}} = \overline{C_{kD}}\Big|_{z_D = \sqrt{\frac{R_3 D_m}{R_1 D_d}}},$$
(A.10)

$$B = \overline{C_{mD}} e^{\sqrt{\lambda_3 \alpha + p} \sqrt{\frac{R_3 D_m}{R_1 D_d}}}.$$
(A.11)

Now one has the relation between  $\overline{C_{kD}}$  and  $\overline{C_{mD}}$ :

$$\overline{C_{kD}} = \overline{C_{mD}} e^{\sqrt{\lambda_3 \alpha + p} \left( \sqrt{\frac{R_3 D_m}{R_1 D_d}} - z_D \right)}.$$
(A.12)

Based on Eq. (A.5), the relation between  $\overline{C_{mD}}$  and  $\overline{C_{imD}}$  is demonstrated:

$$\overline{C_{imD}} = \frac{\omega}{\frac{\theta_{im}R_2p}{\alpha} + \omega + \lambda_2\theta_{im}R_2}}\overline{C_{mD}}.$$
(A.13)

Substituting Eqs. (A.12)-(A.13) into Eq. (A.4), the final solutions will be reached in the Laplace domain.

Converting  $M'_{fm}$ ,  $M'_{fim}$  and  $M'_k$  in Eqs. (2.30)-(2.32) into their dimensionless forms defined above, the dimensionless mass per unit width stored in the fracture-rock matrix system of unilateral flow is given as:

$$M'_{fmD} = 2\theta_m \sqrt{\frac{R_3 D_m}{R_1 D_d}} \int_0^\infty C_{mD} \, dx_D \quad ,$$
 (A.14)

$$M'_{fimD} = 2\theta_{im} \sqrt{\frac{R_3 D_m}{R_1 D_d}} \int_0^\infty C_{imD} dx_D \quad , \tag{A.15}$$

$$M'_{kD} = 2\theta_k \int_{\sqrt{\frac{R_3 D_m}{R_1 D_d}}}^{\infty} \int_0^{\infty} C_{kD} \, dx_D \, dz_D \tag{A.16}$$

## Appendix B: Reactive solute transport in a filled single fracture-matrix system under the radial flow.

The governing equations (Eqs. (2.20)-(2.21)) are transformed to dimensionless formats. The dimensionless variables used in the study of the radial flow model are defined as follows:

$$C_{mD} = \frac{C_m}{C_0} ; \quad C_{imD} = \frac{C_{im}}{C_0} ; \quad C_{kD} = \frac{C_k}{C_0} ; \quad t_D = \frac{At}{R_1 d^2} ; \quad r_D = \frac{r}{d} ; \quad z_D = \left(\frac{z}{d}\right) \sqrt{\frac{R_3 A}{R_1 D_d}} ; \quad \tau_1 = \frac{\theta_2 d}{b} \sqrt{\frac{R_3 D_d}{R_1 A}} ; \quad \tau = \frac{d^2 R_1}{A} ; \quad \theta_1 = \theta_{im} / \theta_m ; \quad \theta_2 = \theta_k / \theta_m ; \quad M_{fmD} = \frac{M_{fm}}{C_0 d^3 \sqrt{\frac{R_1 D_d}{R_3 A}}} ; \quad M_{fimD} = \frac{M_{fm}}{C_0 d^3 \sqrt{\frac{R_1 D_d}{R_3 A}}} ; \quad M_{fimD} = \frac{M_k}{C_0 d^3 \sqrt{\frac{R_1 D_d}{R_3 A}}} ; \quad M_{kD} = \frac{M_k}{C_0 d^3 \sqrt{\frac{R_1 D_d}{R_3 A}}} .$$

Converting the system into the dimensionless format, as done for the unilateral flow model, with details provided above, one has:

$$\frac{\partial C_{mD}}{\partial t_D} + \frac{\theta_1 R_2}{R_1} \left( \frac{\partial C_{imD}}{\partial t_D} \right) = \frac{1}{r_D} \left( \frac{\partial^2 C_{mD}}{\partial r_D^2} \right) - \frac{1}{r_D} \left( \frac{\partial C_{mD}}{\partial r_D} \right) - \lambda_1 \tau C_{mD} - \theta_1 \lambda_2 \frac{R_2}{R_1} \tau C_{imD} + \tau_1 \left( \frac{\partial C_{kD}}{\partial z_D} \right) \bigg|_{z_D = b/d \sqrt{\frac{R_3 A}{R_1 D_d}}},$$
(B.1)

$$\frac{\partial C_{imD}}{\partial t_D} = \frac{\omega\tau}{\theta_{im}R_2} \left( C_{mD} - C_{imD} \right) - \lambda_2 \tau C_{imD} , \qquad (B.2)$$

$$\frac{\partial^2 C_{kD}}{\partial z_D^2} - \frac{\partial C_{kD}}{\partial t_D} - \tau \lambda_3 C_{kD} = 0.$$
(B.3)

Applying the Laplace transform to Eqs. (B.1)-(B.3) would yield to the following equations in the Laplace domain:

$$p\overline{C_{mD}} + \theta_1 \lambda_2 \frac{R_2}{R_1} \tau \overline{C_{imD}} + \frac{\theta_1 p R_2}{R_1} \overline{C_{imD}} = \frac{1}{r_D} \left( \frac{d^2 \overline{C_{mD}}}{dr_D^2} \right) - \frac{1}{r_D} \left( \frac{d \overline{C_{mD}}}{dr_D} \right) - \lambda_1 \tau \overline{C_{mD}} + \tau_1 \left( \frac{\partial \overline{C_{kD}}}{\partial z_D} \right) \bigg|_{z_D = b/d \sqrt{\frac{R_3 A}{R_1 D_d}}}$$
(B.4)

$$p\overline{C_{imD}} = \frac{\omega\tau}{\theta_{im}R_2} \left(\overline{C_{mD}} - \overline{C_{imD}}\right) - \lambda_2 \tau \overline{C_{imD}} , \qquad (B.5)$$

$$\frac{\partial^2 \overline{C_{kD}}}{\partial z_D^2} - \overline{C}_{kD} p - \tau \lambda_3 \overline{C}_{kD} = 0.$$
(B.6)

From Eq. (B.6), we have:

$$\overline{C_{kD}} = a \times exp\left(-\sqrt{\tau\lambda_3 + p}z_D\right) \quad . \tag{B.7}$$

At the interacting surface between the rock matrix and fracture:

$$\overline{C_{mD}}(r_D, p) = \overline{C_{kD}}\left(z_D = b / d\sqrt{\frac{R_3A}{R_1D_d}}, p\right) = a \times \exp\left(-\sqrt{\tau\lambda_3 + p} \times b / d\sqrt{\frac{R_3A}{R_1D_d}}\right).$$
(B.8)

So *a* can be solved as follow:

$$a = \overline{C_{mD}} exp\left(\sqrt{\tau\lambda_3 + p} \times b / d\sqrt{\frac{R_3A}{R_1D_d}}\right).$$
(B.9)

Substituting Eq. (B.9) into Eq. (B.7), the relationship between  $\overline{C_{kD}}$  and  $\overline{C_{mD}}$  can be reached:

$$\overline{C_{kD}} = \overline{C_{mD}} \exp\left[-\sqrt{\tau \lambda_3 + p} \left(z_D - b / d \sqrt{\frac{R_3 A}{R_1 D_d}}\right)\right].$$
(B.10)

From Eq. (B.5), the relation between  $\overline{C_{imD}}$  and  $\overline{C_{mD}}$  is as follow:

$$\overline{C_{imD}} = \frac{\omega}{\frac{\theta_{im} p R_2}{\tau} + \omega + \lambda_2 \theta_{im} R_2}} \overline{C_{mD}} \quad . \tag{B.11}$$

Substituting Eqs. (B.10)-(B.11) to Eq. (B.4):

$$\frac{\partial^2 \overline{C_{mD}}}{\partial r_D^2} - \frac{\partial \overline{C_{mD}}}{\partial r_D} - r_D \beta \overline{C_{mD}} = 0, \qquad (B.12)$$

where 
$$\beta = \left( \tau \lambda_1 + \tau_1 \sqrt{\tau \lambda_3 + p} + p + \frac{R_2}{R_1} \times \frac{\left( p + \lambda_2 \tau \right) \theta_1 \omega}{\frac{\theta_{im} p R_2}{\tau} + \omega + \lambda_2 \theta_{im} R_2} \right).$$

The Eq. (B.12) is an inhomogeneous differential equation. The general solution is

$$\overline{C_{mD}} = A_1 \times \exp\left(\frac{y}{2}\right) Ai\left(\beta^{\frac{1}{3}}y\right) + A_2 \times \exp\left(\frac{y}{2}\right) Bi\left(\beta^{\frac{1}{3}}y\right), \tag{B.13}$$

where  $y = r_D + (4\beta)^{-1}$ .

Since  $Bi(\infty) \to \infty$ , to fulfill the boundary condition below:

$$\overline{C_{mD}}(r_D \to \infty, p) = 0.$$
(B.14)

 $A_2$  has to be zero. Now Eq. (B.13) is

$$\overline{C_{mD}} = A_1 \exp\left(\frac{y}{2}\right) Ai(\beta^{\frac{1}{3}}y).$$
(B.15)

The boundary condition at the interacting surface of the injection well is given as:

$$\overline{C_{mD}}\left(r_{oD} = \frac{r_0}{d}, p\right) = \frac{1}{p} \quad . \tag{B.16}$$

The parameter  $A_1$  can be expressed:

$$A_{1} = \frac{1}{p} \exp\left(-\frac{1}{2}r_{0D} - \frac{1}{2}(4\beta)^{-1}\right) A i^{-1} \left[\beta^{\frac{1}{3}} \left(r_{D} + (4\beta)^{-1}\right)\right].$$
(B.17)

Now, the solutions in the Laplace domain could be reached.

By using the dimensionless parameters above, the dimensionless masses stored in the fracture-rock matrix system of radial flow are given as:

$$M_{fmD} = \int_{r_{0D}}^{\infty} \frac{4\pi b \theta_m \sqrt{R_3 A}}{d\sqrt{R_1 D_d}} r_D C_{mD} dr_D , \qquad (B.18)$$

$$M_{fimD} = \int_{r_{0D}}^{\infty} \frac{4\pi b \theta_{im} \sqrt{R_{3}A}}{d\sqrt{R_{1}D_{d}}} r_{D} C_{imD} dr_{D} , \qquad (B.19)$$

$$M_{kD} = \int_{\frac{b}{d\sqrt{\frac{R_{1}D_{d}}{R_{3}A}}}}^{\infty} \int_{r_{0D}}^{\infty} 4\pi\theta_{k}r_{D}C_{kD} dr_{D}dz_{D} .$$
(B.20)

Appendix C: Reactive solute transport in an asymmetrical fracture-rock matrix system.

The dimensionless variables used in this study are defied as follows:

$$C_D = C/C_0$$
,  $C_{1D} = C_1/C_0$ ,  $C_{2D} = C_2/C_0$ ,  $x_D = x/b$ ,  $z_D = \frac{z}{b}\sqrt{\frac{R_2D}{RD_1}}$ ,  $t_D = \frac{D}{Rb^2}t$ ,

$$Pe = \frac{vb}{D} , \quad \alpha = \frac{Rb^2}{D} , \quad M_D = \frac{M}{C_0 \times b^2 \times \sqrt{\frac{RD_1}{R_2D}}} , \quad M_{1D} = \frac{M_1}{C_0 \times b^2 \times \sqrt{\frac{RD_1}{R_2D}}} ,$$

$$M_{2D} = \frac{M_2}{C_0 \times b^2 \times \sqrt{\frac{RD_1}{R_2D}}}$$

With the help of those dimensionless parameters above, the non-dimensional governing equations (Eqs. (3.1)-(3.3)) are transformed to the dimensionless formats:

$$\frac{\partial C_D}{\partial t_D} = \frac{\partial^2 C_D}{\partial x_D^2} - Pe \frac{\partial C_D}{\partial x_D} - \lambda \alpha C_D + \frac{\theta_1}{2\theta} \sqrt{\frac{R_2 D_1}{RD}} \frac{\partial C_{1D}}{\partial z_D} \bigg|_{z_D = z_{0D}} - \frac{\theta_2}{2\theta} \sqrt{\frac{R_2 D_2^2}{RD_1 D}} \frac{\partial C_{2D}}{\partial z_D} \bigg|_{z_D = -z_{0D}}, \quad (C.1)$$

$$\frac{\partial C_{1D}}{\partial t_D} = \frac{R_2}{R_1} \frac{\partial^2 C_{1D}}{\partial z_D^2} - \lambda_1 \alpha C_{1D}, \qquad (C.2)$$

$$\frac{\partial C_{2D}}{\partial t_D} = \frac{D_2}{D_1} \frac{\partial^2 C_{2D}}{\partial z_D^2} - \lambda_2 \alpha C_{2D}.$$
(C.3)

After applying Laplace transform to Eqs. (C.1)-(C.3), the following equations would be obtained:

$$p\overline{C_D} = \frac{d^2\overline{C_D}}{dx_D^2} - Pe\frac{d\overline{C_D}}{dx_D} - \lambda\alpha\overline{C_D} + \frac{\theta_1}{2\theta}\sqrt{\frac{R_2D_1}{RD}}\frac{\partial\overline{C_{1D}}}{\partial z_D}\bigg|_{z_D = z_{0D}} - \frac{\theta_2}{2\theta}\sqrt{\frac{R_2D_2^2}{RD_1D}}\frac{\partial\overline{C_{2D}}}{\partial z_D}\bigg|_{z_D = -z_{0D}}, (C.4)$$

$$p\overline{C_{1D}} = \frac{R_2}{R_1} \frac{\partial^2 \overline{C_{1D}}}{\partial z_D^2} - \lambda_1 \alpha \overline{C_{1D}}, \qquad (C.5)$$

$$p\overline{C_{2D}} = \frac{D_2}{D_1} \frac{\partial^2 \overline{C_{2D}}}{\partial z_D^2} - \lambda_2 \alpha \overline{C_{2D}}, \qquad (C.6)$$

where p is the Laplace transform parameter in respect to the dimensionless time,  $t_D$  and overbar means the term in Laplace domain. From Eqs. (C.5)-(C.6), one has:

$$\frac{\partial^2 \overline{C_{1D}}}{\partial z_D^2} = \frac{R_1}{R_2} (\lambda_1 \alpha + p) \overline{C_{1D}}, \qquad (C.7)$$

$$\frac{\partial^2 \overline{C_{2D}}}{\partial z_D^2} = \frac{D_1}{D_2} (\lambda_2 \alpha + p) \overline{C_{2D}} .$$
(C.8)

The general solutions of the Eqs. (C.7)-(C.8) are:

$$\overline{C_{1D}} = A_1 e^{w_1 z_D} + B_1 e^{-w_1 z_D} \quad , \tag{C.9}$$

$$\overline{C_{2D}} = A_2 e^{w_2 z_D} + B_2 e^{-w_2 z_D}, \qquad (C.10)$$

Where 
$$w_1 = \sqrt{\frac{R_1}{R_2}(\lambda_1 \alpha + p)}$$
,  $w_2 = \sqrt{\frac{D_1}{D_2}(\lambda_2 \alpha + p)}$ .

Recalling the boundary conditions of rock matrix at infinity (Eq. (3.9)), Eqs. (C.9)-(C.10) can be further simplified as:

$$\overline{C_{1D}} = B_1 e^{-w_1 z_D},$$
(C.11)

$$\overline{C_{2D}} = A_2 e^{w_2 z_D} \,. \tag{C.12}$$

After substituting in boundary conditions (Eqs. (3.6)-(3.8)), one can acquire:

$$\overline{C_{1D}} = \overline{C_D} \times \exp\left[-\sqrt{\frac{R_1}{R_2}(p + \lambda_1 \alpha)} \left(z_D - \sqrt{\frac{R_2 D}{RD_1}}\right)\right] , \qquad (C.13)$$

$$\overline{C_{2D}} = \overline{C_D} \times \exp\left[\sqrt{\frac{D_1}{D_2}(p + \lambda_2 \alpha)} \left(z_D + \sqrt{\frac{R_2 D}{RD_1}}\right)\right] , \qquad (C.14)$$

where 
$$k_1 = \lambda \alpha + p + \frac{\theta_1}{2\theta} \sqrt{\frac{R_1 D_1}{RD} (p + \lambda_1 \alpha)} + \frac{\theta_2}{2\theta} \sqrt{\frac{R_2 D_2}{RD} (p + \lambda_2 \alpha)}$$
.

Substituting Eqs. (C.13)-(C.14) and the first-type boundary condition Eq. (3.10) into Eq. (C.4), the final solutions and the diffusion loss under the first-type condition can be reached:

$$\overline{C_D} = \frac{1}{p} \exp\left(\frac{Pe - \sqrt{Pe^2 + 4k_1}}{2} x_D\right) , \qquad (C.15)$$

$$\overline{C_{1D}} = \frac{1}{p} \exp\left[\frac{Pe - \sqrt{Pe^2 + 4k_1}}{2} x_D - \sqrt{\frac{R_1}{R_2}(p + \lambda_1 \alpha)} \left(z_D - \sqrt{\frac{R_2D}{RD_1}}\right)\right],$$
(C.16)

$$\overline{C_{2D}} = \frac{1}{p} \exp\left[\frac{Pe - \sqrt{Pe^2 + 4k_1}}{2} x_D + \sqrt{\frac{D_1}{D_2}(p + \lambda_2 \alpha)} \left(z_D + \sqrt{\frac{R_2 D}{RD_1}}\right)\right],$$
(C.17)

$$\overline{q_1} = \frac{1}{p} \frac{\theta_1 D_1}{b} \sqrt{\frac{R_1 D}{R D_1} \left(p + \lambda_1 \alpha\right)} \exp\left[\frac{Pe - \sqrt{Pe^2 + 4k_1}}{2} x_D\right],$$
(C.18)

$$\overline{q_2} = \frac{1}{p} \frac{\theta_2 D_2}{b} \sqrt{\frac{R_2 D}{R D_2} \left(p + \lambda_2 \alpha\right)} \exp\left[\frac{Pe - \sqrt{Pe^2 + 4k_1}}{2} x_D\right].$$
(C.19)

It is the similar method to solve the problem under the third-type boundary condition Eq. (3.11), the final solutions are:

$$\overline{C_D} = \frac{1}{p} \times \frac{2}{1 + \sqrt{1 + 4k_1 / Pe^2}} \exp\left(\frac{Pe - \sqrt{Pe^2 + 4k_1}}{2} x_D\right),$$
(C.20)

$$\overline{C_{1D}} = \frac{1}{p} \times \frac{2}{1 + \sqrt{1 + 4k_1 / Pe^2}} \exp\left[\frac{Pe - \sqrt{Pe^2 + 4k_1}}{2} x_D - \sqrt{\frac{R_1}{R_2}(p + \lambda_1 \alpha)} \left(z_D - \sqrt{\frac{R_2D}{RD_1}}\right)\right],$$
(C.21)
$$\overline{C_{2D}} = \frac{1}{p} \times \frac{2}{1 + \sqrt{1 + 4k_1 / Pe^2}} \exp\left[\frac{Pe - \sqrt{Pe^2 + 4k_1}}{2} x_D + \sqrt{\frac{D_1}{D_2}(p + \lambda_2 \alpha)} \left(z_D + \sqrt{\frac{R_2D}{RD_1}}\right)\right].$$
(C.22)

Converting the mass stored in each domain (Eqs. (3.32)-(3.34)) into corresponding dimensionless formats defined above, the dimensionless mass per unit width stored in each domain is given as:

$$M_D = 2\theta \sqrt{\frac{R_2 D}{RD_1}} \int_0^\infty C_D dx_D , \qquad (C.23)$$

$$M_{1D} = \int_{\sqrt{\frac{R_2 D}{RD_1}}}^{\infty} \int_0^{\infty} C_{1D} \times \theta_1 dx_D dz_D, \qquad (C.24)$$

$$M_{2D} = \int_{-\infty}^{-\sqrt{\frac{R_2 D}{RD_1}}} \int_{0}^{\infty} C_{2D} \theta_2 dx_D dz_D.$$
(C.25)

For the back-diffusion problem, the water starts flushing the system after  $t_0$ . The diffusion coefficients after water flushing may change to  $D_{1b}$ ,  $D_{2b}$ ,  $D_b$ :

$$D_{1b} = a_1 D_1, \ D_{2b} = a_2 D_2, D_b = a D.$$
 (C.26)

For the back-diffusion process, the governing equations are similar as:

$$\frac{\partial C_D}{\partial t_D} = a \frac{\partial^2 C_D}{\partial x_D^2} - Pe \frac{\partial C_D}{\partial x_D} - \lambda \alpha C_D + \frac{\theta_1 a_1}{2\theta} \sqrt{\frac{R_2 D_1}{RD}} \frac{\partial C_{1D}}{\partial z_D} \bigg|_{z_D = z_{0D}} - \frac{\theta_2 a_2}{2\theta} \sqrt{\frac{R_2 D_2^2}{RD_1 D}} \frac{\partial C_{2D}}{\partial z_D} \bigg|_{z_D = -z_{0D}} ,$$
(C.27)

$$\frac{\partial C_{1D}}{\partial t_D} = a_1 \frac{R_2}{R_1} \frac{\partial^2 C_{1D}}{\partial z_D^2} - \lambda_1 \alpha C_{1D}, \qquad (C.28)$$

$$\frac{\partial C_{2D}}{\partial t_D} = a_2 \frac{D_2}{D_1} \frac{\partial^2 C_{2D}}{\partial z_D^2} - \lambda_2 \alpha C_{2D} \,. \tag{C.29}$$

Following the similar method, the solutions during back diffusion are:

$$\overline{C_D}' = -\frac{1}{p} \exp\left(\frac{Pe - \sqrt{Pe^2 + 4k_2a}}{2a} x_D\right) , \qquad (C.30)$$

$$\overline{C_{1D}}' = -\frac{1}{p} \exp\left[\frac{Pe - \sqrt{Pe^2 + 4k_2a}}{2a} x_D - \sqrt{\frac{R_1}{a_1R_2}(p + \lambda_1\alpha)} \left(z_D - \sqrt{\frac{R_2D}{RD_1}}\right)\right],$$
 (C.31)

$$\overline{C_{2D}}' = -\frac{1}{p} \exp\left[\frac{Pe - \sqrt{Pe^2 + 4k_2a}}{2a} x_D + \sqrt{\frac{D_1}{a_2D_2}(p + \lambda_2\alpha)} \left(z_D + \sqrt{\frac{R_2D}{RD_1}}\right)\right],$$
 (C.32)

where 
$$k_2 = \lambda \alpha + p + \frac{\theta_1}{2\theta} \sqrt{\frac{R_1 D_1 a_1}{RD} (p + \lambda_1 \alpha)} + \frac{\theta_2}{2\theta} \sqrt{\frac{R_2 D_2 a_2}{RD} (p + \lambda_2 \alpha)}$$
.

The overall final solutions are:

$$C = \begin{cases} f(x, z, t) & t \le t_0 \\ f(x, z, t) + g(x, z, t - t_0) & t > t_0 \end{cases},$$
 (C.33)

where f(x,z,t) is the solution (Eqs. (C.15)-(C.17)) before water flushing, g(x,z,t) is the solution (Eqs. (3.30)-(3.31)) during water flushing time period.

## Appendix D: Reactive solute transport in a fully coupled asymmetric stratified system, comparison of scale dependent and independent dispersion schemes.

The governing equation of solute transport in the permeable layer is as follow:

$$\theta R \frac{\partial C}{\partial t} = \theta \frac{\partial}{\partial x} \left[ D(x) \frac{\partial C}{\partial x} \right] - \theta v \frac{\partial C}{\partial x} - \theta \lambda R C - \frac{q_1}{2b} - \frac{q_2}{2b}.$$
(D.1)

The terms  $q_1$  and  $q_2$  refer to the diffusive mass entering the less permeable layers, which are expressed as:

$$q_1 = -\theta_1 D_1 \left. \frac{\partial C_1}{\partial z} \right|_{z=b} \quad , \tag{D.2}$$

$$q_2 = \theta_2 D_2 \frac{\partial C_2}{\partial z} \bigg|_{z=-b} \quad . \tag{D.3}$$

A contaminant source at constant concentration is placed at the left boundary condition, which is also called the first type boundary condition and is expressed as:

$$C(x=0,t) = C_0$$
. (D.4)

The governing equations of solute transport in the upper layer (layer 1) and lower layer (layer 2) are respectively:

$$R_1 \frac{\partial C_1}{\partial t} = D_1 \frac{\partial^2 C_1}{\partial z^2} - \lambda_1 R_1 C_1 \quad , \tag{D.5}$$

$$R_2 \frac{\partial C_2}{\partial t} = D_2 \frac{\partial^2 C_2}{\partial z^2} - \lambda_2 R_2 C_2.$$
 (D.6)

The entire system is free of solute at beginning:

$$C(x,t=0) = C_1(x,z,t=0) = C_2(x,z,t=0) = 0.$$
 (D.7)

The permeable layer is considered as infinitely long and the less permeable layers are considered as infinity thick. Thus, we have:

$$C(x \to \infty, t) = 0, \quad C_1(x, z \to \infty, t) = 0, \quad C_2(x, z \to -\infty, t) = 0.$$
 (D.8)

The concentrations at the interfaces of different layers are continuous:

$$C_1(x, z = b, t) = C(x, t), \quad C_2(x, z = -b, t) = C(x, t).$$
 (D.9)

The technique of Laplace transform is adopted here. Eqs. (D.1), (D.5) and (D.6) are then transformed into Laplace domain as:

$$D(x)\frac{d^{2}\overline{C}}{dx^{2}} + \left[\frac{dD(x)}{dx} - v\right]\frac{d\overline{C}}{dx} - \Psi\overline{C} = 0, \qquad (D.10)$$

$$R_{1}\overline{C_{1}} = D_{1}\frac{\partial^{2}\overline{C_{1}}}{\partial z^{2}} - \lambda_{1}R_{1}\overline{C_{1}}, \qquad (D.11)$$

$$R_2 \overline{C_2} = D_2 \frac{\partial^2 \overline{C_2}}{\partial z^2} - \lambda_2 R_2 \overline{C_2}, \qquad (D.12)$$

where 
$$\Psi = pR + \lambda R + \frac{\theta_1}{2b\theta} \sqrt{(p+\lambda_1)R_1D_1} + \frac{\theta_2}{2b\theta} \sqrt{(p+\lambda_2)R_2D_2}$$
, p is the Laplace

transform parameter and the over bar means the terms in Laplace domain.

With the consideration of continuous concentration at interfaces of layers (Eq. (D.9)), Eqs. (D.11)-(D.12) can be solved as follows:

$$\overline{C_1} = \overline{C} \times \exp\left[-\sqrt{\frac{pR_1 + \lambda_1 R_1}{D_1}}(z-b)\right], \qquad (D.13)$$

$$\overline{C_2} = \overline{C} \times \exp\left[\sqrt{\frac{pR_2 + \lambda_2 R_2}{D_2}}(z+b)\right] .$$
(D.14)

For the case of a linear scale-dependent dispersivity, one has:  $D(x) = \alpha(x) \times v + D_0$ , where  $\alpha(x) = kx$ . Substituting this relationship into Eq. (D.10), we have:

$$(kvx + D_0)\frac{d^2\overline{C}}{dx^2} + [kv - v]\frac{d\overline{C}}{dx} - \Psi\overline{C} = 0.$$
(D.15)

Defining a new variable  $\xi_1 = \sqrt{kvx + D_0}$ , then the equation above turns to:

$$\xi_{1}^{2} \frac{d^{2} \overline{C}}{d \xi_{1}^{2}} + \left[1 - \frac{2}{k}\right] \xi_{1} \frac{d \overline{C}}{d \xi_{1}} - \left(\frac{2}{k v}\right)^{2} \xi_{1}^{2} \Psi \overline{C} = 0.$$
 (D.16)

This equation has the form of the following Bessel equation:

$$\xi_{1}^{2} \frac{d^{2} \overline{C}}{d\xi^{2}} + [1 - 2\gamma] \xi_{1} \frac{d \overline{C}}{d\xi_{1}} + (-\delta^{2} \eta^{2} \xi_{1}^{2n} + \gamma^{2} - \gamma^{2} \eta^{2}) \overline{C} = 0, \qquad (D.17)$$

where  $\gamma = \frac{1}{k}$ ,  $\delta = \frac{2}{kv}\sqrt{\Psi}$ ,  $\eta = 1$ . It have been proven that  $\xi_1^{\gamma} I_{\gamma}(\delta \xi_1^{\eta})$  and  $\xi_1^{\gamma} K_{\gamma}(\delta \xi_1^{\eta})$  are two independent special solutions of the equation, where  $I_{\gamma}(x)$  and

 $K_{\gamma}(x)$  are the first and second kinds of modified Bessel functions with the order  $\gamma$ . Therefore, the general solution of this equation is:

$$\overline{C} = \xi_1^{\gamma} \left\{ A_1 K_{\gamma}(\delta \xi_1) + B_1 I_{\gamma}(\delta \xi_1) \right\},$$
(D.18)

where  $A_1$  and  $B_1$  are two constants. According to the boundary condition (Eq. (D.8)), when  $\xi_1 \to \infty$ ,  $\overline{C}$  is finite. Thus,  $B_1$  equals to zero. The solution could be simplified as:  $\overline{C} = \xi_1^{\gamma} A_1 K_{\gamma}(\delta \xi_1)$ . (D.19)

After substituting in boundary condition  $\overline{C}(x=0,p) = \frac{C_0}{p}$ , one can acquire:

$$A_{1} = \frac{1}{p} \frac{C_{0}}{\left(\sqrt{D_{0}}\right)^{\gamma} K_{\gamma}(\delta\sqrt{D_{0}})}.$$
 (D.20)

The final solution in Laplace domain can be derived now as:

$$\overline{C} = \xi_1^{\gamma} \frac{1}{p} \frac{C_0}{\left(\sqrt{D_0}\right)^{\gamma} K_{\gamma}(\delta\sqrt{D_0})} K_{\gamma}(\delta\xi_1) .$$
(D.21)

For the case of an exponential scale-dependent dispersivity, the dispersivity can be expressed as:  $\alpha(x) = a(1 - e^{-k_1 x})$ . Thus, the governing equation could be rewritten as:

$$\left[a(1-e^{-k_1x})\times v+D_0\right]\frac{d^2\overline{C}}{dx^2}+\left[ak_1ve^{-k_1x}-v\right]\frac{d\overline{C}}{dx}-\Psi\overline{C}=0.$$
(D.22)

Defining two variables:  $\xi_2 = He^{k_1 x}$ ,  $H = 1 + D_0 / (av)$ , Eq. (D.22) can be expressed as:

$$\xi_{2}(1-\xi_{2})\frac{d^{2}\overline{C}}{d\xi_{2}^{2}} - \left(1-\frac{1}{ak_{1}H}\right)\xi_{2}\frac{d\overline{C}}{d\xi_{2}} + \frac{1}{Havk_{1}^{2}}\psi\overline{C} = 0.$$
 (D.23)

The above equation has the form of the following Gauss hypergeometric equation:

$$\xi_{2}(1-\xi_{2})\frac{d^{2}\overline{C}}{d\xi_{2}^{2}} + \left[Q - (1+m+n)\right]\xi_{2}\frac{d\overline{C}}{d\xi_{2}} - mn\overline{C} = 0, \qquad (D.24)$$

where 
$$Q = 0$$
,  $m = \frac{1}{2ak_1H} \left[ -1 + \sqrt{1 + \frac{4aH}{v}\psi} \right]$ , and  $n = \frac{1}{2ak_1H} \left[ -1 - \sqrt{1 + \frac{4aH}{v}\psi} \right]$ .

As  $1 \le \xi_2 \le \infty$ , the solution can be written in terms of the hypergeometric function as follows:

$$\overline{C} = A_2 \xi_2^{-m} F\left(m, m+1; m-n+1; \xi_2^{-1}\right) + B_2 \xi_2^{-n} F\left(n, n+1; n-m+1; \xi_2^{-1}\right),$$
(D.25)

where  $F(m, m+1; m-n+1; \xi_2^{-1})$  and  $F(n, n+1; n-m+1; \xi_2^{-1})$  are the Gauss hypergeometric functions.

In terms of the outlet boundary condition (Eq. (D.8)), the concentration remain finite when  $\xi_2 \rightarrow \infty$ . Thus, the  $B_2$  must equal zero as *n* is less than zero. The solution can be simplified as:

$$\overline{C} = A_2 \xi_2^{-m} F\left(m, m+1; m-n+1; \xi_2^{-1}\right).$$
(D.26)

After substituting  $\overline{C}(x=0, p) = \frac{C_0}{p}$ ,  $A_2$  could be solved as:

$$A_{2} = \frac{C_{0} \left(1 + \frac{D_{0}}{av}\right)^{m}}{pF\left(m, m+1; m-n+1; \left(1 + \frac{D_{0}}{av}\right)^{-1}\right)}$$
(D.27)

The final solution is then derived as:

$$\overline{C} = \frac{C_0 \left(1 + \frac{D_0}{av}\right)^m}{pF\left(m, m+1; m-n+1; \left(1 + \frac{D_0}{av}\right)^{-1}\right)} \xi_2^{-m} F\left(m, m+1; m-n+1; \xi_2^{-1}\right).$$
(D.28)