



46<sup>TH</sup> TURBOMACHINERY & 33<sup>RD</sup> PUMP SYMPOSIA  
HOUSTON, TEXAS | DECEMBER 11-14, 2017  
GEORGE R. BROWN CONVENTION CENTER

# Pelletizer Motor Bearing Damage Detection Based on Vibration Data

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# Abstract

This presentation provides a case study that pelletizer motor bearing damage on an extruder was detected from on-line remote monitoring vibration data. Though vibration level was well below the acceptable limit, its abnormal signatures warranted a shutdown action. It was then observed that for each bearing, the whole outer raceway was spalled circumferentially into a “washboard” pattern. This was caused by electrical corrosion or fluting due to poor insulation resulted from damaged insulating washers. After replacing the bearings with insulated ones , vibration level and signatures have then become normal ever since its restart.

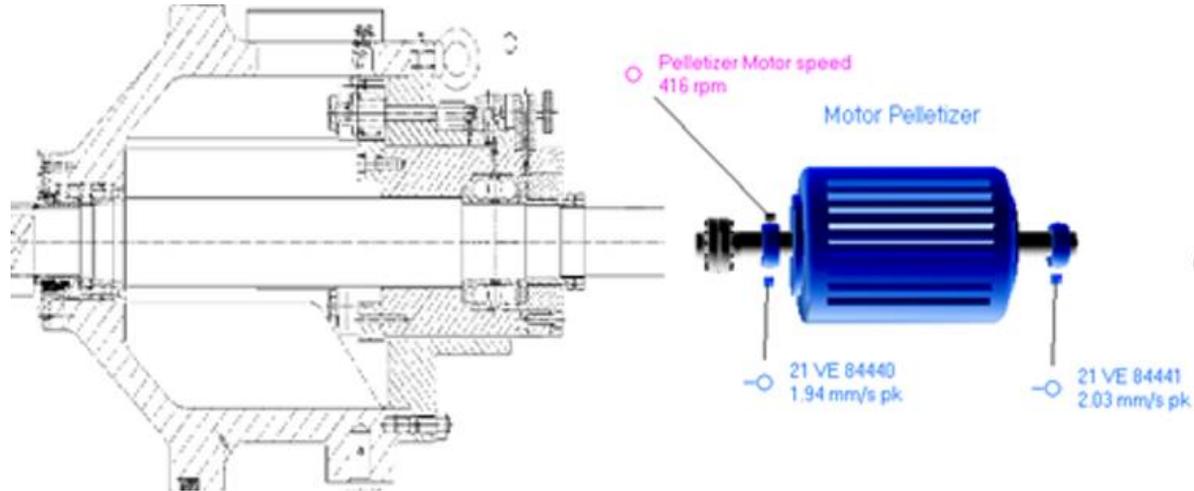


# Outline

- 1. Introduction**
- 2. Problem Statement**
- 3. Data Review**
- 4. Conclusions and Recommendations**
- 5. Inspection and Findings**
- 6. Resolution and Final Vibration Results**
- 7. Lessons Learned**

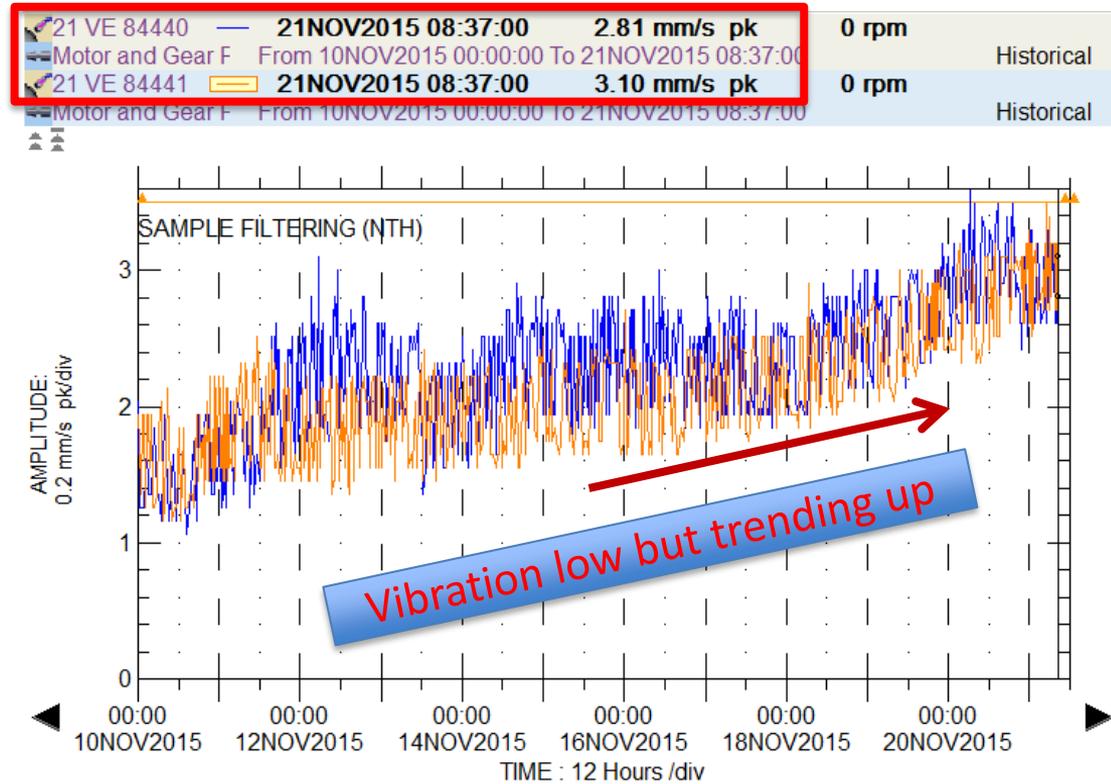
# 1. Introduction

- Pelletizer motor on an extruder
- Supported by two deep groove ball bearings
- Motor running at 350 ~ 390 rpm
- Vibration monitored by velocity transducers at each end of bearing housing



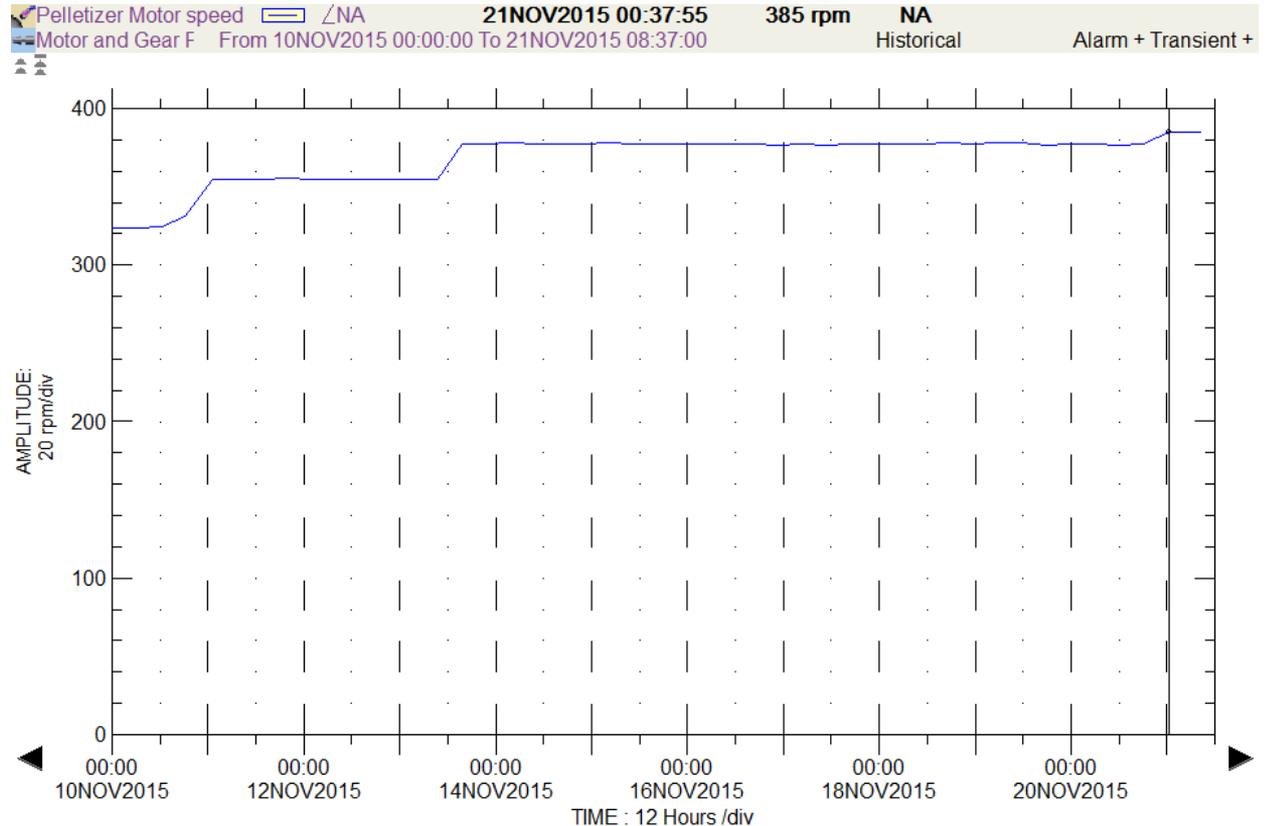
## 2. Problem Statement

- While reviewing high vibration data at other locations, vibration readings on motor bearings was found trending up.
- The motor vibration level was still within the acceptable limit, despite of trending up. Was there any problem?



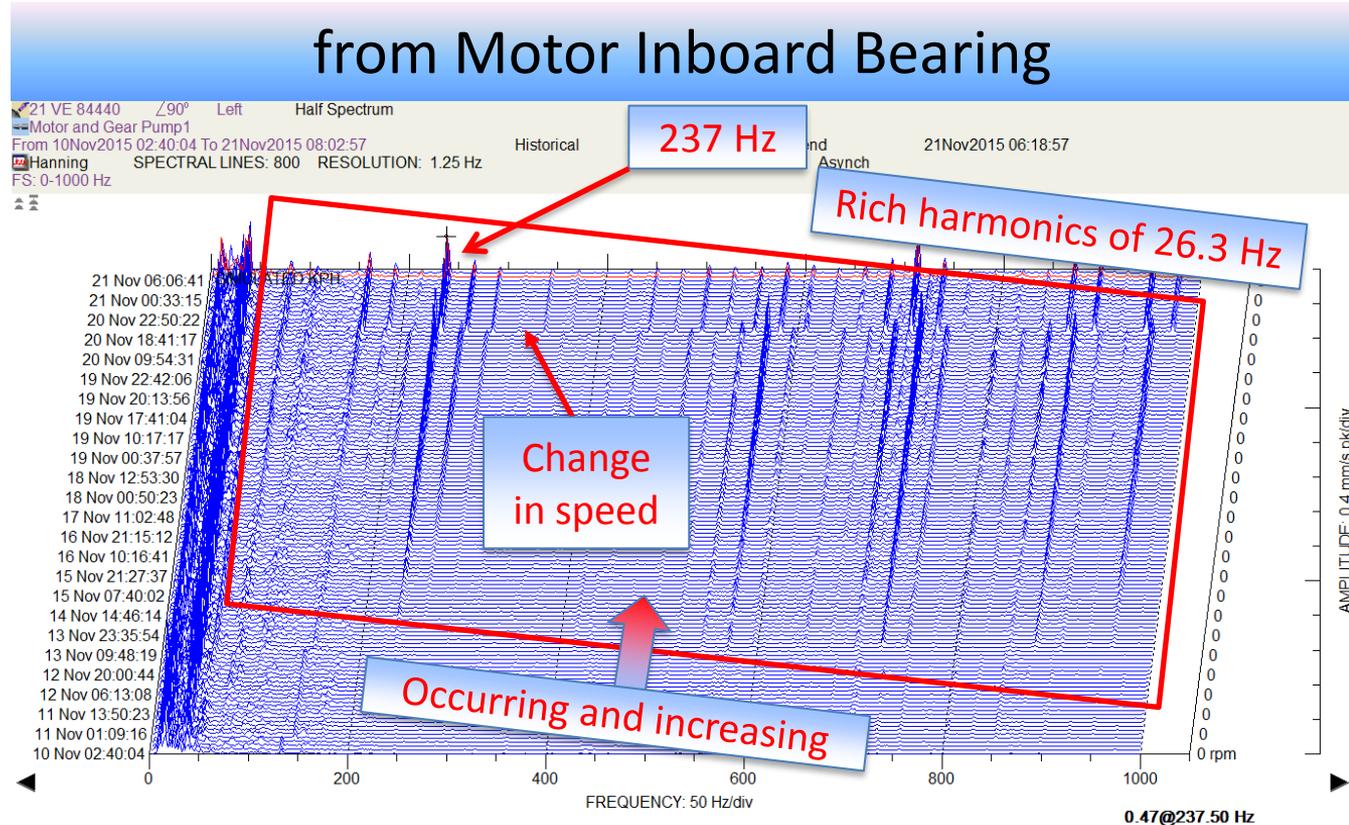
# 3.1 Data Review – Speed trend

- Stable in general, only varied with slight step changes
- 385 rpm used for bearing frequency calculation



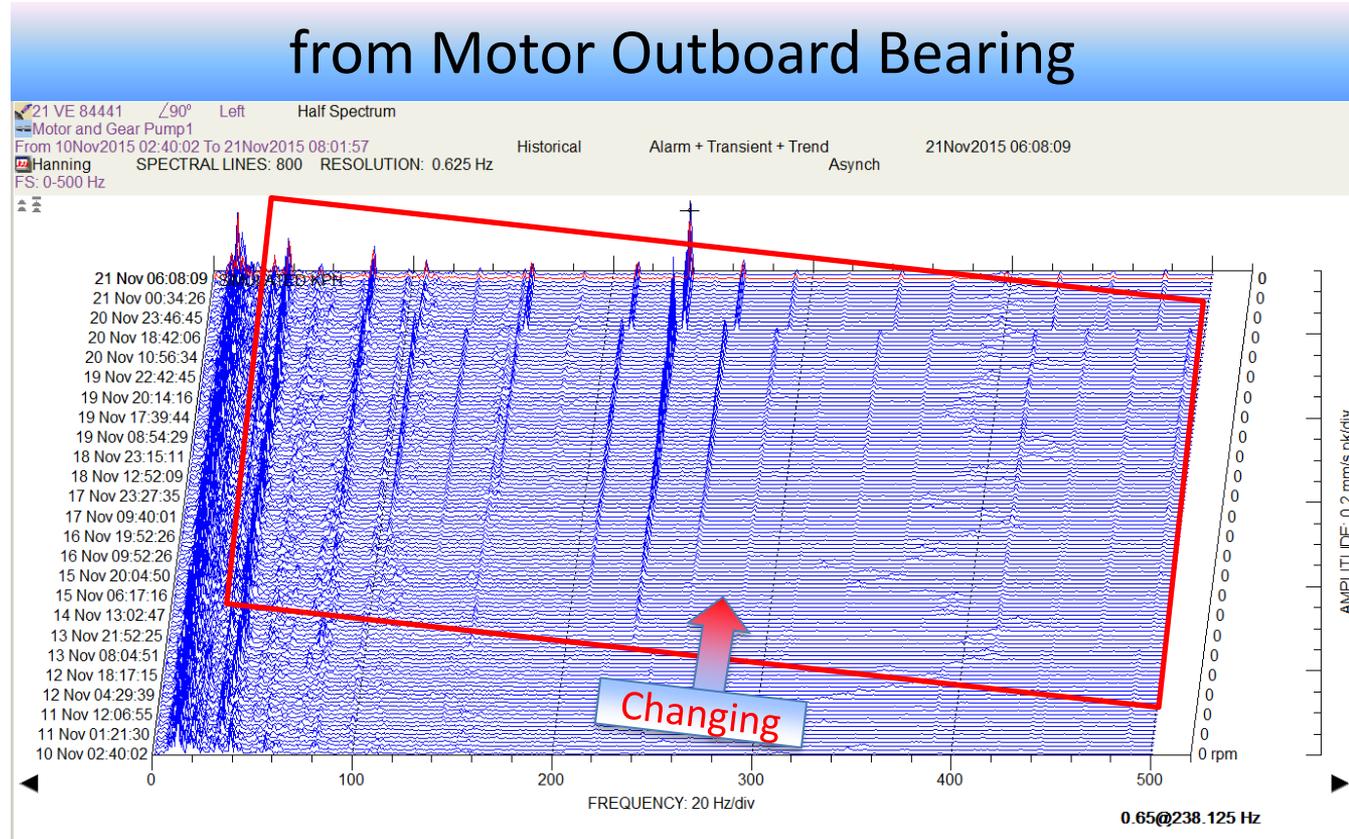
# 3.2 Data Review – Waterfall plot at Motor IB

- Harmonics or side bands appeared and significantly increased – abnormal.
- Highest peak at 237 Hz (~ 9 X 26.3 Hz), and rich harmonics of 26.3 Hz.



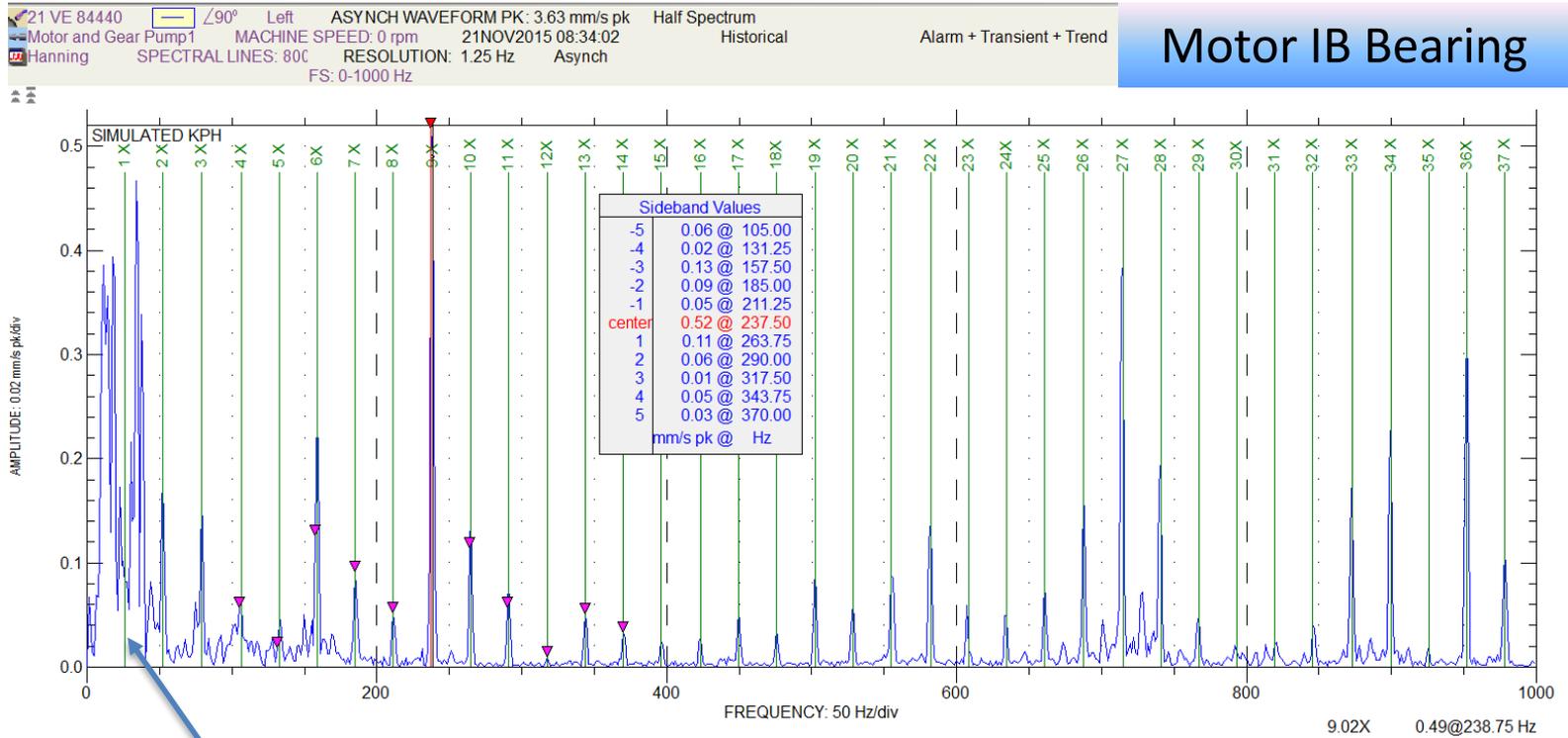
# 3.3 Data Review – Waterfall plot

Same signatures as those from inboard bearing



# 3.4 Data Review – Spectrum plot at 385 rpm

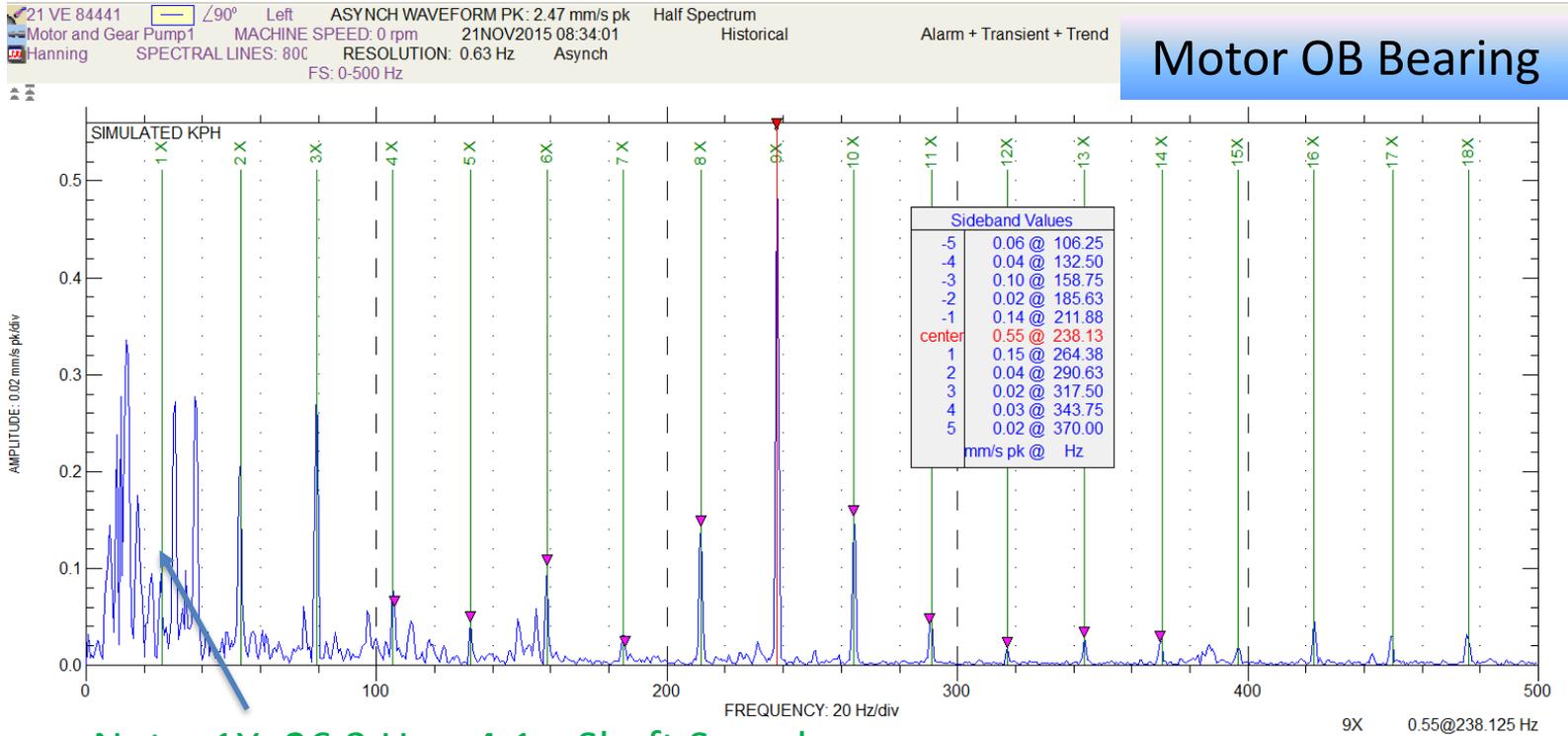
## Confirmation of rising vibration due to 26.3 Hz harmonics



Note: 1X=26.3 Hz = 4.1 x Shaft Speed

# 3.5 Data Review – Spectrum plot at 385 rpm

## Confirmation of rising vibration due to 26.3 Hz harmonics



# 3.6 Data Review – Bearing fault frequencies at 385 rpm

The measured 26.3 Hz matches the calculated Ball Pass Frequency Outer Race (BPFO).

## Bearing Data

- Measurement system:  Metric  Imperial
- Bearing type\*: DGBB
- Pitch diameter\*: 140 mm
- Rolling element diameter\*: 25.4 mm
- Number of rolling elements (per row)\*: 10
- Contact angle\*: 0.0 degrees
- Rotational speed\*: 385 rpm
- Rotating ring\*:  inner  outer

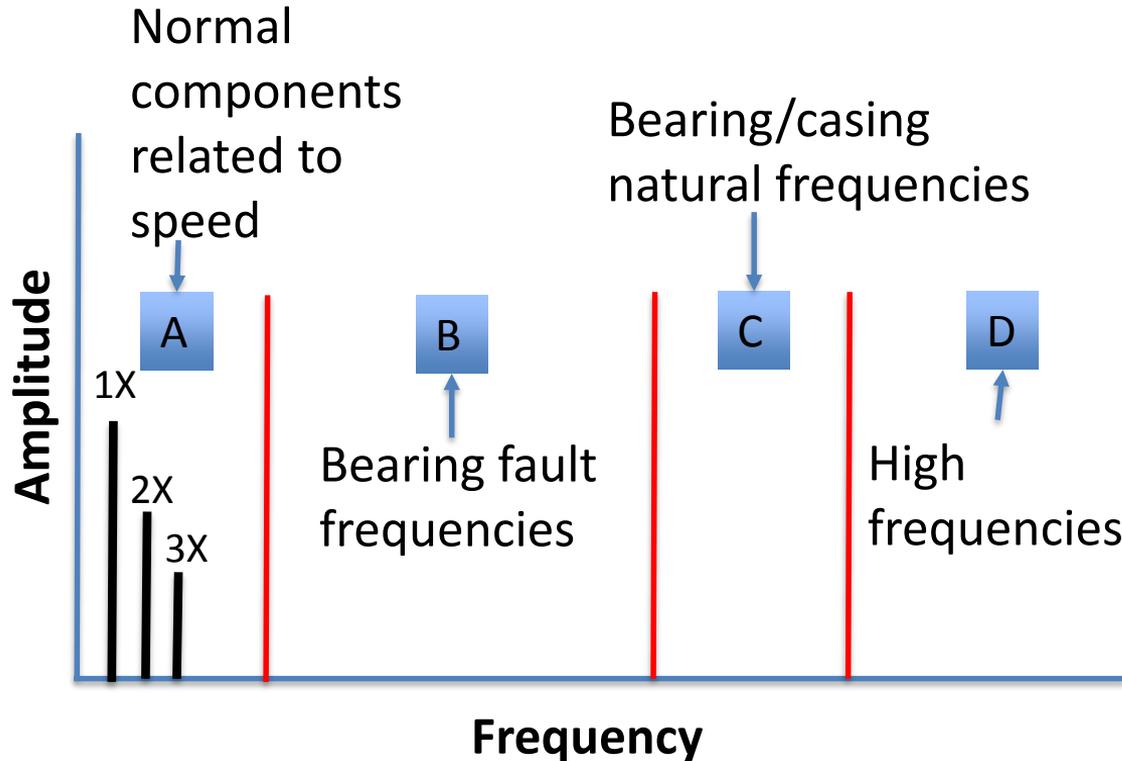
## Output

- Hertz  CPM  Orders
- Shaft speed frequency: 6.417 Hz
- Inner race defect frequency (BPFI): 37.904 Hz
- Outer race defect frequency (BPFO): 26.263 Hz**
- Cage defect frequency (FTF): 2.626 Hz
- Ball spin frequency (BSF): 17.102 Hz
- Rolling element defect frequency: 34.203 Hz

**Outer Race  
Damage  
Suspected!**

BPFO = 4.1 x shaft speed  
BPFI = 5.9 x shaft speed  
FTF = 0.4 x shaft speed  
BSF = 2.7 x shaft speed

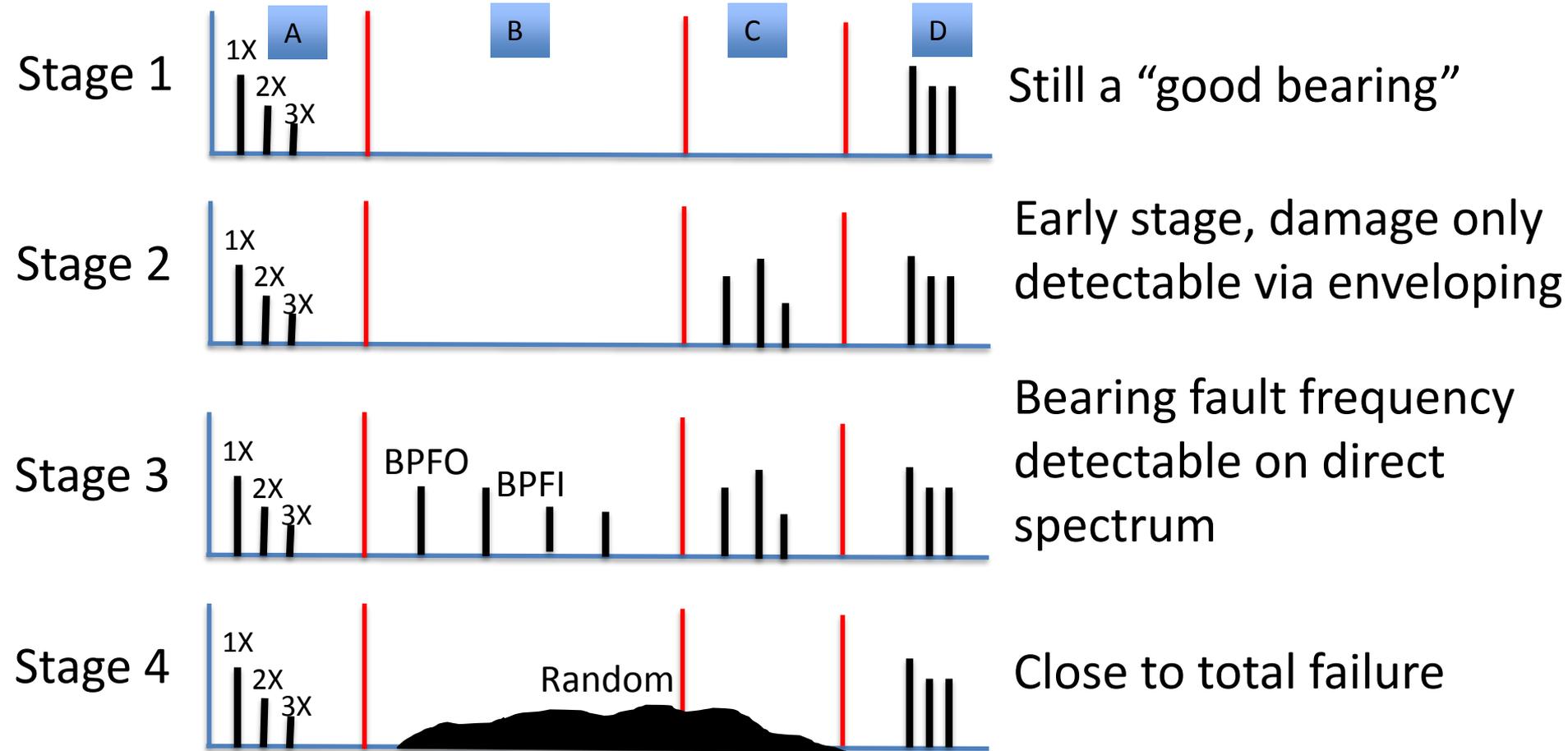
# 4.1 Conclusions and Recommendations



Four Stages of bearing life

- **Stage 1:** 10-20% life left, frequencies in Zone “A” & “D”
- **Stage 2:** 5-10% life left, frequencies in Zone “A” , “C” & “D”
- **Stage 3:** <5% life left, plus additional Zone “B” with bearing frequencies
- **Stage 4:** <1% life left, Zone “B” & “C” replaced with random noise.

## 4.2 Conclusion and Recommendation



## 4.3 Conclusions and Recommendations

After on-line remote data review and diagnosis, similar vibration signatures were measured via off-line portable devices. The following conclusions and recommendations were made:

- Conclusions:
  - Outer race damage occurred on motor bearings.
  - Became severe in a fast progression.
  - Bearing life in later Stage 3, towards Stage 4.
- Recommendations
  - Stop the machine within a few days
  - Inspect the two bearings to confirm the damage
  - Find the root-cause of the damage
  - Install the new bearings

**The motor was then shut down 3 days after the initial diagnostics & recommendation.**

# 5.1 Inspection and Findings



**“Washboard”** pattern across the entire outer race circumferentially, plus wear on inner race and dark discoloration on balls



## 5.2 Inspection and Findings

NDE Bearing Outer Race



Similar damages on  
NDE bearing

NDE Bearing Inner Race



NDE  
Bearing  
Balls



## 5.3 Inspection and Findings

**Insulated washers** damaged on **end cover** of NDE bearing



# 5.4 Inspection and Findings

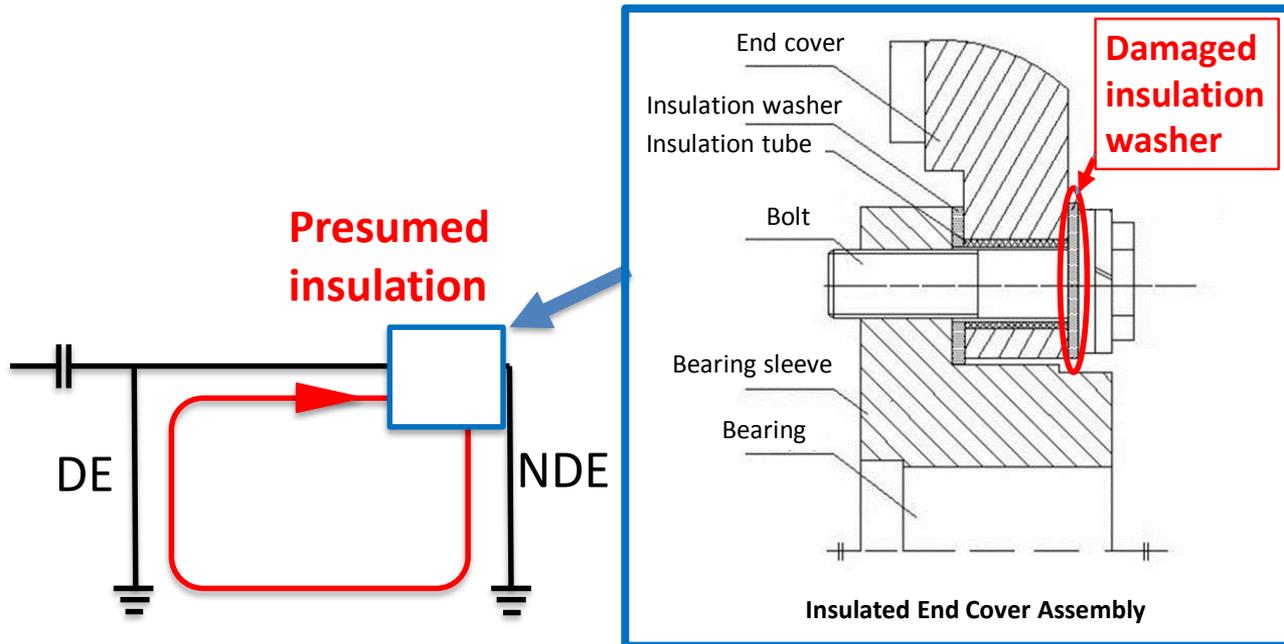
## Root cause of the bearing damage:

**Presumed insulation broken due to damaged insulation washers**



**Electrical Corrosion/Fluting**

The stator and rotor generate charge accumulation, which passes through the motor shaft to the bearings and discharges from the balls with enough energy to pit the race.



Insulated End Cover Assembly

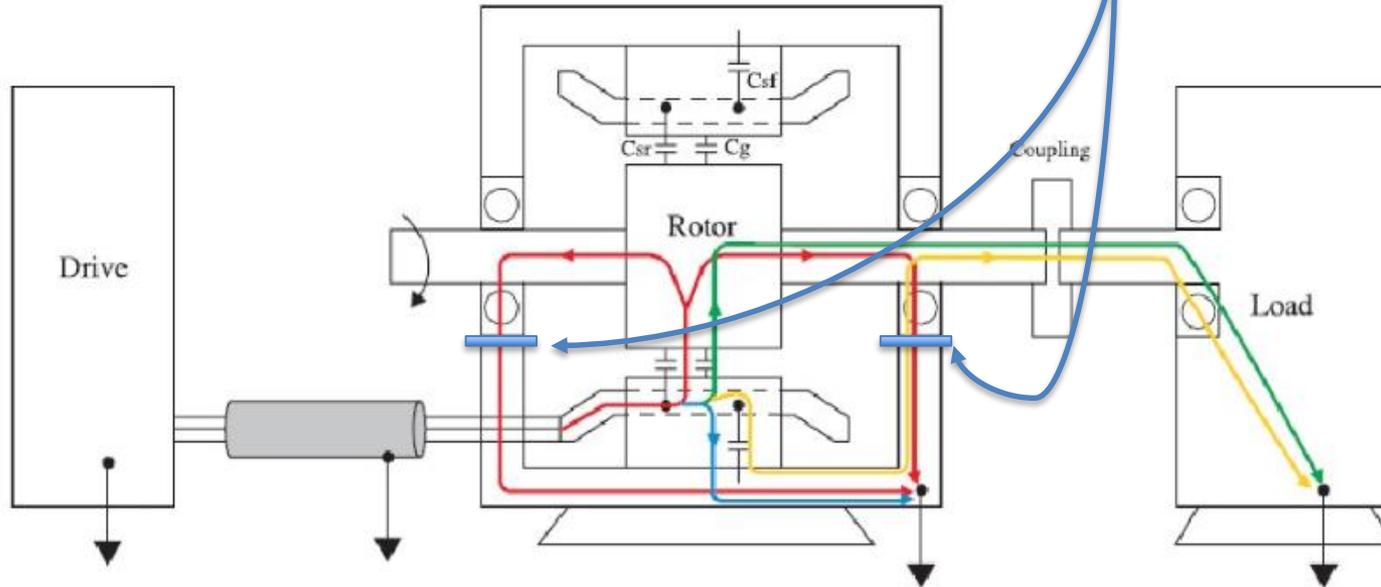
# 6.1 Resolution and Final Vibration Results

## Resolution:

Damaged bearings

Replaced by

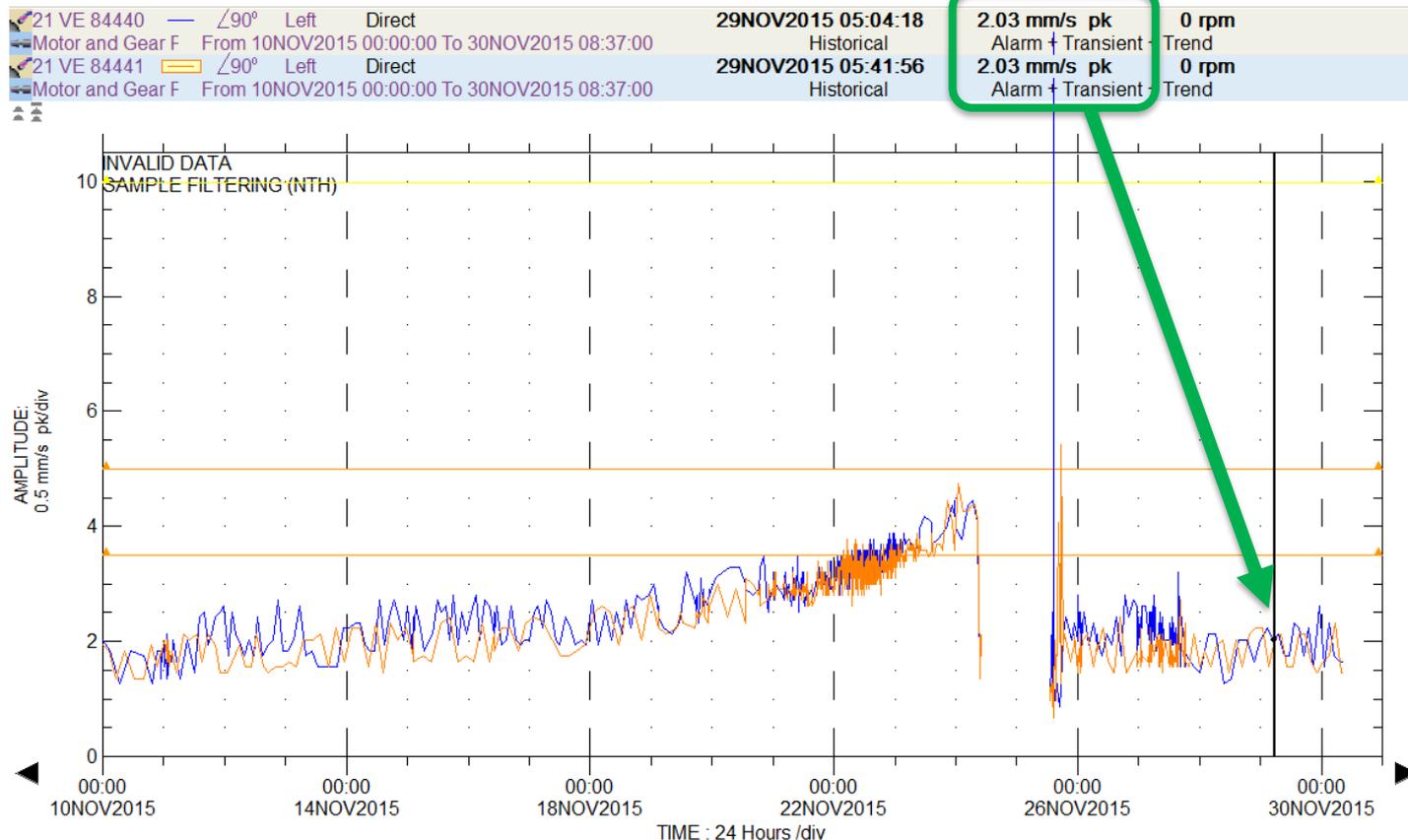
Insulated bearings



Aluminum  
oxide  
coated  
external  
surface of  
outer ring  
for  
electrical  
resistance

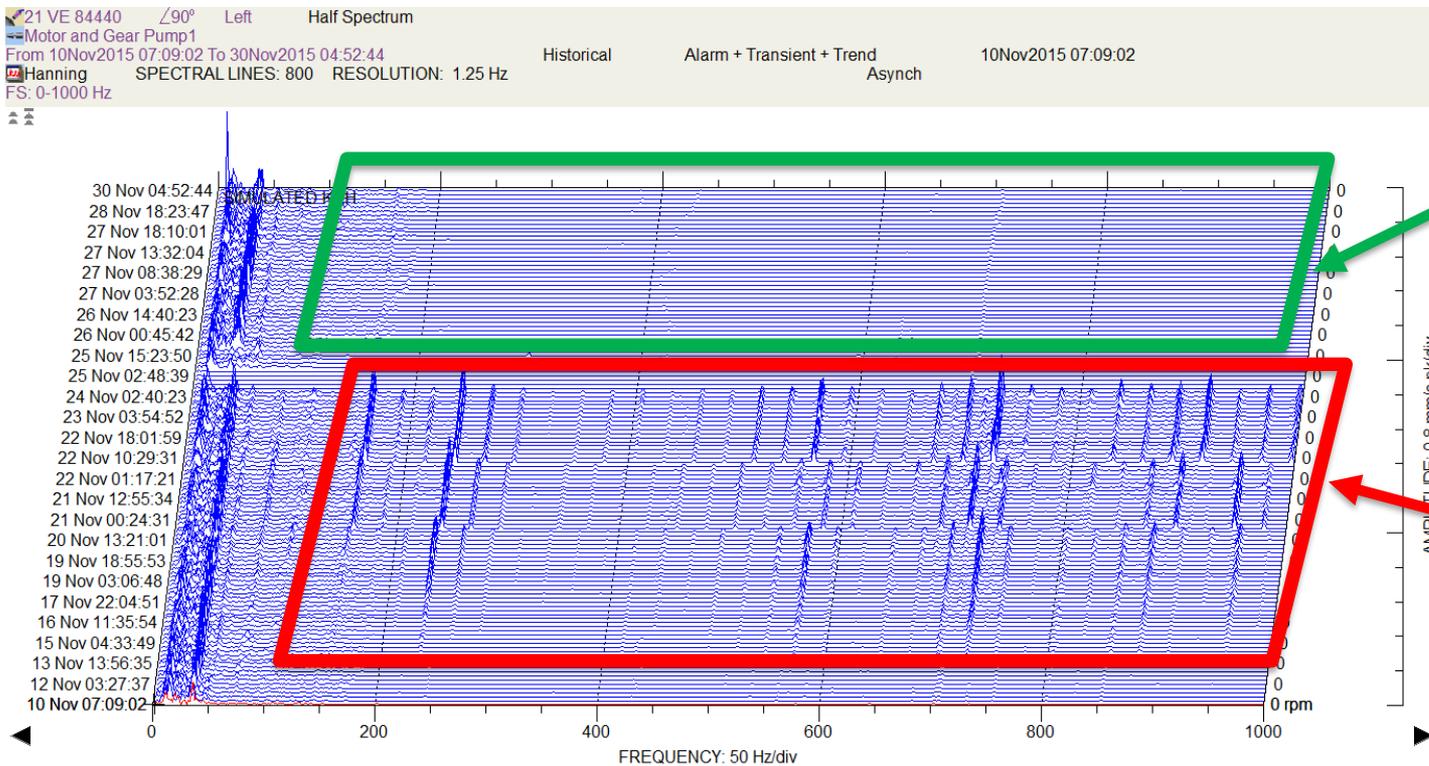
# 6.2 Resolution and Final Vibration Results

Vibration readings became low and stable.



# 6.3 Resolution and Final Vibration Results

Abnormal harmonics disappeared!



after

before

## 7. Lessons Learned

- Even if vibration is still within the acceptable level, it cannot warrant no malfunction. A change in vibration is more important than vibration level itself. Examining and understanding of the change are crucial to ensure a safe reliable operation of the machine.
- If the machine had continued its operation with the damaged bearings while maintaining electric arcing without knowledge, further deterioration would have led to complete bearing failure, and unscheduled equipment downtime and unanticipated maintenance costs would have likely followed. Electric corrosion can damage bearings very fast, and rolling elements can be welded to the raceways.