Analysis and troubleshooting of a piston rod failure of RC

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Presenter / Authors bios

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Abstract

Piston Rods are one of the most vulnerable components in reciprocating compressors and, if failing, one of the most important parts that can cause serious secondary damage. Based on an actual experience with a piston rod failure in a H2 recycle and make-up gas compressor of a Vacuum Residual Hydrocracker (VRHCR) plant, this presentation shows how to find out the root cause of the failure, to take a countermeasure, and to produce lessons learned for maintenance.
Introduction

Compressor is located on a make and recycle loop of reactor in VRHCR (Vacuum Residual Hydrocracker) plant and delivers a H2 rich recycle gas to reactor.

- **1st Stage Suction Pressure**: 19.2 kg/cm²g (273 psig)
- **2nd Stage Suction Pressure**: 42.2 kg/cm²g (600 psig)
- **3rd Stage Suction Pressure**: 90.6 kg/cm²g (1,289 psig)
- **3rd Stage Discharge Pressure**: 200 kg/cm²g (2,844 psig)
- **Motor Rated Power**: 12,020 kW (16,112.6 hp)
Overview of the Problem

The compressor tripped due to high vibration (133mm/s) in 128 days after overhaul. It normally operated at about 5.5m/s of frame vibration and there was no indication just before the event. * Alarm: 11mm/s, Trip: 14mm/s
Overview of the Problem

A crosshead vibration also increased suddenly from normal 0.5G to 56G after failure. 
* Alarm : 1.5G, Trip : null
Inspection and findings

Severely damaged piston rod connecting flange
Inspection and findings

Piston rod broke due to excessive stress and fatigue. There is a beach mark which is the typical fatigue failure on fracture surface. The origin of the crack is located in the center of the arc.
Root Cause Analysis

Performed RCA with OEM through “Why trees” and derived and validated all possible root causes

- Broken piston rod
  - Excessive Load
    - Stress concentration
    - Sudden changes of operation conditions
    - Liquid carryover
    - Incorrect installation
    - Improper Design
  - Insufficient strength of material
    - Manufacturing Defect
    - Material Selection
Root Cause Analysis

The research institute investigated material for defects. There were some small cavities at the microstructure. Additional verification required if these cavities had affected the material properties.

<table>
<thead>
<tr>
<th>Sample point</th>
<th>Surface</th>
<th>Middle</th>
<th>Center</th>
</tr>
</thead>
<tbody>
<tr>
<td>Radial Direction</td>
<td><img src="image1.png" alt="50X" /></td>
<td><img src="image2.png" alt="50X" /></td>
<td><img src="image3.png" alt="50X" /></td>
</tr>
<tr>
<td>Axial Direction</td>
<td><img src="image4.png" alt="50X" /></td>
<td><img src="image5.png" alt="100X" /></td>
<td><img src="image6.png" alt="100X" /></td>
</tr>
</tbody>
</table>

- Small cavities
- Undefined spots
- Deformed microcavity
- Border side
- Middle side
- Bore side
Root Cause Analysis

Destructive testing performed to verify the mechanical properties of the material, and to confirm that all samples met the ASTM standard.

<table>
<thead>
<tr>
<th>Specification</th>
<th>Properties</th>
<th>Tensile Strength (MPa)</th>
<th>Yield Strength (MPa)</th>
<th>Elongation (%)</th>
<th>Impact Test (Joule)</th>
<th>Hardness (0.5kg)</th>
<th>Result</th>
</tr>
</thead>
<tbody>
<tr>
<td>ASTM A564 Type6310, H1150</td>
<td></td>
<td>min. 930</td>
<td>min. 725</td>
<td>min. 16</td>
<td>min. 41</td>
<td>min. 292</td>
<td>Acceptable</td>
</tr>
<tr>
<td>Mill Certificate</td>
<td></td>
<td>1,008</td>
<td>758</td>
<td>22</td>
<td>-</td>
<td>292</td>
<td>Acceptable</td>
</tr>
<tr>
<td>Test Result</td>
<td>①</td>
<td>1,016</td>
<td>871</td>
<td>23</td>
<td>111</td>
<td>① 322.1</td>
<td>Acceptable</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>② 314.5</td>
<td></td>
</tr>
<tr>
<td></td>
<td>②</td>
<td>1,017</td>
<td>871</td>
<td>23</td>
<td>110</td>
<td>① 322.1</td>
<td>Acceptable</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>② 318.0</td>
<td></td>
</tr>
<tr>
<td></td>
<td>③</td>
<td>1,017</td>
<td>871</td>
<td>23</td>
<td>112</td>
<td>① 320.3</td>
<td>Acceptable</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>② 320.9</td>
<td></td>
</tr>
</tbody>
</table>
Root Cause Analysis

The investigation team found traces of non-uniform force applied to the washer of the 2\textsuperscript{nd} cylinder. Fortunately, there were no traces in other cylinders except the broken one. Did further investigation to determine the cause of the non-uniform forces.
Root Cause Analysis

OEM’s instruction manual omitted a procedure to check the inclination of the flange. We performed a test to assemble the piston rod according to OEM’s instruction manual at the OEM’s maintenance shop, and as a result, confirmed there was a 0.5mm of deviation. Since our workers assembled the piston rod according to the OEM’s guide, it is highly likely that they made a similar mistake. Therefore we performed a FEM analysis to find out how much inclination can cause failure of the piston rod.

Case 1: 0.4mm inclination

- CL: 1.055mm
- CL: 0.64mm
- Deviation: 0.415mm

Case 2: 0.7mm inclination

- CL: 1.145mm
- CL: 0.453mm
- Deviation: 0.692mm

Case 3: 0.9mm inclination

- CL: 1.5mm
- CL: 0.63mm
- Deviation: 0.87mm
Confirmed through FEM analysis that if there is a 0.7mm of inclination between a flange and a washer, the stress concentration (68.3 MPa) above the allowable stress occurs at the piston rod. (Maximum allowable stress: 68.1 MPa)

It means the rod may break if the inclination is greater than 0.7mm during assembly.
Solution

For assembling the piston nut with the same torque, the maintenance procedure improved as follows.

1) When assembling the piston rod nut, tighten the multi jackbolts 4 times by increasing the torque sequentially. (5%, 30%, 60%, 100%)

2) Check the clearance between flange and piston rod nut at every step, and adjust so that it is less than 0.1mm.

3) Train maintenance workers on the proper procedure to assemble the multi jackbolt tensioner.
## Solution

The instruction manual supplemented in detail so that the method of operation can be easily understood.

<table>
<thead>
<tr>
<th>Procedure</th>
<th>Before</th>
<th>After</th>
</tr>
</thead>
<tbody>
<tr>
<td>1. Spin the tensioner onto the main thread until it sets against the washer. You have to back off the tensioner to provide 1mm to 3mm gap. If you can’t see the gap, instead you may back off around 180°.</td>
<td>When tightening the multi jackbolts, it is very important to minimize the differential gap between the surface of the bolt body and the flange.</td>
<td></td>
</tr>
<tr>
<td>2. Tighten (4) jack-bolts at 90° apart (12:00 6:00 9:00 and 3:00) with a partial torque (50%).</td>
<td>1. Spin the tensioner onto the main thread until it sets against the washer. You have to back off the tensioner to provide 1mm to 1.5mm gap. If you can’t see the gap, instead you may back off around 120~180°</td>
<td></td>
</tr>
<tr>
<td>3. At 100% target torque, tighten the same (4) jack-bolts.</td>
<td>2. Tightening the jack-bolt by the hand, and then adjust the differential gap between the bolt body and the washer to become less than 0.1mm.</td>
<td></td>
</tr>
<tr>
<td>4. At 100% target torque, tighten all jack-bolts in a circular pattern.(1 round only)</td>
<td>3. Tighten the jack-bolts with 5% of the prescribed torque according to the sequential order (Note) Make sure the differential gap is less than 0.1mm. If the differential gap is bigger than 0.1mm, start over again.</td>
<td></td>
</tr>
</tbody>
</table>
Lessons learned

• Incorrect tightening of bolts can cause fatigue failure by stress concentration, even if there are no problems in design and operation.

• It is most important to assemble the piston rod nut in parallel, to avoid excessive stress.

• The proper procedures should be provided to prevent maintenance errors regardless of the worker’s skill. And it is highly recommended to inspect and verify the critical points.

We checked all the other cylinders and compressors, and there was about 0.3mm of the inclination. We reassembled all of them according to the revised procedure and confirmed the inclination was less than 0.1mm. Since then, for about four years, the reciprocating compressors are operating well without any problem.
ACKNOWLEDGEMENTS

This work has been encouraged by the Korea Rotating Machinery Engineers Association, (KRMEA). The authors are grateful for the encouragement.