

DYNAMIC CHARACTERIZATION OF FULLY PARTITIONED DAMPER SEALS

A Thesis

by

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ABSTRACT

Balance piston gas seals restrict leakage at the discharge of centrifugal compressors. There are multiple types including labyrinth seals, textured seals, pocket damper seals (conventional PDS), and fully-partitioned pocket damper seals (FPDS). These annular seals develop large radial forces due to the high pressure differentials and gas density, which have a measureable impact on the compressor's rotordynamic performance. There is an extensive experimental database available for labyrinth seals and textured seals. However, there is not a comprehensive database for PDS and FPDS to compare against textured seals.

This investigation aimed at evaluating the rotordynamic performance of FPDS. Dynamic force coefficients were experimentally identified for the FPDS operating with three pre-swirl levels (Low, Medium, High), three pressure ratios (25%, 50%, 65%), and three rotor speeds (10, 15, 20 krpm). The results show the FPDS develops either similar effective damping coefficients or higher, for particular cases, when compared to a honeycomb seal. At low preswirl, the FPDS displays similar to higher effective damping values at synchronous to super-synchronous frequencies. The main difference between honeycomb and FPDS lies in their direct stiffness and leakage values. Honeycomb seals develop relatively large stiffness coefficients, whereas FPDS display either negative or negligible stiffness values depending on the pressure ratio. The FPDS leaks roughly ~33% more than the honeycomb seal. With these results, it is concluded that the FPDS

should be chosen in a case-by-case situation, considering the location of the system natural frequencies, rather than an over-all replacement for textured seals.

DEDICATION

To my sister, mother, and father, thank you for the motivation and being my stone. My values come from your teachings and helped me gain the friends and love ones I experience today. I appreciate the sacrifice you did to make the family successful and I only hope I can continue the torch.

To Veronica, I cannot say how much I admire you. Seeing you smile relaxes me and allows the kid in me enjoy the time we have together.

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The principle investigator for this work is Dr. Adolfo Delgado. The thesis committee members include Dr. Adolfo Delgado and Dr. Luis San Andrés from the Mike J. Walker Department of Mechanical Engineering and Dr. Paul Cizmas from the Department of Aerospace Engineering. Undergraduates Andrew Moody and Sean McLean assisted with the collection of high preswirl data. The student completed all other work.

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NOMENCLATURE

e_o	Eccentricity
ω	Rotor frequency
Ω	Excitation frequency
C	Direct Damping
c	Cross-coupled Damping
D	Diameter
F_r	Radial Force
F_t	Tangential Force
K_{ij}	$i=j$ is direct component; $i \neq j$ cross-coupled component
K	Direct Stiffness
k	Cross-coupled Stiffness
L	Length
CC	Cross-coupled
GVF	Gas Volume Fraction
HP	Hole-Pattern Seal
HC	Honeycomb Seal
kcpm	Thousand Cycles Per Minute
krpm	Thousand Revolutions Per Minute
Laby	Labyrinth Seal
PDS	Pocket Damper Seal

PR Pressure Ratio

FPDS Fully-Partitioned Pocket Damper Seal

1. INTRODUCTION

1.1 GAS ANNULAR SEALS

Today's needs in turbomachinery require higher pressures, rotating speeds, and compressor loads while maintaining acceptable levels of vibration. Annular seals can generate large radial forces and have a measurable impact on the rotordynamic performance of centrifugal compressors. Balance piston seals are the longest seals and are subjected to the largest pressure differentials in the machine. These are located at the center of a back-to-back compressor near the rotor's mid length or after the last stage of a straight-through compressor.

Labyrinth seals are a common balance piston used in industry due to their simplicity and manufacturability. These seals are effective in reducing leakage but can cause instability due to circumferential flow [1-4]. Other seal types such as the honeycomb, hole-pattern, and pocket dampers seals provide larger stiffness and damping when compared to labyrinth seals and can increase the stability margin of the machine [5-7].

Figure 1 shows examples of labyrinth, honeycomb, hole-pattern, and FPDS. Honeycomb seals have a hexagon pattern, while hole-pattern seals feature round holes. Similar to labyrinth seals, PDS feature circumferential grooves but also include circumferential buffer walls running axially, dividing the grooves into multiple pockets.

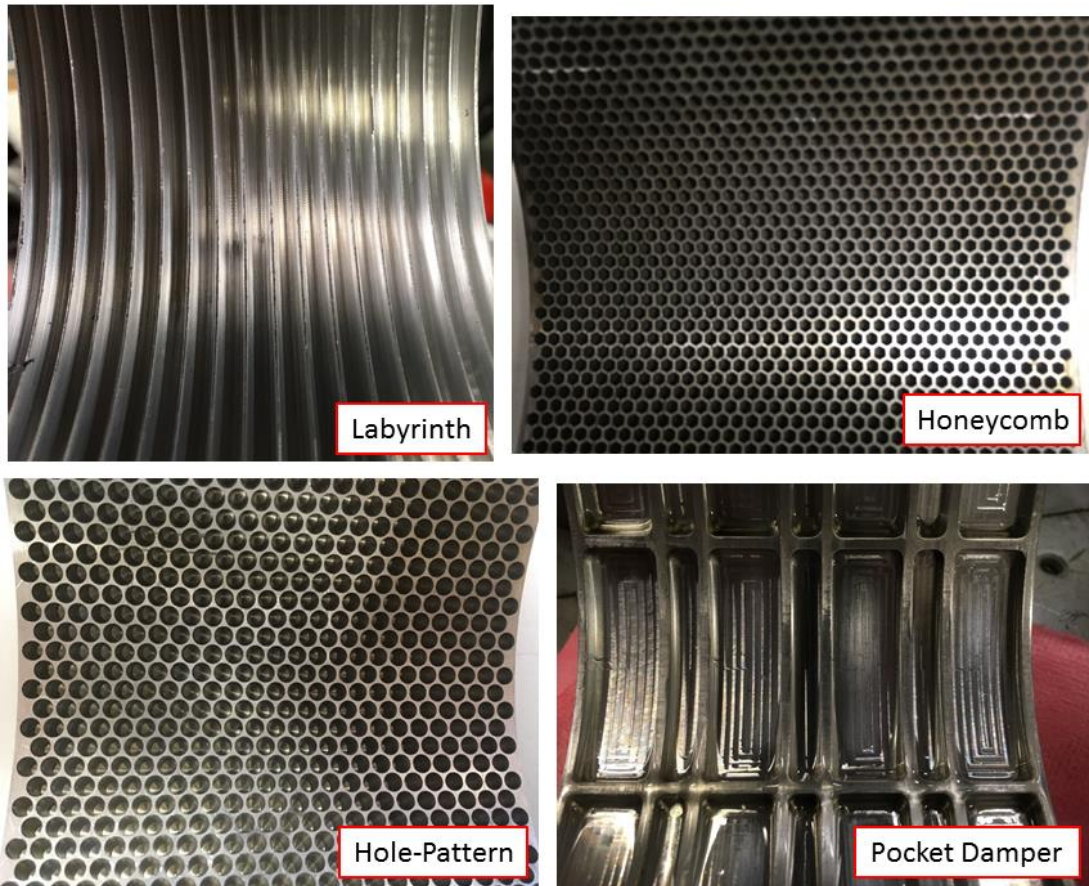


Figure 1 Close-up pictures of labyrinth, honeycomb, hole-pattern, and fully-partitioned pocket damper seals

1.2 POCKET DAMPER SEALS

Figure 2 shows a comparison between the conventional PDS and a FPDS.

Conventional PDS include active and inactive segments alternating along the length of the seal. Inactive segments are continuous circumferential grooves similar to those in labyrinth seals (i.e. without buffer walls). The inactive segments in the PDS are plenums maintaining constant boundary pressure for the cavities during rotor whirl [7, 8]. Active groove segments are segregated with buffer walls. A FPDS includes buffer walls spanning the entire length of the seal, thus including only active segments. The PDS may

include notches toward the exit blade to provide a diverging clearance, where the FPDS only has a straight through clearance.

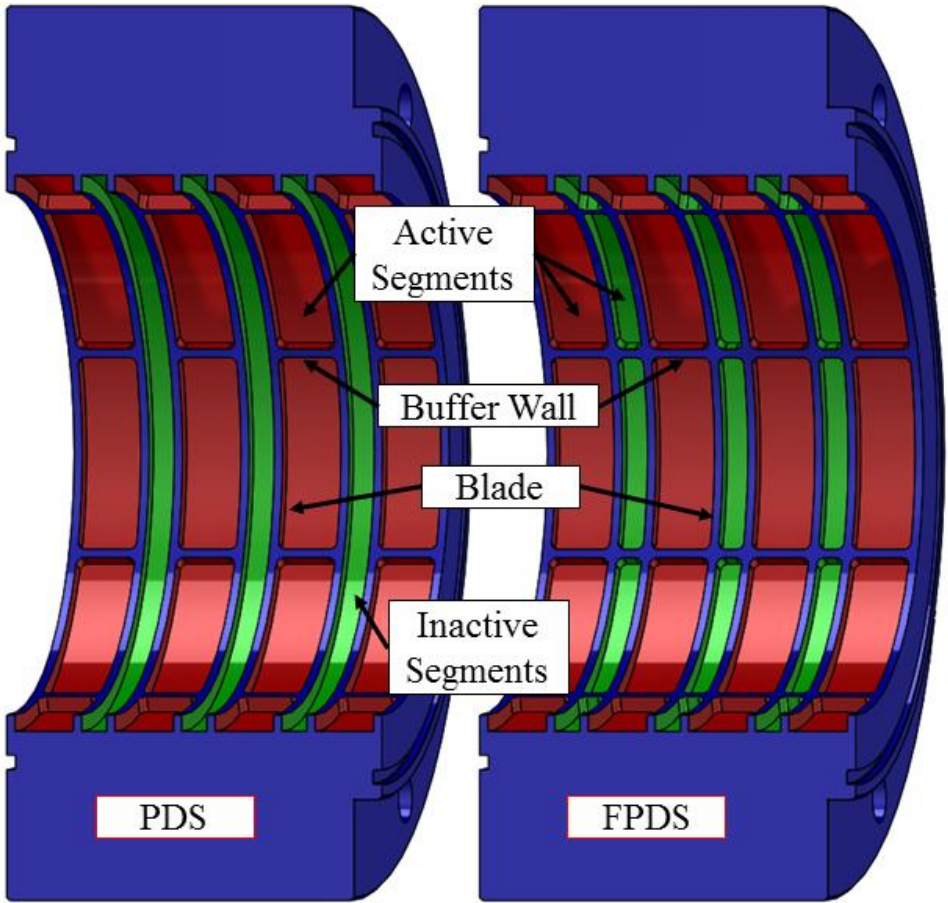


Figure 2 Differences between a standard PDS and FPDS

2. LITERATURE REVIEW

This literature review focuses on the dynamic performance of fully-partitioned pocket damper seals (FPDS) while briefly mentioning work related to textured seals. Please refer to [9-12] for a comprehensive review over textured seals

In 1965, Alford [8] explains the probable causes for destabilizing forces in axial flow turbomachinery. The author covers two main causes. The first one is the non-uniform circumferential static pressure acting on the rotor surface, and the second is the rotor eccentricity caused unequal circumferential blade clearance. The analysis of the labyrinth seals shows that a non-uniform circumferential pressure is directly related to radial deflections. This varying pressure provides a total radial force comprising two components, one parallel to deflection and the other perpendicular. Alford concludes that a labyrinth seal having a diverging clearance (tooth clearance increases along the flow direction) is more stable than a converging clearance, and rotor whirl begins at a torque level proportional to the rotor bearing system stiffness. The author only accounts for axial flow in the analysis, and neglected circumferential flow because it was assumed it had no effect on pressure within the seal. This shows inconsistent to the investigation from Benckert and Wachter [1], who identified circumferential flow in labyrinth seals directly affect the seal's destabilizing forces. Inlet preswirl was identified as a critical parameter and Benckert and Wachter concludes that reducing this value can significantly improve the seal dynamic performance.

Von Pragenau [13] shows that using a textured stator over a smooth stator results in lower circumferential flow and axial thin film fluid velocities, and consequently, decreases cross-coupled stiffness and leakage rate.

Vance and Schultz [14] presents a new invention in 1993 on a damper seal calling it the TAMSEAL. The new seal, later called PDS, provides damping from two distinct features. The first feature is the labyrinth's blade divergence clearance along the length of the seal. The second feature is the buffer walls dividing the circumferential grooves into pockets and reducing circumferential flow. Vance and Li [15] tests and presents the results for this new damper seal. Coast-down tests serve to evaluate the seal effectiveness when crossing a critical speed and impact tests provided force coefficients. The pocket damper seal proves to have significantly more damping than a traditional labyrinth seal.

In 1999, Li et al. [16] creates a bulk-flow model for a single cavity pocket damper seal. The model uses turbulent shear stress parameters and Moody's friction factors. The authors compare the model to experimental data from Li [17] for a 4-pocket single cavity damper seal. Results show the predictions agree with measurements for leakage and direct damping. The model highlights the influence of rotor speed and pressure drop in the pocket damper seal dynamic performance. Results also show the pocket damper seal has larger damping when compared to the labyrinth seal.

Li et al. [18] tests a straight-through honeycomb seal and a pocket damper seal, both with a length to diameter ratio (L/D) of 0.54, on a flexible rotor. The author tests the seals, oriented in a back-to-back configuration, with different eccentricities at

maximum supply pressure of 500 psi and preswirl values ranging from zero to 0.5. The authors only report experimental measurements in direct force coefficients with identifying effective stiffness and damping through a predictive code. The experimental results show that both seals produce high effective damping, where the honeycomb seal has positive stiffness, but the pocket damper seal has negative stiffness. Test results showed the effective damping decreases with eccentricity for both seals.

In 2003, Sprowl [5] tests two seals, a honeycomb seal and a labyrinth seal, with three pressure drops (.15, .35, .50 pressure ratio), three rotor speeds (10, 15, 20 krpm), and three preswirls (0, 30, 60 percent). The results show that preswirl does not affect effective stiffness, but does evidently affect effective damping. Effective stiffness drops 68% when the cavities in the honeycomb seal fill from debris and transits into a smooth seal; simulating a response when the honeycomb seal's holes fill with metal particles and debris. Effective damping also drops to around 25 to 35 percent and increases the crossover frequency. Crossover frequency is the whirl frequency where the effective damping changes from negative to positive values. The lower the crossover frequency the more stable the system is.

Ertas and Ertas et al. [19, 20] measure the stiffness and damping coefficients from eight and twelve bladed pocket damper seals. The authors tests with a supply pressure up to 70 bar, rotor speeds up to 20 krpm, and whirl frequency excitation from 20 to 300 Hz. The eight bladed seal experiences the highest negative magnitude direct stiffness and positive direct damping, but all seals produce positive direct damping and same sign cross-coupling stiffness. Results show a conventional seal, a seal with active

and inactive grooves, has a diverging clearance experiences large negative magnitude direct stiffness, but decreases in magnitude with increasing whirl frequency. The same seal with no clearance ratio has a negative stiffness at lower frequencies, but transitions into positive stiffness at higher frequencies. Pressure in the cavities affect phase and force density. The clearance ratio has the strongest effects of force coefficients when comparing to straight-through clearance. And the pressure ratio only has strong influence under lower frequencies.

Brown and Childs [21] tests a hole pattern seal with negative preswirls. The seal dimensions were similar to those of the seal investigated by Wade and Childs [6]. The authors tests with 70 inlet bar running up to 20 krpm rotor speed, and pressure ratios from 0.5 to 0.7. The pressure ratio is the exit pressure to inlet pressure. Direct coefficients are not affected by changing pressure ratio, speed, nor preswirl. Changing the pressure ratio shows no influence on effective damping. Cross-coupled coefficients increase in magnitude with rotor speed and decrease with an increase in negative preswirl. Changing preswirl shows little influence on direct damping for 20 krpm and 50% pressure ratio. The results provide evidence that negative preswirl helps in stabilizing the rotor. This is shown with increases in peak effective damping and lowering crossover frequency when comparing low and negative preswirl results.

Ertas et al. [7] tests labyrinth, honeycomb, and fully-partitioned pocket damper seals comparing their rotordynamic force coefficients. The authors test all seals with a low pressure ratio and in choked conditions, with a supply pressure of 6.9 bar discharging to atmosphere. All seals experience negative effective damping at low

frequencies and increases in magnitude with preswirl. The pocket damper seal results display the lowest crossover frequency when comparing to other seals. With preswirl, the labyrinth seal has negative effective damping up to 100 Hz excitation frequency. When comparing both the honeycomb seal and FPDS to the labyrinth seal, the crossover frequency is greatly reduced, for both of the seals, to 40-60 Hz and the peak effective damping is increased. From the pocket pressure analysis in the FPDS, the preswirl demonstrates to be the dominant factor affecting seal stability. With preswirl, the effect in destabilizing forces show larger toward upstream than downstream of the seal.

In 2012, Li et al. [22] numerically calculates the leakage and rotordynamic coefficients for both a labyrinth seal and a fully-partition pocket damper seal by supplying both with a multi-frequency excitation whirl orbit and Reynolds-averaged Navier-Stokes solution. The authors simulate two positive preswirls, two negative preswirls, and a low preswirl to predict their effect response of dynamic performance. The authors compare the numerical results to Ertas et al. [19] experimental values and show good agreement. The labyrinth seal's direct stiffness decreases and direct damping increases with increasing preswirl. The pocket damper seal shows no effect in direct force coefficients from increasing preswirl. For both seals, increasing the positive preswirl increases the cross-coupled stiffness resulting in a reduction of effective damping.

In 2013, Vannini et al. [2] builds a test rig to investigate a labyrinth and pocket damper seals response over negative preswirl, differences between single and multi-frequency excitation, and the difference between centered and offset seals. The authors

find that negative preswirl shows a stabilizing effect in the seals. Results show testing with a multi frequency excitation proves to have a similar effect to single frequency excitation. Having the seal with a static offset, within 10% of seal clearance, shows negligible effect on the dynamic performance when comparing to a centered seal. The pocket damper seal displays a higher effective stiffness and damping coefficients when compared to the labyrinth seal.

Li et al. [23] presents a transient CFD method on the effects of preswirl, rotor speed, and pressure ratio of a fully-partitioned pocket damper seal. The authors use a previous analysis from Li et al. [22] and compare predictions to experimental results from Ertas et al. [7]. From the numerical results, coefficients are mostly affected by inlet pressure more than the discharge pressure. The dynamic forces and effective damping show a dependence on pressure ratio. Results show the crossover frequency increases and effective damping values decrease when increasing either rotor speed or preswirl.

Vannini et al. [4] in 2015, presents a case study with experimental measurements and theoretical results from a single stage compressor for a wet-gas compression application. Wet-gas refers to the presence of liquid within a mostly air volume. The labyrinth seal predictions results agreed with the experimental sub-synchronous vibration experienced in the compressor in field operation. CFD contour plots were created, showing swirl is significant in the labyrinth seals. Inserting a fully-partitioned pocket damper seal into the CFD model theoretically reduces swirl, but in effect causes a higher leakage than the labyrinth seal. Their choice in reducing the vibration was decided a higher priority than leakage.

3. MODELING BEARING OR SEAL

In 1993, Rovas and Childs [24] derived a model to characterize the dynamic performance of a seal's reaction force with linear rotordynamic coefficients:

$$-\begin{Bmatrix} r_x \\ r_y \end{Bmatrix} = \begin{bmatrix} K_{xx} & K_{xy} \\ K_{yx} & K_{yy} \end{bmatrix} \begin{Bmatrix} \delta x \\ \delta y \end{Bmatrix} + \begin{bmatrix} C_{xx} & C_{xy} \\ C_{yx} & C_{yy} \end{bmatrix} \begin{Bmatrix} \delta \dot{x} \\ \delta \dot{y} \end{Bmatrix} + \begin{bmatrix} M_{xx} & M_{xy} \\ M_{yx} & M_{yy} \end{bmatrix} \begin{Bmatrix} \delta \ddot{x} \\ \delta \ddot{y} \end{Bmatrix} \quad (1)$$

where r_x and r_y represent seals reaction forces. K_{xx} and K_{yy} are direct stiffness. K_{xy} and K_{yx} are cross-couple stiffness. C_{xx} and C_{yy} are direct damping. C_{yx} and C_{xy} cross-coupling damping. M_{xx} and M_{yy} are direct virtual masses. M_{xy} and M_{yx} are cross-coupled virtual masses. δx and δy are displacements, $\delta \dot{x}$ and $\delta \dot{y}$ are velocities, and $\delta \ddot{x}$ and $\delta \ddot{y}$ are accelerations.

Assuming small motions within the center, equation 1 reduces to,

$$-\begin{Bmatrix} r_x \\ r_y \end{Bmatrix} = \begin{bmatrix} K & k \\ k & K \end{bmatrix} \begin{Bmatrix} \delta x \\ \delta y \end{Bmatrix} + \begin{bmatrix} C & c \\ c & C \end{bmatrix} \begin{Bmatrix} \delta \dot{x} \\ \delta \dot{y} \end{Bmatrix} + \begin{bmatrix} M & m \\ m & M \end{bmatrix} \begin{Bmatrix} \delta \ddot{x} \\ \delta \ddot{y} \end{Bmatrix} \quad (2)$$

As the rotor displaces from the center, the fluid responds with a force in the radial and tangential direction. The radial force is in line with the rotor displacement vector, where the tangential force is in line with the rotor velocity vector. Figure 3 below shows a rotor moving in a forward procession, circling at an excitation frequency. The rotor displaced from the seal's center is called journal eccentricity and is denoted as e_o in the figure below [25].

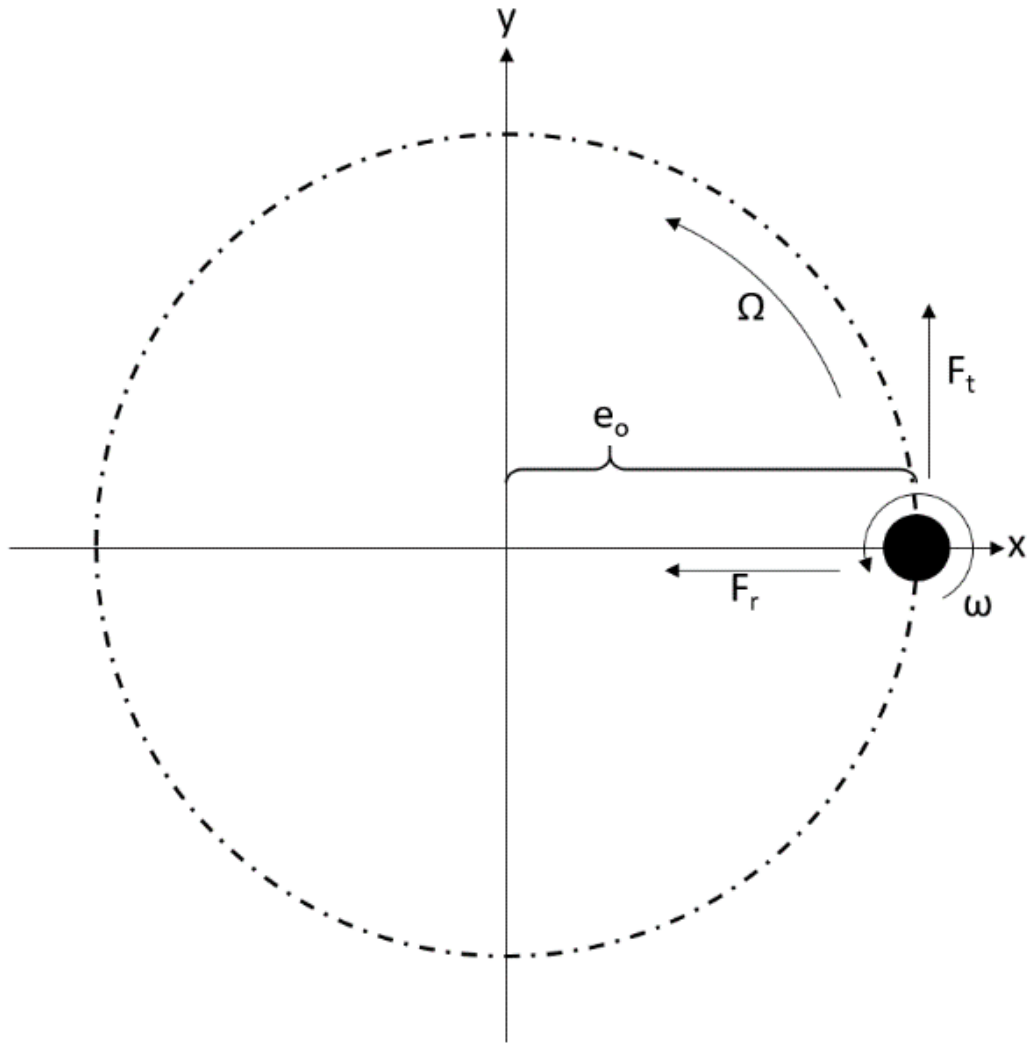


Figure 3 Rotor precession with radial and tangential forces

The radial and tangential forces shown above are called the effective stiffness and effective damping forces, respectively. Using terms from equation (2), the radial and tangential forces can be derived as,

$$\begin{aligned}
 F_r &= (K + c\Omega - M\Omega^2)e_o \\
 F_t &= (-k + C\Omega - m\Omega^2)e_o
 \end{aligned}
 \tag{3}$$

4. TEST RIG DESCRIPTION

4.1 TEST RIG

Figure 4 shows the test rig detailing stator assembly components. The test stand was originally designed in 1994 to test hydrostatic bearings [26]. Two stainless steel pedestals each hold a hydrostatic bearing that supports a 4.5 inch diameter rotor. The pedestals are 15 inches apart to accept a stator assembly in between. The cage surrounding the entire test section supports the hydraulic shakers, horizontal and vertical stiffeners. All components share this foundation to provide an increased structural stiffness to the stator assembly. The hydrostatic bearings housing includes pressure transducers to measure supply pressures within the bearing. Pressure transducers also measure the supply pressure at stator inlet and seal exit. The accelerometers, located orthogonally to each other, measure acceleration of the stator assembly. Four proximity probes, also orthogonal to the accelerometers, measure the position of the stator in reference to rotor shaft. Temperature probes are located at seal inlet, outlets, and piping system. The oil supply splits into two sections to the test rig. One is specifically for the seal inlet and the other is for the bearing lubrication. Two pumps provide oil supply for the bearings. Temperature probe readings help maintain acceptable operating conditions for the hydrostatic bearings.

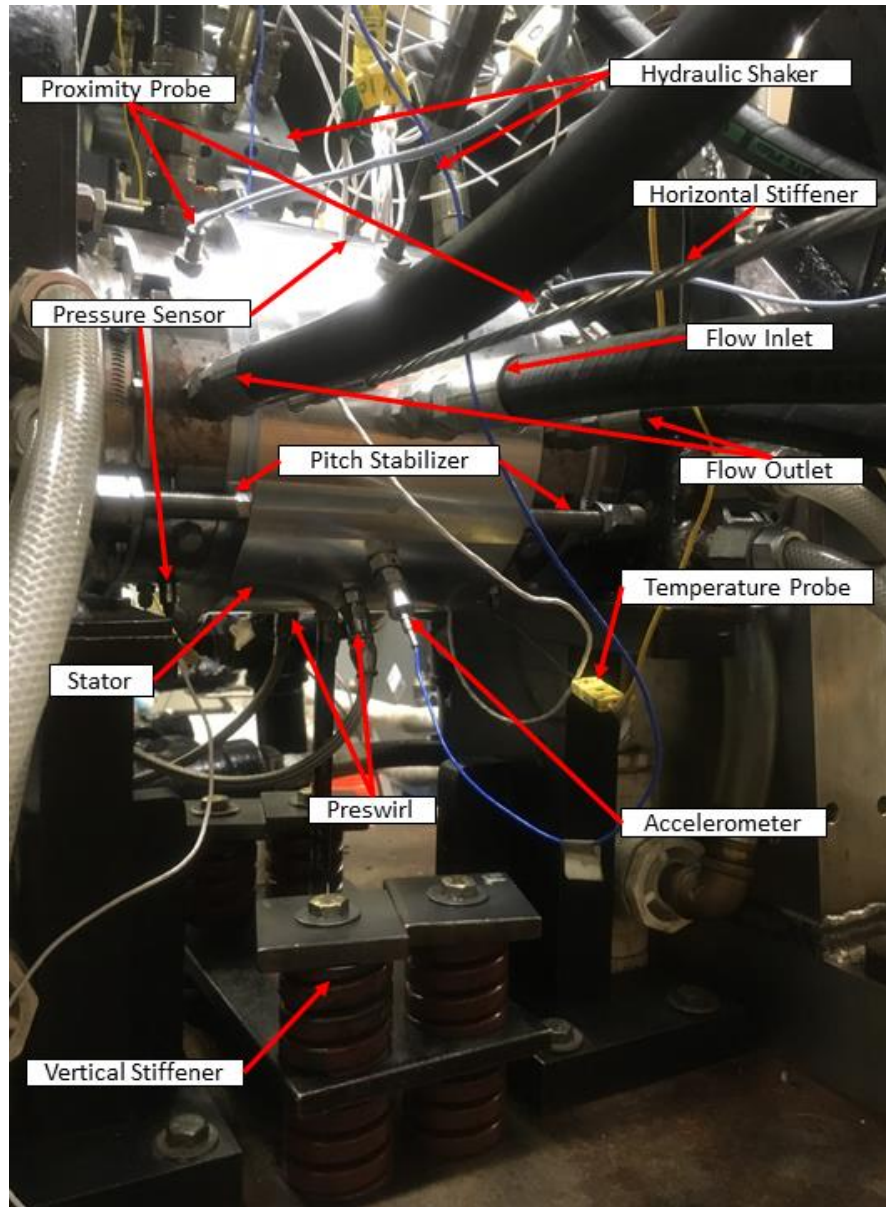


Figure 4 Close-up of the test section depicting stator assembly components

Figure 5 shows the cross-section of the stator assembly. Both a static and pitot tube connect to a differential pressure sensor. The measured value defines the preswirl ratio over a rotor speed.

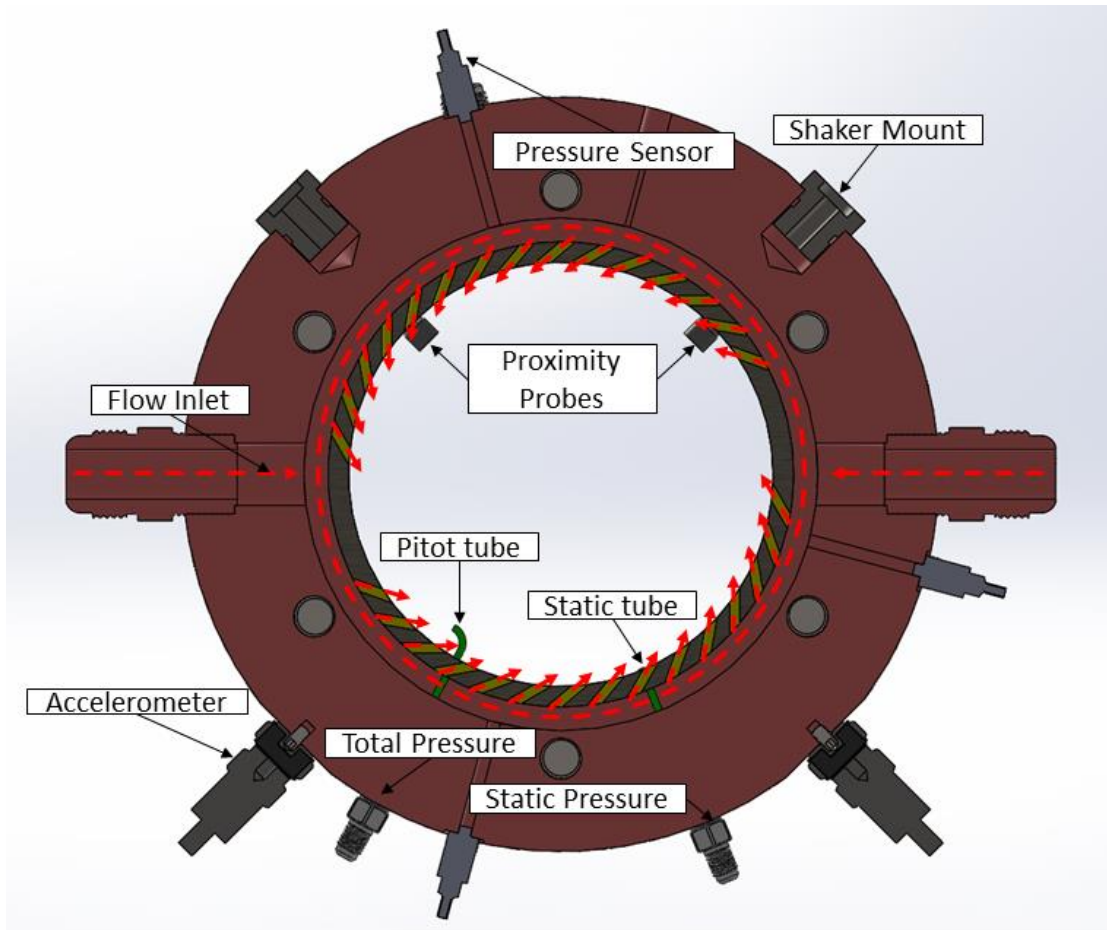


Figure 5 Cross-section of the stator assembly

4.2 TEST SEAL

Table 1 and Figure 6 provides the test seal properties and dimensions, respectively. As mentioned before, comparing to a FPDS, a conventional PDS features baffle walls only within its active pockets and not within its inactive pockets. This allows fluid to flow circumferentially within the inactive segment. For a FPDS, all segments restrict circumferential flow. The seal material is aluminum 7075 T6 and is

CNC milled from an entire billet. The seals fit into the stator in a back-to-back configuration to reduce axial thrust.

Table 1 Seal properties

ID (inches [mm]):	4.531 [115]	# of Pockets per Cavity:	8
Length (inches [mm]):	3.375 [85.7]	# of Buffer Walls (Circumferential):	8
L/D ratio:	0.745	# of Axial Pockets:	7
Material:	7075-T6	# of Small and Large Active Cavities:	3,4
Radial Clearance (inches [mm]):	.008 [.2]	# of Blades:	8
Pocket Depth (inches [mm]):	.1425 [3.6]	Small to Large Active Length Ratio:	0.429

5. EXPERIMENTAL RESULTS

5.1 TEST PROCEDURE

Table 2 shows the test matrix. When beginning the experiment, the inlet pressure and pressure ratio are first adjusted before increasing rotor to the desired speed. The test rig's first test condition, for any preswirl, is 25% pressure ratio with the rotor operating at 10 krpm. This specific test condition has the inlet pressure and exit pressure at 70 and 17.5 bar, respectively. The flow is choked at this pressure ratio. Once the system reaches steady state condition, the electrohydraulic shakers input a pseudorandom excitation sequentially for each axis, following the procedure described in [24]. The pseudorandom excitation lasts roughly 30 seconds providing 10 averages, and it is repeated 3 times for each axis. This procedure is repeated for the 15 and 20 krpm rotor speeds, before adjusting the discharge pressure to achieve the next pressure ratio.

Table 2 Test Matrix

Preswirl	Inlet/Exit Pressure (Bar [psi])	Pressure Ratio (%)	Rotor Speed (krpm)	Rotor Surface Speed (m/s)
Low, Medium, and High	70/17.5 [1015/254]	25	10	60
			15	90
			20	120
	70/35 [1015/508]	50	10	60
			15	90
			20	120
	70/45.5 [1015/660]	65	10	60
			15	90
			20	120

5.2 RESULTS

5.2.1 FULLY-PARTITIONED POCKET DAMPER SEAL

Figure 7 through Figure 11 represents the direct stiffness, cross-coupled stiffness, damping, effective damping, and effective stiffness for the FPDS, respectively.

Each figure is arranged into a three by three matrix. Each column represents rotor speed increasing from the left to right from 10 krpm, 15krpm, to 20krpm. Each row represents the inlet preswirl increasing from the top to bottom from low, medium, to high preswirl. Each graph in the matrix shows measured values from the FPDS. There are three sets of pressure ratios for the FPDS- 25%, 50%, and 65%. Each graph has a black dashed line representing the rotor's operating speed. Data to the left is excitation that is sub-synchronous to rotor speed and data to the right is excitation that is super-synchronous.

Figure 7 shows the direct stiffness vs excitation frequency for the FPDSs. Measured values show an overall increase in stiffness values with increasing excitation frequencies. The FPDS experiences negative direct stiffness for lower excitation frequencies. At high preswirl, the FPDS displays a decreasing trend resulting in negative direct stiffness for high excitation frequencies. Rotor speed and preswirl show no apparent influence on direct stiffness. The FPDS could potentially lower the machine natural frequency due to the negative direct stiffness and its axial location, but these values are relatively small when compared to an oil-lubricated tilting pad bearing (i.e. a 4" bearing with L/D: 0.3 would develop 10x to 20x larger direct stiffness coefficients).

Hence, even if the FPDS has negative stiffness, it is insignificant compared to the rotor-bearing system stiffness.

Figure 8 shows the cross-coupled stiffness vs excitation frequency. The measured values for the FPDS show frequency independence except for high preswirl. The cross-coupled stiffness values grow with an increase in rotor speeds and preswirls. At high preswirl, the measured values decrease when operating toward high excitation frequencies.

Figure 9 shows the damping versus excitation frequency for the FPDS. The measured values for the FPDS shows no apparent change with an increase in rotor speed nor preswirl. Measured values for the FPDS shows no influence from excitation frequency. Increasing from low to high preswirl increases damping to 25 percent at most.

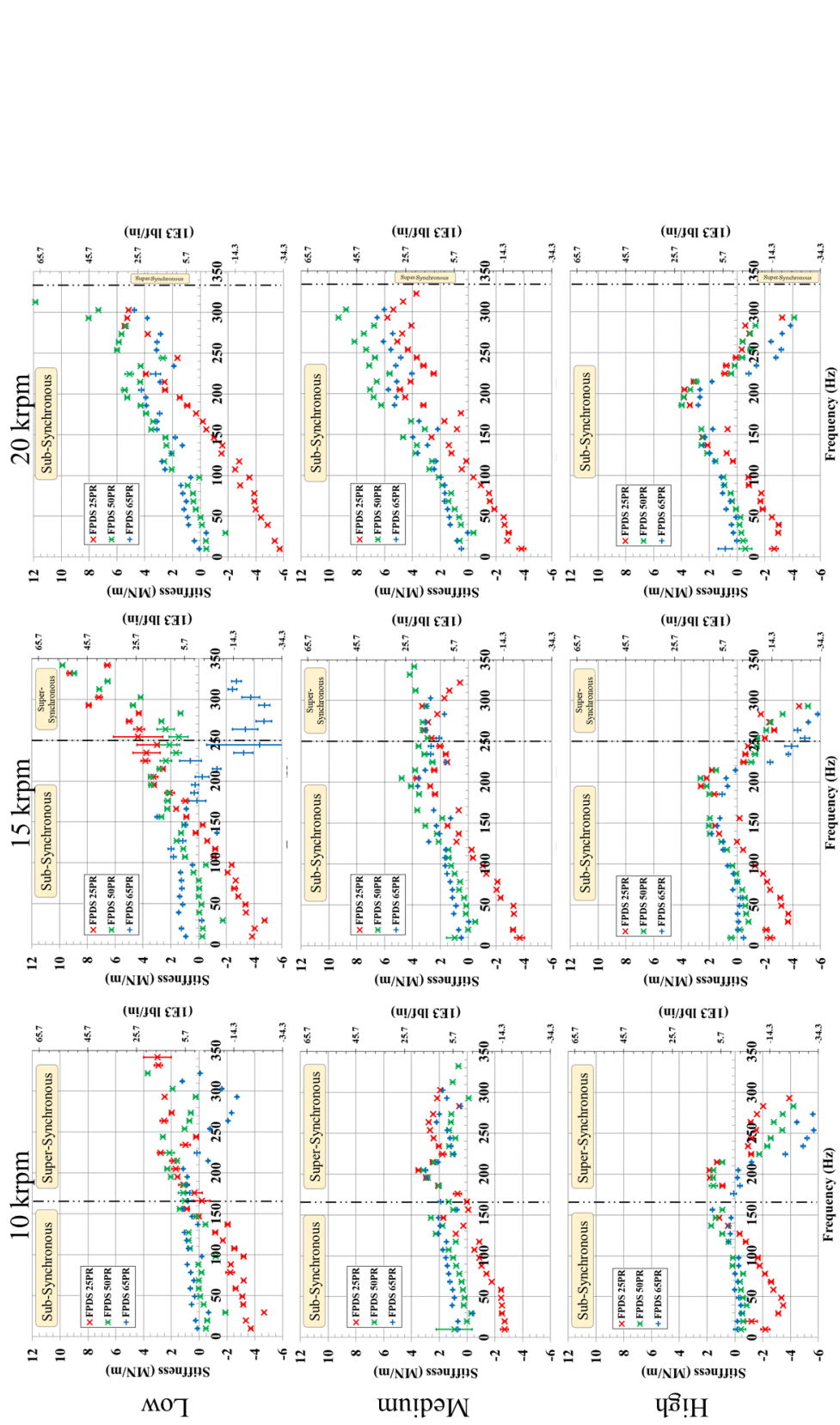


Figure 7 Direct stiffness coefficients versus frequency for FPDS, three pressure ratios (25%, 50%, 65%), three preswirls (low, medium, high), and three rotor speeds (10, 15, 20 krpm).

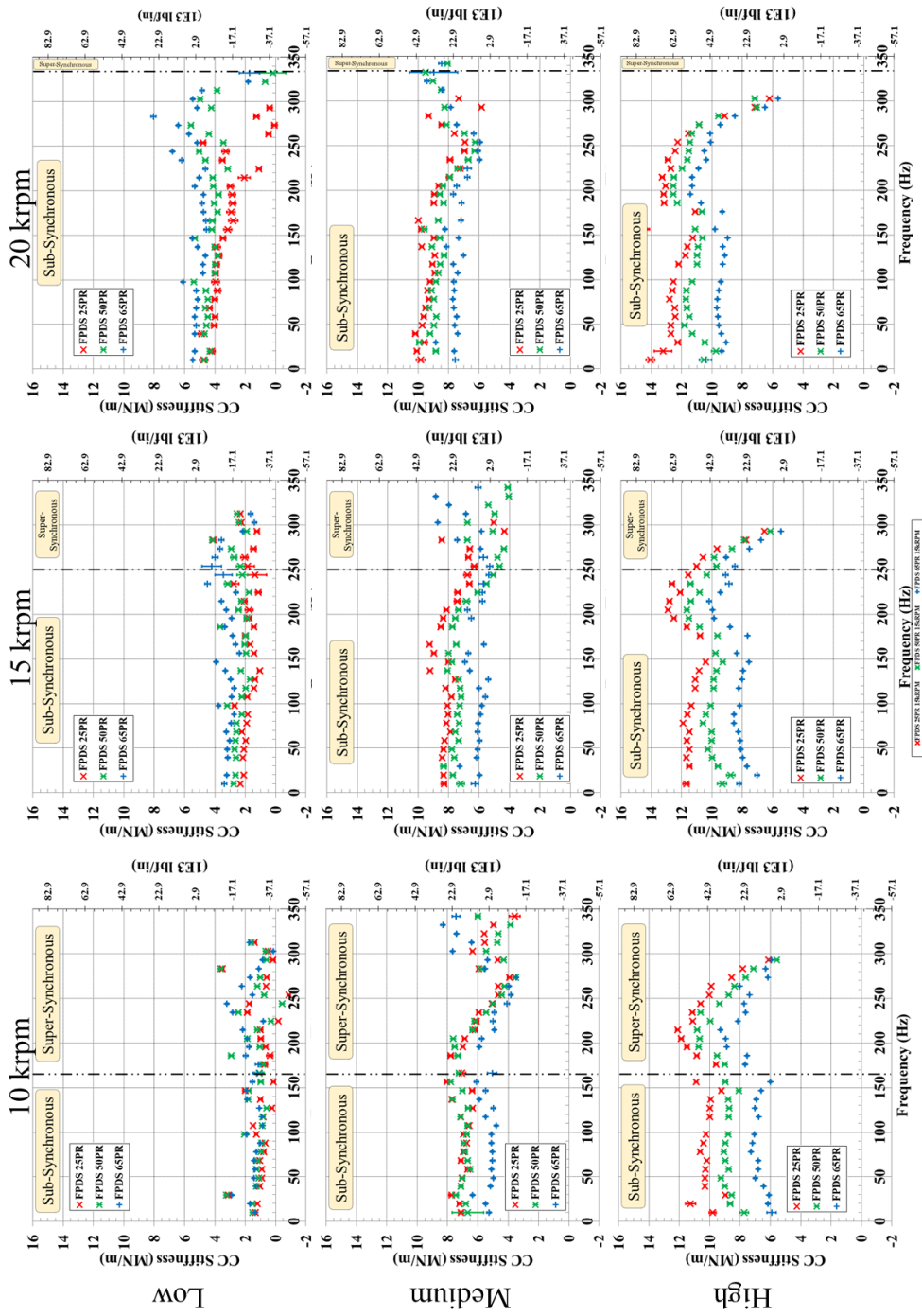


Figure 8 Cross-coupled stiffness coefficients versus frequency for FPDS, three pressure ratios (25%, 50%, 65%), three preswirls (low, medium, high), and three rotor speeds (10, 15, 20 krpm).

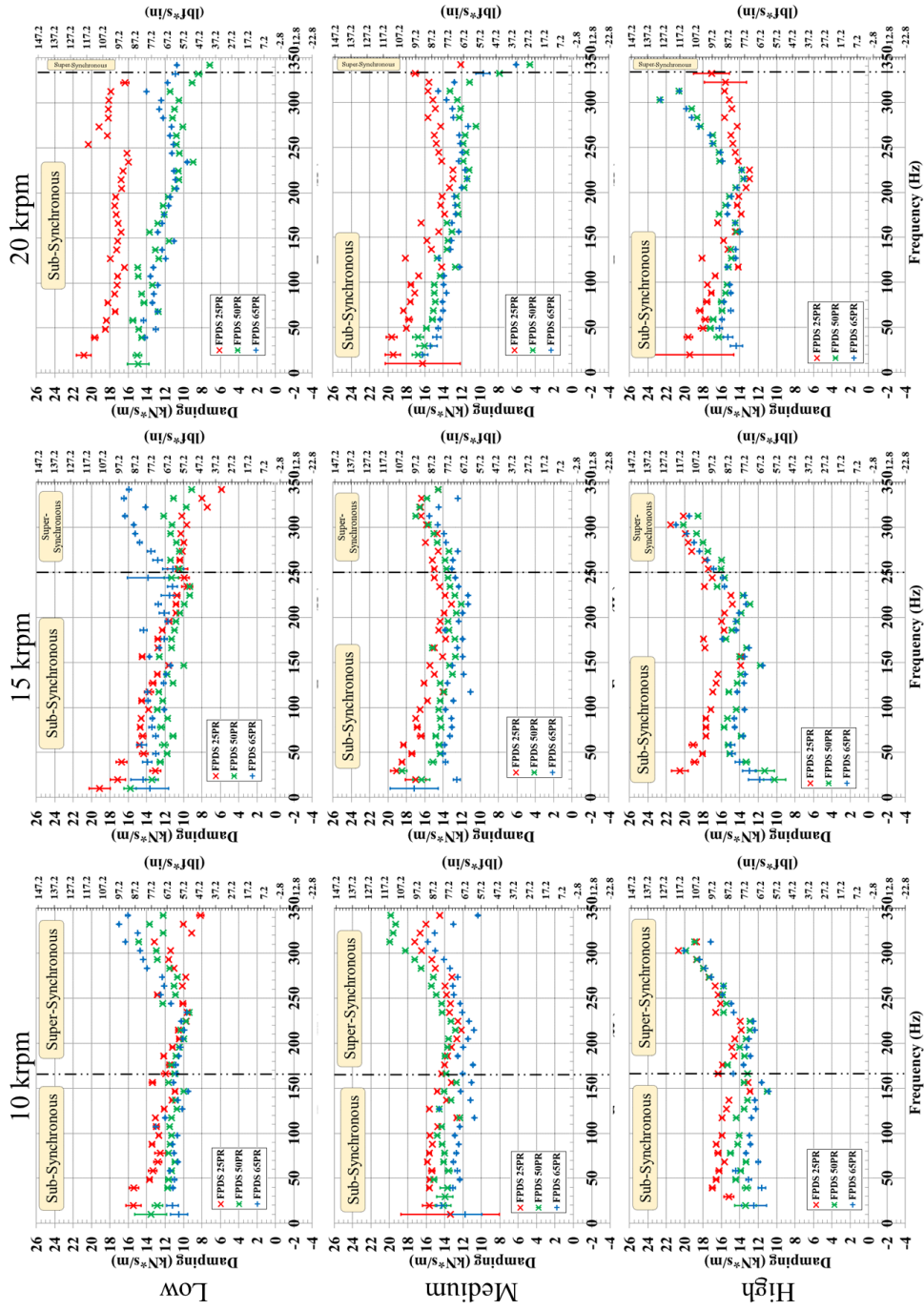


Figure 9 Direct damping coefficients versus frequency for FPDS, three pressure ratios (25%, 50%, 65%), three preswirls (low, medium, high), and three rotor speeds (10, 15, 20 krpm).

Figure 10 shows the effective damping versus excitation frequency, with the effective damping defined as [3, 10]

$$C_{eff} = C \left(1 - \frac{k}{C\omega} \right) \quad (4)$$

Effective damping combines the stabilizing and destabilizing contributions of the direct damping, “C”, and cross-coupled stiffness, “k”, respectively. The larger the positive value, the more stable the seal. Measured values for the FPDS shows higher influence for low excitation frequencies. At low excitation frequencies, the measured values are negative and can be a cause for concern if the systems natural frequency falls within this region. The frequency at which values for effective damping transfers from negative to positive is denominated crossover frequency. Crossover frequency for the FPDS increases with increasing rotor speed and preswirl. For 20 krpm, the crossover frequency increases from roughly 60 Hz to 120 Hz when transitioning from low to high preswirl. For low excitation frequencies the values are extremely negative as in the case of textured seals. The magnitudes at low frequencies grow with rotor speed and preswirl.

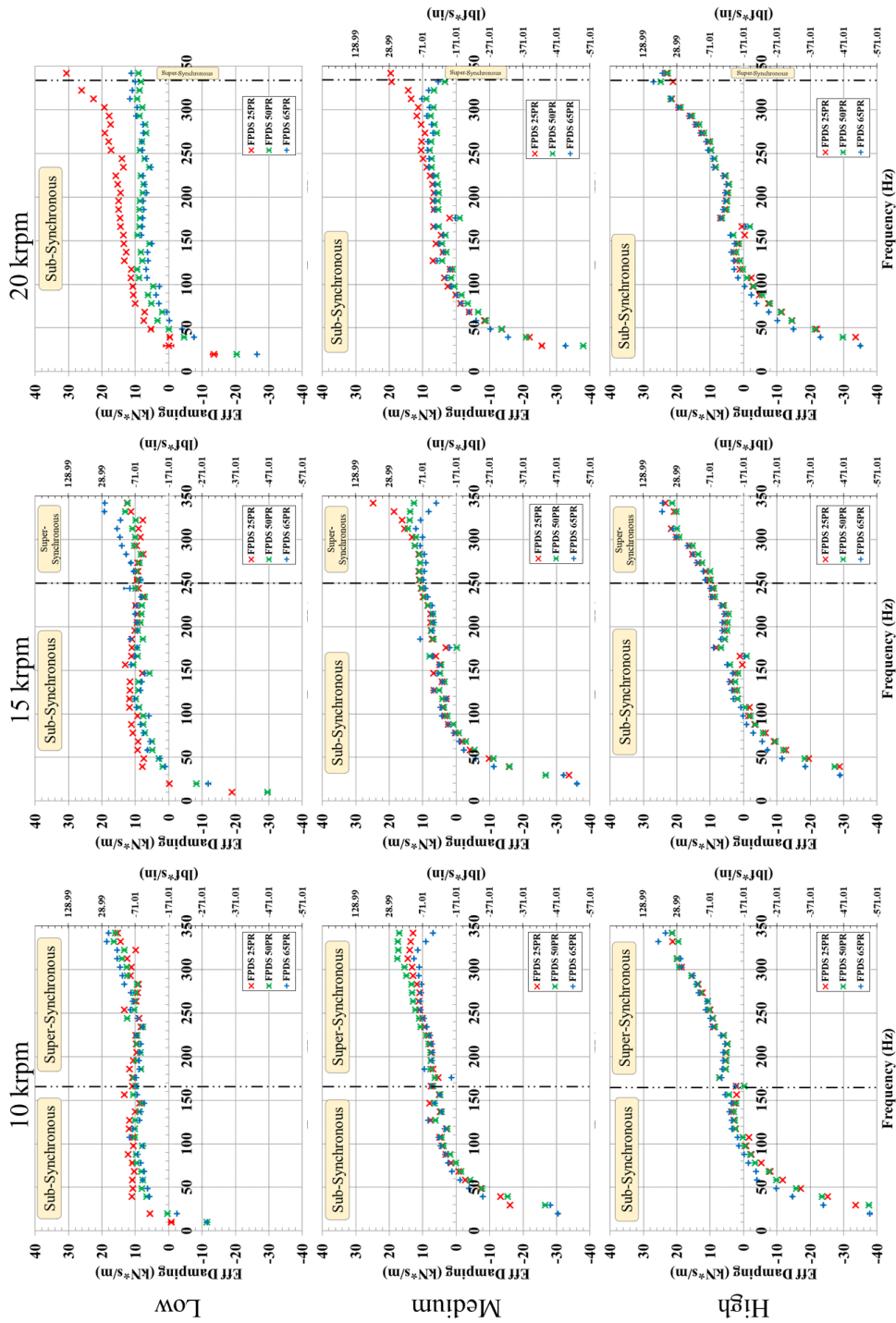


Figure 10 Effective damping coefficients versus frequency for FPDS, three pressure ratios (25%, 50%, 65%), three preswiris (low, medium, high), and three rotor speeds (10, 15, 20 krpm).

Figure 11 shows the effective stiffness vs excitation frequency for the FPDS. Effective stiffness combines both the cross-coupled damping and direct stiffness to provide the overall seal stiffness. Effective stiffness is defined as [3, 10]

$$\mathbf{K}_{eff} = (\mathbf{K} + \mathbf{c}\omega) \quad (5)$$

The experiments show effective stiffness values enlarge with an increase in excitation frequency except for high preswirl. At high preswirl, the measured values begin decreasing at 180 Hz. The values show the larger the pressure ratio the higher the influence of excitation frequency. The 65 percent pressure ratio shows to have a larger negative linear digression than the 50 and 25 percent pressure ratios. No explanation is determined for this phenomenon.

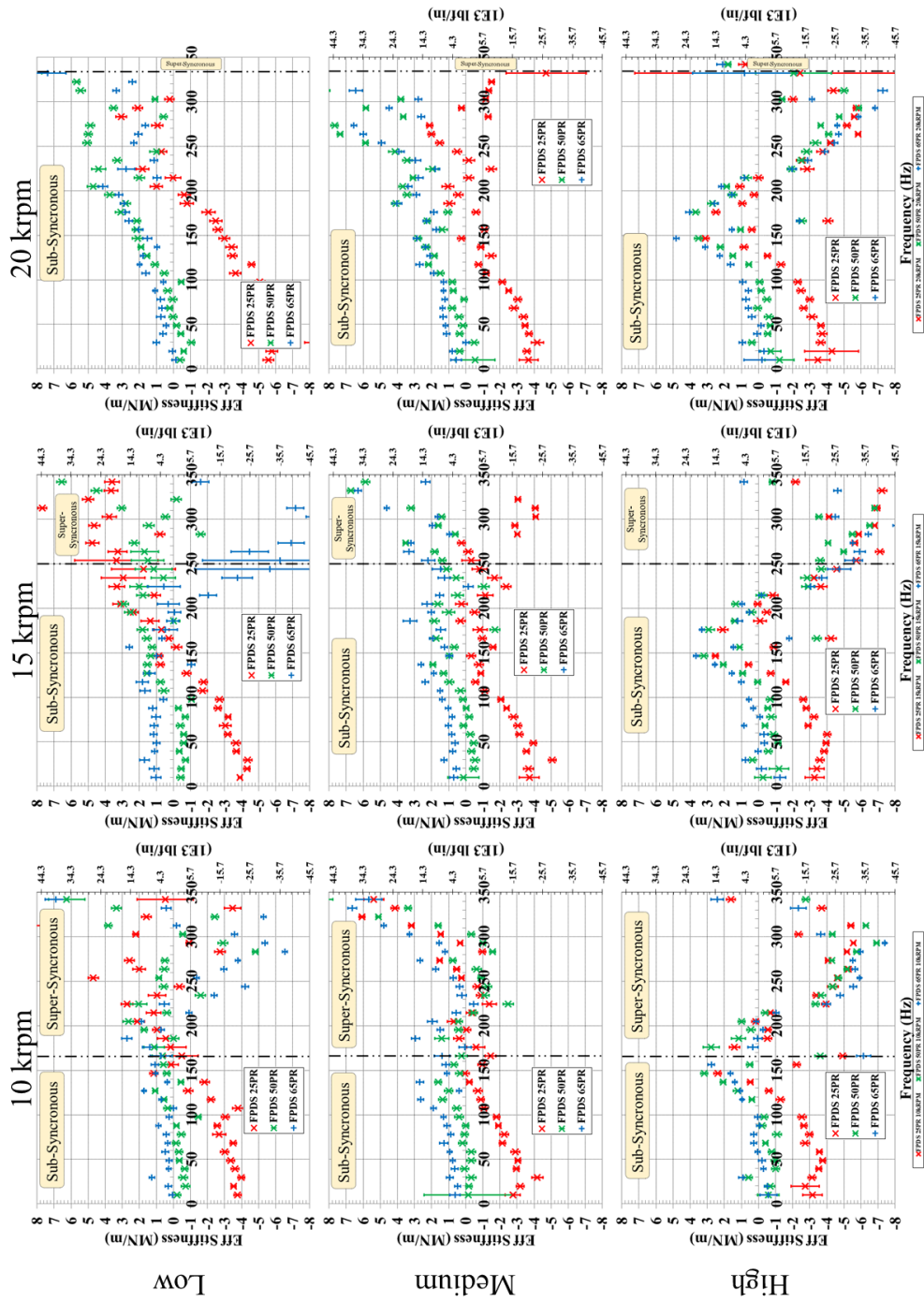


Figure 11 Effective stiffness coefficients versus frequency for FPDS, three pressure ratios (25%, 50%, 65%), three pressure ratios (25%, 50%, 65%), and three rotor speeds (10, 15, 20 krpm).

5.2.2 TEXTURED SEAL COMPARISON

Figure 12 through Figure 19 compares the FPDS to the honeycomb and labyrinth from previous investigations under similar conditions. Measured values of the honeycomb seal are from Sprowl's thesis [5]. For comparison purposes, the data is normalized respect to clearance and supply pressure following the expression given in [5].

$$K^* = \frac{K \cdot C_r}{F_o} = K \left(\frac{C_r}{\Delta P \cdot D_{in} \cdot L} \right) \quad (6)$$

Normalizing the measured values results in non-dimensional values for stiffness and seconds for damping. Measured values of the labyrinth seal are from Picardo's thesis [27].

The original honeycomb seal would be expensive to manufacture, which in turn places an advantage to the FPDS. However, a hole-pattern seal can produce similar benefits as a honeycomb seal and have simpler manufacturability when compared to the FPDS. Manufacturability does not differ between the FPDS and these textured seals if plunge EDM is used to create the honeycomb pattern or a simple right-angle drill to create a hole pattern.

Each figure is arranged into either a one by three or three by three matrix. The one by three matrix compares three graphs with columns referencing to the rotor speed from left to right. The three by three matrix shows columns as a thousand cycles per minute (kcpm) and rows as rotor speed in thousand revolutions per minute. The columns increase from the left to right from 10 kcpm, 15kcpm, to 20kcpm. Note that kcpm refers to excitation frequency, as opposed to rotor speed given in thousand revolutions per

minute (krpm). The rows increase with rotor speed from the top to bottom from 10, 15, to 20 krpm. Each graph shows measured values from both seals, the honeycomb and the FPDS. Each seal has three sets of pressure ratios; the honeycomb seal- 15%, 35%, and 50% and the FPDS- 25%, 50%, and 65%.

Figure 12 shows the stiffness vs excitation frequency for the honeycomb, labyrinth, and FPDSs at low preswirl. Similar to Figure 7 through Figure 11, the dashed line represents the rotor's operating speed. The rationale for only showing low preswirl and not including medium nor high inlet preswirl is explained hereafter in this section. Measured values for the FPDS show lower stiffness values when compared to the honeycomb seal. Stiffness values follow a similar trend to the honeycomb seal with increasing excitation frequency and rotor speed. Yet, the honeycomb seal has positive stiffness and the FPDS has low or negative stiffness. Though it is not evidently shown in the FPDS experimental results, the honeycomb seal shows an increase in stiffness with an increase in pressure ratio or decrease in pressure drop.

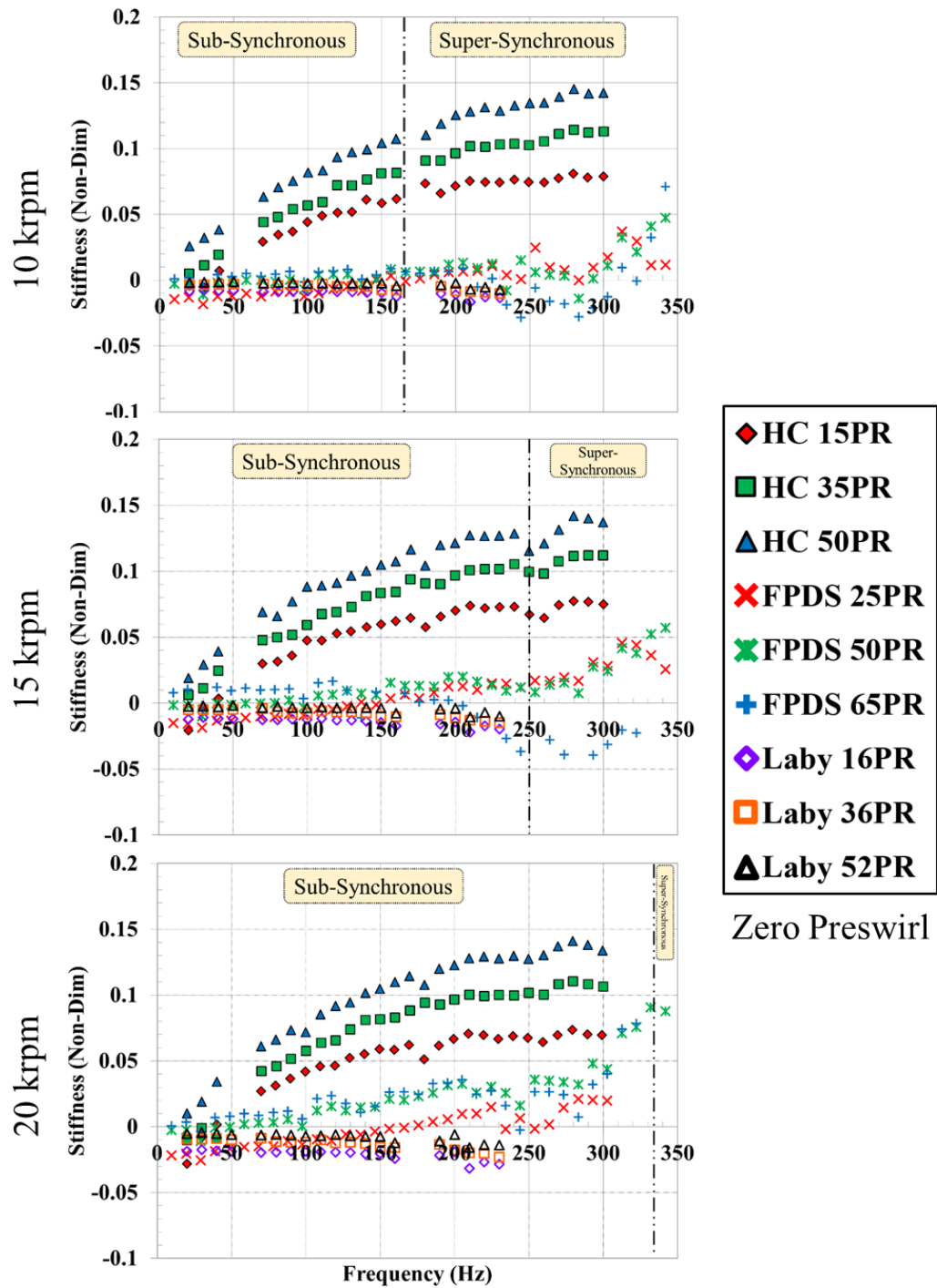


Figure 12 Direct Stiffness coefficients versus frequency for FPDS, honeycomb [5] and labyrinth [27] seals, multiple pressure ratios (15% – 65%), three rotor speeds (10, 15, 20 krpm), and low preswirl.

Figure 13 shows the cross-coupled stiffness versus excitation frequency for the honeycomb, labyrinth, and FPDS at low preswirl. Measured values for the FPDS show no influence from excitation frequency when compared to the honeycomb and labyrinth seals. The FPDS shows a similar cross-coupled stiffness values from mid to high excitation frequencies ranging from 150 to 350 Hz when compared to honeycomb seal.

Figure 14 shows the damping versus excitation frequency for the honeycomb, labyrinth, and FPDSs at low preswirl. Comparing the FPDS to the other two seals, the damping values display little influence from excitation frequency and rotor speed. At lower frequencies, the honeycomb seal shows larger values but decrease with increasing excitation frequency. The FPDS has larger damping values than the honeycomb seal at around 150 to 170 Hz.

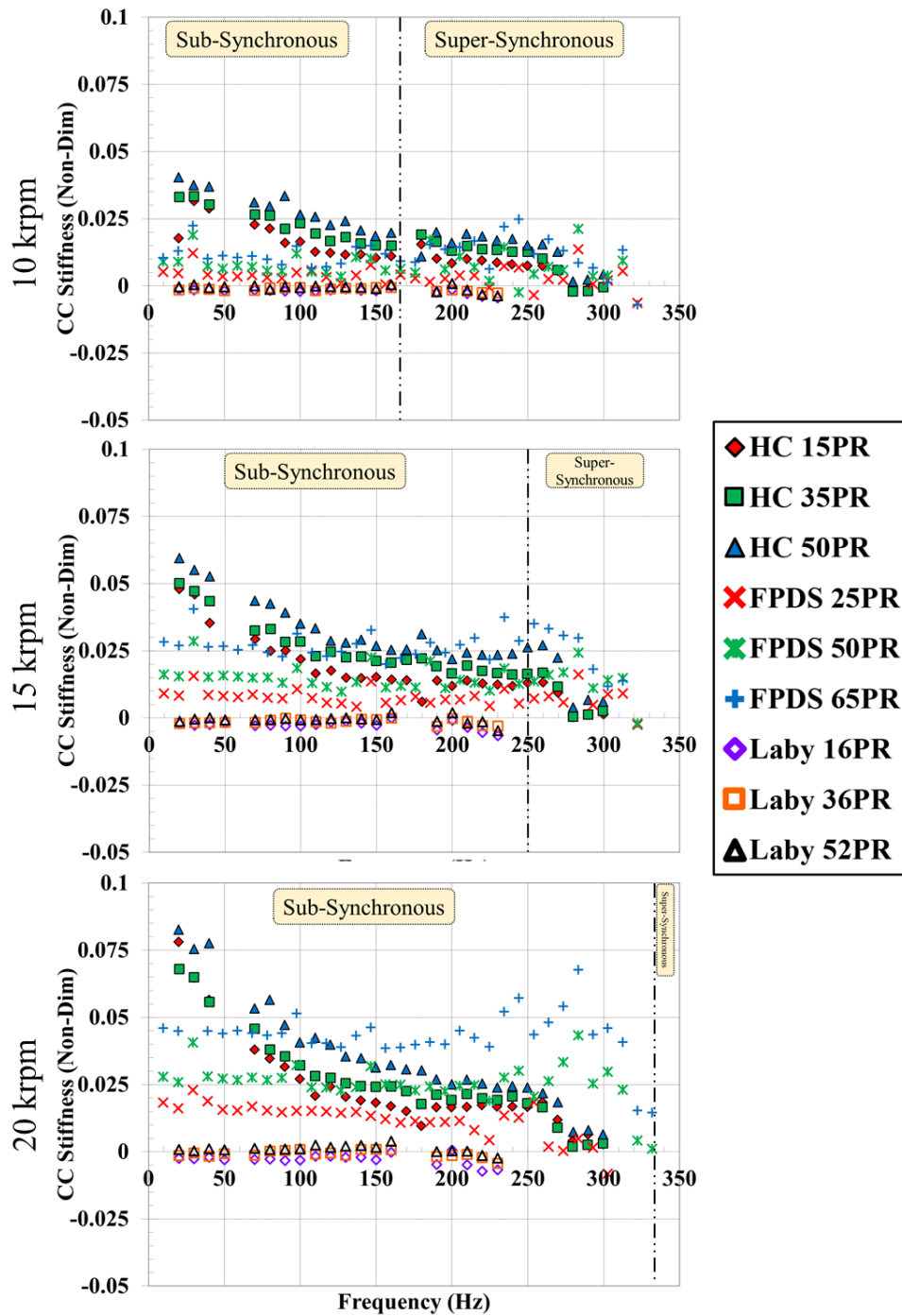


Figure 13 Cross-coupled stiffness coefficients versus frequency for FPDS, honeycomb [5] and labyrinth [27] seals, multiple pressure ratios (15% – 65%), three rotor speeds (10, 15, 20 krpm), and low preswirl.

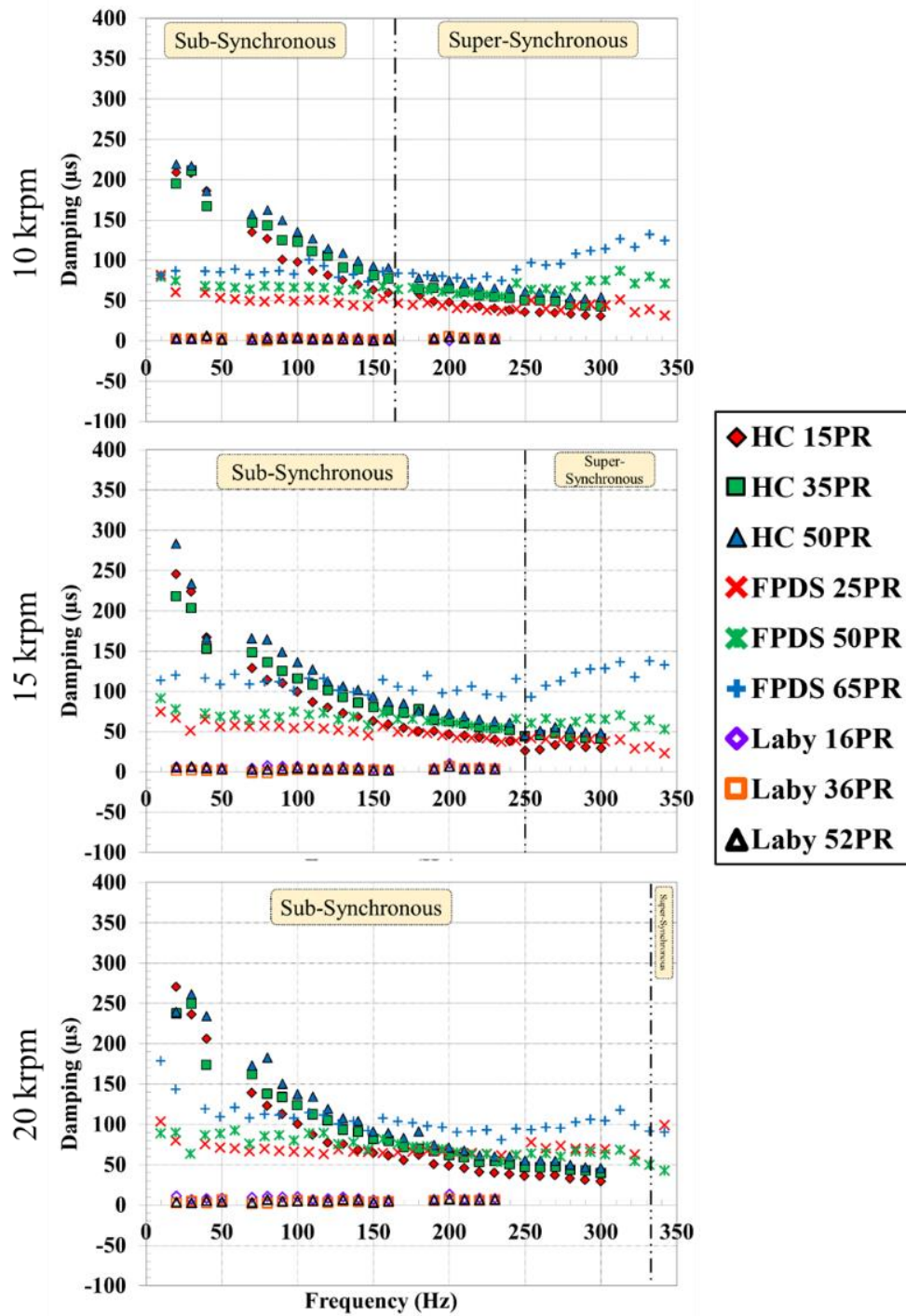


Figure 14 Direct Damping coefficients versus frequency for FPDS, honeycomb [5] and labyrinth [27] seals, multiple pressure ratios (15% – 65%), three rotor speeds (10, 15, 20 krpm), and low preswirl.

The following figures compare force coefficients for all the seals versus preswirl ratios. Comparisons of the force coefficients versus frequency are not possible for the medium and high preswirl rings. While the preswirl rings are the same for all the seals, the actual swirl ratio is a function of the seal leakage. Since the FPDS leakage rate is higher than that of the honeycomb seal, the preswirl values for the FPDS are larger for the medium and high preswirl rings.

Figure 15 shows the effective damping versus excitation frequency for the honeycomb, labyrinth, and FPDS at low preswirl. Measured values for the FPDS show an overall higher influence at the lower excitation frequencies. When comparing to the honeycomb seal, the measurements follow a similar trend with increasing excitation frequency. The FPDS shows a higher effective damping at synchronous vibration frequency when compared to the honeycomb seal, which presents higher values near cross-over frequency. The crossover frequency for the two seals have similar values and both increase with rotor speed. Due to limited data from Sprowl [5], it is unknown how the measurements from the FPDS compare to the negative effective damping values for the honeycomb seal.

Figure 16 shows the effective damping versus preswirl for the honeycomb, labyrinth, and FPDS. Each data point corresponds to the stator preswirl ring at low, medium, or high preswirl. Testing with a higher preswirl ring is denoted with a larger size data point. Sprowl's data does not reach excitation frequencies up to 330 Hz and as a result, only the FPDS has values for 20kcpm.

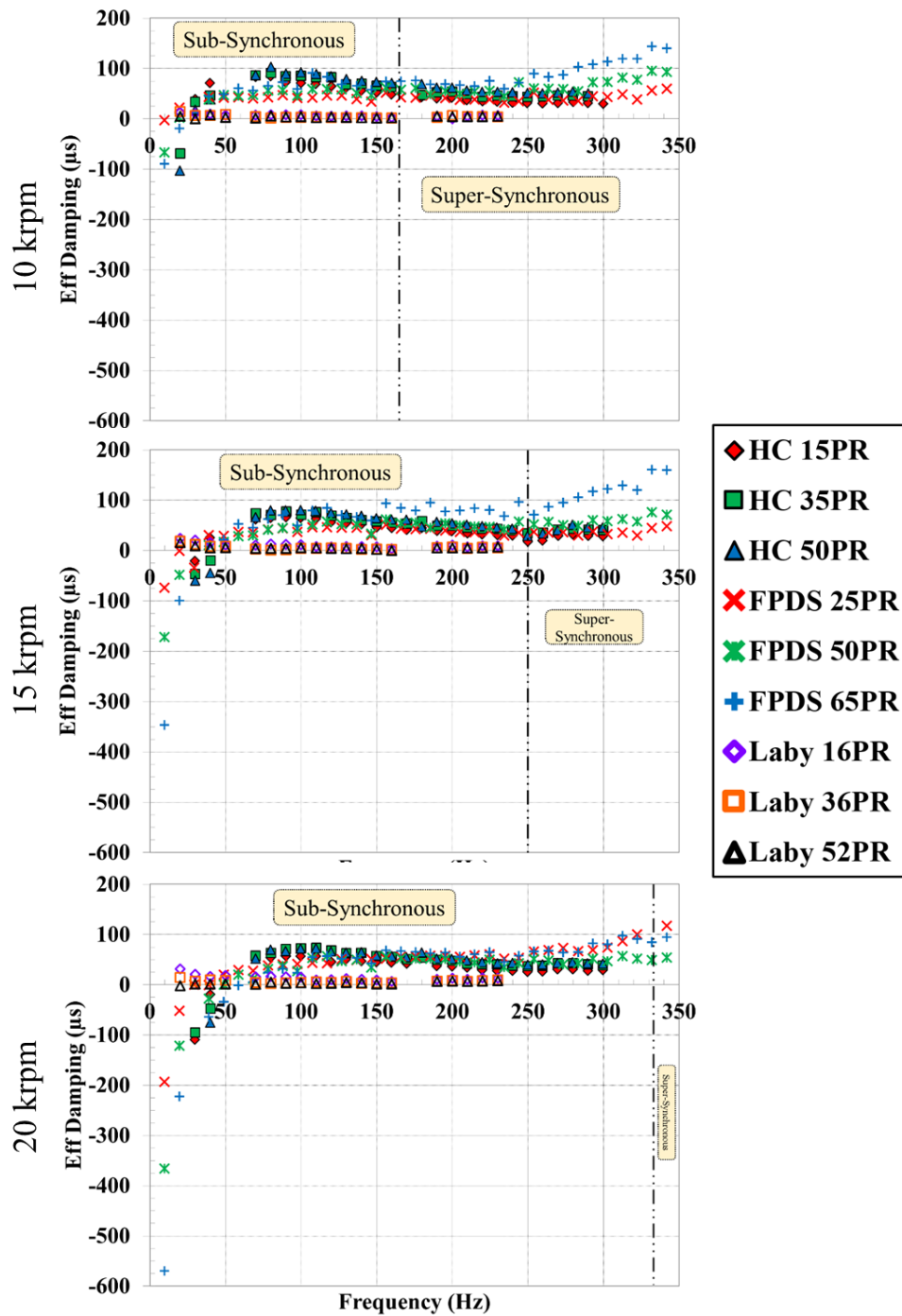


Figure 15 Effective damping coefficients versus frequency for FPDS, honeycomb [5] and labyrinth [27] seals, multiple pressure ratios (15% – 65%), three rotor speeds (10, 15, 20 krpm), and low preswirl.

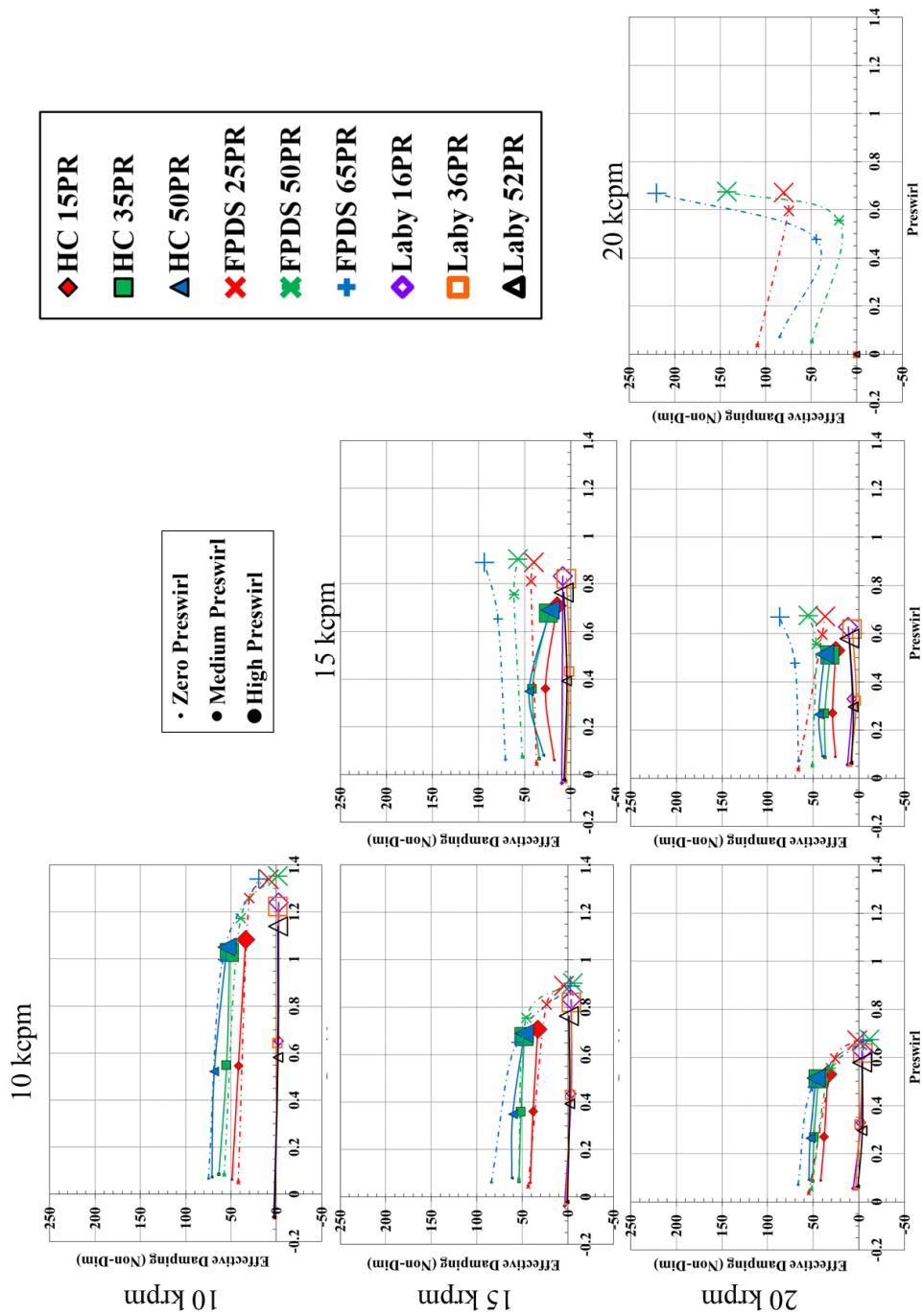
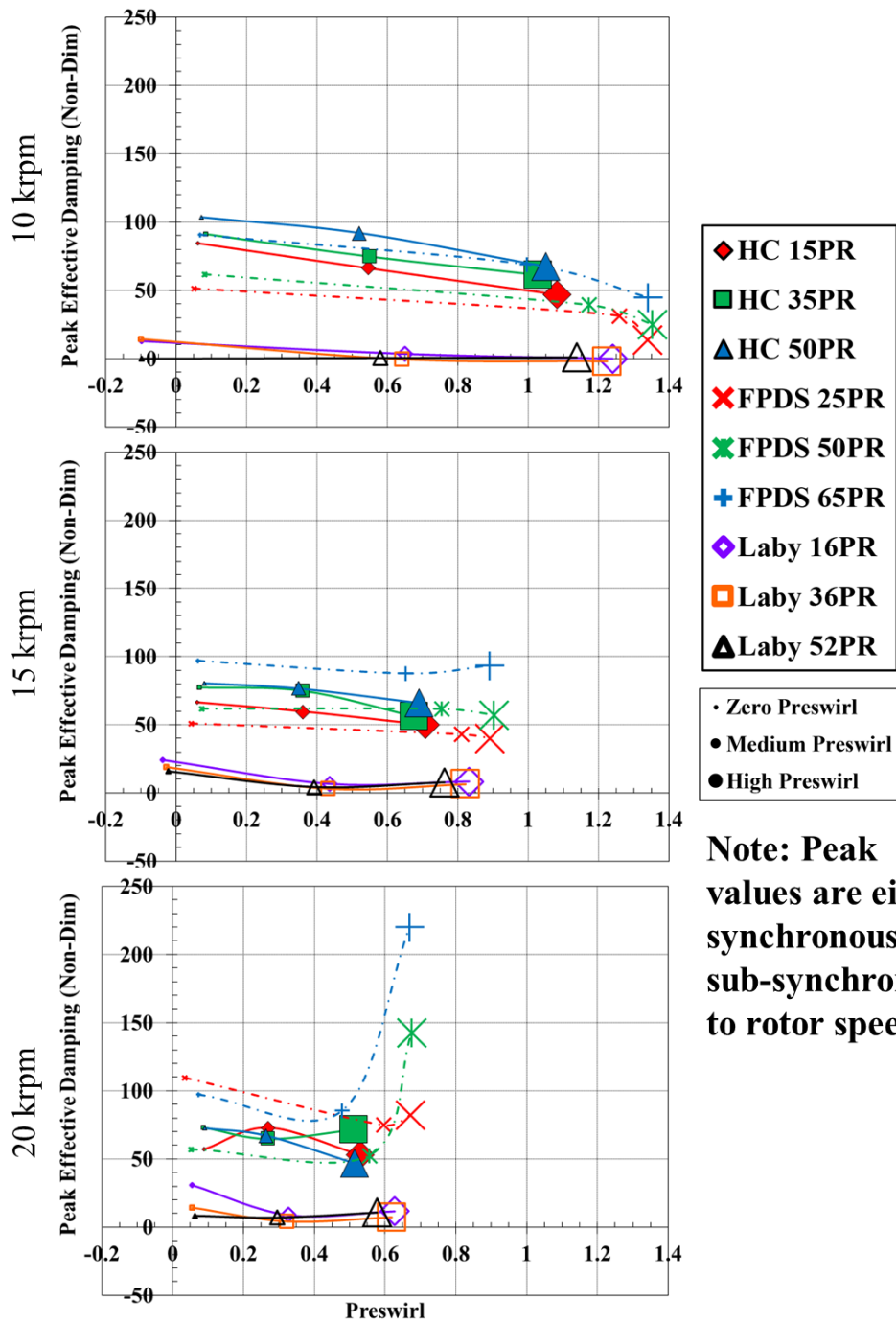


Figure 16 Effective damping coefficients versus preswirl for FPDS, honeycomb [5] and labyrinth [27] seals, multiple pressure ratios (15% – 65%), three rotor speeds (10, 15, 20 krpm), three synchronous excitations (10, 15, 20 kcpm), and three preswirls (low, medium, high).

Figure 17 shows peak effective damping vs preswirl at differing rotor speeds for the honeycomb, labyrinth, and FPDS from sub-synchronous to synchronous frequency. When comparing to experimental values from Sprowl [5], the FPDS shows comparable magnitudes but has higher inlet preswirl. The honeycomb seal shows no apparent change in peak effective damping with an increase in rotor speed, while the FPDS has differing values between rotor speeds. Peak values for the honeycomb seal lie closer to the crossover frequency, where peak values for the FPDS lie closer to synchronous excitation.

Figure 18 shows the crossover frequency versus preswirl for the honeycomb, labyrinth, and FPDS. Measured values for the FPDS show high crossover frequencies for medium and high preswirl ring. Measured and experimental values for all seals at the low preswirl ring show a comparable range. Data points for the low preswirl show both the honeycomb and FPDS having similar values in preswirl and range between 28 and 62 Hz. The labyrinth seal has no crossover frequency at low preswirl as the effective damping is positive over entire frequency range.

Figure 19 shows the leakage versus preswirl for the honeycomb, labyrinth, and FPDS. Measured values for the FPDS are much higher, by a factor of roughly one-third, when compared to the other two seals for most operating conditions. Increasing the rotor speed does decrease the leakage, but the FPDS still vastly underperforms respect the honeycomb and labyrinth seal. Pressure shows more influence in leakage than increasing the inlet preswirl. Low preswirl shows the highest leakage where high preswirl has the lowest.



Note: Peak values are either synchronous or sub-synchronous to rotor speed

Figure 17 Peak effective damping coefficients versus preswirl for FPDS, honeycomb [5] and labyrinth [27] seals, multiple pressure ratios (15% – 65%), three preswirls (low, medium, high), and three rotor speeds (10, 15, 20 krpm).

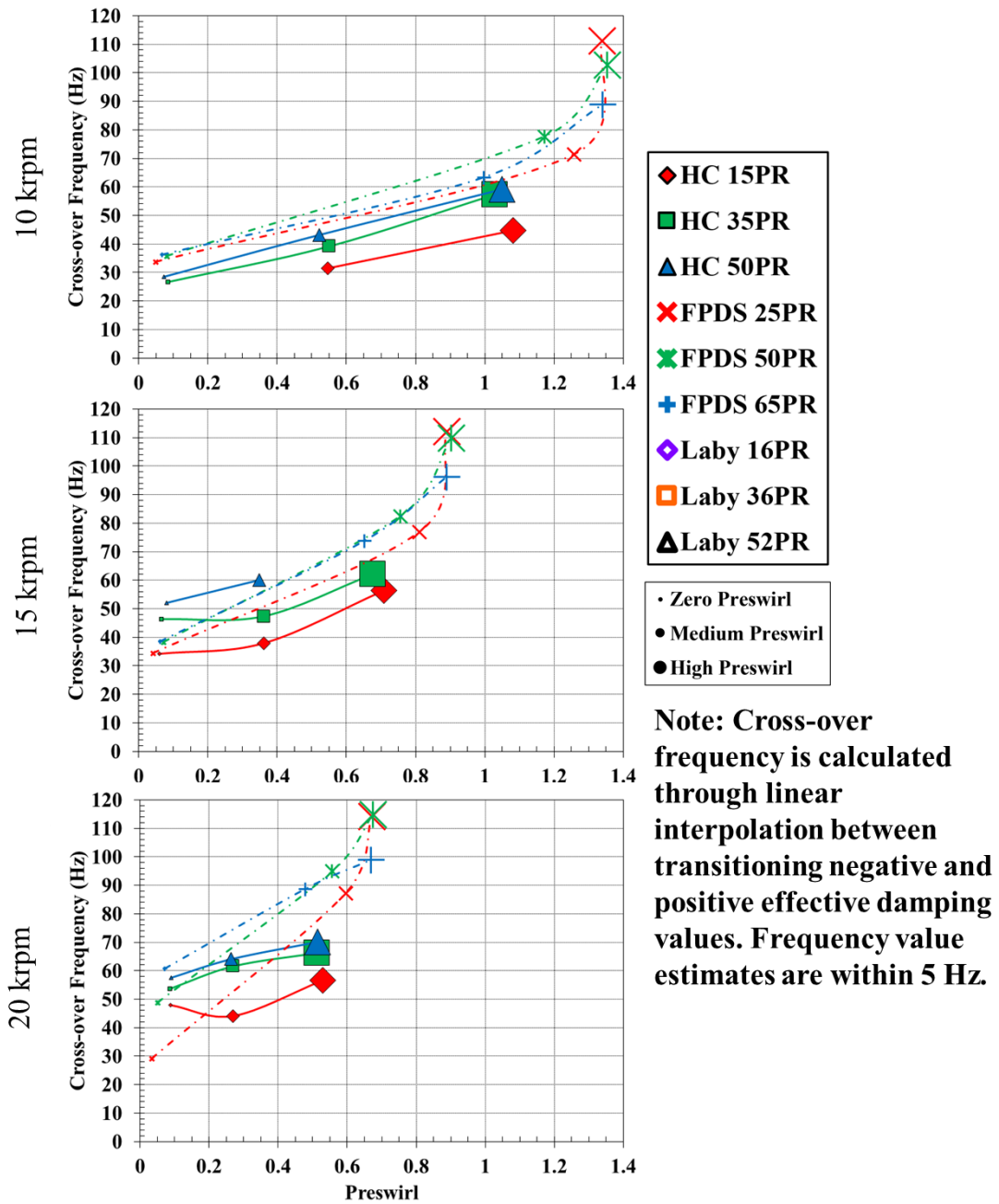


Figure 18 Crossover frequency versus preswirl for FPDS, honeycomb [5] and labyrinth [27] seals, multiple pressure ratios (15% – 65%), three preswirls (low, medium, high), and three rotor speeds (10, 15, 20 krpm).

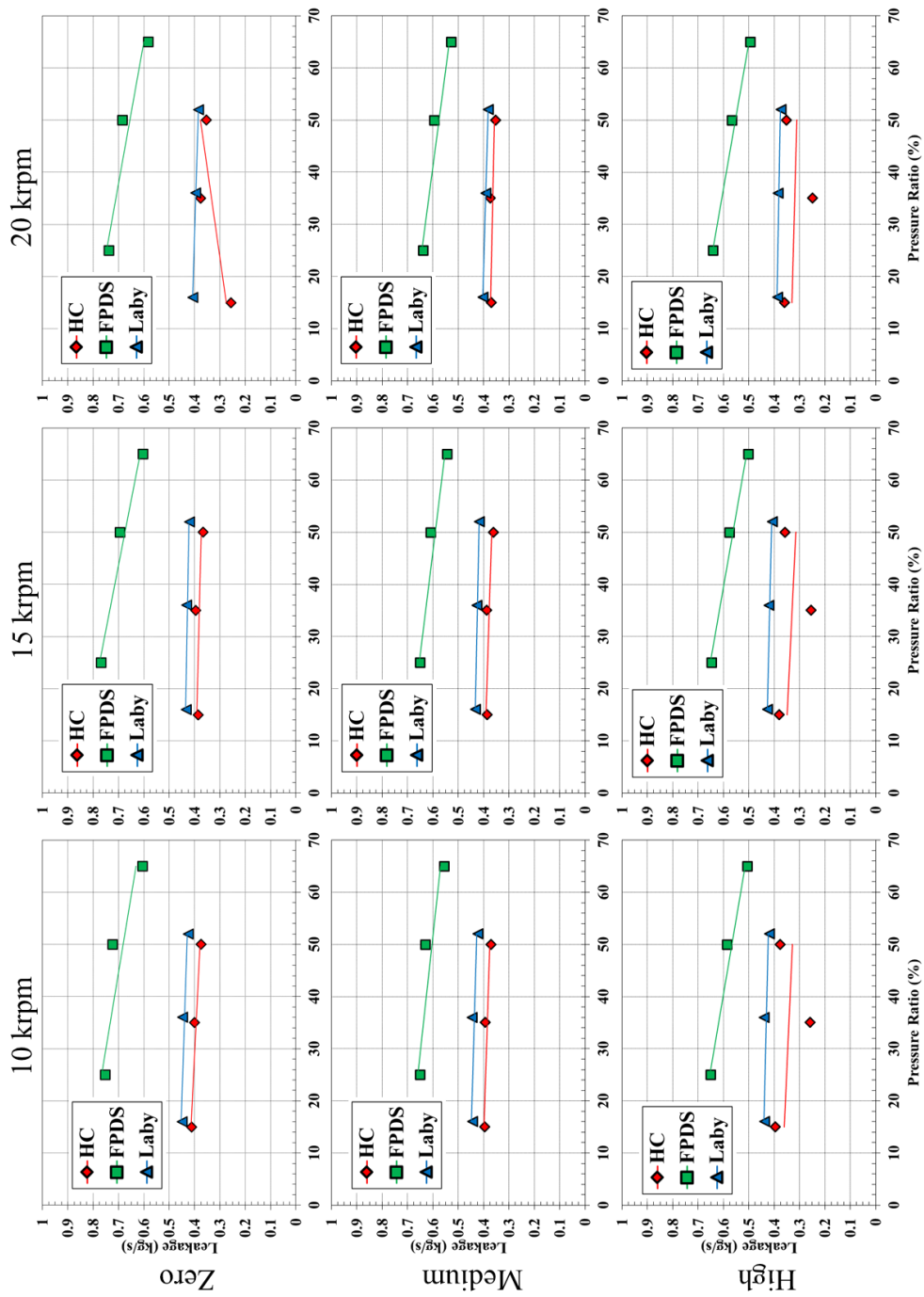


Figure 19 Leakage versus pressure ratio for FPDS, honeycomb [5] and labyrinth [27] seals, three preswirls (low, medium, high), and three rotor speeds (10, 15, 20 krpm).

6. SUMMARY

6.1 CONCLUSIONS

A characterization of the dynamic and leakage performance of a FPDS is presented. The seal was tested with a supply pressure of 70 bars and multiple pressure ratios (35,50,65%) speeds (10,15,20 krpm) and preswirls (0.2-1.2). The test results are compared to leakage and dynamic performance data from a honeycomb and a labyrinth seal tested at similar operating conditions. The following are the main findings from the experimental results and comparisons between the three seals:

- (1) The FPDS possesses very low to negative direct stiffness at low frequencies.

Comparing to the honeycomb seals, the FPDS provide little stiffness, which magnitude decreases as the pressure ratio increases

- (2) The FPDS cross-coupled stiffness is frequency independent, but increases in magnitude with rotor speed and preswirl. Cross-coupled stiffness decreases as the pressure ratio increases.

- (3) The direct damping of the FPDS decreases as the pressure ratio increases.

The magnitude increases as the preswirl increases

- (4) Effective damping values are negative at low excitation frequencies. The measurement values increase in magnitude with increasing rotor speed and inlet preswirl. Effective damping increases with increasing synchronous excitation frequency. The crossover frequencies improve greatly when

transitioning from high to low preswirl. The values decrease from ~100 Hz to ~50 Hz.

- (5) The FPDS leaks roughly 33% more than the honeycomb seal.
- (6) The FPDS exhibits lower stiffness when compared to the honeycomb seal.
- (7) The FPDS exhibits less cross-coupled stiffness at low frequencies when compared to the honeycomb seal. At mid to high excitation frequencies the FPDS is comparable to the honeycomb seal.
- (8) The FPDS exhibits less damping than the honeycomb seal at lower excitation frequencies.
- (9) The FPDS and honeycomb seals have similar effective damping values.

Specific conditions do provide the FPDS with an advantage. At low preswirl, the FPDS has favorable crossover frequencies when compared to the honeycomb seal. While the honeycomb seal has lower crossover frequency when inlet preswirl increases.

Considering that the FPDS presents higher leakage, small overall improvements in effective damping and smaller stiffness when compared to the honeycomb seal, it is suggested the selections of the seal should be done in a case-by-case basis. Besides manufacturing considerations, the FPDS may be a better alternative to a textured seal in the case that adding stiffness to the system will decrease the separation margin between the compressor running speed and natural frequency, which could place the compressor out of API compliance. In these cases, the FPDS will have a better advantage in providing damping to the system.

6.2 RECOMMENDATIONS

Further testing is needed for mainly air conditions as in 90% to 98% gas volume fraction (GVF). These conditions provide a response on how these seals behave when small amounts of liquid is present in the compressor core flow.

Another seal design, scallop, could provide a needed compromise between manufacturing time and equivalent dynamic response to the textured seal and FPDS. The scallop design uses a groove as a labyrinth seals except the grooves are separated as in PDS [28].

Flow meter calibration for higher pressures will further verify measurements for needed test conditions. Adding thicker wires for the horizontal stiffener can increase the testing envelope for lower pressure ratios.

REFERENCES

- [1] Benckert, H., and Wachter, J., 1980, "Flow Induced Spring Coefficients of Labyrinth Seals for Application in Rotor Dynamics," Proc. NASA. Lewis Res. Center Rotodyn. Instability Probl. in High-Performance Turbomachinery, NASA, ed., United States, pp. 189-212.
- [2] Vannini, G., Cioncolini, S., Del Vescovo, G., and Rovini, M., 2013, "Labyrinth Seal and Pocket Damper Seal High Pressure Rotordynamic Test Data," Journal of Engineering for Gas Turbines and Power, 136(2).
- [3] Childs, D. W., 1993, Turbomachinery rotordynamics : phenomena, modeling, and analysis. Dara Childs, New York : Wiley, 1993.
- [4] Vannini, G., Bertoneri, M., Nielsen, K. K., Iudiciani, P., and Stronach, R., 2015, "Experimental Results and Computational Fluid Dynamics Simulations of Labyrinth and Pocket Damper Seals for Wet Gas Compression," Journal of Engineering for Gas Turbines and Power, 138(5).
- [5] Sprowl, T. B., 2003, A study of the effects of inlet preswirl on the dynamic coefficients of a straight-bore honeycomb gas damper seal. by Tony Brandon Sprowl, [College Station, Tex.] : [Texas A&M University], [2003].
- [6] Childs, D. W., and Wade, J., 2004, "Rotordynamic-Coefficient and Leakage Characteristics for Hole-Pattern-Stator Annular Gas Seals - Measurements Versus Predictions," J Tribol-T Asme, 126(2), pp. 326-333.
- [7] Ertas, B. H., Delgado, A., and Vannini, G., 2012, "Rotordynamic Force Coefficients for Three Types of Annular Gas Seals With Inlet Preswirl and High Differential Pressure Ratio," Journal of Engineering for Gas Turbines and Power, 134(4).

- [8] Alford, J. S., 1965, "Protecting Turbomachinery From Self-Excited Rotor Whirl," *Journal of Engineering for Power*, 87(4), pp. 333-343.
- [9] Vannini, G., Mazzali, C., and Underbakke, H., 2016, "Rotordynamic Computational and Experimental Characterization of a Convergent Honeycomb Seal Tested With Negative Pre-Swirl, High Pressure With Static Eccentricity and Angular Misalignment," *Proceedings of the Asme Turbo Expo: Turbine Technical Conference and Exposition*, 2016, Vol 7b(49842).
- [10] Childs, D. W., 2013, *Turbomachinery rotordynamics with case studies*. Dara W. Childs, The Leland T. Jordan Professor of Mechanical Engineering, Department of Mechanical Engineering, Director Turbomachinery Laboratory, Texas A&M University, Wellborn, Texas : Minter Spring Publishing, [2013].
- [11] Vance, J. M., Murphy, B., and Zeidan, F., 2010, *Machinery vibration and rotordynamics*. John Vance, Brian Murphy, Fouad Zeidan, Hoboken, N.J. : Wiley, [2010].
- [12] Vannarsdall, M. L., and Childs, D. W., 2012, *Measured results for a new hole-pattern annular gas seal incorporating larger diameter holes, comparisons to results for a traditional hole-pattern seal and predictions*. by Michael Lloyd Vannarsdall, [College Station, Tex.] : [Texas A&M University], [2012].
- [13] Von Pragenau, G. L., 1982, "Damping Seals for Turbomachinery," *National Aeronautics and Space Administration Marshall Space Flight Center*, Alabama.
- [14] Vance, J. M., and Schultz, R. R., 1993, *A New Damper Seal for Turbomachinery*, New York : American Society of Mechanical Engineers, [1993].

- [15] Vance, J. M., and Li, J., 1996, "Test Results of a New Damper Seal for Vibration Reduction in Turbomachinery," *J Eng Gas Turb Power*, 118(4), pp. 843-846.
- [16] Li, J., San Andrés, L., and Vance, J., 1999, "A Bulk-Flow Analysis of Multiple-Pocket Gas Damper Seals," *J Eng Gas Turb Power*, 121(2), pp. 355-363.
- [17] Li, Q., 1995, The effect of a new damper seal on rotordynamics, Texas A&M University, College Station, TX.
- [18] Li, J., Kushner, F., and DeChoudhury, P., 2000, Gas Damper Seal Test Results, Theoretical Correlation, And Applications In Design Of High-Pressure Compressors, Texas A&M University. Turbomachinery Laboratories.
- [19] Ertas, B., Gamal, A., and Vance, J., 2006, "Rotordynamic Force Coefficients of Pocket Damper Seals," *Journal of Turbomachinery*, 128(4), pp. 725-737.
- [20] Ertas, B. H., 2005, "Rotordynamic force coefficients of pocket damper seals," Doctoral Doctor of Philosophy, Texas A&M University, College Station, TX.
- [21] Brown, P. D., and Childs, D. W., 2012, "Measurement Versus Predictions of Rotordynamic Coefficients of a Hole-Pattern Gas Seal With Negative Preswirl," *Journal of Engineering for Gas Turbines and Power*, 134(12).
- [22] Li, J., Li, Z., and Feng, Z., 2012, "Investigations on the Rotordynamic Coefficients of Pocket Damper Seals Using the Multifrequency, One-Dimensional, Whirling Orbit Model and RANS Solutions," *J Eng Gas Turb Power*, 134(10).

- [23] Li, Z., Li, J., and Feng, Z., 2014, "Numerical Investigations on the Leakage and Rotordynamic Characteristics of Pocket Damper Seals—Part I: Effects of Pressure Ratio, Rotational Speed, and Inlet Preswirl," *Journal of Engineering for Gas Turbines and Power*, 137(3).
- [24] Rouvas, C., and Childs, D. W., 1993, "A Parameter Identification Method for the Rotordynamic Coefficients of a High Reynolds Number Hydrostatic Bearing," *J Vib Acoust*, 115(3), pp. 264-270.
- [25] San Andrés, L., 2012, "Kinematics of Journal Bearings."
- [26] Childs, D., and Hale, K., 1994, "A Test Apparatus and Facility to Identify the Rotordynamic Coefficients of High-Speed Hydrostatic Bearings," *Journal of Tribology*, 116(2), pp. 337-343.
- [27] Picardo, A. M., 2003, High pressure testing of see-through labyrinth seals. by Arthur Michael Picardo, [Texas A&M University], 2003.
- [28] Takahashi, N., Miura, H., Narita, M., Nishijima, N., and Magara, Y., 2014, "Development of Scallop Cut Type Damper Seal for Centrifugal Compressors," *Journal of Engineering for Gas Turbines and Power*, 137(3).

APPENDIX

APPENDIX A: TEST CODE

Table 3 below is a key decoder for describing a specific the test condition. The code is in a four digit format. First digit represents either low, medium, or high preswirl. Second digit represents the rotor speed from either 10, 15, or 20 krpm. The third digit represents the pressure ratio from either 25%, 35%, 50%, or 65%. The four digit represents the GVF from either 100%, 98%, 96%, 94%, 92%, or 90%.

Table 3 Test condition key decoder

Test Code			
[ABCD]			
A	B	C	D
0-Zero Preswirl	0-10 krpm	0-25 PR	0-100% GVF
1-Medium Preswirl	1-15 krpm	1-35 PR	1-98% GVF
2-High Preswirl	2-20 krpm	2-50 PR	2-96% GVF
		3-65 PR	3-94% GVF
			4-92% GVF
			5-90% GVF

APPENDIX B: TEST CONDITIONS

Table 4 through Table 6 are test conditions for low, medium, and high preswirl.

These tables provide values for inlet pressure, exit pressure, leakage rate, and other sensor readings.

Table 4 Test conditions for low preswirl

Test Conditions [Code]	Inlet pressure [PSI]	Exit pressure [PSI]	Pressure Ratio (Exit/Inlet) [%]	GVF [%]	Temp Inlet [°F]	Rotor Speed [krpm]	Air Flow Rate per seal [kg/s]	Oil Flow Rate per seal [kg/s]	Oil Density [kg/m ³]	Preswirl Ratio [%]
0000	1024	281	0.27	100	59	10	0.964	0	0	0.049
0100	1021	282	0.28	100	64	15	0.914	0	0	0.042
0200	1025	270	0.26	100	38	20	0.798	0	0	0.034
0020	1020	523	0.51	100	50	10	0.971	0	0	0.080
0120	1028	530	0.52	100	57	15	0.900	0	0	0.072
0220	1019	534	0.52	100	60	20	0.791	0	0	0.050
0030	1022	648	0.63	100	49	10	0.940	0	0	0.067
0130	1022	675	0.66	100	52	15	0.877	0	0	0.061
0230	1017	673	0.66	100	58	20	0.766	0	0	0.072

Table 5 Test conditions for medium preswirl

Test Conditions [Code]	Inlet pressure [PSI]	Exit pressure [PSI]	Pressure Ratio (Exit/Inlet) [%]	GVF [%]	Temp Inlet [°F]	Rotor Speed [krpm]	Air Flow Rate per seal [kg/s]	Oil Flow Rate per seal [kg/s]	Oil Density [kg/m ³]	Preswirl Ratio [%]
1000	1005	278	0.28	100	50	10	0.805	0	0	1.258
1100	1018	275	0.27	100	45	15	0.803	0	0	0.810
1200	1019	274	0.27	100	49	20	0.790	0	0	0.595
1020	1021	517	0.51	100	42	10	0.778	0	0	1.173
1120	1025	521	0.51	100	41	15	0.752	0	0	0.755
1220	1020	527	0.52	100	46	20	0.734	0	0	0.556
1030	1022	673	0.66	100	40	10	0.686	0	0	0.997
1130	1030	673	0.65	100	39	15	0.671	0	0	0.652
1230	1022	674	0.66	100	46	20	0.650	0	0	0.478

Table 6 Test conditions for high preswirl

Test Conditions [Code]	Inlet pressure [PSI]	Exit pressure [PSI]	Pressure Ratio (Exit/Inlet) [%]	GVF [%]	Temp Inlet [°F]	Rotor Speed [krpm]	Air Flow Rate per seal [kg/s]	Oil Flow Rate per seal [kg/s]	Oil Density [kg/m ³]	Preswirl Ratio [%]
2000	1030	269	0.26	100	32	10	0.803	0	0	0.921627
2100	1025	267	0.26	100	29	15	0.800	0	0	0.610222
2200	1029	270	0.26	100	34	20	0.791	0	0	0.456402
2020	1027	521	0.51	100	41	10	0.723	0	0	0.846373
2120	1023	520	0.51	100	39	15	0.713	0	0	0.55658
2220	1024	522	0.51	100	38	20	0.699	0	0	0.407386
2030	1029	674	0.65	100	37	10	0.624	0	0	0.723667
2130	1026	670	0.65	100	33	15	0.620	0	0	0.47615
2230	1025	670	0.65	100	36	20	0.609	0	0	0.353322

APPENDIX C: TEST CONDITION DYNAMIC RESPONSE

Table 7 through Table 33 correspond to the complex dynamic response over the excitation frequency for each test condition. Each table has the test code for that detailed test condition. The order of test conditions will follow beginning with the listings from Table 4, the listings from Table 5, and ending with the listings from Table 6. The units are in N/m.

Table 7 Test condition: Low preswirl-10 krpm-25% Pressure Ratio-100% GVF

0000 Freq Hz	Test Data								Uncertainties							
	Re Hxx	Re Hxy	Re Hyx	Re Hyy	Im Hxx	Im Hxy	Im Hyy	Im Hyy	Re eHxx	Re eHxy	Re eHyy	Re eHyy	Im eHxx	Im eHxy	Im eHyy	Im eHyy
9.765625	-3719621	1329310.801	-2751067.71	-4177631	1286575	-50080.05	85460.6	1164845	117190.286	59475.0044	158571.686	82961.0276	102548.66	93463.378	159872.92	55925.937
19.53125	-3360147	1207200.139	-2818079.3	-3970069	1896176	-173193.9	479179.8	1933568	65582.8737	72042.0313	97867.5865	71897.4611	101881.44	84749.275	108437.92	51754.979
29.296875	-4672344	3120349.802	-632996.129	-6245341	1475226	691103.1	1352230	1791746	71009.3524	82808.8125	112760.421	82230.9735	60304.663	133945.01	138585.94	120802.33
39.0625	-3157321	1061067.725	-2698156.04	-3768568	3776517	-457123.5	734537.2	3811385	126556.725	94196.0442	119137.539	59930.5135	124520.11	101487.74	171075.05	81201.664
48.828125	-3101376	905183.9006	-2318541.81	-3643449	4201415	-265094.9	367185.4	4392493	134133.001	79752.0628	213794.904	109561.811	71407.234	90154.301	177949.52	64137.32
58.59375	-2614216	906170.828	-2309942.63	-3411486	4915818	-394714.7	261268.1	5492898	137296.403	77465.7109	173212.415	129678.624	161624.6	106836.43	132226.05	83937.926
68.359375	-3189766	1036987.637	-1931308.39	-3286096	5497678	-321210	495652.6	6266328	87734.4026	60783.8139	98415.5163	68292.5077	182742.5	91093.028	146308.75	76685.013
78.125	-2223278	784758.9791	-2388616.36	-2892586	6147549	-462575.9	949780.6	7518479	294267.293	104688.878	363240.381	84513.4784	287512.53	86255.584	198587.64	112465.44
87.890625	-2260799	707411.2837	-2426702.87	-2458061	7411617	-314021.7	278275.9	8144317	97342.7534	97529.7717	168702.024	74151.59	136574.05	98532.522	143428.76	101926.17
97.65625	-3182520	1288041.389	-1398963.23	-3209105	7789190	136824.9	978680.7	8545343	148350.413	85724.6121	150193.084	108559.995	91491.356	90502.772	92356.851	118770.63
107.42188	-2532289	1482475.697	-1811329.87	-2608167	8759029	-1249175	34327.36	11011117	179799.599	91016.6951	208890.631	67125.2002	211625.66	130385.35	202967.52	101568.7
117.1875	-1692339	834614.4846	-2677852.83	-1250226	9600435	-503189.8	397408.5	10642931	104996.663	76945.167	254311.183	125381.751	103891.37	106785.11	141586.53	69623.497
126.95313	-1156131	254793.7422	-2296110.77	-684815.1	9669735	285269.9	1546184	10819591	167311.947	103794.486	260669.731	119508.477	147703.53	101257.83	221040.55	110257.64
136.71875	-2037656	1010368.979	-967652.482	-1309311	9688522	199386.5	1734119	11343722	162892.582	109651.591	178851.773	120689.098	109583.16	120782.42	128843.02	108847.74
146.48438	30782.148	1997443.617	-2658005	-1884212	10050715	1118507	2929375	11241596	131073.749	158365.383	143269.094	109289.424	193594.51	112682.94	187466.96	106380.04
156.25	887711.99	139385.5612	-3712376.47	323023.6	13151756	-758856.7	-532981.5	13658615	198779.643	108362.787	227772.808	193842.732	305085.28	214087.97	151292.18	176957.92
166.01563	-202006.9	1079866.669	-2791767.38	938482.92	12448434	-299055.3	1303261	13476719	570358.326	277452.604	544556.96	282846.827	467528.42	390956.66	386628.01	321507.46
175.78125	362560.8	723533.3645	-3042447.4	-1183147	12707697	-192013	2647959	14105248	591076.667	188255	533912.457	271777.177	364354.94	324747.06	658859.83	233600.15
185.54688	1142395.7	390377.7446	-1945720.21	2337140.5	14162398	-702373.6	348805.8	15309384	329271.789	212565.524	363681.79	147106.14	251768.97	166433.65	462630.97	164480.96
195.3125	1552138	681287.2119	-2762682.77	1822955	13743929	-592571.9	4811182	15308763	99699.7021	144377.571	242631.209	79985.5012	249629.92	163641.13	252180.11	125394.79
205.07813	1702431.1	984807.8856	-2951130.13	1889608.3	13443091	419488.6	1783067	14933433	277262.189	172531.332	296126.718	153754.751	358325.09	147594.19	169631.35	177619.7
214.84375	1836899.7	1004171.054	-1323917.32	945227.67	14235435	-687224.8	2041788	16525514	260985.01	152198.007	339881.027	104549.373	358383.59	161714.39	242017.21	112430.24
224.60938	2770185.6	-180282.232	-2505372.25	2863829.5	13719031	-52436.11	1921170	16961592	235211.732	87917.4858	366487.495	84349.623	208921.57	112376.17	339956.33	143962.94
234.375	986812.51	1871332.295	-1231013.13	1540893.5	14105533	-28790.48	1541139	17703942	344604.058	139543.128	199480.186	148514.689	275399.43	167410.27	275800.02	98273.303
244.14063	213075.52	1736825.276	316142.6977	1877240.5	15427507	-568601.4	437937.6	19011178	164143.683	98737.7817	296814.365	94587.7359	468241.33	121781.76	408061.32	155495.82
253.90625	6320423.3	-866653.009	-2123781.15	4021602.1	20484403	-1617842	-1108547	20897229	193279.418	87765.3974	231521.832	80375.9655	318271.33	104135.85	481671.96	96079.655
263.67188	2531349.9	643321.5148	-1426714.19	3768468.7	16755162	-515235.4	304875.7	20447497	271973.561	76587.8169	234970.602	83039.005	112343.39	91612.965	270771.08	103206.2
273.4375	1988070.3	873550.0965	-1628663.27	4439090.3	16755373	594144.2	50912.79	21047597	136735.294	103937.868	262173.14	95970.6987	178234.91	154385.27	171842.05	98012.065
283.20313	-19022.72	3495863.86	-2930876.08	5764263.7	19666807	-2711685	1405108	19972924	149368.11	94789.6045	245188.039	156228.809	216357.89	159635.75	197310.72	104444.29
292.96875	2477998.5	180263.1368	-950699.936	5982888.8	21381185	-3395389	-1295713	22311931	85344.9052	128912.532	205909.261	150988.048	230854.43	86764.362	295524.15	115428.74
302.73438	4462904.5	502240.1848	-3134501.45	6558642.4	21667097	-2259435	-1471896	20378733	73662.2725	125499.04	207109.442	128912.859	177793.56	90949.899	186730.71	137032.32
312.5	9498422.1	1404293.304	-2138477.63	4342408.6	25892398	-1446683	1303707	23018043	222923.906	119161.019	284107.139	133541.172	152242.34	141037.7	244852.66	136655.72
322.26563	7613235.4	-1646996.79	-4690096.06	2507636.7	18441310	-6033919	1405507	25204777	182474.476	152424.622	127035.189	124323.018	165612.19	104826.37	229196.04	113326.32
332.03125	2950030.3	-9294027.55	-1475607.92	5353078.4	20900557	-6414972	-5725579	23614560	285763.759	190929.624	361535.459	228474.875	328945.69	191875.21	309722.98	233457.88
341.79688	3004458.8	-15467042.9	-14492501.4	-4586344	17495585	-2528979	-9262370	19369453	999992.598	636531.969	1247045.61	933692.659	792485.87	651859.02	1517399.8	1028612.5

Table 8 Test condition: Low preswirl-15 krpm-25% Pressure Ratio-100% GVF

0100	Test Data										Uncertainties					
	Freq Hz	Re Hxx	Re Hxy	Re Hyx	Re Hyx	Im Hxx	Im Hxy	Im Hyx	Im Hyx	Re eHxx	Re eHxy	Re eHyx	Re eHyx	Im eHxx	Im eHxy	Im eHyx
9.765625	-3857604	2330265.507	-3331449.88	-4408925	1173051	-46092.96	124243.7	1129696	47401.7248	65502.5682	130675.811	68513.3953	69391.158	55031.514	90469.405	73353.273
19.53125	-4027084	2117392.992	-3544525.57	-4264534	2104260	-289051.7	473426.6	2259618	82149.3462	75757.4766	163335.122	71812.9162	103069.72	110957.91	177137.35	7358.3
29.296875	-4754409	3991686.06	-1898850.18	-6291751	2403570	389294.7	1069897	2596409	123177.277	103596.15	125054.809	80064.4791	105286.11	119013.27	187609.5	100332.57
39.0625	-3401338	2170776.22	-3635184.29	-3787560	4102987	-285996.9	422876.7	4391539	78303.5834	75422.3541	122158.74	95613.1717	144422.63	98927.567	68575.616	129936.02
48.828125	-3377954	2093790.848	-3411508.07	-3656656	4396517	-294171.5	798475.7	5235470	136331.23	86653.799	118588.61	96113.8928	139296.19	130215.56	150012.81	99677.223
58.59375	-2848420	1979171.377	-3574022.78	-3389034	5441768	-351599.5	300337.5	6251418	108733.622	90935.0644	128317.377	110609.465	75958.778	91589.993	62692.342	95168.377
68.359375	-2578533	2224758.841	-3123037.01	-3146706	6195496	-468621.9	208346.5	6988002	212648.591	91042.1878	194064.383	101955.853	159728.33	128659.4	325461.75	105342.22
78.125	-2678503	1921695.589	-3552916.69	-2613793	7218102	-527090.4	455451.5	8198173	55508.1285	68558.4071	88846.9983	132324.455	102813.4	101165.15	110357.15	118500.05
87.890625	-207342	1844932.369	-3437007.17	-2247317	8055231	-537895.4	295836.2	8888532	99510.8151	73009.5254	74644.5444	83186.1145	84802.685	108243.28	119446.39	85270.373
97.65625	-2381732	2714979.527	-2281959.28	-2732884	8483464	-310306.8	814448.7	9641223	115383.369	112544.939	179091.196	137120.354	89047.627	110962.13	108799.07	102037.81
107.42188	-1103629	1877913.22	-4113333.94	-899656.7	9813046	-619125.3	488925.5	11347081	119737.961	135389.738	138752.158	122836.401	180112.02	149686.14	210753.51	95917.448
117.1875	-1196902	1429856.309	-4162555.57	-630954.6	10132661	-561709.2	657441.4	11435379	173190.374	86473.2636	41062.545	125152.925	339953.01	75822.395	605904.66	113307.67
126.95313	-611873.4	1377707.5	-3948224.27	-73671.2	10650129	-161581	1271440	11840344	127410.957	124474.149	148090.366	99004.6071	260876.67	134829.15	313847.4	100320.35
136.71875	214111.69	1064042.007	-3816735.82	512384.65	11033208	554731.8	1952549	12240678	157822.964	115924.243	121426.036	147500.776	212933.59	80091.623	117424.83	135575.3
146.48438	-294387.5	3484286.113	-2807404.32	-1569760	10715318	-1149980	2462344	1207607	142134.26	166890.68	239899.202	114067.162	132003.96	104824.28	146963.46	167211.67
156.25	871692.9	1419268.374	-3347500.85	1345275.6	14258273	-1063939	466387.1	1490834	154338.871	122116.082	281588.206	173577.699	256285.93	134709.7	24795.37	194298.45
166.01563	166004.64	1684022.913	-3396763.25	113621.6	13341086	-1337695	634433.8	14983412	133838.297	106279.17	377852.77	123164.906	188948.89	154664.1	168894.13	88986.11
175.78125	956607.04	2018155.767	-3952060.89	-187451.5	14156339	-258799.8	888631.7	15213516	257602.249	134113.578	506377.227	148894.077	275433.49	181033.64	380911.83	143518.91
185.54688	2081584.4	1442882.104	-4044002.82	3195907.2	14340289	-713554.8	1752643	16117883	334703.322	144873.336	277728.082	207517.637	206882.49	188888.82	283970.72	159245.7
195.3125	3214871.7	1743942.13	-3272365.63	2099702.4	14217254	-849529.4	-148165.5	16388910	146204.537	184867.633	164680.579	334466.75	143350.17	234210.72	151992.41	
205.07813	3263248	1751356.894	-4063796.49	2722543	13927909	-171599.2	1919508	16250328	326943.745	261175.152	388180.516	152079.236	328610.19	126839.47	411395.68	122078.58
214.84375	2593012.2	2084975.686	-2335446.92	3296080.4	14605770	-1471707	2264928	18065272	181996.529	207172.727	209365.816	257263.142	232010.19	178506.58	243000.63	137382.12
224.60938	3823728.8	1142949.055	-2898589.03	4347376.3	15150402	-519199.3	2114807	17701147	304868.97	202545.474	359831.564	134374.485	469302.11	149692.88	301842.82	174067.67
234.375	375053.2	2768817.761	-2172587.55	3305996.3	14162571	-809389.2	2619718	18797866	97601.634	346087.873	1371812.75	461754.962	878084.77	292161.05	1275512.4	298414.1
244.14063	3000533.8	1372394.673	-2620542.28	4523437.3	15241958	-1246124	2090352	19930472	1443324.59	778355.784	1426982.23	576971.595	865002.92	429755.8	1447198.4	810047.95
253.90625	4358358.5	1858679.46	-1610214.01	5257335.6	16976722	-1008097	821149.6	20409702	176589.375	464476.044	3007262.59	957209.551	1704637.2	670592.85	2286151.3	646954.35
263.67188	4278494.1	2052299.825	-2031241.14	5924323.9	17240636	-1007454	945703.2	21106946	383279.687	228064.255	902623.002	240330.866	437749.82	175966.81	599505.98	249538.44
273.4375	4998174.8	1458020.871	-2789943.58	6441723	17423553	-240693.9	383772.7	22320360	215009.544	183588.726	367524.689	147167.844	211006.86	163930.72	156055.33	246296.96
283.20313	4309113	4113598.446	-3507050.32	8847754	17759366	-3517107	94380.19	20410966	156060.391	171395.81	268742.303	213200.623	250498.88	192512.34	342009.9	162521.67
292.96875	7901839.6	1228444.133	-3187305.27	8632203.3	18968627	-3256275	-660959.2	21705267	176272.173	147131.28	338975.029	155923.954	186344.11	149002.54	219064.28	178475.2
302.73438	7167301.2	2267584.498	-3829268.78	8862027.2	18371567	-3402321	-629316.6	19957130	245379.858	98096.9849	217059.776	142631.39	137118.76	168982.29	198043.93	147744.07
312.5	11619012	2327742.356	-4076669	6862099	20049059	-3924004	-246335.9	21538651	152625.006	105142.434	176814.487	131979.2	102416.94	97779.547	208677.01	120709.38
322.26563	11261531	-631912.687	-5499409.46	5829374.4	15019373	-6257046	914306.2	24361901	185219.864	117450.638	161836.779	117469.47	171735.13	131926.51	152115.5	116589.81
332.03125	9250634.5	-7088045.38	-4896707.43	7677493.1	16691716	-5591308	-6149803	21609526	227674.532	110231.82	300482.892	168206.591	209912.65	164177.19	154768.17	1529579.1
341.79688	6560049	-14042288.3	-14628199.8	-2463563	12625690	-2956363	-7581862	20059120	219101.516	165277.809	237955.401	208172.965	311572.1	198799.09	286466.19	166571.33

Table 9 Test condition: Low preswirl-20 krpm-25% Pressure Ratio-100% GVF

0200	Test Data										Uncertainties					
	Freq Hz	Re Hxx	Re Hxy	Re Hyx	Re Hyx	Im Hxx	Im Hxy	Im Hyx	Im Hyx	Re eHxx	Re eHxy	Re eHyx	Re eHyx	Im eHxx	Im eHxy	Im eHyx
9.765625	-5711633	47513285.86	-6846496.43	-3196840	1657418	130628.6	3078.21	1193299	115084.999	268705.408	156456.109	359214.646	159812.17	199952.21	20111.41	259904.11
19.53125	-5354186	4212074.78	-7115444.86	-1928062	2554865	-419913.7	924362.1	2186538	88596.1426	223205.728	96965.2934	354614.174	97879.964	258448.41	207157.23	258109.75
29.296875	-4622634	5988691.707	-4911753.29	-4794250	5922788	-1675422	-1316031	6116044	130379.596	390605.532	205556.619	514178.207	124346.37	449453.42	187365.38	390492.73
39.0625	-4861250	4889959.977	-6758256.15	-689140.7	4826201	-851873.6	1853318	4907986	104796.238	209383.029	87798.4126	469388.058	86137.618	371979.19	12976.38	179711.15
48.828125	-4347358	4054944.534	-6579444.91	-836523.4	5681647	-605806.6	1648407	8616513	73592.7902	196951.433	72618.8955	309005.051	57578.887	227334.74	76301.317	214997.12
58.59375	-3981174	3988992.626	-6347890.41	-1003382	6764366	-1009629	2032570	7104104	81897.2996	175533.97	99062.2339	235908.254	61718.587	163670.56	129623.3	205350.42
68.359375	-3885579	4364937.237	-6229132.92	-790232.2	7488501	-1042324	1937530	8718798	111829.384	199300.335	99606.6987	267252.626	89040.433	223652.61	61117.031	245621.17
78.125	-3866694	4012201.199	-5694061.83	-188354.8	8958003	-907673.9	2464677	9307575	88363.612	176441.157	134114.824	249627.072	91503.228	272419.68	98215.944	184526.57
87.890625	-2868319	3827018.241	-5728818.02	821487.99	9668999	-1391852	1057442	10373582	74444.6375	219570.878	58852.1192	267407.882	81598.666	124295.72	97896.142	285933.94
97.65625	-3514634	3957539.865	-5034239.63	828466.47	10570255	-1555277	2538171	11315886	100558.308	253211.949	94980.1131	260733.229	43863.397	194860.08	103118.44	227695.8
107.42188	-2492639	3967954.572	-469036.13	1038693.3	11591257											

Table 10 Test condition: Low preswirl-10 krpm-50% Pressure Ratio-100% GVF

0020		Test Data										Uncertainties							
Freq Hz	Re Hxx	Re Hxy	Re Hyx	Re Hyy	Im Hxx	Im Hxy	Im Hyy	Im Hyy	Re eHxx	Re eHxy	Re eHyy	Re eHyy	Im eHxx	Im eHxy	Im eHyy	Im eHyy			
9.765625	-476518.9	1533009.808	-2252774.62	-754880.1	832664.2	283157.7	330908.7	960061.3	89229.719	90746.0003	162893.173	75962.3553	105918.33	148828.94	116641.41	154450.64			
19.53125	-573408.6	1534144.39	-1786241.6	-735953.3	1576470	-137232.9	67961.44	1742120	148412.606	95701.6286	104273.223	86987.6118	68544.404	109083.93	117330.03	96352.649			
29.296875	-1876443	3260202.706	48677.39658	-2903333	798837.1	1297581	1908330	536150.6	136967.829	73512.5216	133163.654	82167.1408	98846.73	120127.36	116313.02	86826.463			
39.0625	-324978.2	1258962.673	-1948699.89	-399968.3	2873754	-337254.8	-72460.81	3126566	86080.5874	76081.1288	54647.2203	92284.9362	76044.536	110080.38	110921.98	49880.638			
48.828125	-54596.49	1102929.368	-1916633.55	-218878.3	3561230	-278567.3	255830.6	3732466	42739.0279	98027.1913	73957.2274	110881.72	107620.34	113450.37	129785.12	70997.526			
58.59375	31035.655	1274845.101	-2040700.65	-391750	4159580	-354115.6	305126.1	4739163	123085.345	101407.684	88134.5508	82092.7332	70534.546	86950.405	134491.62	106742.37			
68.359375	22374.931	1205687.127	-1745669.1	-379623.9	4703527	-182442.9	685017	5474469	86943.8109	101478.502	55535.8385	104416.537	100086.24	114860.03	106046.19	114353.88			
78.125	-170433.6	975750.0176	-1673918.78	-106865.2	5717332	-287515.1	67136.9	6214050	103559.142	70147.6675	129970.206	92481.6908	75197.876	130327.71	104442.1	108492.26			
87.890625	49363.177	931476.8668	-1967102.55	186534.58	6347219	-223235.9	88146.96	6999239	57426.2671	83137.7771	65353.2621	96551.7138	48841.377	84890.83	72918.828	106893.13			
97.65625	-1184938	2071095.131	-697327.847	-1066236	6939706	-259088.9	18433.86	8099002	77275.566	62218.2971	93962.1595	92160.9474	88504.414	108072.67	9548.609	83701.587			
107.42188	658469.15	887087.9492	-2381927.54	421847.99	7762351	-332340.2	87515.51	8438815	110943.995	86343.2705	171819.764	108312.043	80622.553	114357.3	164235.97	114842.59			
117.1875	77643.74	872310.6319	-2192630.44	807689.99	8334237	-219876.6	115902.4	9113417	70512.5387	78574.7485	113034.176	115327.662	96795.531	93751.917	92533.54	98643.46			
126.953125	752672.67	602484.4965	-1899816.83	1242023.2	8569520	317877.2	553278.3	9528608	41559.9186	98802.8415	83189.7151	80193.4554	68363.035	87863.247	84544.232	74547.48			
136.71875	-463636.1	1829689.034	-848320.362	473106.76	9339817	20908.23	516925.8	10701022	55040.83	92437.6687	69863.6111	64184.8866	93031.781	102443.38	88978.285	109466.88			
146.48438	210545.27	1774356.969	-1444763.62	882617.26	9165867	178577.3	1235841	11054543	101332.994	117307.713	101683.786	112883.038	89900.226	101538.47	129264.33	897831.297			
156.25	1490005	985662.9129	-2848755.91	1785776.8	11416094	-814472	-377098.3	1263156.3	17786.763	15097.473	116654.314	151664.486	128214.4	133114.04	154099.93	116537.81			
166.01563	1023087.6	1086479.76	-2280742.82	1995779.8	11428364	-373691.7	-64235.27	3276273	32762.072	326546.765	301863.54	346029.422	228961.04	319755.9	346988.96	395481.18			
175.78125	1143757.5	859885.4459	-2652255.02	322659.75	12509999	-15451.06	558142.2	12883726	349591.975	192868.299	520574.187	255862.009	379457.41	245468.48	389020.42	234251.49			
185.54688	1098991	2944305.645	-1981274.77	1268123.6	1268160	-1109005	737199.3	1686407	164476.828	140666.317	239598.838	146340.121	92135.733	154824.86	212886.81	157993.77			
195.3125	20479329	1053225.007	-247694.24	2618288.6	12813137	-335079	647474.9	13689946	66218.2192	111810.948	216070.604	75526.0154	104109.97	116630.29	144505.5	125991.77			
205.07813	2300951.9	1871192.878	-2820250.72	1744983.4	12868389	34583.7	1362287	1364281.1	172505.785	110359.324	158696.199	109220.443	188875.32	118683.45	183906.54	117022.69			
214.84375	167012.8	1194704.299	-2149486.16	2955859.9	13904615	-1211773	153310.7	16518210	98159.1576	155495.631	125411.52	196620.175	145968.3	135655.32	110833.43	80296.592			
224.60938	2146892.9	317074.4341	-2131594.5	2960651.2	13768199	-105840.1	656325.3	15572671	345190.095	91006.0746	314888.71	80656.3103	297051.29	133243.18	294339.17	73714.274			
234.375	-1346142	2463365.877	-237240.519	1072455.6	13826622	-244711.9	1078249	16662769	117911.708	136010.519	174505.334	93698.0971	104088.24	121194.94	180978.73	108221.69			
244.14063	260460.91	1053225.007	-247694.24	2618288.6	12813137	-335079	647474.9	13689946	66218.2192	111810.948	216070.604	75526.0154	104109.97	116630.29	144505.5	125991.77			
253.90625	1062897.8	767520.6099	-1649379.96	2989425.6	17332718	-204905.5	59414.25	19969514	7026.9185	8034.0749	103294.666	68011.2106	141746.99	100578.206	190805.89	51371.584			
263.67188	717043.41	1223604.035	-1488815.09	298481.4	18275438	-188330.9	2015612	116241.006	156241.906	92057.0482	78164.3759	57391.2624	110433.17	100286.85	54802.981	79211.141			
273.4375	594855.73	1021720.321	-1980492.55	3580044.2	18356851	-9930.33	-801583.3	2015650.1	138753.001	107548.205	123302.934	97670.6418	100250.89	83327.84	83582.184	89358.592			
283.20313	-2376973	3634410.011	-3101421.69	4537195.3	20472201	-2437065	13261.03	20509344	89747.3192	98530.0917	104176.947	68870.3886	90599.698	80736.406	97781.88	97855.387			
292.96875	243498.2	611810.9345	-1693072	4294767.2	23621221	-3145052	-1441986	22327309	154477.801	119545.892	90286.1923	79881.6042	155325.49	129206.88	119195.76	73480.489			
302.73438	1923488.1	662823.0875	-3168698.87	4872294.4	24610167	-2480373	-1794255	21709321	66082.3861	97931.821	97101.1139	85887.7847	120931.57	107259.72	90208.712	96992.201			
312.5	558620.73	1609414.883	-3638425.79	3573508.7	29199786	-1767710	413845.9	24879429	102144.82	119111.289	80225.2421	77148.9491	102108.04	105626.78	108614.07	84300.701			
322.26563	7312449.8	-2179758.95	-2561115.9	3816269.4	24756376	-6145851	-25729.24	26571200	118075.48	112233.54	173591.321	80534.9168	81278.931	101874.19	125397.14	125978.57			
332.03125	7016828.1	-5567115.72	-4520292.47	4851140.9	28597441	-3672464	-7408000	23311492	245292.301	161668.163	166777.538	205337.961	213361.76	153903.9	373420.2	175008.08			
341.79688	8153039.8	-8034936.49	-6862811.07	2071894.6	26255334	-1893192	-8214728	21846277	639480.886	334834.375	170406.673	579442.418	417324.63	420987.82	1151590.5	608496.81			

Table 11 Test condition: Low preswirl-15 krpm-50% Pressure Ratio-100% GVF

0120		Test Data										Uncertainties							
Freq Hz	Re Hxx	Re Hxy	Re Hyx	Re Hyy	Im Hxx	Im Hxy	Im Hyy	Im Hyy	Re eHxx	Re eHxy	Re eHyy	Re eHyy	Im eHxx	Im eHxy	Im eHyy	Im eHyy			
9.765625	-265818.6	2786197.997	-3493384.34	-619842.4	969907.9	-162196.4	116494	978089.4	109746.621	78048.9815	153329.309	145742.996	9652.464	101097.32	95344.46	85846.62			
19.53125	-287471.5	2662336.414	-3203422.35	-470344.5	1648868	-162578.9	257623.9	1833585	90251.3355	92330.4182	97561.0771	69874.3872	85462.093	85033.278	57476.43	80142.468			
29.296875	-1739649	4926676.632	-1394966.83	-3000491	1287840	1035266	1744462	988794.3	89758.6137	61711.4631	125746.589	106236.495	103759.27	101096.54	106681.088	87210.624			
39.0625	-3805.79	2625975.497	-3193980.28	-262587.1	3071581	-304621.5	436748.7	3537309	93774.7075	62970.9617	178020.675	73581.6694	78385.697	64578.388	70053.97	97369.829			
48.828125	-202066.9	2719109.416	-3082237.96	-151921.9	3618893	-390629.2	299309.4	4220897	84090.8672	72975.9249	184466.42	105176.447	63368.402	91033.285	148556.22	89322.571			
58.59375	-15347.08	1164939.412	-3361629.06	-167456.9	4461419	-990496.1	88102.06	5009466	86993.8202	82569.5359	143590.527	113799.595	169034.55	93221.917	113733.58	91277.732			
68.359375	-38423.2	2584277.604	-2660391.69	10251.71	4791803	-362922.5	327075.1	5470888	147666.979	80487.9568	215038.78	82531.5071	133599.01	77918.017	90782.924	72361.169			
78.125	-948.1115	2589071.117	-3187304.85	417630.87	6104384	-691551.9	483019.1	667578	97566.4848	173671.347	124240.711	182702.08	90391.085	197819.24	96567.921				
87.890625	381107.6	2242537.317	-3133024.72	399922.48	6492973	-667528.5	261029.9	7412970	61562.3981	71000.7933	127902.579	85747.5814	53521.953	97007.63	74325.704	77354.11			
97.65625	-53251.51	3197399.168	-2302623.02	-360256.7	7877972	-525067.3	158591.5	9198817	60373.7437	74335.7231	167732.764	71653.5946	145621.67	74879.345	179028.78	90651.034			
107.42188	97957																		

Table 12 Test condition: Low preswirl-20 krpm-50% Pressure Ratio-100% GVF

0220	Test Data										Uncertainties							
	Re Hxx	Re Hxy	Re Hxz	Re Hyy	Im Hxx	Im Hxy	Im Hxz	Im Hyy	Re eHxx	Re eHxy	Re eHxz	Re eHyy	Im eHxx	Im eHxy	Im eHxz	Im eHyy		
9.765625	-436547.5	4678614.116	-5057866.79	77868.443	916099.9	47221.3	247392.6	1255953	96068.426	154685.542	109280.562	119444.35	73387.165	138235.66	92841.052	142177.6		
19.53125	-384528.1	4335610.89	-4842767.66	-120384.2	1843532	-224584.4	463096.4	2117808	65272.5702	96721.894	99420.8423	67394.6453	56610.268	71899.413	64651.301	82442.919		
29.296875	-1812578	6822056.539	-2879401.75	-2460622	1964665	757792.4	1400840	2052227	114036.459	96980.955	101038.838	79642.6523	86674.053	99289.166	112817.31	69441.431		
39.0625	-115343.2	4694410.282	-5093545.77	412202.16	3571486	-315412.1	335823.1	4115698	56447.9165	86268.5531	91241.5769	65697.2052	47113.352	125368.9	94497.561	82281.943		
48.828125	-18687.78	4564443.641	-4955954.18	476479.01	4559642	-167618.3	399577.8	5109430	118805.399	87979.5758	58384.577	97191.0595	59295.611	69215.3	64456.435	47246.859		
58.59375	328069.76	4475126.328	-4758650.98	705766.24	5714595	-304404.8	676139.5	6091995	134939.466	120549.03	146556.853	93890.95	121363.43	84907.879	94406.163	93683.737		
68.359375	493664.14	4625839.888	-4478385.17	1068510.5	5480777	-265471.9	658925	6658271	54148.0483	79901.1272	121777.883	69733.9578	68096.762	112563.99	127370.66	73902.211		
78.125	535449.37	4465230.39	-4757331.38	1432122.1	7027524	-494417.3	801031.2	7676015	120674.051	96685.3775	89758.8044	87995.153	149661.79	112315.6	116942.78	112262.86		
87.890625	9247809.3	4596049.629	-5226849.45	1626630.8	8026647	-593457.1	345148.9	8544713	119888.272	119164.815	109983.125	64812.2071	46996.614	97625.516	102187.7	83386.132		
97.65625	74571.641	5409487.96	-4000895.91	746133.04	8225581	-530994.8	1039919	9009660	81679.2189	94693.11	115232.723	89508.4292	64666.709	70214.748	72012.053	90989.996		
107.42188	2079443.1	4024524.467	-5537528.84	2613165.4	10072660	-1547720	-198190.7	10641549	85166.4276	85107.2486	192512.065	134824.49	96958.025	135781.31	246599.55	117942.15		
117.1875	2611969.9	4003730.682	-5435038.25	2619516.8	11036932	-1535187	136362.5	11375113	102349.177	108941.674	176021.816	83122.6784	102855.62	111296.34	109144.87	104898.71		
126.95313	2072596.1	3820672.029	-5148491.26	3066937.4	10125245	-507547.6	1553000	11981828	74258.9066	118013.392	113127.194	94505.6894	68964.417	111704.63	96941.841	146629.25		
136.71875	2447809.3	4033156.11	-4860061.01	3522904.3	11237450	-546545.8	981194.3	12640984	67542.0969	90357.3414	86570.2809	109623.856	70997.057	85748.849	121328.78	115105.25		
146.48438	2512618.8	5330204.797	-4533942.6	3081047.3	10654810	-408850.3	3129092	12460693	148251.539	138475.058	172603.384	149515.372	78892.653	149151.37	176241.36	137061.17		
156.25	3522547.8	4209803.884	-5292908.21	4191609.5	13448540	-1370145	4660379	1994350	119640.228	134686.996	146837.998	113709.306	103734.12	128544.85	16244.56	206822.38		
166.01563	3392965.3	4177379.311	-5400953.26	5248608.4	13329296	-1250087	1023514	15307815	113374.512	180085.11	112641.243	162885.451	611274.93	111689.87	104083.7	125905.22		
175.78125	3905924.9	3815883.336	-5905480.6	3456029	13382700	-821435.5	1169042	15827296	175198.932	120914.349	256778.833	112561.468	146256.58	138476.38	291215.26	135229.44		
185.54688	4287563.5	4062266.178	-5715081.88	6905671.5	14267468	-1479000	1789901	16767050	159853.383	80655.3026	309495.492	159366.781	243127.69	130335.61	157607.35	131767.99		
195.3125	5271130.9	3776314.994	-5641020.5	6234199.6	14305952	-1520441	1511054	16623943	158182.83	163775.745	131380.36	140446.994	179044.3	113825.79	226056.52	128734.32		
205.07813	5468012.3	4104517.77	-5617610.78	5688582.2	14171038	-760000.6	3290621	16172358	107256.524	108450.738	208129.488	131764.72	223021.33	114447.28	226248.58	156946.13		
214.84375	4374433.5	4153980.757	-3760091.59	6004098.6	14180559	-2333911	2817493	18822893	132349.366	133236.041	110785.864	177121.827	80355.526	171305.32	140350.21	120956.86		
224.60938	5114280.2	3163935.233	-4857819.1	7393753.8	14939543	-730014.4	4258842	18325377	297284.785	107125.817	269134.699	128017.733	252738.72	142719.84	330386.52	109348.21		
234.375	4293610.8	4618920.433	-2924561.09	5805707.9	13234285	-1011295	3523494	19213921	115364.41	122720.955	94807.5692	108054.53	152937.21	133662.32	88252.773	123965.13		
244.14063	2707395.4	5043642.713	-2336002.04	6317910.9	16035759	-1712650	866818.5	20864252	255288.568	135025.076	185758.048	130953.63	210286.34	128191.15	165203.91	100018.51		
253.90625	590255.6	3443254.742	-4697229.93	9242226.69	17154581	-928802.9	1549940	18176912	158462.287	87970.2079	141561.722	60309.1863	115340.33	88932.135	179033.74	9059.187		
263.67188	5876427.4	4393325.741	-3835740.09	8700498.1	17836656	-874347.9	1417514	21762583	142940.645	87732.3394	229708.913	87537.3068	111444.78	86384.307	138376.91	102957.92		
273.4375	5682675.7	5773447.638	-3777935.23	9395355.5	17324175	-810857.7	411428.7	2293602	122225.56	104552.353	160817.849	107553.109	151906.39	130384.93	164249.62	129248.79		
283.20313	5357910.2	7249803.856	-4563733.74	10005598	19918613	-4778039	1851528	21597342	144184.8526	124680.211	152881.186	125433.192	142138.87	116200.51	123215.52	149957.66		
292.96875	8027711.2	4243350.251	-4428804.79	9928883.5	20272006	-4513212	-148400	2531644	92516.642	102032.292	162364.247	98960.0099	85630.614	102083.27	178924	97553.147		
302.73438	7333112	4987790.993	-4600482.07	10658602	19978838	-6252692	-283543.6	22268052	74345.0721	95351.269	137541.354	136633.912	120733.9	86972.863	202558.5	104472.32		
312.5	11879652	3861348.748	-3653954.17	10121735	22527668	-6438696	-750816.7	25308843	154481.107	107030.684	173680.544	129639.336	120130.38	118040.36	128002.51	103604.06		
322.26563	12680231	688586.288	-6745791.05	10078233	18361804	-6994185	-334590.8	25736851	118324.477	119698.467	210040.701	170963.104	85438.4	103510.45	282570.26	147371.31		
332.03125	15184221	191482.8088	-6619736.78	10762662	17483207	-6121862	-3721686	22245741	578907.619	875405.492	1022139.88	1252748.65	795308.83	769809.6	1075995.5	1403793.6		
341.79688	14719023	-4067830.99	-6898709.15	7596873.7	15401160	-5020396	-3408431	25984959	174478.932	128112.014	120534.137	180528.031	204095.27	132137	263277.82	161380.51		

Table 13 Test condition: Low preswirl-10 krpm-65% Pressure Ratio-100% GVF

0030	Test Data										Uncertainties							
	Re Hxx	Re Hxy	Re Hxz	Re Hyy	Im Hxx	Im Hxy	Im Hxz	Im Hyy	Re eHxx	Re eHxy	Re eHxz	Re eHyy	Im eHxx	Im eHxy	Im eHxz	Im eHyy		
9.765625	134239.12	1348509.469	-2143993.09	346380.25	643465.3	-93145.84	-85823.32	1321825	63353.7524	80828.1973	105316.983	116323.4	57969.727	157092.76	62115.587	114912.34		
19.53125	266997.02	1677170.98	-1609259.6	165653.27	1374502	28462.03	34392.8	1530099	82455.2245	77441.1596	62867.7836	59705.5845	78707.528	97867.106	68608.379	82734.068		
29.296875	-668467.2	2897996.371	-422912.754	-1316073	338578.6	1931575	2335169	64348.87	64914.8731	88030.353	107335.99	55054.7979	85622.56	95972.584	76612.489	73618.677		
39.0625	545959.39	1307156.54	-1758154.59	1015383.5	2734378	-273406	-5387.33	3561866	33607.272	73361.3867	70014.7779	72840.5126	43051.547	94031.288	66726.218	74958.308		
48.828125	325370.27	1439606.941	-1682251.52	817449.21	3369856	-83399.16	121359.7	3866877	38838.5373	72173.7433	76838.5405	87021.9405	62061.018	127948.87	94629.521	80791.71		
58.59375	630788.45	1352670.757	-1773116.33	946361.19	4221819	-160845.4	101329.4	4544891	104846.973	75188.2929	95215.8139	78368.2681	65460.389	88659.277	67535.979	75964.646		
68.359375	378839.78	1428978.985	-1722473.45	588068.39	4560445	-44904.56	383130.7	5505713	55076.7774	66165.4275	95292.1582	55047.2101	59410.912	90588.437	57341.59	61515.544		
78.125	592934.28	1276449.147	-1855924.27	1300369.8	5407275	-171823.8	283374.3	6073755	63272.1716	68645.597	109746.629	69008.9382	36846.723	118480.82	71505.351	76388.273		
87.890625	857493.15	1018725.917	-1714764.63	1256136.6	6196114	9659.233	-19421.95	6891579	50723.6202	87495.3916	99668.9088	76492.998	59731.533	90966.577	63691.207	59158.595		
97.65625	-184875.7	1902518.515	-820336.921	360661.3	6561761	435301.5	381402.3	7148466	66934.1305	82893.624	55699.6566	75358.0156	45698.648	111379.48	79111.917	84355.169		
107.42188	777875.66	869425.6782	-1741756.97	1752688.9	8767040	-784203.2	-1600182	9665903	84320.8362	79156.6245	64793.1675	89036.2955	108043.19	86895.804	137658.91	82431.647		
117.1875	887969.33	911194.9797	-1888721.51	1901906.5	8826635	-187051.3	-632715.7	982146	59119.5305	56921.8068	102539.915	90616.1718	67803.138	85521.618	126396.7	57666.488		
126.95313	1053595.3	1070965.805	-1990933.53	1770749.4	8098351	660582.6	216808.6	9726671	38917.338	51725.1948	44803.4631	77486.6994	49532.676	67007.442	44372.752	80440.416		
136.71875	85194.76	1868002.409	-1275124.36	1050955.3	9098498	290927.1	111821	10861574	29799.0167	78433.8								

Table 14 Test condition: Low preswir-15 krpm-65% Pressure Ratio-100% GVF

0130	Test Data										Uncertainties							
	Re Hxx	Re Hxy	Re Hxz	Re Hyy	Im Hxx	Im Hxy	Im Hxz	Im Hyy	Re eHxx	Re eHxy	Re eHxz	Re eHyy	Im eHxx	Im eHxy	Im eHxz	Im eHyy		
9.765625	922038.73	3385592.353	-2703933.44	365641.13	837829.1	89721.46	398772.2	1529601	82599.2539	159653.497	109784.011	98573.9536	125536.83	191786.62	95118.778	127556.61		
19.53125	1236622.4	3222930.965	-2706401.48	366150.11	1764571	-108690.8	-16159.51	1893695	137407.911	95085.2149	107417.615	88935.0808	168020.66	134460.83	111093.49	116161.86		
29.296875	-225462	4849064.898	-1304712.96	-1449835	923551.7	1924610	2428921	347552	148879.163	105060.839	116640.576	79652.1873	164223.63	130036.89	159791.72	84601.605		
39.0625	1438795.3	3164580.498	-2709677.87	908518.19	3422011	-334679	308863.7	3434630	84659.2298	88301.7247	98755.9118	69786.8289	125037.7	84141.464	102834.25	54251.765		
48.828125	1131230.3	3192266.787	-3008881.92	794256.75	3990972	-140592.1	147279.3	4356191	113648.326	103339.413	121221.762	73783.1012	96275.939	92555.926	89139.391	69101.379		
58.59375	1349743.6	3033667.806	-2691829.68	933585.61	5358015	-188976.3	-236121.8	5154631	103659.124	94410.3632	129710.275	104353.799	190271.25	96657.038	137079.72	88226.039		
68.359375	1196304.9	3244057.199	-2804003.02	765198.26	5598011	-60721.49	598223.2	5800196	142728.56	91171.3424	89006.0148	69902.2652	119170.84	79326.32	136991.57	51677.473		
78.125	1224583.4	2919395.521	-2840855.12	997637.21	6598340	-214807.4	267598.6	6698739	154193.57	97462.5731	158909.817	73807.9104	158543.82	98795.338	117716.96	82885.937		
87.890625	1297613.2	2739964.589	-2978475.73	1275402.1	7401168	-79893.2	89048.23	7369248	110455.946	76222.0779	132924.306	71391.0727	103527.52	106051.68	116686.88	61886.88		
97.65625	424240.48	3749424.398	-2400697.69	184811.47	7419257	171287.4	432824.6	7988434	101492.259	66248.5362	170376.778	88327.3091	87758.998	95396.611	99427.799	99247.799		
107.42188	1815968.2	2902737.948	-4011344.72	1500136.5	9367036	-159537.3	-234636.3	9959952	192924.789	97965.3145	339344.388	95209.463	138998.92	101023.83	246626.61	102569.77		
117.1875	1975532.4	2756417.464	-3159685.06	1939520	10232070	-154438	226786.3	9980004	212176.454	116673.143	132640.694	126552.162	194206.43	134325.19	266094.82	69321.143		
126.95313	1140727.4	2957089.313	-3451542.89	2331479.5	9705826	269626.8	894440.1	10512670	236394.972	92128.6458	164021.2	110318.322	184679.45	113213.35	210713.71	83583.451		
136.71875	-1320658	3202644.295	-1470592.85	1724718.3	10219914	273581.4	1025737	11230480	104686.941	76394.919	149425.814	75044.7384	160295.54	99330.815	93548.871	78994.66		
146.48438	992343.42	3900909.581	-4052214.56	1695794.1	10519714	-3026.404	2366250	12014358	191166.394	109713.879	257249.331	137679.585	158994.74	89285.62	117130.34	113985.78		
156.25	299998.1	2400207.69	-5971858.28	3261211.9	13454241	-415221.2	-1228588	12895258	108544.662	108102.45	166559.588	79461.0049	112209.25	74384.991	247426.61	70362.595		
166.01563	871790.57	2662605.895	-3505623.17	3118628.8	13206854	-204124.5	543436.5	14030237	96563.3015	98487.9557	163318.823	74640.403	172919.11	81022.376	150990.52	110554.87		
175.78125	10309.62	2849465.386	-2603701.95	1368281.6	13363469	382653.1	486748.7	14259441	67359.547	55685.6006	659757.851	80482.4725	345271.09	93614.79	405652.12	81695.34		
185.54688	294680.11	3354253.031	-6406011.99	5159159.1	16716304	-258720.1	3240572	15835614	253772.4	105441.783	277368.94	116763.67	410032.13	105353.43	376211.91	98568.963		
195.3125	248681.35	2915927.5	-4591457.91	3851455	14366378	-311367.3	1372713	15380414	264844.636	77882.364	267002.12	91526.7856	358073.13	109732.46	411025.03	85925.089		
205.07813	-264168.7	3252315.99	-4746000.08	3186517.6	15604666	559272.7	2269622	15106664	494561.646	93964.8101	498471.793	99564.8033	68999.38	152187.71	432305.83	95033.093		
214.84375	-1308972	3560085.945	-3988010.26	3379730.9	17181377	-733317	1487173	17515481	29336.108	120504.463	475430.325	130174.546	419320.48	204111.26	349861.47	109623.1		
224.60938	584213.66	2600127.91	-3788966.47	3872482	16241758	-20463.28	1018014	17266964	784241.563	119999.183	1058816.37	156205.836	327610.7	180945.95	1091825.6	163945.26		
234.375	-3228765	4484683.593	-3670468.4	2104131.4	16580039	-517195.3	2661338	18245411	689396.679	190819.135	900134.095	228527.448	798457.41	210017.88	675463.43	166509.14		
244.14063	-4400417	3432920.562	-417723.21	2721548.5	21269523	-1267867	-523890.6	19863413	3799389.49	549718.822	3204885.21	544362.696	3408406.8	599290.88	4504684.9	625362.71		
253.90625	-5733181	4197451.201	-6135667.61	3856648.5	17742734	-528263.5	5804565	20754393	4121781.44	638282.64	3979526.17	704995.036	1789089.8	414878.66	4122114.9	620813.27		
263.67188	-3352740	3977694.906	-4515009.84	3488783.9	21231639	-1125214	569359	21822500	917236.24	190106.078	1247808.65	240064.282	824995.84	175869.74	869191.34	168679.40		
273.4375	-4695218	3674300.486	-4181376.83	3495019.1	23240260	-2226635	122010.9	21629596	545899.731	165554.941	637209.776	235399.255	690399.37	222215.91	725581.25	166010.05		
283.20313	-6846813	3569329.233	-5426425.49	3314715.6	26238439	-4882700	-696459.8	22487395	31474.804	170835.95	441801.702	180468.081	402308.19	148289.29	539295.4	126253.21		
292.9675	-4729665	2173941.029	-4985653.49	4010162.6	28111328	-4284901	-1495998	24212163	396963.802	94952.1213	584934.539	136440.736	168582.72	156223.31	329583.47	193889.11		
302.73438	-3760755	1405797.435	-7567664.47	4929016.6	29272921	-4941529	-2326016	23513148	638363.137	128065.99	236525.632	172402.442	209602.25	273625.14	411466.39	128643.03		
312.5	-2439230	1640021.376	-7874217.63	3180472.5	32102790	-4719498	-1001394	2550427	326030.938	152851.651	449209.006	125599.443	398346.48	107576.17	215698.03	164393.06		
322.26563	-2721478	-632530.788	-7640836.09	2058213	28587432	-7561152	2636373	38275421	132143.513	108425.929	444424.854	145711.864	165681.69	341259.29	67356.82	82		
332.03125	-7589080	-572415.92	1065033.119	6167657.5	34422677	-8955435	-5559904	28225231	4289903.014	211522.502	421789.668	147677.061	522277.94	212622.24	299085.97	196058.61		
341.79688	2878439.9	-7048933.94	-8355885.28	2374719.8	34181662	-4478437	-6069921	25958137	330748.367	227323.087	455696.095	197396.426	476141.69	162471.91	389448.16	213155.66		

Table 15 Test condition: Low preswir-20 krpm-65% Pressure Ratio-100% GVF

0230	Test Data										Uncertainties							
	Re Hxx	Re Hxy	Re Hxz	Re Hyy	Im Hxx	Im Hxy	Im Hxz	Im Hyy	Re eHxx	Re eHxy	Re eHxz	Re eHyy	Im eHxx	Im eHxy	Im eHxz	Im eHyy		
9.765625	77865.64	5457798.739	-4600658.65	290747.12	1303805	-229278.4	179176.7	1647152	96321.4845	92842.0757	99141.4567	92884.956	94877.674	126972.7	116242.3	120881.9		
19.53125	424845.18	5333116.522	-4485722.92	312599.89	2095889	-360881.1	-57054.87	2190962	83141.9904	98127.9934	62018.2116	111332.886	99203.464	101517.11	119860.9	96392.856		
29.296875	-427961.9	7215138.774	-3022787.97	-1797374	884318.5	1429267	1951612	981090.9	93884.2437	76398.9421	130137.798	87191.0607	62238.143	84269.797	82124.852	73205.098		
39.0625	841770.7	5330908.354	-4694357.6	722880.52	3479199	-235944.4	120873.2	4136239	82681.9106	69725.7708	83852.7984	48395.356	102095.29	84698.815	86554.942	82		
48.828125	930106.62	5219797.053	-4903316.88	516388.42	3992028	-499555.6	36635.99	5028362	52760.4352	132319.912	74248.4157	84507.7249	87942.678	111861.92	50507.69	65447.464		
58.59375	1182715.2	5346776.295	-4842101.82	902952.58	5288305	-438229.2	-94134.93	5969674	111638.603	78899.3198	124223.18	84373.1855	96738.155	122192.05	98878.21	107657.42		
68.359375	1003177	5248349.459	-4944151.3	1001982.8	5506974	-333818.6	536343.1	6883198	93210.3671	96144.9092	72459.6513	82798.5589	107983.59	90558.011	99276.417	91815.701		
78.125	1263920.3	5145029.795	-5002087.03	1571426.6	6562835	-515295.4	45679.41	7596263	111598.313	87869.5272	125881.402	90737.3807	84008.206	91252.663	140547.73	99874.068		
87.890625	1391638	5241557.896	-5113780.88	1644058.6	7308928	-324797.2	118010.3	8707260	35325.5991	106488.406	77635.6228	100755.232	46288.631	94160.185	78004.272	97299.475		
97.65625	699015.32	6108081.341	-4312569.72	756998.55	7843542	-111659.5	438795.9	9170609	73363.4801	70374.1402	73508.4113	101682.8	57190.635	76360.003	99460.93	109684.88		
107.42188	2540148.3	4799414.901	-5354845.03	2472195.6	9194094	-917176.2	-301053	10960456	104939.609	77186.7208	21947.181	171263.564	71312.178	116563.75	228081.01	112130.01		
117.1875	2777634.2	4801955.453	-5649839.81	2733840.6	9773425	-790575.2	52191.54	11292529	39507.5767	64708.6296	144947.276	75899.6431	64377.375	82884.912	125587.02	89045.778		
126.95313	2093583.4	4631523.111	-5050239.96	3281269.5	9534113	-319820.8	871964	11700180	51012.2727	92306.4404	75840.5812	88038.956	53135.371	105240.73	96868.684	139755.09		
136.71875	1283229.1	5135358.991	-4144474.52	2986603.2	10600710	-319294.1	367171.3	12595278	67140.3193	94746.2371	58117.3003							

Table 16 Test condition: Med Preswirl-10 krpm-25% Pressure Ratio-100% GVF

1000 Freq Hz	Test Data									Uncertainties							
	Re Hxx	Re Hxy	Re Hyx	Re Hyy	Im Hxx	Im Hxy	Im Hyx	Im Hyy	Re eHxx	Re eHxy	Re eHyx	Re eHyy	Im eHxx	Im eHxy	Im eHyx	Im eHyy	
9.765625	-2680187	7106881.886	-10511176	-3303802	821753.7	-74617.4	-555544	1657783	277137.518	171959.851	351619.31	158514.379	327120.41	164141.56	291667.65	179114.14	
19.53125	-2687021	7210155.646	-9505426.14	-2949900	1918908	-490109.5	116488.4	2393453	99720.4734	122652.851	98810.1583	113047.666	92312.545	124877.33	106634.09	114129.83	
29.296875	-2490405	7738538.095	-9282634.51	-3424278	4784759	-1698175	-1489663	4405265	135132.316	168808.262	187766.338	332314.196	139042.45	190819.43	260799.55	217133.82	
39.0625	-2493718	7109195.929	-9438744.71	-2548291	3848754	-466674	506078.9	4250690	42666.1085	85905.2701	90720.0177	105183.545	46098.563	116153.11	55092.731	90326.732	
48.828125	-2445011	7044785.414	-9195208.21	-2419473	4791479	-601379.3	587435.7	5323428	70497.7479	113837.407	76706.3002	123316.918	60633.479	85807.261	92414.169	106462.79	
58.59375	-2441957	6661667.058	-9303745.46	-2235369	5670671	-454702.3	806977.1	6427841	128666.089	144886.087	131692.192	100606.759	113879.59	125854.18	181645.069	127885.77	
68.359375	-1762146	7121766.279	-9161862.29	-1914922	6820858	-388573.5	913490	7937071	70878.3118	133750.427	113239.953	66065.9957	79456.441	103299.64	60984.768	105037.7	
78.125	-1395689	6965485.51	-9162042.72	-1162993	7694367	-851309.2	943415.4	8427778	112735.115	101678.943	91912.1208	90543.522	100793.49	133223.03	76942.552	121011.53	
87.890625	-1038326	6737613.405	-9333663.45	-706075.5	8476333	-866508.4	1034461	9251389	60408.6597	64778.4508	71201.0095	119287.642	58895.943	82937.324	88526.506	103629.65	
97.65625	-887901	6957049.633	-9479367.22	-610515.3	9580699	-911934.5	892740.8	10030431	70173.2924	98925.2474	56037.3318	108456.356	85732.671	107908.53	87133.775	126466.38	
107.42188	-523948.3	6593195.664	-9253451.97	-167949.4	9949856	-535365.9	1223410	18021523	89507.9573	108597.072	147493.336	134546.071	57260.763	148007.3	133123.98	155081.71	
117.1875	-879980.5	7125535.793	-8785674.82	163543.71	9330513	1962.45	2845705	11029792	88485.0982	84200.1188	71640.5036	76022.0513	128710.4	117928.71	70586.551	113000.21	
126.95313	80698.77	6358959.51	-10211639.4	1500134.2	12497796	-1531551	618263.6	12915252	90683.6552	93780.7632	97490.4446	94166.095	114468.57	169262.84	82678.464	127284.14	
136.71875	266455.25	733657.523	-8983630.67	-202740.6	11831616	-481609.6	2726540	1202049	49815.378	103768.678	84694.9215	73921.4079	67860.07	116218.97	134629.31	133432.35	
146.48438	1715175.6	6373884.107	-10187994.8	2811726.7	13636115	-1669928	467522.9	15578843	125237.178	134836.884	119175.15	185532.824	131559.17	134609.58	144445.03	144445.03	
156.25	-76213.39	8047819.137	-8845736.59	1849211.9	13003766	-890472.2	2487342	14504704	79633.6435	139953.986	110305.733	150323.346	140539.89	167876.95	134735.31	134735.31	
166.01563	246525.02	9047039.043	-9321056.05	3063064	14925928	-1467605	1816239	16004699	128603.821	253169.796	173494.578	266179.902	195375.52	185858.88	195841.78	235661.02	
175.78125	702922.01	9504689.853	-7621890.75	662527.73	15452883	-1297322	2586658	19683679	248268.923	210460.906	280476.448	158773.707	177120.12	232194.66	198066.08	331922.92	
185.54688	2113251.8	7797680.192	-9275394.1	4083159.5	15945327	-1710981	2581352	17844728	114953.595	155424.744	94362.793	156499.211	187471.09	189048.55	251230.43	160624.48	
195.3125	2968972.2	7002417.781	-9185226.7	4510019.1	16259304	-3000791	2207966	17309387	106937.139	95217.8761	146753	156971.16	87929.764	152169	150278.81	191307.25	
205.07813	3496777.5	6876086.696	-970339.97	4973739.9	16332032	-2792935	2067078	18604167	157584.973	115062.322	199825.804	194323.299	124239.07	224911.47	159999.24	211371.41	
214.84375	249823.9	620820.166	-982422.8	6200304	16457788	-2836342	2528909	18916458	137446.158	161983.877	147523.072	215040.854	82624.955	159297.44	159486.2	168965.08	
224.60938	1764469	6091543.658	-10060317.2	5673970.3	17699163	-3142701	3123266	20025876	252617.678	142294.618	175606.064	136845.276	137126	157705.16	267760.56	174483.94	
234.375	2045847.8	594842.565	-11009043.7	6031346.7	19880058	-2936944	2134335	21301511	133753.258	126381.812	150013.894	156920.124	106982.97	116144.73	101038.78	154810.58	
244.14063	2411691	5065227.537	-1096163.3	7830890	20508559	-3103463	1857465	22213816	99944.5438	79269.2002	121245.317	120868.882	132457.43	153069.46	160742.17	159137.62	
253.90625	2677582.4	4672740.063	-1194966.4	9198262.3	21972358	-2422281	3272611	22959419	70740.3285	80100.5119	77512.834	69660.8398	103256.84	14731.744	113631.61	149758.14	
263.67188	2764949.9	4671828.427	-12032353.9	11019654	23108100	-2243503	3884291	23881775	77084.476	66518.8366	63364.7399	67622.7957	83141.922	91664.978	57259.954	112559.41	
273.4375	2449447.8	3926573.605	-13607434.3	14184566	22716726	-920664.1	4931810	23514292	54905.3574	115999.891	108876.723	110039.833	46354.722	80541.164	89850.506	151001.63	
283.20313	5499878.1	5927581.81	-10138614.3	13168454	26759295	-1530960	5722274	19762418	94333.8109	90724.7198	90110.3929	105764.838	67627.801	99355.454	78845.734	112728.94	
292.96875	2149780.6	4691798.212	-10142289	11883927	28321767	-1832279	5673389	20412824	70783.8709	101913.664	75468.6715	89304.6469	74327.302	79452.311	80158.384	146276.16	
302.73438	1936579.3	6359546.756	-10509663.1	12462470	31414690	-474133	5749919	19048008	42556.6029	81623.1678	80797.7173	94910.0534	63462.417	85895.533	93936.358	104158.71	
312.5	429092.2	5540378.963	-9510685.04	11502237	33909921	-1741188	4075953	19638708	83600.9486	84978.1999	83213.7251	90229.7354	65841.684	80200.375	37855.855	104928.37	
322.26563	7115069.5	5572779.406	-10419265.7	9955931.1	33762450	-1046778	522775	21905906	60783.2482	81491.6047	59988.5754	72056.7441	64446.965	83586.512	88012.341	101635.24	
332.03125	5577370	4986873.128	-13626283.3	4393819.3	33389196	-1435925	-2852311	17903525	120597.609	99941.7704	153900.033	135042.451	106170.41	118227.32	127446.32	192289.97	
341.79688	8209704.1	3565503.265	-15344835	-1721494	31188570	-2828540	-14010623	17452007	307908.565	354362.481	458187.155	565430.424	277676.53	268469.4	616273.64	601400.27	

Table 16 Test condition: Med Preswirl-15 krpm-25% Pressure Ratio-100% GVF

1100 Freq Hz	Test Data									Uncertainties							
	Re Hxx	Re Hxy	Re Hyx	Re Hyy	Im Hxx	Im Hxy	Im Hyx	Im Hyy	Re eHxx	Re eHxy	Re eHyx	Re eHyy	Im eHxx	Im eHxy	Im eHyx	Im eHyy	
9.765625	-3680809	8304928.54	-10432620.6	-3913467	698244.9	-38147.2	-540507.6	1048864	356836.717	173798.703	303415.041	180104.68	195389.37	224118.68	344225.72	187482.07	
19.53125	-3212071	8340207.038	-10322849	-3726143	2085119	-460865.1	-213257	2405685	151455.358	116571.107	161188.181	94829.7325	137383.26	140676.44	122077.26	170071.44	
29.296875	-4913680	9720952.941	-9315471.3	-5267073	3515175	-148346	3001609	3853664	102449.558	100208.239	134277.661	106985.707	111468.2	122575.57	96323.213	209647.72	
39.0625	-3264003	8433218.327	-10506622.2	-3342707	4541342	-290005.9	1071870	4779537	73226.6536	85110.9563	99886.2155	88394.9343	48287.542	112786.67	64389.052	135787.63	
48.828125	-3240426	8383907.34	-10359112.3	-3161599	5343021	-171657.9	871724.8	6034625	94000.1024	109823.93	76699.5324	115930.236	89500.967	105355.96	55064.075	131654.1	
58.59375	-2318172	8266755.488	-1071662.5	-2585929	6743736	-824649.3	878337.1	7389005	100807.108	94136.7573	144773.852	95858.8404	77560.447	111769.66	86513.413	91349.12	
68.359375	-2037333	7881684.401	-10980057.3	-1833922	7058814	-1012210	1069021	8563623	92710.0941	68532.2844	123013.909	125394.149	144756.53	132272.81	96820.46	137972.3	
78.125	-2097391	8135082.215	-10414620	-1263740	8258081	-679961.5	1329717	1413989	10294.755	98798.5907	66568.8535	105430.087	135407.72	153950.54	118432.96	117923.78	
87.890625	-1287644	8033224.204	-10951726.2	-786009.3	9384785	-1106182	1431429	1027796	59249.855	113045.427	72896.1397	91238.2906	72278.411	88233.499	83634.737	116412.33	
97.65625	-1031777	8081688.45	-10398355.4	-577746.6	10153999	-1015063	1646309	11102646	70958.9108	93078.498	69314.112	109054.221	79188.425	102650.04	70614.624	101934.95	
107.42188	-315186.7	7818025.698	-10380683.2	-320187.8	10622827	-811592.1	1520419	11553429	100434.428	107012.919	145618.891	135652.76	108931.58	125843.34	91856.827	105386.19	
117.1875	-226762.1	8192456.383	-10248869.1	258595.43	10343255	-336394.3	2921532	11936031	90256.0826	115105.662	91742.8415	89966.3035	111699.29	119511.77	134111.69	132518.49	
126.95313	855501.52	7578177.207	-10976654.2	1535230.8	12838041	-1730133	1691367	13712009	70674.7209	107961.897	111316.77	82321.4618	147419.42	91751.463	112576.7	134940.68	
136.71875	682666.75	9234593.933	-10196020.2	-274478.5	12848448	-1466335	2882228	14459335	117491.196	91663.0534	113130.762	93424.2748	93165.318	140123.15	92251.977	168039.27</	

Table 18 Test condition: Med Preswirl-20 krpm-25% Pressure Ratio-100% GVF

1200 Freq Hz	Test Data										Uncertainties							
	Re Hxx	Re Hxy	Re Hxz	Re Hyy	Im Hxx	Im Hxy	Im Hxz	Im Hyy	Re eHxx	Re eHxy	Re eHxz	Re eHyy	Im eHxx	Im eHxy	Im eHxz	Im eHyy		
9.765625	-3817864	9840832.049	-13687701	-4162420	966852.1	135933.8	-575590	2104616	329203.496	277577.377	400453.645	275753.512	249941.89	231862.63	359092.18	342192.24		
19.53125	-2804679	10083099.29	-12473054.8	-3487302	2390000	-770220.8	839784.6	2650886	89545.726	128712.467	152789.348	157457.536	102760.9	125332.17	118912.38	194962.18		
29.296875	-2892529	9605211.653	-12838620.3	-3259561	4893621	-1298820	-766746.1	5168307	178347.784	217861.241	150288.407	161851.948	150814.63	174049.96	172575.78	187735.17		
39.0625	-2591010	10198384.83	-12489725.4	-2992089	4812362	-1106026	1415565	5096599	91836.5642	148962.762	93460.1763	144079.555	143017.81	108500.51	100696.26	107732.49		
48.828125	-2543498	9732713.24	-12109385.7	-2897686	5529869	-927010.9	1412392	6228716	84286.9364	78264.4731	107887.091	114819.07	53804.677	94919.501	127702.44	131585.85		
58.59375	-1859222	9631341.623	-12346029.2	-2336900	6527358	-1524328	1490004	7949763	126223.1	141278.564	160811.773	108606.156	133313.67	114786.79	107167.93	120395.91		
68.359375	-1544929	951262.839	-12596501	-1600741	7885075	-1269163	1724936	8696078	117013.832	119587.321	113875.32	89838.1019	69920.966	137447.51	86436.029	146389.82		
78.125	-1487526	9300332.837	-12209219.5	-1157351	8631605	-1565337	1955276	9413963	100561.735	113684.648	166807.644	107706.681	88607.707	128186.82	79126.534	105476.45		
87.890625	-909311.9	9377053.752	-12063056.5	-766599.9	9445737	-1604806	2153092	10562315	65866.9458	91221.4357	88659.8515	104720.243	45452.679	89006.615	56262.012	113142.86		
97.65625	-317349.2	9220431.53	-11938573.1	-2017138	10748522	-1765619	2150973	11271656	61491.4894	144665.021	79409.2022	86159.9294	134092.82	127241.45	88377.643	128062.14		
107.42188	464724.83	8910286.877	-11834629.7	368681.21	11247477	-1674408	2801826	12327502	72231.9417	116374.911	125856.91	131342.263	83691.155	102151.58	132377.14	172418.48		
117.1875	146307.41	9066792.136	-11721985.6	953867.78	10443801	-893674.1	4127949	12836637	84436.8244	123058.501	94605.5158	122608.244	88944.154	107917.24	93280.47	131868.14		
126.95313	1214593.5	8916359.534	-11865948.7	2030101.6	14453375	-2689075	1543371	14668806	111163.078	106147.533	53048.726	114283.318	84289.244	18194.99	91107.702	106394.47		
136.71875	1407091.3	9777053.053	-11549286.1	1106131.2	13167229	-2287634	3834709	15581344	104875.037	86434.9237	101156.218	75787.292	101156.218	75787.292	101156.218	101156.218		
146.48438	2641763.2	8979907.951	-12050108.7	3207543.7	14512280	-2379122	3016865	16313472	88615.8098	121736.173	109793.29	156399.809	89188.488	130560.8	143599.66	159857.73		
156.25	810938.94	9817374.383	-10546445	2811874.6	14225706	-1900389	3815464	16801027	116675.834	88282.4798	138732.451	68602.154	136387.03	117938.71	143062.48	143062.48		
166.01663	1719876.4	9981620.758	-10547147	4581156.4	17108950	-5185463	19674896	25149257	108024.6791	88871.2048	125517.51	149898.881	70663.377	145688.96	16282.99	199268.3		
175.78125	539331.96	1133197.78	-6726648.32	-1063706	15327588	-1136966	6321810	15616052	10921.225	169113.525	184995.97	177604.399	139983.39	124186.59	132499.18	236887.8		
185.54688	3222310.6	8987447.864	-10773357.9	5357036.9	16678161	-2273385	4332530	19352115	170009.885	148335.849	201822.652	112878.88	167521.42	141737.79	159081.69	212224.11		
195.3125	453933.5	8937287.551	-11192663.6	6347688.1	17351807	-4101763	3575032	19561197	108662.381	176475.996	198460.153	131061.297	156207.33	171569.5	114557.74	208911.67		
205.07813	4910280.9	8653120.407	-11067890.7	7253939.4	17162516	-3867303	4361574	19795966	178370.524	127717.981	219457.692	175350.31	116817	174177.06	221748.81	160480.57		
214.84375	4145345.2	7962848.849	-11691667.8	8118222.1	17509994	-4330310	4365334	20970507	122888.427	178418.678	179330.56	140713.771	150158.47	161312.38	154518.09	243156.1		
224.60938	2487058.6	7233571.432	-11777110.4	8083770.7	18290599	-3974751	4948413	22457443	17950.521	121364.292	271816.121	181638.845	110800.26	118264.85	258110.44	253191.01		
234.375	3219929.3	7912846.816	-10946955.8	9390977.9	20917186	-3401840	5102511	23383410	192742.396	177160.332	150021.789	207873.66	144615.33	137503.59	167778.58	190827.94		
244.14063	3699672	6960153.097	-11230892.9	12245497	22254492	-3203282	4775340	24120017	147663.354	162306.628	235934.099	109038.392	119628.32	103096.51	106491.91	153788.77		
253.90625	4388871	6930227.629	-11832999.9	13792543	23577167	-2813049	4569794	23548271	144646.117	110175.221	139937.407	58810.7439	98777.024	89973.338	183104.28	131237.06		
263.67188	5091444.2	7617151.993	-12045888.3	15719395	24778404	-3076198	4685430	23163955	109252.969	86693.7869	106925.563	113299.654	79610.252	97512.415	75254.693	112182.59		
273.4375	4741405.9	8452079.827	-13808307.8	17539599	24516358	-2623059	5908809	20683601	56402.5751	161242.86	48783.5988	138674.538	85865.974	127308.84	87747.247	165984.7		
283.20313	4087359.2	9325934.192	-10755870.7	14440410	27882420	-5403343	7553773	18672869	71501.6829	119045.75	95734.4851	107818.057	109759.56	92275.531	132121.12	112781.98		
292.96875	5796237.7	5835429.36	-9981748.45	14356073	27429362	-5551518	1114319	2010334	87738.1019	91324.079	78713.668	89885.5757	71631.457	91185.614	91480.18	133523.02		
302.73438	5381153.2	7336581.188	-10210159.5	12507880	28782589	-6550906	2553777	16570645	66428.9133	83661.7111	87704.5385	104298.315	74964.801	75415.998	92993.535	100117.87		
312.5	4674098.4	4327806.847	-14738801.2	8203513.6	30728755	-6025798	-2580681	18478743	60193.2611	104470.759	76430.0193	80818.7185	85999.765	90439.293	113204.74	110490.69		
322.26563	3739607.8	2490374.698	-21091750.7	5777575.8	31550757	-5251704	-1693211	22204533	82934.8376	84477.163	98989.2431	60933.951	81332.43	130589.79	135715.03	135715.03		
332.03125	-3613463	-4605227.08	-29210759.5	-44348.15	35634716	-1089893	2650976	27334017	1045327.76	1177766.91	430642.295	739067.965	851873.83	1298979.8	581734.4	683322.98		
341.79688	-10598534	-16085985.7	-38903172.6	-12041046	25968916	-2171968	-9464255	26973478	336382.42	381759.524	200096.218	216777.611	272471.31	264401.84	138609.11	180450.26		

Table 19 Test condition: Med Preswirl-10 krpm-50% Pressure Ratio-100% GVF

1020 Freq Hz	Test Data										Uncertainties							
	Re Hxx	Re Hxy	Re Hxz	Re Hyy	Im Hxx	Im Hxy	Im Hxz	Im Hyy	Re eHxx	Re eHxy	Re eHxz	Re eHyy	Im eHxx	Im eHxy	Im eHxz	Im eHyy		
9.765625	925316.11	6666517.696	-7588715.52	-1202731	466630.3	-1080414	-956890.6	1014267	1298237.41	1038607.68	1037510.97	971209.267	1092313.3	1293276.8	1044087.6	1019785.2		
19.53125	6713.6187	6810946.67	-8595583.65	-379676.3	1737845	-190783.7	44262.33	2197775	77987.3772	98959.1208	114027.771	143740.125	104286.94	109240.52	83943.708	109775.17		
29.296875	-302124.2	7479902.451	-7717514.56	-489833.1	2572124	-4085.745	713903.8	2348989	107645.979	198965.376	185564.199	143033.378	163077.76	176569.14	198699.53	153987.02		
39.0625	247426.5	7111988.539	-8701368.28	-9276.069	3353318	-177356.5	262568.3	3998667	91629.6177	115231.423	204752.87	126885.18	81596.402	93097.213	93097.213	93097.213		
48.828125	167685.33	7016298.523	-8335686.27	59495.208	4649627	-479007.8	312600.3	4733779	121309.318	130466.484	150307.073	136474.339	85058.414	136692.58	110950.32	117734.62		
58.59375	304746.66	6511636.67	-8546981.88	-23438.79	4990168	-630357.7	280526.1	5971308	106709.473	77455.7045	106682.689	109544.721	128994.69	143009.97	119082.82	139999.61		
68.359375	401943.92	6688643.583	-8284212.46	349846.1	6062795	-216143	580309.2	7029935	121342.16	112929.217	78304.611	93094.9405	85596.548	125113.71	110235.65	102018.3		
78.125	565942.5	6857646.363	-7949537.71	1167109.2	6887679	-495765.7	570845.3	7620974	66248.3554	145960.537	79965.5471	123211.523	83593.747	142840.59	127668.67	139124.08		
87.890625	793340.9	6923628.237	-8096758.04	1326709.5	7899475	-795424.9	432923.1	8824694	96646.3091	109571.912	86533.0754	76011.0714	92127.928	87418.956	144944.86	123485.8		
97.65625	104223.7	6752408.213	-8201193.99	1549419.4	9076931	-627042.2	378487.6	9552725	125094.516	139806.772	66248.3879	135416.83	79195.443	130680.18	103678.81	111555.03		
107.42188	1340078.2	6688243.255	-8494699.05	1558062.9	9670197	-819605.3	423442.5	10510894	123625.14	147240.855	123337.224	66177.9048	98856.908	123375.1	106843.58	146381.47		
117.1875	815045.02	7151098.252	-8007079.3	1571495.6	9093778	-532528.2	1573407	10334633	97327.1104	95235.3446	115853.906	85648.9563	79809.086	125816.19	75899.504	118330.72		
126.95313	2263091.6	6653105.988	-8765177.57	2850713.3	11651060	-1265885	3939766.9	11973737	95222.7362	140746.824	71789.4674	142854.022	98114.506	142671.12	89152.911	123356.55		
136.71875	1766937.9	7673822.292	-8333116.52	1346945.9	11447611	-160021.9	2046110	11779693	76885.0864	109940.819	114344.712	131256.943	8					

Table 20 Test condition: Med Preswirl-15 krpm-50% Pressure Ratio-100% GVF

1120 Freq Hz	Test Data										Uncertainties							
	Re Hxx	Re Hxy	Re Hyx	Re Hyy	Im Hxx	Im Hxy	Im Hyx	Im Hyy	Re eHxx	Re eHxy	Re eHyx	Re eHyy	Im eHxx	Im eHxy	Im eHyx	Im eHyy		
9.765625	982470.46	7223800.258	-8960438.23	-563991.7	-295207.6	-839486.4	-2426652	826067.8	583968.767	252383.147	539249.814	262582.504	475870.33	321105.41	478918.36	301001.94		
19.53125	5481.9598	7729207.796	-9238796.72	442986.66	2009286	-472783.2	266821.5	2166437	92763.1743	117435.857	109007.985	174764.45	114375.88	153588.05	104550.15	110996.03		
29.296875	-497121.5	8331371.913	-8574140.03	179815.71	3402823	-43271.36	-146993	2552067	149899.998	184896.099	167600.347	126181.207	92196.795	107136.52	201307.83	167838.71		
39.0625	186023.13	7635667.464	-9383742.38	882470.98	3720946	-525065	584733.7	4051772	94171.62	89023.0498	85551.1979	114106.341	98647.065	111084.66	137467.67	100371.94		
48.828125	149886.66	7802210.571	-9041437.81	1020583.6	4405563	-620713.8	357273.9	5025246	85227.826	81457.1926	53952.9076	98063.5746	51804.405	123484.79	94836.39	95312.227		
58.59375	297288.23	7336907.821	-8986362.71	1218589.2	5321517	-56211.4	763603.2	5733741	121409.758	131469.59	95315.4671	100431.789	116276.76	110834.63	117134.47	153952.27		
68.359375	660882.52	7573483.691	-8681974.14	1528956.4	6363996	-518681.9	852764.6	6992633	98537.5913	100376.799	82492.8763	104787.851	120892.47	96433.315	119506.69	116281.78		
78.125	595340.53	7323579.991	-8744430.09	1932473.8	6988399	-796823.9	851646.5	7665655	62403.809	90240.1718	123269.125	105550.101	90552.408	136860.65	78388.484	157622.79		
87.890625	991635.15	7443627.237	-887510.11	2038189.7	7909485	-1016267	682559.8	8776398	55975.8389	136337.294	121402.397	119305.849	76342.219	101440.67	56879.633	104009.26		
97.65625	1226017.7	7267473.145	-8988214.68	2278470.3	8910969	-1066204	607588	9620353	59500.3447	121209.513	69432.5498	81887.942	74720.899	134180.89	60197.826	95813.938		
107.42188	1416678.1	7184705.646	-9366734.05	2442193.6	9670404	-1112168	507172.7	10689868	168255.755	123314.498	138359.076	90311.9607	127406.59	107962.53	107022.58	95169.439		
117.1875	1428550.5	7239327.486	-9091727.98	3087066.8	10262858	-459103.1	1043653	10517974	132134.82	110408.76	115899.211	135025.73	119999.48	121409.54	125872.56	109454.93		
126.95313	2123017.4	7350369.194	-9379997.44	3663415.7	11431867	-813861.7	1178039	11622898	73697.0452	79900.1491	66856.3872	106747.862	89756.435	129065.27	89900.206	143300.1		
136.71875	2260512.2	8093775.835	-9122933.1	2368696.9	11165676	-341032	2487564	11470890	80769.5413	120211.29	72516.0627	80722.893	84603.759	93104.508	57740.185	111779.17		
146.48438	3081211.1	7780132.698	-9088313.34	3275075.6	12258872	-2130496	895129.9	14945800	85757.6477	114141.38	143836.124	132086.265	102441.01	114573.5	80450.1	158912.94		
156.25	1876412.1	8022510.496	-9106352.79	4223780.2	12456792	-1198089	1417806	14175713	98643.4712	64245.6083	103707.808	119608.215	72072.435	128276.12	128226.77	144649.14		
166.01563	3655072	7500990.629	-9991533.28	5461391.4	15828648	-1942350	1102869	15911754	126701.425	147815.933	148277.761	143269.589	90152.334	213689.58	83096.755	105750.56		
175.78125	1156905	14204203.4	-1126821.24	-5786212	14064652	-131094.7	3811787	136911616	163510.626	209224.606	147899.86	163242.847	122713.97	135678.78	12026.59	187568.01		
185.54688	3527020.3	7758607.723	-9727600.08	6400619.5	15632925	-1698209	2654020	17614345	132601.905	170728.952	200445.71	137803.053	160748.14	143352.93	148957.21	169664.76		
195.3125	4122220.2	7560968.93	-9534133.01	6276818.3	16527578	-3128284	1198052	17732412	163413.342	147079.129	116779.765	117583.52	135062.22	194689.02	118209.67	123431.68		
205.07813	4795297.2	7357180.177	-982795.52	6621849.2	16229189	-3153786	2064037	18801013	114783.106	185460.852	148327.323	111113.049	189150.95	180339.36	129703.45	222774.97		
214.84375	3817668.9	6839603.189	-9685416.57	7544355.2	16283582	-3344083	1689287	19548909	154266.319	219972.651	191343.005	157764.948	151878.62	184180.89	106367.91	201997.84		
224.60938	2581486.1	6113854.883	-10163314	6989928.4	17991826	-3647319	5548489	20139201	182426.388	128390.095	155342.993	108020.648	198721.12	128369.13	184595.5	144979.13		
234.375	3140789.2	5537635.172	-10993242.6	7479002.7	19586155	-2588355	982353.3	21466502	169485.168	185693.172	169539.721	221150.629	139693.82	214797.09	249414.15	137926.59		
244.14063	3561758.2	5069034.306	-10993767	8727568.6	20706017	-2432355	1221021	22176146	160992.546	132678.259	175018.127	146076.715	113701.21	122996.61	131894.51	173754.96		
253.90625	2918584.2	4662944.326	-11897114.6	9561037.7	21797668	-1537455	2160218	23490515	74287.4801	108139.51	138519.323	131607.481	143235.76	141295.31	170621.73	122410.23		
263.67188	3277273.8	4795910.282	-12521616.9	11905094	22897603	-1457263	2366572	24365262	105037.962	92997.1907	151409.151	104553.83	118064.56	107948.13	126213.7	115130.57		
273.4375	3285805	4371291.67	-14745654.3	14862428	22964215	-221301.9	3294617	23072083	63763.4361	120009.298	59807.3304	90931.7571	90401.197	94859.987	89777.956	134850.2		
283.20313	1332499.5	6773771.286	-11450522	12124615	26083019	-703747.7	5962851	19897703	78420.8424	110996.226	72818.9443	118301.533	72150.663	88665.227	92880.284	103425.86		
292.96875	3009980.2	5098179.498	-11836077.6	10790901	27655680	-1400093	3976340	17182303	67545.8482	73521.1097	79438.5832	90176.742	85804.143	91258.68	66600.77	113231.01		
302.73438	2062128.3	6769364.564	-13074005	10337783	29757490	-645921.5	3771595	20378247	88970.2457	70423.8536	63957.0679	75620.1421	65918.891	109564.2	71728.616	86118.888		
312.5	3777042.9	4992991.087	-13115444.2	9057953.5	33443703	-560355.2	2883863	23031155	197675.467	126989.241	66996.5539	102290.884	90787.274	71531.988	115629.58	90444.32		
322.26563	7003190.9	5402237.677	-15796119.5	6770939.1	33610474	-1607356	865359	25556835	93763.8676	68816.271	101979.911	78695.3348	72199.317	77697.725	62285.752	93748.098		
332.03125	4200774.9	4065287.453	-22087178	247048.69	32882866	-2524212	1173506	20661802	98952.002	97695.0129	77809.5695	91408.195	108347.84	108353.03	111792.72	114580.18		
341.79688	3882396.7	4106743.065	-23736751.4	-7577229	31308557	1980491	-7354409	26836966	122731.63	147727.131	137088.939	144246.047	149392.08	125916.77	162585.13	175955.05		

Table 21 Test condition: Med Preswirl-20 krpm-50% Pressure Ratio-100% GVF

1120 Freq Hz	Test Data										Uncertainties							
	Re Hxx	Re Hxy	Re Hyx	Re Hyy	Im Hxx	Im Hxy	Im Hyx	Im Hyy	Re eHxx	Re eHxy	Re eHyx	Re eHyy	Im eHxx	Im eHxy	Im eHyx	Im eHyy		
9.765625	-1846720	6303558.913	-9641656.98	2737233.4	-840659	1305234	1718057	1649666.9	542672.537	1213878.45	638955.097	1137328.23	1144065.1	625108.25	1125306.3	712279.33		
19.53125	630461.72	8843337.256	-10494049.7	823958.4	2056422	-267691	353357.6	1985906	100060.051	153460.292	83451.5227	106639.489	79376.627	112637.06	68771.441	122650.83		
29.296875	-3763577	9948212.394	-9669345.28	-393075.5	2952364	-114854.4	315082.1	3222122	147336.553	142385.564	129031.925	127434.703	148457.28	111677.08	124453.53	127252.34		
39.0625	520871.8	9230832.11	-10593978.6	927724.79	4105913	-146824.6	761648.2	4131722	81699.9747	115582.265	93743.3982	93404.2204	142649.98	117252.56	103051.61	107198.18		
48.828125	675412.12	8985705.443	-10259842.5	1178355.3	4857256	-505225.4	868895.6	5048841	83110.7058	98039.719	71835.3461	71729.2256	76087.287	153814.32	56021.866	80662.661		
58.59375	988192.18	882832.343	-10557677.3	1260329.1	5584935	-590608.2	776594.1	5897673	1112080.019	90149.7458	84042.222	128276.304	103484.63	122153.16	49729.988	106625.03		
68.359375	1419258	9309598.972	-10303559.3	1319106.1	6480011	-617465.5	1169768	7437818	83143.781	102481.623	104060.688	112245.95	56827.263	134380.74	97177.492	113305.22		
78.125	1242428.9	8968013.166	-9824226.97	2276175.2	7310525	-1142692	1156719	7990081	89335.6226	98670.7666	111286.43	119333.971	54570.106	90275.84	92657.851	99290.703		
87.890625	1884666.9	9125409.652	-10187471.3	2255486.4	8265124	-1157357	1135944	8964558	65755.8001	92777.3253	83133.6083	78473.0981	50036.079	96589.819	56977.428	108200.05		
97.65625	218946.9	8837020.363	-10192938	2696932.4	9205903	-1317570	1411199	9730920	77903.1956	118947.436	124448.476	102209.809	126778.86	122548.06	91387.726	155285.83		
107.42188	2786529.5	6886866.275	-10534441.9	2943354.7	9678566	-1281336	1648086	10806567	123265.725	92841.6217	74150.8331	93978.4021	84806.512	114476.41	95055.343	156894.18		
117.1875	260538	8551902.711	-10411442.7	3427610.1	9336967	-418577.9	2529828	10780102	80346.2623	108265.72	156252.9	109021.379	78904.577	101385.68	104878.43	119360.77		
126.95313	3789323.1	8296087.728	-11076572.2	4811065.4	11706240	-1941913	1675516	12590614	76736.8168	166189.901	93619.747	108600.292	79705.199	110759.1	81851.844	175639.28		
136.71875	3687253.7	9102660.022	-10397570.5	3308024.2	11666736	-1354623	2561612	12866174	84716.2403	85159.9122								

Table 22 Test condition: Med Preswirl-10 krpm-65% Pressure Ratio-100% GVF

1030 Freq Hz	Test Data										Uncertainties							
	Re Hxx	Re Hxy	Re Hxz	Re Hyy	Im Hxx	Im Hxy	Im Hxz	Im Hyy	Re eHxx	Re eHxy	Re eHxz	Re eHyy	Im eHxx	Im eHxy	Im eHxz	Im eHyy		
9.765625	661949.93	5273601.31	-6900211.73	482376.51	722529.8	-38306.98	-51646.45	1211631	134182.342	115239.837	132720.478	114912.729	110934.88	162432.28	131825.8	147195.25		
19.53125	655002.42	5494280.597	-6229431.66	771839.15	1758327	-170112.9	97014.64	1934205	68522.4169	95948.6302	94447.2875	126681.876	66737.377	98317.712	52481.29	113981.54		
29.296875	-395784	6363345.001	-5010316.67	-412203.1	1180253	1322805	1624605	1042582	106740.046	89768.3009	121328.439	68622.2748	93676.273	97696.106	78435.065	93406.593		
39.0625	1070593.2	5162080.653	-6507306.54	937808.77	3214972	-430774.2	139432.1	3792502	55174.4282	93783.2719	89995.0002	95356.9739	70837.548	147385.22	80903.016	131932.08		
48.828125	912233.85	4969511.195	-6531463.03	997116.74	3785469	-155137.6	4188.634	4464111	55160.221	88177.8038	67041.7594	102757.695	47946.418	77771.328	55086.843	105778.86		
58.59375	1032708.7	5101047.587	-6533635.75	1259715.5	4652572	-88429.24	36017.3	5091879	42363.3617	75307.9839	76626.2828	78878.3785	95213.641	78662.276	108780.65	124959.5		
68.359375	1237768.5	5037186.781	-6325063.98	1215322.5	5602285	40823.68	351248.2	6399507	119426.986	115670.037	99239.9544	84710.1835	78629.269	125883.09	86745.502	130503.56		
78.125	1318264.1	5051573.458	-6376707.3	1700560.9	6255701	-437021.1	210369	6866317	76175.3599	86873.4163	42686.2593	86001.7144	89534.112	99027.82	107177.34	127431.28		
87.890625	1437602.8	5114402.399	-6616702.82	1805954.1	6884512	-346202.1	228721.1	7864009	74492.1656	95723.3347	59101.6795	66865.6386	45537.866	108548.94	56664.925	104123.23		
97.65625	1527515.6	5093779.821	-6625414.4	1706315.3	7921261	-228420.1	-113482.6	8272179	48827.1153	65117.6525	78150.0933	118089.392	86476.631	96654.709	107420.36	88968.826		
107.42188	1759793.5	4782152.495	-6680282.3	1980216.8	8348801	128136.9	252061.4	8932504	72506.9787	95012.3033	112310.679	137923.66	75017.822	85212.499	147120.38	88561.006		
117.1875	1479857	5493300.947	-6465300.8	1636164.4	7934056	1157322	1424295	8971985	52706.6615	76152.8407	91473.8582	77132.0923	60942.682	108205.01	85848.418	105327.29		
126.95313	2063901.4	4981990.128	-7150183.42	2770278.5	11621157	-1670049	-1204889	11912834	58909.9105	123138.229	73707.3642	136418.013	70438.095	93633.639	76709.39	112807.61		
136.71875	1940845.6	5897625.471	-6428164.2	1144773.2	9624526	741720.3	1794078	10084163	84356.0297	92089.7463	67133.2868	128766.817	42016.299	121316.91	87953.421	154373.1		
146.48438	2078534.4	5489000.206	-6119168.3	1733310.5	11290661	-967823.4	-397769.1	14536443	44650.6555	114911.557	104247.552	112955.181	80185.856	96915.136	111766.27	138898.64		
156.25	737339.66	6095226.707	-654213.41	2508986.3	10849894	433992.4	902495.2	13106881	73806.7794	135987.503	91265.7678	159782.49	96012.29	150095.73	61288.564	143337.04		
166.01653	1914777.8	5065155.862	-7052778.76	3667611.3	1253514.1	-533413.1	240628.9	14057019	192827.441	294084.304	281852.963	330766.456	182133.066	270154.49	273829.72	470187.41		
175.78125	1315704	10464511.27	-1170014.23	-5061856	12059998	1333144	3054101	24202266	154669.944	193263.149	235682.58	270814.377	150337.56	203234.69	158402.38	246313.33		
185.54688	4386811.3	3551969.75	-9918461.51	8292951.6	14667411	-1442570	412112.9	17992167	103148.491	134048.085	139993.762	259304.123	198854.74	137634.84	240602.22	163082.51		
195.3125	2894803.6	5913361.838	-7171917.69	411867.5	14731830	-1407560	395683.3	16191507	70296.6083	103657.353	75749.1326	135190.915	66808.054	125849.53	105546.62	120344.16		
205.07813	3073840.6	5757795.962	-6976338.1	3653508.5	14787381	-1049304	750113.1	17208317	127166.045	118234.218	122196.993	114625.191	84709.373	150699.96	102510.72	128662.74		
214.84375	2095703.6	4909280.96	-7007614.49	4106514.8	14620505	-1547912	142679.4	17956683	82888.2114	87099.8065	84868.8362	162386.672	76195.434	149117.63	78385.943	131630.62		
224.60938	953331.75	5025359.9	-7046291.19	3687205.9	16016292	-1426441	1424062	19019280	117210.443	136279.941	111060.102	92185.0124	111467.26	115815.5	125414.93	134043.15		
234.375	1156927.4	4912840.753	-8133142.82	2950894.3	17764942	-930372.9	-352571.7	20641498	110959.569	117363.131	82870.5537	116920.654	66940.397	157982.26	83761.959	163422.32		
244.14063	1226649.1	4084397.163	-8739405.74	5037760	18881833	-862892.6	-150455.6	21960449	93898.7363	156477.831	99636.7499	153716.121	117309.83	116261.8	112047.78	121461.46		
253.90625	1417819.6	3841998.187	-9527932.81	5605845.9	20759613	-683259.2	11392.88	23177580	6713.2727	104980.481	68128.7052	58429.0583	76432.416	102615.89	39547.814	92130.817		
263.67188	2020967.5	3940910.009	-835808.3	7470989.9	21701671	-453787	691901.5	24414908	73965.2145	75364.3653	89384.5181	85234.0283	62179.675	89779.283	84019.257	109544.04		
273.4375	1990670.4	3491746.293	-11092551.3	9603028.6	21607522	684571.8	1266260	24009085	55391.5161	110726.664	57290.9978	134041.021	40499.485	103996.52	60924.148	142467.09		
283.20313	4830580.04	55245153.806	-9919893.12	8488281.7	23855946	738809.5	3570197	24114734	56501.8253	68157.1525	63302.6963	102299.105	38321.358	89205.571	43792.672	98114.386		
292.96875	1464808.6	5531055.876	-9464111.61	7085059.7	25903602	91927.11	2587289	22618124	35820.2669	76404.8761	44385.7393	65525.3398	57352.206	100431.33	81082.818	94988.212		
302.73438	1756192	7679202.496	-10196111.1	7532319.6	28556035	1537522	2636399	22372716	36272.6882	81424.3471	63846.5667	93102.304	66971.715	84942.859	63001.753	111825.09		
312.5	5186540.5	6409903.918	-9713137.5	5975586.2	31059100	-390609.2	1241951	22508978	62380.9191	76615.8679	57740.8784	91424.964	51531.932	80297.349	55829.521	109804.18		
322.26563	8695516.4	7624056.479	-10241439.9	4762340.4	30568488	480803.9	-136016	22554835	48499.6873	77391.5843	55966.8174	80413.923	64624.475	86319.367	61401.853	84781.61		
332.03125	9368493.8	8317592.682	-1138017.3	599044.8	27235725	-2730569	-4329840	20363637	99805.9456	110466.052	149252.541	225397.764	98713.104	147561.16	170616.35	164072.65		
341.79688	10845573	7438103.647	-10801874.7	-5906122	22272215	-5175591	-18164357	15321596	320002.934	260853.328	498007.912	804162.781	320933.73	448540.35	624997.09	520481.31		

Table 23 Test condition: Med Preswirl-15 krpm-65% Pressure Ratio-100% GVF

1130 Freq Hz	Test Data										Uncertainties							
	Re Hxx	Re Hxy	Re Hxz	Re Hyy	Im Hxx	Im Hxy	Im Hxz	Im Hyy	Re eHxx	Re eHxy	Re eHxz	Re eHyy	Im eHxx	Im eHxy	Im eHxz	Im eHyy		
9.765625	511210	6264058.194	-7605128.8	485939.76	1053876	186931.7	-338930.2	1045210	84882.1972	149798.006	174716.144	152909.212	144855.22	104906.09	272125.81			
19.53125	693526.06	5973466.941	-7375387.92	1080201	1538456	-138882.8	166194.9	1790990	57135.788	100214.776	53945.8808	94102.3196	44789.782	126654.63	50828.892	87850.157		
29.296875	-57894.98	7266621.354	-6151904.64	-251940.7	1356789	1324967	1809573	923684.5	70676.2951	89992.6476	69705.3054	106716.367	126408.24	101609.86	70626.55	117576.19		
39.0625	1032627.7	6150840.7	-7373050.27	1159539.3	3377866	-278155.9	287883.8	3584637	56167.0053	105950.417	57556.0125	74639.5744	68584.257	120388.79	80913.993	101057.27		
48.828125	877211.23	6084084.574	-7653050.56	1244336.5	4307209	-255131.6	166998.6	4672273	76370.962	98087.932	75552.7452	50272.888	6950.377	105391.53	79035.994	89040.525		
58.59375	1143320.4	5908801.419	-7879088.46	1366111.5	5113257	-320022.2	267326.1	5492447	59340.3889	112043.315	67482.7745	89682.8067	65410.439	115327.18	126445.32	111187.59		
68.359375	1138594.3	6096712.322	-7510333.45	1370935	5698457	-111892.4	745301.9	6370976	72729.4573	114847.189	83724.9515	72462.6508	77656.905	95589.946	73192.016	107809.67		
78.125	1297835.6	6065556.649	-7571055.57	2147462.9	6415544	-500959.5	301364.5	7142276	55594.087	85818.4164	65674.4314	48561.9339	50337.589	98720.549	71997.893	109298.27		
87.890625	1524000.6	5921247.437	-7522774.89	2028378.8	7229670	-496819.4	4461771.2	8025248	50131.7481	77288.2344	101128.965	104737.72	46053.884	118408.63	106759.17	135120.22		
97.65625	1652107	582219.408	-7600173.88	2281090.7	8445810	-273973.5	178828.4	8887617	52428.8912	80574.5335	120577.505	94524.1586	62582.721	102027.93	78258.828	117801.95		
107.42188	1669812	5590849.467	-7710348.75	2341810.4	8719264	-167469.9	486226.8	9676058	56406.3038	118465.994	157301.181	129744.289	88265.589	90268.13	146903.22	158167.08		
117.1875	1694041	6006491.834	-7566654.74	2675891.4	8122264	759250.5	1580579	9755255	96995.4586	132943.036	117040.191	133138.899	42735.846	79174.075	104003.48	134830.91		
126.95313	2830768.6	5388568.007	-8247061.63	3588855.3	10818142	-963884.1	156246.5	11522006	52882.9617	123159.446	88214.5754	111816.234	62751.042	90523.894	94682.51	142347.04		
136.71875	2056881.2	6616479.936	-7446510.17	1833866.4	10112566	563710.8	1975702	10615										

Table 24 Test condition: Med Preswirl-20 krpm-65% Pressure Ratio-100% GVF

1230	Test Data										Uncertainties							
	Re Hxx	Re Hxy	Re Hxz	Re Hyy	Im Hxx	Im Hxy	Im Hxz	Im Hyy	Re eHxx	Re eHxy	Re eHxz	Re eHyy	Im eHxx	Im eHxy	Im eHxz	Im eHyy		
9.765625	489762.62	7559296.315	-8957628.83	501388.29	1354194	74884.99	-401667.1	1236251	157537.204	171049.672	217530.342	260576.336	177082.97	154051.34	242724.43	207486.87		
19.53125	820629.76	7646749.164	-8813569.96	1065352	1996896	-35547.31	425250.7	2106592	78562.0851	86424.7795	103132.67	134818.221	71136.885	76868.108	101246.44	130227.15		
29.296875	43701.228	8840513.835	-7415079.9	-425989.2	2833580	-96999.62	207984.5	2789407	88239.0807	103633.639	119493.97	77874.1854	130842.43	89349.128	99835.236	157045.9		
39.0625	1297003	7422973.73	-9001678.24	1239430.9	3608385	-171215.3	350427	4054294	90344.9544	86995.7463	84653.1407	102514.793	110132.64	90968.317	68700.358	100424.64		
48.828125	1355463.2	7610284.747	-8843102.45	1396108.9	4457936	-182225.8	50006.58	4967750	49667.4848	82444.8382	107386.725	95451.5156	72671.127	87090.785	100311.31	132515.97		
58.59375	1477448.9	7471841.485	-8755171.95	1620826.6	5277572	-161469.3	407276.2	5881756	81589.1313	86735.2072	62839.2213	115815.094	64060.678	102055.21	113457.59	102136.44		
68.359375	1705887.4	7662546.839	-8742195.02	1625340.8	6029695	-343506.5	747857.8	7071835	55201.2513	62605.643	89345.2629	69257.8062	78892.497	90550.617	44669.874	95567.149		
78.125	1667691.9	7714491.12	-8357255.65	2246400.1	6920718	-448551	665240.6	7544920	59819.5121	89101.7075	62534.6535	92241.4546	69799.676	100482.23	64014.094	107865.72		
87.890625	1687923.2	7618548.941	-8541380.51	2293413.8	7540582	-390218.1	503825.5	8570349	33689.4059	65479.6987	118304.318	76055.9163	39007.573	81647.617	92712.993	109247.9		
97.65625	1974864.1	7649454.97	-8614332.96	2680429.7	8572875	-679518.4	674983.8	9267834	48467.8097	112053.044	93496.8672	84038.7837	51025.031	111624.57	83119.864	135341.79		
107.42188	2460642.5	7407304.592	-9131517.99	2795852.5	9395712	-598680	560123	1067881	98609.1039	104920.149	139933.107	136579.768	74813.216	109737.45	136282.04	141710		
117.1875	2331244.8	7703283.226	-8758174.68	2930152.1	8999541	371260.6	1558465	10235990	106956.199	86598.7962	134559.514	96292.9856	84775.147	108957.31	61589.576	101052.54		
126.95313	3621419.2	7036851.457	-9345106	4367995.6	11569040	-1528926	621004.1	12418902	63088.1835	123249.923	80096.8666	62059.645	68793.225	122346.4	51866.995	146800.58		
136.71875	2935453.9	8134889.61	-850695.69	2422034.3	11350685	-577871.2	1455480	12395194	82525.7716	123579.968	103277.308	83111.6678	55629.507	108746.95	62365.429	143223.98		
146.48438	3979494.1	7348522.346	-9119963.24	4476309.5	12095523	-1115494	1716955.2	13872141	77927.8685	93860.5184	90260.5229	168917.706	72785.46	110034.36	94465.888	189743.66		
156.25	2199402.5	8253116.982	-8419669.61	4321979.4	12099594	-466112.6	1498871	14284732	6404.5641	105596.194	99194.7926	83653.2593	110862.91	115302.32	89418.299	127082.71		
166.01563	3531444.9	7195358.068	-9248718.92	5455232.1	13635989	-1225760	967688.9	15436678	73175.0958	152463.472	74162.6289	100042.685	61296.385	113696.51	86830.616	117599.39		
175.78125	733282.33	1366390.46	-2078167.94	-3479888	13984625	1125219	3766978	13488284	71915.7971	90184.3701	89800.1018	159890.781	74979.648	129760.01	63026.134	123124.59		
185.54688	527845.6	7156838.551	-10068647.7	7259064.6	14769350	-1260577	1814125	17744710	112828.851	154944.962	194976.343	187699.604	98704.305	149203.36	104169.28	219057.21		
195.3125	5171104.9	7710496.611	-9169629.93	6020965.2	15700123	-2279968	9839596	17332718	16670.2495	147842.241	115956.131	130663.043	78275.777	125928.44	122789.37	259200.22		
205.07813	5736120.8	7482210.902	-9703940.59	6381836.3	15472271	-2350252	1370061	19197630	113644.115	165446.936	183349.184	129353.133	118921.01	135163.15	119555.31	271016.63		
214.84375	5141213.9	6778909.638	-9519094.84	6905272	15433998	-2374253	1298459	1924364	45623.7995	99120.3325	50835.9876	120672.188	61301.185	107551.22	76806.127	106214.91		
224.60938	4048199.1	6760032.872	-9886204.82	6544436	16394638	-2273309	1410028	20934766	141067.486	246675.132	134053.448	102687.049	120696.69	99159.696	103140	146533.73		
234.375	5204180.2	5981276.676	-10551382.1	7903759.9	18129880	-2262716	509612	22095354	121146.878	112588.767	176278.665	147260.603	58779.681	198447.5	111705.18	311591.37		
244.14063	4855008.4	6058177.815	-11280058.1	9317088.7	18362272	-951278.4	1111869	23824644	112162.881	126854.127	85227.6048	110535.978	153589.49	175549.09	129519.97	128069.69		
253.96063	5552027.2	5946585.699	-12138894.1	10227770	19420478	-626581.4	1764716	22645608	78952.0199	114662.821	75845.6407	92910.2456	69190.623	115302.07	103130.59	159715.95		
263.67188	6099942.9	6357719.775	-12529124.6	12064964	20331731	-1005357	5192219	24003800	83171.5354	133176.764	99561.4969	110991.45	77309.343	108111.37	78840.77	919729.71		
273.4375	5430856.8	7477500.356	-13534003.8	13923195	19399749	-1118711	3789334	22011336	45623.7995	99120.3325	50835.9876	120672.188	61301.185	107551.22	76806.127	106214.91		
283.20313	4136967.3	10005298.2	-10971368.4	10838352	23004296	-1532502	5428835	20265378	73586.324	94705.8402	86441.4768	87356.9207	61381.894	114555.22	106039.74	144329.51		
292.96875	6538276.6	7864956.016	-10973705.2	10645338	23940308	-2061099	3774480	22688429	57377.7344	84402.4101	64579.0004	76055.978	81222.511	114608.34	52215.34	118333.86		
302.73438	6032528.1	10729536.17	-10871242	9491281.9	25926230	-3258516	3288822	21326990	62485.4987	146027.98	99892.6786	146933.412	97840.649	127199.68	88877.731	115664		
312.5	10738376	8416907.144	-10868313	9453142.8	28546968	-4304881	959254.5	23568204	143889.82	123611.708	225507.399	230364.902	165116.32	232793.7	145513.55	280087.46		
322.26563	14976822	9453585.973	-12864425	9575514.4	25911527	-3124904	-902626.2	2793499	118431.788	155829.369	260106.702	206790.553	179201.08	155302.72	183609.46	265465.4		
332.03125	17114558	8988107.238	-15924450	4090613.2	20189945	-8255021	-3537097	20807220	1365004.47	1581933.53	2418933.77	3020387.42	1574609.7	2140938.7	1889853.3	2502973.7		
341.79688	21059084	8450014.088	-12726046.3	1240516.3	13078991	-10631954	-13019526	19864627	218918.905	196340.965	162976.133	168530.154	183457.75	269569.79	197407.31	269964.54		

Table 25 Test condition: High Preswirl-10 krpm-25% Pressure Ratio-100% GVF

2000	Test Data										Uncertainties							
	Re Hxx	Re Hxy	Re Hxz	Re Hyy	Im Hxx	Im Hxy	Im Hxz	Im Hyy	Re eHxx	Re eHxy	Re eHxz	Re eHyy	Im eHxx	Im eHxy	Im eHxz	Im eHyy		
9.765625	-2175365	9806720.63	-12021587	-2143423	1976301	-987558.4	1549751	648095.2	315116.414	219278.065	176264.952	141842.323	311801.49	254509.48	167275.39	174062.31		
19.53125	-1199852	11264784.45	-10061292.1	-1991213	3080345	-1541932	744703.8	5120.831	412041.661	328974.821	216298.865	263097.203	288332.04	409000.74	313425.25	265630.47		
29.296875	-3110670	8965660.508	-14438629.25	-405955	2798004	-25101.32	1150910	3954260	118829.208	78412.7126	158895.076	57782.9154	96274.307	101166.5	81024.77	109914.8		
39.0625	-3474795	1031376.11	-13491872.6	-2325915	4168102	-51020.34	48251.51	4914312	79228.0252	55941.7109	124758.363	80007.3787	70623.641	91252.655	102026.75	90390.91		
48.828125	-3320774	10314659.76	-13630638.8	-1826169	5082723	-417583.7	915048.3	5862835	81920.9438	64412.4896	93233.3559	62279.7375	84521.888	76882.89	78229.858	64177.442		
58.59375	-2767793	10271831.02	-13454007.6	-1376879	5993141	-796721.6	1162857	6055688	91591.8904	58224.6375	121161.801	83244.9978	109405.77	79078.923	113107.81	88361.179		
68.359375	-2583713	10188913.7	-13436465.5	-1207257	6742913	-151440.3	1621476	8053321	173536.372	60610.1472	146993.623	54636.5437	54379.089	87964.229	85866.421	80666.656		
78.125	-2165567	10637206.53	-13348963	-679528.2	8042764	-816442.8	1698814	8887519	115567.642	104799.177	98645.5166	64950.446	149435.69	95570.895	79661.41	74750.49		
87.890625	-1761895	10419960.79	-13666675.5	-174166.6	9145853	-900354.6	1319862	1066570	118328.187	81607.4903	93365.6702	79002.7535	92661.965	71994.608	138151.32	91952.437		
97.65625	-1645788	10253540.79	-13680111.3	317003.55	9794057	-895168.1	1374358	11067431	141728.129	65320.2839	94957.6795	64984.3243	112338.38	96743.526	95296.825	54875.18		
107.42188	-8004877	6531841.425	-19515982.1	-2173739	5454118	-4235634	-1376057	10061694	163548.354	106699.622	195355.503	88096.2689	210290.17	131675.16	197789.8	92528.169		
117.1875	-772112	9986386.14	-13653389.1	1480969.6	11732386	-501979	1896269	1286919	146507.29	82228.5435	87126.8237	45077.3748	114429.61	79092.309	86298.025	59045.168		
126.95313	-331645.8	9989851.584	-14276995.7	2572431.3	12329896	-261075.2	2704349	5313236	118061.676	85130.3641	52191.384	48633.3079	52009.255	72723.547	82435.215	68369.389		
136.71875	498542.24	9945876.682	-14616849.8	2985729.6	13050221	-14236.42	2724662	13815950	77352.057	84670.4982	91103.2859	67187.9157	78392.9					

Table 26 Test condition: High Preswirl-15 krpm-25% Pressure Ratio-100% GVF

2100 Freq Hz	Test Data										Uncertainties							
	Re Hxx	Re Hxy	Re Hxz	Re Hyy	Im Hxx	Im Hxy	Im Hxz	Im Hyy	Re eHxx	Re eHxy	Re eHxz	Re eHyy	Im eHxx	Im eHxy	Im eHxz	Im eHyy		
9.765625	-2365690	11706053.41	-13849450.7	-2448799	2693238	-917636.3	718293	1291224	318782.913	193992.661	214737.855	214224.083	252417.51	227381.15	260818.95	217251.45		
19.53125	-2085010	1309217.77	-13498549	-980910.5	3739091	-1329782	1515054	1851737	221164.636	306952.656	252925.574	208515.896	342077.64	205637.24	181970.25	255661.73		
29.296875	-3647013	11491272.11	-15710291.4	-1226693	3776706	54227.67	802354.5	3633940	123660.278	154460.707	125290.804	117437.658	170617.39	112905.33	138347.5	116828.33		
39.0625	-3677987	11697770.29	-15675507.4	-1609975	4638841	-160944	1064993	5690560	106858.366	79628.2387	126378.11	96178.5782	99671.154	96186.185	103823.23	96346.442		
48.828125	-3189913	11500030.77	-15225619.8	-1490820	5536576	-765194.9	1243974	6238063	97752.3281	69309.8908	89309.4672	59222.3608	80660.701	79053.178	81708.948	73282.499		
58.59375	-3099119	11673478.77	-14821370.5	-1001197	7023236	-918077.2	1613431	6951446	137144.265	96321.9099	106002.977	45890.5785	153238.48	81077.03	92054.011	78628.025		
68.359375	-2372456	11489033.03	-15354627.9	-529037.3	7593370	-528911.3	2098373	8653348	80809.6008	86812.8102	109675.673	62988.3097	77818.51	87963.622	52617.725	69173.92		
78.125	-2145132	11913749.82	-14542416.2	265870.95	8677698	-1106767	2655077	9171061	118234.996	73800.7208	99464.3221	74011.7126	110370.46	104147.89	86418.829	104607.52		
87.890625	-1874338	11628798.05	-14770240.6	789298.68	9780000	-926690.5	2091314	10759393	92638.3772	95837.0454	83030.7207	86806.3882	118556.84	86915.926	91103.215	69233.592		
97.65625	-1278832	11374697.62	-14933911.7	1224937.8	10526027	-1342947	2418463	11596317	122412.135	79527.0691	89213.2994	60004.6609	101457.32	67702.076	96186.565	79574.484		
107.42188	-9141970	6426676.54	-21097752.2	-1659281	5213384	-3865303	-692234.5	11311490	158441.805	102457.316	149088.916	90154.9813	185618.69	84441.647	206532.92	122290.66		
117.1875	-412655.6	11111239.91	-15166145.1	2394338.1	12463919	-1186961	3008907	13392482	94256.3942	65433.7817	108400.209	73227.1517	112045.98	69340.209	91627.857	70853.023		
126.95313	9970.5722	11099535.76	-15363858.5	3559038.8	13212048	-719459.5	3249276	13980074	82390.3789	89578.2224	91848.8627	94826.2641	86757.495	113437.96	108039.9	61181.554		
136.71875	1293438	10866139.76	-1485676.3	7413136.7	20205801	-2152281	5436333	20114304	114078.433	81836.4119	116197.964	78415.569	175874.04	91242.62	104512.2	109054.09		
146.48438	1601132.7	10479238.82	-16039102.5	5079738.2	12807314	917390.8	6340282	12814576	98526.8348	74066.4554	68255.909	109552.019	88830.187	75104.53	198158.7	86695.442		
156.25	-172301.8	13221238.82	-13431646.8	2758268.6	13601530	-716208	7106648	16052292	100881.07	100726.764	126089.819	84396.9971	101206.38	97946.365	68440.788	68440.788		
166.01653	-346239.2	17351727.35	-13870871.9	1193310.6	18559975	-992370.7	2375701	19420007	181153.399	148683.099	151011.05	166527.201	122876.72	143066.53	177713.4	124716.6		
175.78125	462462.6	10802259.89	-18322472.3	6664733	19835504	-2605335	2794976	19503290	191356.226	128958.146	145156.536	135498.078	175234.12	107082.12	117500.62	92368.12		
185.54688	1661581.8	11672443.87	-15319230.5	6679899.3	18319727	-1762413	5388569	19069271	258154.127	108570.584	237604.877	66448.9712	187581.93	112834.92	113879.07	108534.15		
195.3125	2596575.6	112512348.36	-14384806.4	7206597.1	19600499	-3073351	4582022	18927004	140078.433	117304.008	194432.824	101258.469	190162.8	95869.097	114809.07	105930.51		
205.07813	2200931.62	12907732.68	-14485676.3	7413136.7	20205801	-2152281	5436333	20114304	114078.433	81836.4119	116197.964	78415.569	175874.04	91242.62	104512.2	109054.09		
214.84375	1822640.3	12817528.45	-14055871.7	8485437.2	20013106	-2633691	5390755	20356986	159575.714	129791.679	157140.376	123187.432	159938.9	160690	155235.06	144477.02		
224.60938	-454401.1	12097822.7	-13571254.9	8953612.2	21120128	-3196480	5177581	21284502	206087.851	115069.636	118718.782	79322.7703	195746.06	165336.19	173071.16	103778.22		
234.375	-594107.5	12637626.24	-12653373.3	9666757.8	26309822	-2654913	7692323	22977619	168279.19	160566.69	292852.937	148370.138	236842.81	137531.4	159253.6	14798.98		
244.14063	-766418.3	11566185.59	-14918604.9	9919357.1	26127529	-3807443	3855658	22976226	97965.6435	101031.389	172379.785	127499.642	163041.14	118944.54	191655.13	163153.3		
253.90625	-1994989	11013227.91	-15603212.6	11458243	27771845	-3728605	5017672	24236298	134831.656	91251.9467	198760.894	137739.466	136566.47	86925.341	21267.98	116733.98		
263.67188	-2664699	10591955.4	-18574044.3	11682075	29463297	-4438777	5999011	24485078	148619.346	57731.3362	174456.663	91685.9529	143989.83	92381.828	183538.81	91344.961		
273.4375	-2324520	9661590.714	-19229951.7	14519854	33070966	-3312281	7737364	25593349	70596.9344	72226.0019	61790.2859	90173.2047	96162.006	104849.75	116897.89	82786.899		
283.20313	-1702548	7744997.376	-17076106.2	13015514	34892536	-4169660	9993485	24841610	84481.982	41018.9313	84332.921	48421.1965	74732.327	47832.416	44207.578	28818.582		
292.96875	-4466324	6560504.061	-16813228	12561924	36661907	-2324352	9891811	24984156	71752.3581	42502.8828	63667.1791	62844.7769	91818.617	46758.189	73615.566	46510.864		
302.73438	-6525452	2536810.709	-18878711.1	9055800.4	40969251	-2399760	8712754	28054419	69688.8732	29546.8738	69790.6249	37898.6039	81925.307	66028.802	72191.791	57953.66		
312.5	-8339682	-2963502.19	-22435345.9	2140310.9	39602543	1394879	3251499	25066564	93628.2755	64291.0149	87634.8472	46148.0589	86122.131	80925.841	84276.799	82600.768		
322.26563	-93340898	-69945662.5	-100228240	-57150177	1.6E+08	1.98E+08	1.21E+08	2.31E+08	1545614.48	1621164.51	1697056.49	1826463.3	1851409.1	1550191.1	1982544.8	1597887.7		
332.03125	1415555.8	30540916.04	-6263133.34	32535492	74067765	-8641304	34518604	27166867	13025915.91	110885.386	141468.169	149463.382	103820.61	138224.44	142797.47	144567.97		
341.79688	7682702.9	23988659.46	-11331831.4	35074383	74271558	-9860695	25105235	31133122	137076.366	78455.2284	113725.523	59688.8807	80453.505	91038.777	67622.183	72306.88		

Table 27 Test condition: High Preswirl-20 krpm-25% Pressure Ratio-100% GVF

2200 Freq Hz	Test Data										Uncertainties							
	Re Hxx	Re Hxy	Re Hxz	Re Hyy	Im Hxx	Im Hxy	Im Hxz	Im Hyy	Re eHxx	Re eHxy	Re eHxz	Re eHyy	Im eHxx	Im eHxy	Im eHxz	Im eHyy		
9.765625	-2657858	14057106.11	-16702072.1	-1401068	2870402	-811605.2	793762.2	1138304	300387.68	289900.744	551865.148	340881.918	313613.83	409940.6	451873.79	474975.26		
19.53125	-726168.6	13223243.14	-15031419.7	-1201126	3791177	-3555641	1918065	622248.3	712791.43	567415.344	752313.097	733341.434	590060.86	867652.11	752676.04	918310.16		
29.296875	-2938625	12262285.3	-17577464.7	581404.92	3844541	-699668.6	1900782	4348742	128770.343	140566.568	213438.317	109905.806	143910.87	126480.37	142618.65	176882.08		
39.0625	-2999118	12707548.11	-16858327.5	-890642.5	4457061	-729472.3	1664597	5348121	147370.896	82447.9133	87191.6212	88600.6664	110496.86	120860.32	140384.51	98652.458		
48.828125	-2504973	12717670.42	-16582060	-601028.1	6011786	-1151606	1927745	6397527	90231.1567	79481.0663	97387.3337	80603.8351	140955.43	91092.435	112242	84144.276		
58.59375	-1842293	12439084.71	-16582749.6	-112983.9	7093075	-1291864	2106119	7135284	174488.482	82783.6659	111034.599	61646.0013	150515.95	105882.01	120607.5	74437.248		
68.359375	-1678418	12471537.32	-16788381	314978.49	7577893	-958904.8	2797286	8674892	140879.575	79415.2169	52205.722	48593.1332	145619.39	74464.792	73209.198	54601.089		
78.125	-1727994	12797494.95	-16309178.8	786904.74	9127161	-1265309	2758808	9552066	180261.0714	88347.1543	68898.4165	84213.7761	155932.72	125111.22	129398.57	71673.64		
87.890625	-844973	12613717.45	-16385905.1	1434172.1	10026801	-1642495	2550102	10899409	109589.1714	116271.633	124694.218	90601.8766	133004.85	86352.363	104721.92	73269.523		
97.65625	-824694.3	12550961.47	-16230808.2	2061146.3	10886445	-1474300	2712629	11749985	134622.247	81293.4068	143550.041	84543.0084	81618.314	83338.122	68963.456	74342.842		
107.42188	-7663662	8342195.444	-22340488	-1708891	6745562	-5072016	843858.2	10846311	166481.456	121522.878	156417.307	91363.537	136850.62	88088.744	181523.16	77164.53		
117.1875	296237.34	12207898	-16589696.1	3503090.9	12970382	-1604615	3819674	13836096	140851.138	107332.12	102067.088	86321.0322	141306.79	85253.72	190551.78	82229.238		
126.95313	743631.95	11754471.46	-16570303.9	4850807.9	13465720	-1277965	4615823	14425137	108905.142	94990.6402	155477.464	118018.98	122128.13	71477.992	17450.199	122196.22		
136.71875	2131891.4	11630656.17	-16950573.7	5868438.7	14189853	-1283414	5040595	14468349	124103.975	86721.7573	127184.061	72641.2398	82030.794	99149.787	109267.12	875		

Table 28 Test condition: High Preswirl-10 krpm-50% Pressure Ratio-100% GVF

2020 Freq Hz	Test Data								Uncertainties							
	Re Hxx	Re Hxy	Re Hyx	Re Hyy	Im Hxx	Im Hxy	Im Hyx	Im Hyy	Re eHxx	Re eHxy	Re eHyx	Re eHyy	Im eHxx	Im eHxy	Im eHyx	Im eHyy
9.765625	-418755.6	7720508.159	-10292182.1	-1462344	63730.98	-152520.8	-1429092	6710762	350101.159	282079.505	376662.216	255311.441	230217.71	275455.61	284728.66	368836.75
19.53125	-574729.8	8644650.959	-10215364.9	-61030.33	1641822	-119712.3	219080.4	2099749	121106.87	164961.468	185693.224	142138.116	146084.54	135109.41	163039.51	157283.23
29.296875	-533637.8	8557491.089	-10854020.1	1201282.8	1643668	1111096	1246362	1957417	135584.157	107028.714	133888.655	86431.9628	182191.35	92742.777	154035.18	70325.611
39.0625	-827029.3	9004552.783	-10595521.5	581471.23	3258256	-170185	299226.8	4222389	124745.665	80044.761	168210.264	59045.6864	104530.7	107410.96	143349.91	99405.628
48.828125	-565965.1	9270754.708	-10297789.3	664841.14	4434320	-428781.8	450795.2	4467613	166562.487	77603.6112	131679.852	69708.1219	81048.589	95650.712	109249.93	54132.337
58.59375	-436354.8	8742705.166	-10266820.6	592807.34	5116295	-335456.8	314229.6	5455496	114136.309	65817.0895	118343	76507.2494	92532.939	89866.673	159219.09	60423.063
68.359375	-347043	8982143.372	-10642552.4	1000099.3	5736945	-68406.03	787662.1	6981135	68235.4139	71716.7011	64877.5426	61755.5833	104717.8	59965.894	70117.598	56488.911
78.125	-576240.1	9064602.788	-10372080.3	1347571.5	7367731	-516303.1	752051.6	7224095	151057.428	82275.715	167785.206	108371.954	153072.68	97246.715	148302.57	92810.148
87.890625	173996.14	8977116.804	-10688269	1717990.9	7859999	-393102.6	630928.1	8710786	120282.575	80746.449	70966.1396	84990.801	96281.645	79434.92	56028.563	58977.423
97.65625	158438.44	8795780.211	-10676592.3	1896711.9	8637291	-468161.7	846577.9	9466718	128855.519	69004.0987	89405.5702	81562.4383	112388.37	93779.596	161521.38	90484.367
107.42188	-735885	4427731.409	-17203119.8	-1082514	4586232	-3151075	-1486689	9376993	204205.472	80140.2977	138960.37	75373.5055	146551.7	82746.343	230184.28	80098.418
117.1875	465871.66	8756356.059	-10899493.9	2538760.4	10584354	-79788.66	857339.4	11374452	88525.3685	65949.6866	148251.032	73819.9856	93281.555	54088.854	148714.33	65106.006
126.95313	907901.74	8708279.833	-11338351.3	3745071.5	10791893	300210.2	156439	11955171	166285.945	84022.5153	169473.871	75661.6356	124178.83	84927.234	112013.92	73980.3
136.71875	1725147	8772603.434	-11740703.8	3977810	11326300	350045	1692942	12323050	78344.3096	76082.3943	76659.5539	58004.5495	85629.107	80797.842	85256.543	64842.933
146.48438	1406169.9	8083986.065	-11820944	4080095.6	10146618	1771120	3821408	11311052	98194.419	69430.3166	117039.56	11776.6385	144878.19	111642.1	114836.41	101808.92
156.25	901345.01	8973832.607	-11062067.9	3551464.1	13319591	-388884.6	277116	15014941	874175.5504	117161.688	97207.8119	58550.6158	196033.13	89690.213	71811.972	53504.504
166.01663	-3993783	13949213.86	-7327072.83	843824.14	13725283	371433.5	2388440	16015065	183547.028	91094.8309	143879.79	97210.83	76181.557	127916.34	152040.49	98973.775
175.78125	3585203.8	9010402.595	-13776012.2	5262928	16983096	-815126.9	954362.4	1659301	33731.2281	101996.69	185495.09	92689.8732	333288.46	138146.82	239918.09	93628.27
185.54688	1562983.6	9524508.369	-12256636.6	5216378.1	15753092	-392406.9	3513677	17351182	280497.993	98990.7792	221715.838	77287.4098	194678.57	132146.63	119646	98873.979
195.3125	1580204.8	10740105.3	-11367555.5	5375349.6	17213021	-1138622	206530	1715145	120556.188	80499.3447	80845.3144	80792.7526	117130.46	114340.97	154413.79	101075.51
205.07813	1568924.3	10673025.42	-11360589.2	5466611.5	17183672	-583631	2853482	18541893	110551.667	54777.6038	142202.089	56813.6065	154830.27	84132.383	121340.25	70699.357
214.84375	905037.1	10816443.22	-10381932.5	5946737.5	17387043	-1321074	2720389	18872670	146499.791	109732.968	127578.808	92514.5764	102690.3	97956.04	81787.644	89209.221
224.60938	-1738305	9949230.391	-10635517.6	6019752	18228551	-1598050	1646497	19915246	134436.927	89593.5197	194180.12	93029.4067	180559.97	70500.207	232528.35	75884.503
234.375	-2320980	10593382.32	-10126387.9	7149516.9	23226931	-1312882	4776115	21847341	178049.393	75286.3281	126379.132	134225.433	139124.67	119242.19	182974.02	95979.242
244.14063	-2527723	9365589.867	-11683205.5	6610152	23696197	-1767311	1205268	21907783	153338.134	102664.96	141044.285	78703.8747	130159.21	81269.041	172701.57	84242.279
253.90625	-3398617	8736437.067	-12579490.6	7609134.4	25312060	-1279777	1788947	23766144	105469.634	54995.0857	107371.903	63436.2735	122236.51	68879.386	110526.11	58262.33
263.67188	-2785531	8376560.781	-14278128.8	7661455.2	26140653	-2377383	1382857	24223671	96015.3559	49420.1538	78338.836	31200.2805	125264.44	49234.33	148028.8	36899.656
273.4375	-3441200	7644493.869	-15382568.6	9976680	29777916	-857284.3	2597729	25856150	34615.0291	77161.8643	65664.6462	51933.0743	72842.839	56242.985	82836.859	71018.925
283.20313	-4204588	1272968.838	-14530439.6	9048110.5	31947521	-1538452	5706825	24590820	180403.108	67184.4952	62610.7869	39823.1739	128656.62	67343.043	74966.557	37921.36
292.96875	-6023411	5582177.312	-13866852.1	8146996.5	34342247	-876719.1	5392306	25107964	10810.7427	52080.9643	73682.7047	42521.7535	85695.151	57706.411	5615.756	41572.424
302.73438	-6827042	1059306.254	-15484309.6	3898861.7	37838839	2511716	2019043	26188010	90803.8558	53831.0082	53538.1001	55485.9876	81870.99	57305.78	50332.606	36110.348
312.5	-7809253	-2202136.86	-19129250.1	-3032609	37184998	1533294	-2519344	22905450	72918.7034	69683.5366	68798.5766	48787.8338	91762.657	51388.742	104440.24	7647.519
322.26563	-2256+08	-228908563	-236632341	-2.27E+08	1.72E+08	2.58E+08	1.42E+08	3.09E+08	181631.12	2420406.92	2240709.04	2689869.18	30063037.2	2941908.1	3457332.7	589428.5
332.03125	-1093714	26204632.81	-16446822.2	24989625	67106808	-8658241	24859555	34337063	188913.219	122389.981	255150.454	150700.735	122553.3	187588.77	129743.28	250295.16
341.79688	5924419.8	21138558.32	-12473490.8	28740524	67226904	-8697473	21009013	32867631	139498.277	69447.5245	157185.747	92173.5128	100077.1	82214.41	170273.85	103024.68

Table 29 Test condition: High Preswirl-15 krpm-50% Pressure Ratio-100% GVF

2120 Freq Hz	Test Data								Uncertainties							
	Re Hxx	Re Hxy	Re Hyx	Re Hyy	Im Hxx	Im Hxy	Im Hyx	Im Hyy	Re eHxx	Re eHxy	Re eHyx	Re eHyy	Im eHxx	Im eHxy	Im eHyx	Im eHyy
9.765625	449271.89	9331269.958	-11138463.8	-139658.3	199753.2	-715746.6	-60499.72	564878.5	225251.955	299231.829	187636.909	212535.261	343722.56	261766.44	238406.1	219467.85
19.53125	-185469.2	8768408.047	-11880872.6	-534370.9	1254254	-1022680	408451.2	2557400	246611.168	271927.959	288209.845	300227.088	146978.55	322974.32	178872.55	356347.28
29.296875	-168282.6	9625092.647	-12286425.6	1691711.7	2078223	1178387	1701101	2010712	115344.126	144856.105	143624.369	111412.881	192185.7	107593.09	164957.28	110749.27
39.0625	-653787.1	9983162.974	-12043994.5	907608.28	3275905	78241.04	798018.6	4727466	135541.004	76732.1539	158896.506	75774.4565	89415.179	103396.89	125542.62	91922.166
48.828125	-598390.3	10275200.37	-11785992	1243217	4633288	-546880.7	900841.5	4970633	931584.8573	75211.2058	82867.7183	64494.4554	75356.196	85140.165	109802.13	77477.987
58.59375	-544871.6	110026209.08	-11746982.8	1231682.1	5619859	-307880.2	714628.4	5732086	175664.664	75536.1285	103471.93	62570.2809	117899.25	9151.252	164237.3	62566.421
68.359375	-361161.1	10025728.34	-11901249.9	1554181.1	5954359	-25974.68	1238971	7212042	86353.0246	73191.2414	44843.9807	65077.5624	119815.53	75206.946	143354.67	55511.417
78.125	-13279.93	1052962.84	-11486513.6	1976334.2	7711938	-733390.5	1159607	7504599	157555.924	95289.6912	195214.047	88238.0368	122067.61	113357.52	135222.6	86420.778
87.890625	45743.159	10414900.09	-12324575.3	2193979.5	8469441	-596837.2	853261.7	9419573	84686.9145	75843.6507	106490.875	63108.1169	74660.177	81508.83	100229.51	68480.489
97.65625	334687.65	10085957.74	-11909115.4	2670789	8822941	-1016214	1142838	10247596	117504.344	61233.4837	147408.017	71616.3929	86096.063	90593.812	53263.762	71013.392
107.42188	-7369525	6075663.147	-18739403.9	177928.63	5661063	-3525926	-903575.6	9683649	123368.338	85535.3689	183194.94	101407.466	160106.49	85468.888	211719.92	84129.495
117.1875	737496.6	9890173.007	-12288280.4	3474529.1	11196208	-685047.2	991068.6	11838743	65449.9404	70838.2669	125114.169	73050.4389	182276.54	99337.287	137750.4	65720.509
126.95313	1132575.5	9895861.632	-13054032.2	4446059.2	11413829	-204982.4	2032974	12880220	90598.6815	74998.4592	100733.726	81394.8951	99465.793	82644.906	137899.28	46562.257
136.71875	1984388.3	9721972.728	-1312143.5	4737871.6	11936663	78132.15	1958688	12853041	97146.6973	58942.4106	87395.5871	54456.1004	7312			

Table 30 Test condition: High Preswirl-20 krpm-50% Pressure Ratio-100% GVF

2220	Test Data									Uncertainties							
	Re Hxx	Re Hxy	Re Hxz	Re Hyy	Im Hxx	Im Hxy	Im Hxz	Im Hyy	Re eHxx	Re eHxy	Re eHxz	Re eHyy	Im eHxx	Im eHxy	Im eHxz	Im eHyy	
9.765625	-598663.4	10544230.48	-13696012.7	711763.73	708058.3	-622136.8	290404.4	1430268	467084.118	277181.354	460276.014	400628.128	232900.85	379770.59	548170.45	471633.67	
19.53125	-414563.2	9727569.862	-14184713.1	1618251.7	1155488	-297792.1	1207529	2712279	292030.826	285695.864	263714.551	225111.179	261875.52	306035.51	229007.35	292559.24	
29.296875	-296193.1	10491444.29	-14184106.6	2276171.5	2016668	676050.2	2062504	2828611	108848.785	124283.149	173957.996	114049.519	187807.96	88736.802	165759.78	92211.413	
39.0625	-167466	11292789.99	-13887554.6	1905258.1	4005221	-367083.6	971626.5	4609622	89496.5716	84773.2373	128904.396	108994.881	113087.96	85796.107	188501.52	90138.563	
48.828125	-228402.5	11834070.85	-13629459.1	2127489.2	5275865	-455490.7	860351.2	5381867	94779.6653	115725.636	100942.126	87060.8882	88749.357	77535.425	59532.516	81918.487	
58.59375	78232.793	11508676.28	-14175213.9	2365295	6225711	-687594.2	1129133	6217630	167216.876	84481.4578	183944.026	95435.6288	110215.85	86444.213	201406.84	94964.269	
68.359375	382040.44	11642936.56	-13395707.5	2700089.3	6848629	-332624.4	1576474	7699510	147358.92	108406.757	89383.3728	82066.4629	102557.03	69443.092	94291.272	64142.688	
78.125	463171.48	11717163.44	-13343809.9	3022464.7	7859402	-942472.1	1598527	8257586	138862.61	89736.4724	143890.871	90063.9973	157704.95	85122.338	94824.798	76222.946	
87.890625	917336.35	11704407.35	-13797793	3389766.6	8590852	-1079555	1233928	9693022	104798.724	79241.5732	72343.7	98559.1814	106084.1	82071.364	136000.6	61883.569	
97.65625	987256.82	11305845.92	-13747923.1	3704230.6	9465591	-1054706	1663326	10658218	114871.076	62442.9812	142874.542	90503.4068	99967.629	84791.548	119798.45	96803.754	
107.42188	-4888944	8230084.375	-18439758.9	2447881.4	7556644	-4809216	1198905	9193594	124751.071	74212.8418	175740.408	64180.4651	128363.44	74019.781	141807.68	69781.099	
117.1875	1570184.5	1099969.84	-13975182.1	4823217.8	11210810	-1001659	2192251	12092916	59379.8773	63961.3993	148047.662	92739.3115	104207.33	93433.759	174775.8	101033.26	
126.95313	2146428.7	11000119.38	-14323408.8	5928407.2	11896578	-640728.8	3073578	13206439	86616.805	66889.4517	79927.5496	69224.7981	96389.753	68553.178	93356.111	78654.692	
136.71875	2572003.9	10912260.49	-14727588	6448288.8	12861622	-345421.9	3160672	13483610	103390.571	69487.1155	161715.323	92821.2633	115022.61	81782.271	105469.96	113769.78	
146.48438	2455701.2	10632763.7	-14532989.4	7019905.4	11850267	1061524	5584585	12725965	97564.4591	90761.2704	116787.667	91631.6156	107143.71	121448.08	146436.52	93352.039	
156.25	2581566.8	11123543.89	-14131792.8	7121978.6	14100671	-1528062	2755218	15997277	61159.5863	69110.5127	134445.212	81147.924	109892.65	82990.076	127127.16	84916.241	
166.01563	-3052477	117160970.74	-10796118	2794767.9	15132239	507305.8	3991668	16629433	139678.032	81866.7	196657.274	77139.2784	118533.19	99772.22	122128.2	124549.76	
175.78125	5627552.5	10679305.44	-16174099.9	7885247.9	17936699	-1935195	2351788	17276554	152854.819	99724.8366	253923.325	119660.651	119677.64	84092.819	185473.85	93223.182	
185.54688	3997935.4	12282667.44	-13896540.6	8705438.8	18150367	-1308211	4885705	17936611	178760.123	84639.5973	145694.987	108871.07	102932.52	101329.81	224624.73	119380.97	
195.3125	3859407.3	12564681.9	-13356296.4	8662466	18590590	-2341477	3685685	18100743	186116.376	83769.8684	129720.967	99024.9573	124195.24	92858.296	80764.683	60301.563	
205.07813	3387881.6	12554085.98	-13036977.1	8660040.4	18597774	-1516739	3989842	19009073	91726.7326	86401.7679	189135.25	57535.8257	151997.11	81624.621	117025.31	100473.25	
214.84375	2945148.3	12516141.14	-11924964.6	9682998	18345684	-2221087	4282944	19251588	120177.509	143433.568	102304.307	102917.59	182378.46	111570.77	113229.04	89866.535	
224.60938	431228.89	11974510.33	-12383311.1	10642884	19505651	-2356571	4332601	20594947	150007.004	78966.9425	171271.303	108105.122	107121.74	96964.534	184563.1	103218.01	
234.375	182330.93	11631994.49	-11241478.5	10582789	23872052	-2697773	6034436	21452604	127392.502	102095.95	144460.584	118997.82	147401.87	112339.13	222217.89	77571.637	
244.14063	-358941.8	11529880.61	-13488202.7	11538174	24906165	-2496255	3200290	22133785	183658.3064	221589.74	107359.427	158887.05	109626.05	132934.75	137573.33		
253.90625	-982108.7	11454979.8	-14650152.5	12539841	26970677	-2354527	3325827	23477273	208280.593	55506.9267	210284.5	83029.304	118499.04	87888.84	13009.88	72390.364	
263.67188	-406653.1	11346118.44	-15933581.2	12584506	28073778	-3698972	3507918	23168559	128303.595	62159.1513	148063.59	51495.3024	121959.54	55201.562	142386.32	68407.991	
273.4375	-929575.9	10853459.84	-17430789.3	14129078	31415810	-2698907	5230698	24296444	76578.3363	54776.5736	80149.8836	52543.9462	92235.921	59873.793	106701.95	70198.878	
283.20313	-1325015	9582206.707	-16338981.4	13119452	33214739	-3401815	7946214	24520022	74145.79	55350.0134	77134.5769	49710.4383	119778.23	55789.362	106972.64	48390.796	
292.96875	-4113887	7053938.305	-16053739.5	12159866	35414390	-1478866	7645910	25663152	102304.552	51804.9568	81968.0007	54519.2013	112442.18	55833.89	67595.819	39675.6	
302.73438	-6086567	7189108.179	-18341744.9	13099735	43184408	-4707966	9181871	30288514	106654.839	69915.8685	69587.9169	49999.1401	78437.447	53374.929	96820.557	50249.907	
312.5	-11297537	-2309505.93	-26048540.8	585487.91	40457072	6292556	2755930	29944519	95522.2821	85218.13	132938.027	93602.115	164068.76	139051.53	103799.24	111414.41	
322.26563	32320564	61729879.98	-36879153.71	81501430	1.98E+08	1.73E+08	1.52E+08	1.99E+08	2491055.73	2151041.79	2282719.85	1980069.05	2461009.5	1936093.4	2097435	1730451.7	
332.03125	-137680.8	17214972.97	-17108259.9	19293572	68928521	-1914335	27975519	36919586	983644.822	1172511.64	169864.38	1985612.66	969065.52	121896.6	1614497.7	1995269.9	
341.79688	7032437.8	19130784.24	-13223000.2	29515476	67991364	-5245388	23225667	34671136	83808.9155	108853.119	240884.594	162288.456	160940.88	96703.607	232252.36	181500.92	

Table 31 Test condition: High Preswirl-10 krpm-65% Pressure Ratio-100% GVF

2030	Test Data									Uncertainties							
	Re Hxx	Re Hxy	Re Hxz	Re Hyy	Im Hxx	Im Hxy	Im Hxz	Im Hyy	Re eHxx	Re eHxy	Re eHxz	Re eHyy	Im eHxx	Im eHxy	Im eHxz	Im eHyy	
9.765625	-181427	5908551.765	-7472904.38	669466.87	-11521.13	-400004.6	534428.8	6707718.8	253593.847	304329.148	709143.911	545068.17	300154.73	243057	592276.8	639797.16	
19.53125	-185622	6168168.748	-8294371.97	-147132.1	1530474	-334849.1	-75175.04	2302290	82848.1256	98207.0379	113794.981	64630.1994	166746.15	102713.32	112027.99	108220.47	
29.296875	-450700.6	6085829.536	-8316119.4	1251967.1	1693393	1364339	1100022	2382695	1563647.041	85351.2354	93937.415	73452.3759	106013.19	82344.182	84230.213	50671.719	
39.0625	-430380.5	6446005.56	-7941742	464280.64	2852030	140840.1	-47107.95	3882264	868904.041	46230.1373	118967.231	78347.4454	98512.865	54564.519	102330.76	63732.474	
48.828125	-254539.9	7000076.774	-8217185.72	645461.02	4000180	42069.61	321782	4403781	142274.473	96374.8411	78177.0426	59491.4606	84739.013	59384.096	50329.452	66216.455	
58.59375	14296.908	6799437.99	-8006879.85	902067.62	5325500	31844.8	40103.5	4987070	84052.2076	51257.121	105463.214	50733.015	110424.34	64143.953	129657.22	54327.921	
68.359375	-1895662	6785973.01	-8013637.23	1169076.5	5158085	466864.7	401689.5	6289649	87566.3199	70353.4381	65143.0354	38713.3807	88543.138	69458.809	86178.795	55093.953	
78.125	-4421837	7271849.572	-7964115.23	1005050.9	6551421	277910.6	480965.2	6865926	93000.999	62695.226	89328.6443	67169.6424	68717.925	64665.474	100387.85	67408.296	
87.890625	-2785509	7172562.087	-8134661.67	1513061.6	7093484	206106.1	1146991.2	8365751	81401.9259	41654.8995	109636.148	82020.3052	81445.905	102110.23	95590.249	68339.118	
97.65625	-275610	7071150.577	-8437344.52	1490041.5	7956644	322652.6	28310.35	8955608	95652.1995	62495.9504	65194.2206	42328.8624	52025.624	71800.714	85897.466	37813.136	
107.42188	-6601913	3786094.288	-13672825.3	-586717.5	4992992	-4186307	-1020440	7143743	162322.442	77885.6926	129299.788	52730.7852	132872.48	57771.243	118924.02	107702.09	
117.1875	460884.46	6780611.6	-8549851.28	2052406.7	9360993	496568.5	408235.1	10889377	43514.8999	58102.774	86038.293	52329.5068	52098.595	48537.659	64230.357	51686.468	
126.95313	335814.01	7013139.277	-8778433.74	2626740.3	9772208	731275.2	612849.9	11522822	45848.2776	46291.33	58147.8287	38908.0146	58116.584	48459.358	56589.772	30613.094	
136.71875	438484.37	6938089.474	-9043310.89	2580126.1	10614405	949494.5	644801.6	12084200	63627.931	77248.703	52567.8104	40633.2574	79775.413	39990			

Table 32 Test condition: High Preswirl-15 krpm-65% Pressure Ratio-100% GVF

2130 Freq Hz	Test Data								Uncertainties							
	Re Hxx	Re Hxy	Re Hyx	Re Hyy	Im Hxx	Im Hxy	Im Hyx	Im Hyy	Re eHxx	Re eHxy	Re eHyx	Re eHyy	Im eHxx	Im eHxy	Im eHyx	Im eHyy
9.765625	-444810.1	8222023.405	-9757322.23	-90945.59	1211018	-812846.7	-640370.5	1032088	144960.555	156325.534	333504.87	346401.245	193189.6	207411.8	357681.27	338750.82
19.53125	-67651.13	7030931.206	-9864813.5	460144.44	1451957	-107542.8	374945	2798838	149762.317	140566.414	97487.6621	130861.121	150455.47	126492.5	132464.48	122746.94
29.296875	-98022.82	7711364.737	-9825585.52	1781247.3	2385377	868010.8	573992.5	3024806	115658.788	81866.8887	143129.777	85294.0085	140938.1	74313.77	163112.81	93783.984
39.0625	-58902.09	7980243.437	-9620486.93	1117383.6	3443858	83495.51	109091.8	4740499	107549.458	62966.2238	45834.3519	52367.9153	114552.28	53210.395	92761.69	44395.648
48.828125	-184860.9	8104448.87	-9411813.35	1522491	4571265	-148662.8	365248.4	4918237	117251.374	88731.933	75294.0586	55459.1655	116839.21	65099.211	127810.55	55214.941
58.59375	-236307.5	8151010.742	-9523948.33	1805730.5	5531120	-90667.26	375560.1	5534863	162153.294	60807.4212	104044.907	47238.458	164698.82	60889.15	115147.95	42064.201
68.359375	313348.29	8271320.025	-9620230.02	1907184.6	5873774	520059.3	613574.6	6924541	67213.9816	66242.8023	68851.223	49552.8733	97956.388	63831.345	79390.593	59056.691
78.125	-7867.262	8557205.883	-9862967.77	1983660.2	7139619	-7526.86	548925.6	7582446	92548.5671	69072.8402	91855.5711	60914.5248	84081.92	70913.355	81847.783	69249.043
87.890625	292274.41	8549388.472	-9869602.13	2467215.8	8064150	27769.12	137464.8	8938851	58285.6895	87264.462	54767.4463	71304.704	101042.76	76574.767	11849.178	72654.969
97.65625	685626.75	8182823.348	-10038171.2	2591635.9	8281981	-133482.2	439008.7	9792156	77300.513	56911.0209	67969.0338	58170.2069	78688.677	55511.098	68775.058	57755.773
107.42188	-6561664	4672619.196	-16251845.5	237138.42	5202940	-4000684	-1730257	8759555	124410.934	80158.9047	166311.516	68714.6216	133675.94	68281.266	181458.24	84603.864
117.1875	1014468.5	8248313.153	-10079136.8	3404340.7	10519013	-8156.855	766682	11731472	85588.7001	59505.6731	60356.4999	62356.0509	114395.85	67146.351	78402.009	52317.399
126.95313	1003887.2	8023082.654	-10404618.3	4194894.2	10823134	561772.4	952008.5	12244184	79883.3296	52416.6788	81963.292	56346.0385	45911.241	56148.661	60891.024	62066.702
136.71875	1838271.4	7945337.541	-10920673.3	4199274.9	11529233	719649.1	11529233	17270402	50804.2031	59386.9866	67901.3854	68798.1629	57050.552	55345.47	61869.402	49255.497
146.48438	1422335.7	7567903.16	-10883769.5	4665011.2	10602671	2246795	3690508	12060177	68499.4712	58931.3441	125316.539	52727.4384	86770.592	5092.399	59347.855	64750.21
156.25	1222515.6	8372284.586	-10499621.1	4398327.7	13252994	251415.9	734535.1	10539077	57309.4637	50310.7975	94046.9708	50757.7407	73330.031	59179.745	69537.38	60226.386
166.01653	-4477350	13905174.16	-7164819.72	-226128.7	13594318	2683020	1775125	15574552	84831.6037	60734.7375	91933.7666	56279.0603	68011.279	65297.597	97928.217	61043.311
175.78125	4003469	7651783.147	-13126312.5	5851203.1	17525466	700308.3	556260.5	17169125	76701.1893	58910.1643	93343.8516	51178.8792	122567.15	64730.424	140867.02	56288.862
185.54688	1067651.6	8796854.295	-10866163.3	5427519.2	16787738	149324.1	2802830	17558703	190499.632	87410.279	205602.824	84942.3778	193115.76	94556.248	188072.76	101116.14
195.3125	67162.37	9874957.813	-10517875.3	5841275.8	17715039	-140323.6	1974490	17780194	862193.9319	54469.2268	59120.4161	73165.0673	84272.997	91959.51	101115.94	71229.709
205.07813	795013.54	9963059.85	-1060370.4	5212566.7	18115039	159122.9	2231932	19202475	60629.2535	52178.4518	71466.6117	54239.1663	13452.36	8254.931	116863.94	59591.271
214.84375	127503.49	10189605.33	-9538892.05	6083602	17980196	-315905.5	2368137	19598374	89901.0142	113269.295	146930.75	100429.954	90293.993	90408.824	136992.81	126731.53
224.60938	-2377091	9445885.197	-10077645.1	6139881.3	19016981	-660652.4	1283185	21198120	182227.653	83722.2319	152261.032	115249.779	108527.33	85777.08	142148.36	101399.38
234.375	-3680529	8886234.934	-9128600.54	6054534.5	23089808	-9784.478	3829310	23308713	169930.364	213258.23	468826.083	192709.613	331309.25	151118.74	296411.82	292629.42
244.14063	-3902189	10309133.483	-10497204.3	6596422.7	24327091	-814727	3838553	23163686	459231.965	171914.289	502310.742	365643.498	340124.9	218399.29	735412.38	304387.37
253.90625	-4871393	8495627.463	-11166334.5	7234855.8	26859010	-703591.5	1159367	2521600	334871.185	164093.538	694506.918	346001.791	365425.12	175940.46	728376.16	307065.63
263.67188	-44384326	9077252.613	-11643963.2	8384355.2	29070771	-1575406	271588.3	25151054	239914.442	93947.7045	330565.462	91635.4465	202446.43	82534.137	250270.17	94776.755
273.4375	-5123093	7546988.103	-14149042.8	10012876	31577868	-395422.8	1003852	26416322	90749.3939	43158.625	95317.4296	56636.3584	66137.012	66027.947	97614.889	82155.854
283.20313	-5785082	6788055.328	-14169543	8165800.7	33784267	-650545.8	3046102	25546250	118822.262	44309.6341	35031.2139	57973.6484	115266.69	46875.029	122568.44	45210.428
292.96875	-7746907	5455563.342	-13092453.4	7037197.3	36357832	-242953.5	4304967	26824834	79328.1192	36368.2501	53247.1016	43575.0255	76362.599	48032.207	97473.188	32309.734
302.73438	-10034416	1152967.48	-17102933	4278381.7	39814227	5542660	2356052	30210069	112705.091	75967.7511	69242.5806	61241.096	120908.03	76532.361	77670.101	48835.303
312.5	-11476331	-3500271.78	-18877810.2	-4808545	38348365	1631381	-4444139	23190799	133745.373	90897.0128	64647.8701	47538.9467	129481.89	97082.538	65842.644	55403.018
322.26563	-89166946	-67356028	-86088135.8	-59678661	1.74E+08	1.95E+08	1.31E+08	2.33E+08	2565102.17	2756030.1	3021273.61	2901851.56	2742350.6	2363405.3	2514981	2206427.7
332.03125	-3478442	23545913.11	-14045008.9	21129818	74338024	-1156122	28050506	41821617	102322.024	102726.261	140987.112	140104.955	102896.36	111908.84	141590.86	139790
341.79688	2777305.2	20530037.89	-11603969.6	23774552	72624652	-1918592	19935724	40541715	134133.204	78949.8049	168560.684	78447.8476	93748.919	83343.475	125591.7	93664.519

Table 33 Test condition: High Preswirl-20 krpm-65% Pressure Ratio-100% GVF

2230 Freq Hz	Test Data								Uncertainties							
	Re Hxx	Re Hxy	Re Hyx	Re Hyy	Im Hxx	Im Hxy	Im Hyx	Im Hyy	Re eHxx	Re eHxy	Re eHyx	Re eHyy	Im eHxx	Im eHxy	Im eHyx	Im eHyy
9.765625	851697.51	10428004.92	-13097536.3	937843.2	1978981	-1064981	155544.5	3060770	506142.262	408830.675	454483.879	248035.028	413269.75	559172.61	232214.61	440225.77
19.53125	5915.83	9366368.207	-11605949.9	1772542.6	2493020	-316039.4	832028.5	2496628	131225.348	89926.1151	162208.071	129788.52	104584.68	154313.81	218046.44	166169.48
29.296875	272816.81	9084395.216	-11495538	2076738.6	2645547	608688.6	1116937	3027764	105477.164	64718.0474	167335.804	76731.9993	126288.02	79607.597	140572.68	83630.151
39.0625	407668.54	9394102.698	-11408085.1	2140207.8	3752338	-318662.6	320218.4	4194562	115710.91	71254.1776	126900.185	92305.801	127270.77	87580.694	146134.11	79439.677
48.828125	84799.607	9547292.482	-11143491.5	2218332.8	4979301	-227263.1	505037.2	5964272	73319.5393	60468.8516	98237.4127	48594.7872	103681.85	98954.818	35591.828	90082.785
58.59375	795348.57	95508123.97	-11402438.9	2575194.7	8666040	-403366.9	832552.3	5914047	113189.095	92855.7935	126794.366	76305.5447	70454.296	74024.637	72254.664	62914.865
68.359375	475788.46	9667855.824	-11330246.5	2877811.7	6428836	116014.9	776321	7135915	102512.768	64812.112	131088.26	70851.3044	115004.55	79115.599	144519.71	86261.161
78.125	1039687.6	9648564.441	-11560250.7	2945376.3	7731135	-316444.4	78664.12	8034568	107168.873	66471.9336	96975.8035	58439.6233	90948.681	91221.566	67334.766	49964.903
87.890625	972000.49	9562848.213	-11723734.3	3589162	8271983	-373402.8	1217742	9415437	105245.4565	53887.8387	70975.36	73123.7769	79584.759	84553.563	99885.745	79793.911
97.65625	1129961.4	9419920.149	-11289417.6	3666021.9	9252676	-209446.2	822838.2	10107267	98154.7344	86568.8351	69642.1221	64430.0234	83070.057	76108.983	99972.442	66106.175
107.42188	-3945734	6006679.187	-16130341.6	1968677.6	7720347	-4431126	-245807.7	8264718	122050.989	87120.5807	205784.565	99139.2692	149341.76	72635.699	150662.25	76833.419
117.1875	1628833.2	9299118.138	-11997248.7	4463028.4	11320290	-197.1762	1010886	11876300	100766.722	47391.2127	105054.004	52984.1882	129900.81	76019.739	158488.81	89391.83
126.95313	1959058.3	9150743.841	-11987007.7	5149471.4	11542747	300290.1	1847660	12442584	75371.1316	67251.2023	77220.0774	43480.827	94598.368	60283.402	65737.516	49150.242
136.71875	2423199.9	9277669.35	-12691672.2	5573766.4	12429147	694793.1	1938702	13076054	72171.2637	56442.						

APPENDIX D: ESTIMATED PRESWIRL

This appendix details the calculation of the preswirl ratio from experimental measurements. Readings from the flowmeter, pressure sensor before the flowmeter, pressure sensor after the flowmeter, pressure sensor at the stator inlet, temperature at the flowmeter, temperature at the stator inlet, and the rotor speed are all converted to SI units and combined into calculating the preswirl ratio. The last equation provides variables for inserting measurement readings with US units.

Flowmeter actual volumetric flow (converted to SCFM):

$$[x_1]ACFM \rightarrow [x_1] \frac{P_A T_S}{P_S T_A} SCFM \quad (D1)$$

ACFM(Actual Cubic Feet per Minute)

SCFM(Standard Cubic Feet per Minute)

Converting average pressure between before and after flowmeter to Pascals:

$$[x_2]psig \rightarrow ([x_2] + 14.696)psia \rightarrow \frac{([x_2] + 14.696)(4.448222)}{(0.0254)^2} Pa \quad (D2)$$

Temperature at Flowmeter (converted to Kelvin):

$$[x_3]^{\circ}F \rightarrow ([x_3] + 459.67)^{\circ}R \rightarrow ([x_3] + 459.67) \frac{5}{9} K \quad (D3)$$

Assignment of variables:

$$\Rightarrow P_A = \frac{([x_2] + 14.696)(4.448222)}{(0.0254)^2} Pa \quad (D4)$$

$$\Rightarrow T_A = ([x_3] + 459.67) \frac{5}{9} K \quad (D5)$$

$$\Rightarrow P_s = 101325 Pa \quad (D6)$$

$$\Rightarrow T_s = 293.15 K \quad (D7)$$

Density for air at standard conditions:

$$\rho_s = \frac{P_s}{R T_s} \quad (D8)$$

Density for air at inlet (Brown pressure sensor):

$$\rho_I = \frac{P_I}{R T_I} \quad (D9)$$

Air specific gas constant:

$$R = 287.058 \frac{J}{kgK} \quad (D10)$$

Pressure at inlet (Brown sensor):

$$\Rightarrow P_I = \frac{([x_4] + 14.696)(4.448222)}{(0.0254)^2} Pa \quad (D11)$$

Temperature at inlet:

$$\Rightarrow T_I = ([x_5] + 459.67) \frac{5}{9} K \quad (D12)$$

Total area from 32 holes of the preswirl ring:

$$A = (32)\pi \left(\frac{0.130 * 0.0254}{2} \right)^2 m^2 \quad (D13)$$

Converting SCFM to $\frac{m^3}{s}$:

$$\frac{ft^3}{min} \left(\frac{12 \text{ in} * 0.0254 \text{ m}}{ft * in} \right)^3 \frac{min}{60 \text{ s}} = \left(\frac{12 * 0.0254}{60} \right)^3 \frac{m^3}{s} \quad (D14)$$

Fluid velocity normal to holes in preswirl ring:

$$V_N = SCFM \left(\frac{12 * 0.0254}{60} \right)^3 \rho_S \frac{1}{\rho_I A} \quad (D15)$$

Fluid velocity tangent to holes in preswirl ring:

$$V_T = V_N \sin(60) \quad (D16)$$

Combining pressures (P_A and P_S) and temperatures (T_A and T_S) in SCFM equation:

$$\begin{aligned} [x_1] \frac{P_A T_S}{P_S T_A} &= \frac{[x_1]([x_2] + 14.696)(4.448222)(293.15)(9)}{(0.0254)^2(101325)([x_3] + 459.67)(5)} \frac{ft^3}{min} \\ &= \frac{[x_1]([x_2] + 14.696)(4.448222)(293.15)(9)(12 * 0.0254)^3}{(0.0254)^2(101325)([x_3] + 459.67)(5)(60)} \frac{m^3}{s} \end{aligned} \quad (D17)$$

Metric volumetric flow:

$$\begin{aligned} &\Rightarrow \text{VolumetricFlow} \\ &= \frac{(4.448222)(0.0254)(9)(12)^3(293.15)[x_1]([x_2] + 14.696)}{(5)(60)(101325)([x_3] + 459.67)} \frac{m^3}{s} \end{aligned} \quad (D18)$$

Mass flow rate:

$$\text{Massflowrate} = \text{Metric volumetric flow} * \rho_S \quad (D19)$$

Combining volumetric flow with standard density:

$$\begin{aligned} &\text{Mass flow rate} \\ &= \frac{(0.0254)(4.448222)(9)(12)^3(293.15)[x_1]([x_2] + 14.696)}{(5)(60)(287.058)([x_3] + 459.67)} \frac{kg}{s} \end{aligned} \quad (D20)$$

Metric volumetric flow rate at inlet:

$$\text{Metric Volumetric flow at inlet} = \text{Mass flow rate} * \frac{1}{\rho_I} \quad (\text{D21})$$

Combining volumetric flow with density at inlet:

$$\begin{aligned} & \text{Metric volumetric flow rate} \\ &= \frac{(0.0254)^3(12)^3(293.15)[x_1]([x_2] + 14.696)([x_5] + 459.67)}{(60)(287.058)([x_3] + 459.67)([x_4] + 14.696)} \frac{m^3}{s} \end{aligned} \quad (\text{D22})$$

Fluid velocity from volumetric flow rate:

$$\text{Fluid velocity} = \text{volumetric flow rate} * \frac{1}{A} = V_N = \frac{V_T}{\sin(60)} \quad (\text{D23})$$

Combining equations for Fluid velocity:

$$\begin{aligned} & \text{Fluid Velocity} \\ &= \frac{(0.0254)^3(12)^3(293.15)[x_1]([x_2] + 14.696)([x_5] + 459.67)(4)}{(60)([x_3] + 459.67)([x_4] + 14.696)(32)(0.130)^2\pi} \frac{m}{s} \\ &= \frac{(0.0254)^3(12)^3(293.15)[x_1]([x_2] + 14.696)([x_5] + 459.67)}{\pi(60)([x_3] + 459.67)([x_4] + 14.696)(8)(0.130)^2} \frac{m}{s} \\ &= \frac{(0.0254)^3(12)^3(293.15)[x_1]([x_2] + 14.696)([x_5] + 459.67)}{\pi(0.130)^2(480)([x_3] + 459.67)([x_4] + 14.696)} \frac{m}{s} \end{aligned} \quad (\text{D24})$$

Tangent Velocity for fluid:

$$\begin{aligned} & V_T \\ &= \frac{(0.0254)^3(12)^3(293.15)[x_1]([x_2] + 14.696)([x_5] + 459.67) \sin(60)}{\pi(0.130)^2(480)([x_3] + 459.67)([x_4] + 14.696)} \frac{m}{s} \end{aligned} \quad (\text{D25})$$

Rotor speed converted into rad/s:

$$[x_6]rpm \rightarrow [x_6] \frac{rev}{min} * \frac{2\pi \text{ rad } min}{rev 60 s} \quad (\text{D26})$$

$$\omega = \frac{\pi}{30} [x_6] \frac{rad}{s} \quad (\text{D27})$$

Rotor surface speed:

$$V_R = R\omega \quad (D28)$$

$$\Rightarrow R = \frac{D}{2}m \quad (D29)$$

$$\Rightarrow D = 4.5125 \text{ in} = (4.5125)(0.0254) m \quad (D30)$$

Combining into Rotor Surface Speed:

$$V_R = \frac{(4.5125)(0.0254)}{2} \frac{\pi}{30} [x_6] \frac{m}{s} = \pi \frac{(0.0254)(4.5125)}{60} [x_6] \frac{m}{s} \quad (D31)$$

Preswirl equation:

$$Preswirl = \frac{V_T}{V_R} \quad (D32)$$

Combining Tangent Velocity and Rotor Surface Speed:

$$\begin{aligned} &= \frac{(12)^3 [x_1] ([x_2] + 14.696) ([x_5] + 459.67) \sin(60)}{\pi^2 (0.130)^2 (8) ([x_3] + 459.67) ([x_4] + 14.696) (4.5125) [x_6]} \\ &= \frac{(12)^3 [x_1] ([x_2] + 14.696) ([x_5] + 459.67) \sin(60)}{\pi^2 (0.130)^2 (4.5125) (8) ([x_3] + 459.67) ([x_4] + 14.696) [x_6]} \end{aligned} \quad (D33)$$

Resultant Estimate to Preswirl:

$$\begin{aligned} & \Rightarrow \text{Estimated Preswirl} \\ & = \frac{(12)^3 [x_1] ([x_2] + 14.696) ([x_5] + 459.67) \sin(60)}{\pi^2 (0.130)^2 (4.5125) (8) ([x_3] + 459.67) ([x_4] + 14.696) [x_6]} \end{aligned}$$

$[x_1] \rightarrow \text{Flowmeter}[ACFM]$

$[x_2] \rightarrow \text{Average pressure between before and after flowmeter}[psig]$

$[x_3] \rightarrow \text{Temperature at flowmeter}[^\circ\text{F}]$

(D34)

$[x_4] \rightarrow \text{Pressure Inlet(Brown pressure sensor)}[psig]$

$[x_5] \rightarrow \text{Temperature at Inlet}[^\circ\text{F}]$

$[x_6] \rightarrow \text{Rotor speed}[rpm]$

APPENDIX E: MASS FLOW CALCULATION

This appendix details the calculation of the mass flow rate from the flowmeter. Readings from the flowmeter, pressure sensor at the flowmeter, and the temperature sensor at the flowmeter are all converted to SI units and combined into calculating the mass flow rate. Equation (E13) provides variables for inserting measurement readings with US units.

Mass flow rate:

$$\text{Mass flow rate} = \rho_s * \text{Volumetric flow(SCFM)} \quad (\text{E1})$$

Standard Density Equation:

$$\rho_s = \frac{P_s}{RT_s} \quad (\text{E2})$$

$$\rightarrow P_s \rightarrow \text{Standard Air Pressure} \quad (\text{E3})$$

$$\rightarrow T_s \rightarrow \text{Standard Air Temperature} \quad (\text{E4})$$

$$\rightarrow R = 53.353 \frac{\text{ft lb}_f}{\text{lb}_m \text{ } ^\circ\text{R}} \rightarrow \text{Air Specific Gas Constant} \quad (\text{E5})$$

Flowmeter actual volumetric flow (converted to SCFM):

$$[x_1]ACFM \rightarrow [x_1] \frac{P_A T_s}{P_s T_A} SCFM \quad (\text{E6})$$

ACFM(Actual Cubic Feet per Minute)

SCFM(Standard Cubic Feet per Minute)

$$\rightarrow P_A \rightarrow \text{Flowmeter Absolute Pressure} \quad (\text{E7})$$

$$\rightarrow T_A \rightarrow \text{Flowmeter Absolute Temperature} \quad (\text{E8})$$

Converting Flowmeter reading ACFM to Actual Cubic Feet per Second:

$$[x_1] \frac{ft^3 \text{ min}}{\text{min } 60s} = \frac{[x_1] ft^3}{60 \text{ s}} \quad (\text{E9})$$

Converting Pressure Inlet psia to pounds-force per foot squared:

$$P_A = ([x_2] + 14.696)psia \frac{144in^2}{ft^2} = 144([x_2] + 14.696) \frac{lb_f}{ft^2} \quad (\text{E10})$$

Converting Temperature Inlet °F to °R:

$$T_A = ([x_3] + 459.67)^\circ R \quad (\text{E11})$$

Combining standard density and volumetric flow rate:

$$\begin{aligned} \text{massflowrate} &= \frac{P_s}{RT_s} [x_1] \frac{P_A T_s}{P_s T_A} \\ &= \frac{144}{(60)(53.353)} \frac{[x_1]([x_2] + 14.696)}{([x_3] + 459.67)} \frac{\frac{ft^3 \text{ lb}_f}{s \text{ ft}^2}}{\frac{ft \text{ lb}_f}{\text{lb}_m \text{ }^\circ R}} \\ &\approx \frac{1}{22.2304} \frac{[x_1]([x_2] + 14.696) \text{ lb}_m}{([x_3] + 459.67) \text{ s}} \\ &\approx \frac{1}{22.2304} \frac{[x_1]([x_2] + 14.696) \text{ lb}_m}{([x_3] + 459.67) \text{ s}} \frac{kg}{2.20462 \text{ lb}_m} \end{aligned} \quad (\text{E12})$$

Resultant Mass Flow Calculation:

$$\Rightarrow \text{MassFlowRate} \approx \frac{1}{49.0096} \frac{[x_1]([x_2] + 14.696) \text{ kg}}{([x_3] + 459.67) \text{ s}}$$

$[x_1] \rightarrow \text{FlowmeterReading}[\text{ACFM}]$

$[x_2] \rightarrow \text{FlowmeterPressure}[\text{psig}]$

$[x_3] \rightarrow \text{FlowmeterTemperature}[^{\circ}\text{F}]$

(E13)

APPENDIX F: PRESWIRL RATIO CALCULATION

This appendix details the calculation of the preswirl ratio from experimental measurements of the differential pressure sensor. Readings from the differential pressure sensor, pressure sensor at the stator inlet, temperature sensor at the stator inlet, and rotor speed are all combined into calculating the preswirl ratio. Equation (F21) provides variables for inserting measurement readings with US units.

Preswirl Ratio:

$$Preswirl = \frac{V_{Fluid}}{V_{Rotor}} \quad (F1)$$

Fluid velocity after it enters preswirl ring:

$$V_{Fluid} = \sqrt{\frac{2g\rho_w H_w}{\rho_a}} \frac{ft}{s} \quad (F2)$$

$$g = 32.174 \frac{ft}{s} \rightarrow gravity \quad (F3)$$

$$\rho_w = 1.94 \frac{slug}{ft^3} \rightarrow waterdensity \quad (F4)$$

$$H_w = [x_1] in \rightarrow water height measurement \quad (F5)$$

$$\rho_a = \frac{P_a}{R T_a} \frac{slug}{ft^3} \rightarrow air density \quad (F6)$$

Air Density Equation:

$$\rho_a = \frac{P_a}{R T_a} \frac{slug}{ft^3} \quad (F7)$$

$$\rightarrow P_a = ([x_2]psig + 14.696)psia = 144([x_2]psig + 14.696) \frac{lb_f}{ft^2} \quad (F8)$$

$$\rightarrow T_a = ([x_3]^{\circ}F + 459.67) ^{\circ}R \quad (F9)$$

$$\rightarrow R = 1717 \frac{ft * lb_f}{slug ^{\circ}R} \quad (F10)$$

$$\Rightarrow \rho_a = \frac{144([x_2]psig + 14.696) slug}{1717([x_3]^{\circ}F + 459.67) ft^3} \quad (F11)$$

Water Height:

$$\rightarrow H_w = \frac{[x_1]}{12} ft \quad (F12)$$

Combining variables into Fluid velocity:

$$V_{Fluid} = \sqrt{\frac{2g\rho_w H_w}{\rho_a}} = \sqrt{\frac{(2)(32.174)(1.94)(1717)[x_1]([x_3]^{\circ}F + 459.67)}{(12)(144)([x_2] + 14.696)}} \quad (F13)$$

$$\Rightarrow V_{Fluid} \approx \sqrt{\frac{(124.0405)[x_1]([x_3] + 459.67)}{([x_2] + 14.696)}} \frac{ft}{s}$$

Rotor surface speed:

$$V_{Rotor} = R\omega \quad (F14)$$

$$\rightarrow [x_4]rpm \rightarrow \omega = [x_4] \frac{rev}{min} * \frac{2\pi rad}{rev} \frac{min}{60 s} = \frac{2\pi}{60} [x_4] \frac{rad}{s} \quad (F15)$$

$$\rightarrow R = \frac{D}{2} in \frac{ft}{12 in} = \frac{D}{24} ft \quad (F16)$$

$$\rightarrow D = 4.5125 in \quad (F17)$$

$$V_{Rotor} = \frac{(4.5125)}{24} \frac{2\pi [x_4]}{60} = \frac{(4.5125)\pi}{720} [x_4] \frac{ft}{s} \quad (F18)$$

$$\Rightarrow V_{Rotor} \approx 0.01969[x_4] \frac{ft}{s} \quad (F19)$$

Combing Fluid and Rotor Velocity:

$$\frac{V_{Fluid}}{V_{Rotor}} = \frac{\sqrt{\frac{(124.0405)[x_1]([x_3] + 459.67)}{([x_2] + 14.696)}}}{0.01969[x_4]} \frac{\frac{ft}{s}}{\frac{ft}{s}} \quad (F20)$$

Resultant Preswirl Ratio Calculation:

$$\Rightarrow PreswirlRatio \approx \frac{50.7885 \sqrt{\frac{(124.0405)[x_1]([x_3] + 459.67)}{(12)(144)([x_2] + 14.696)}}}{[x_4]}$$

$[x_1]$ → *Water Height Measurement [inchesH₂O]*

$[x_2]$ → *Pressure Inlet [psig]*

$[x_3]$ → *Temperature Inlet [°F]*

$[x_4]$ → *Rotor Speed [rpm]*

(F21)