

**SIMULATION OF DISCRETE FRACTURE NETWORK
USING FLEXIBLE VORONOI GRIDDING**

A Dissertation

by

ZUHER SYIHAB

Submitted to the Office of Graduate Studies of
Texas A&M University
in partial fulfillment of the requirements for the degree of

DOCTOR OF PHILOSOPHY

December 2009

Major Subject: Petroleum Engineering

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Approved by:

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ABSTRACT

Simulation of Discrete Fracture Network Using Flexible Voronoi Gridding.

(December 2009)

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Chair of Advisory Committee: Dr. David S. Schechter

Fractured reservoirs are generally simulated using Warren and Root²⁶ dual-porosity (DP) approach. The main assumption of this approach is that the geometry of fractures are uniformly distributed and interconnected in reservoirs. This may be true for many cases of naturally fractured reservoirs. However, for a large scale and disconnected fractured reservoirs, DP is often not applicable. Due to the latter case, it is necessary to have more sophisticated simulation studies which allow the fracture to be geometry explicitly represented into the static model using Discrete Fracture Network (DFN) approach.

Most work on DFN grid model up to recently has been done with Delaunay tessellations. This research proposes an alternative technique to discretize the two-dimensional DFN using Voronoi diagrams, nevertheless applying the same DFN principles outlined in previous work.

Through complicated procedures to generate DFN model, grid system based on Voronoi polygons has been developed. The procedure will force Voronoi edges follow the exact geometry of fractures. Furthermore, implementing the Voronoi diagrams allows the use of fewer polygons than the traditional Local Grid Refinement (LGR). And most importantly, due to the nature of the Voronoi polygons or locally orthogonal grids, the transmissibility calculations can be simplified and are more accurate than corner point formulation for non-square grid blocks.

Finally, the main and most important goal of this study is to develop a black-oil Control Volume Finite Difference (CVFD) reservoir simulator that allows us to model

DFN more realistically. One of the features of the developed simulator is the capability to model individual fractures with non-uniform aperture distribution, such as log-normally distributed apertures as shown using X-Ray CT scanner measurements.

Prior to using the DFN simulator to model reservoirs with fractures and their apertures distribution, the simulator was validated against commercial simulators. The simulator provides results in close agreement with those of a reference finite-difference simulator in cases where direct comparisons are possible.

Several simulations of synthetic DFN were presented to demonstrate the robustness of the Voronoi diagrams to represent fracture networks and its aperture distributions. In summary, the simulation of the DFN using the proposed approaches is capable to model both fractured and unfractured systems. However, the DFN model with Voronoi grids requires more efforts on building the grid model compared to other methods. Numerically, simulations of fractured systems are very challenging.

DEDICATION

My graduate studies at Texas A&M University would not have been possible without the help from God and prayer of my parents and family members.

This dissertation is dedicated to:

My late mother, Budur Syihab,

My late father, Ali Syihab,

My brothers and sisters,

I want to give my very special dedication to my beautiful wife, *FNU Hanifah* for her sacrifices and patience while accompanying me in the most challenging times during this journey.

ACKNOWLEDGMENTS

I would like to express my highest gratitude to my research advisor, Dr. David Schechter for his ideas, encouragement, patience and financial support through research assistantship during this study. The sources of the assistantship were from DOE (2003-2006) and Crisman Institut (2007-2008).

My appreciation is also extended to members of the reading committee, Dr. Wattenbarger for his direction in some of the contents of this dissertation, Dr. Maggard for his introduction to simulation through his class and Dr. Efendiev for his comments in some areas of this research.

My special thanks to Erwin Putra and his family for their support in many ways. Putra has been my discussion partner, especially at the early stage of this research. The support from him and his family will never be forgotten.

I would like to thank my friends Darmo and his family, Jooned, Siswo, Fitrix, Rifky, Moses, Vaibhav, Kalwant, Roly Simangunsong, Moses, Pahala, Koko and many others for their friendship during my stay in Texas.

Finally, I would like to thank my family for their continuous support, encouragement and love. This dissertation is dedicated to my wife, Hanifa, parents, brothers and sisters. Without their support and prayers this work would not have been possible.

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CHAPTER I

INTRODUCTION

1.1 Research Background

Dual-porosity (DP) models to represent fractured reservoirs were pioneered in the early sixties by Warren and Root¹. This method has been used extensively and is the most widely applied model to simulate flow through porous media in a fractured reservoir. This approach has some important limitations which are due to the mathematical and geometrical formulations. Dual-porosity formulation represents fractured reservoirs as an array of parallelepiped matrix blocks interspersed by a set of uniform orthogonal connected fractures (**Fig. 1.1**).

The flow in DP models is dominated by a large number and small-scale fractures. Transfer functions between matrix and fractures in DP are evaluated based on the idealized fracture geometry introduced by Warren and Root. Therefore, DP models are not well suited to model a realistic fracture network^{2,3}.

Reservoir simulation involves application of numerical methods to model a system of conservation laws to describe flow in a porous medium in the form of linear discretization. The results of a reservoir simulation model are clearly dependent upon the computational grid and the geometrical representation⁴. The most common gridding system used in the reservoir simulation is the regular Cartesian grid system. The grids are generally non-aligned with reservoir heterogeneities, such as faults, fractures and consequently are not able to provide an accurate representation of those valuable properties.

Studies on fracture networks and its properties have recently advanced in many aspects due to improvements in areas such as computational power, advances in reservoir

This dissertation follows the style of *SPE Journal*.

description technology and laboratory experiments of fracture apertures distribution. All these aspects have created the opportunity for improved modeling and ultimately, better understanding of the behavior of flow in fractured systems. Thus the need for a more robust simulation tool is unarguably necessary.

In light of those limitations (the gridding technique to accurately represent fracture geometry and the capability to model fracture aperture distribution) and in contending with the advancements in fracture networks, discrete-fracture modeling (DFN), a tool which represents fractures individually along with flexible gridding techniques is required to model complex fractured porous medium.

Although some attempts in this area have been pursued, the utilization of Voronoi grid systems, particularly to represent fracture networks and its aperture distributions provided by laboratory experiments (X-Ray CT Scan) has not been yet investigated.

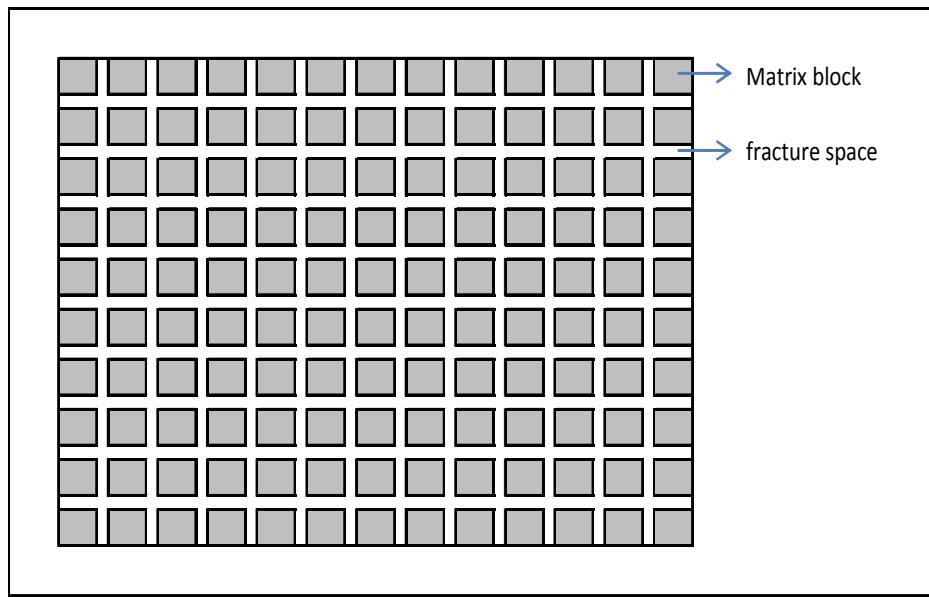


Fig. 1.1-Dual-porosity model¹

1.2 Literature Review

In this section, important works related to the topics developed in this thesis are briefly discussed. It consists of historical background about reservoir simulation, gridding techniques, DFN modeling, and fracture aperture measurements using X-Ray CT Scanning. Some specific aspects that need a more thorough discussion are presented in chapters where the corresponding topics are studied.

1.2.1 History of Reservoir Simulation

The evolution of reservoir simulation can be traced back to the 1950's. It was initiated by Aronofsky and Jenkins's radial gas flow model⁵. Over the past fifty years, reservoir simulation has rapidly developed in physical and mathematical models, discretization methods, linear equations solvers, pre-processing, post-processing and reservoir visualization. The physical models were developed from the simplest model of 1D, one-phase into 3D, three-phase complex models, such as the black oil, pseudo-black oil, compositional, chemical, thermal, dual-porosity/dual-permeability models and most recently, discrete fracture models (DFN).

The discretization methods developed earlier used finite difference (FD) methods^{4,6} with rectangular parallelepiped grids to more sophisticated methods with unstructured grids, such as mixed finite element methods⁷ (MFEM), control volume finite element (CVFE) method and the Perpendicular Bisection (PEBI) method^{8,9}.

Solving a linear system of equations initially was implemented using direct solver, Gaussian elimination method. It has been further improved into Gaussian elimination method and sparse Gaussian elimination method¹⁰. The iterative methods have also developed, such as slice and line successive over relaxation methods (SSOR and LSOR). Stability and convergence problems in iterative methods¹⁰ have been reduced or solved using the preconditioned conjugate-gradient-like method, orthogonal minimized residual error (ORTHOMIN) method¹¹, Conjugate Gradient¹², stabilized Bi-conjugate-gradient

(BICG-STAB) and general minimized residual error (GMRES) method⁷. These iterative methods combined with the linear equations preconditioner have become popular and well suited to solve complex engineering problems such as finite difference and finite element applications.

The pre-processing technique has improved from data card preparation to automatic grid generation based on geological structure and well completions. The post-processing has enhanced from static 2D visualization into dynamic 3D visualization. The software scale has also improved from small packages to large platforms, which allows the integration of various data, such as geological, geophysical, reservoir simulation, oil field management, risk analysis, sensitivity, and optimization.

Several factors need to be taken into account to carry out a reservoir simulation. These include the size and type of reservoir, software packages, data availability, objectives, computer hardware, computing cost and time limit. In the early development period of reservoir simulation, computer associated factors are the crucial factors to be considered due to the speed limit of CPU and size of memory.

However in recent time, the capacity of computer hardware has improved. Computer's processors are very fast, memory is inexpensive and therefore, the size of simulation models have increased from hundreds and thousands to millions in the number of grid blocks.

1.2.2 Gridding Techniques

Well completion techniques, such as non-conventional wells and the increasing requirements on the accuracy of history matching require a fine scale reservoir simulation model. The finite difference (FD) method is a mature and widely implemented technique for black oil, compositional, thermal, and chemical simulation. FD is strictly limited for structured grids¹², i.e., a rectangular grid in 2D and parallelepiped grid in 3D. The structured grids cannot efficiently represent the irregular geological complexity of a

reservoir, such as faults, fractures, irregular boundaries, pitchouts and deviated wells. Therefore, various unstructured or flexible gridding techniques⁸ have been developed to reduce the limitations. There are several gridding techniques found in the literature; this section will briefly review some of the most well-known and widely applied gridding techniques.

1.2.2.1 Globally Orthogonal Grid

The rectangular and parallelepiped grids known as Cartesian grids are used in the two and three dimensional spaces respectively. They are globally orthogonal and have regular structures. There are two kinds of Cartesian grids which are commonly adopted in the reservoir simulation; point-distributed and block-centered grid⁵ (Fig. 1.2). The latter one is widely used, since it is easier to generate the grid system.

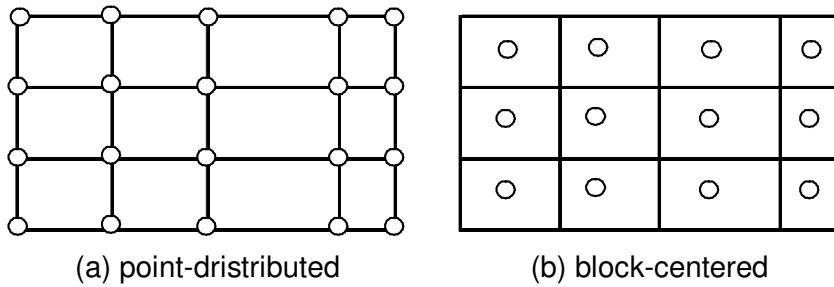


Fig 1.2-Globally orthogonal grid systems

1.2.2.2 Corner Point Grid

In order to accurately represent the complexity of geometrical features of reservoir structure, the vertices of grid blocks are first set and then the corresponding grid points are determined (**Fig. 1.3**). Although this kind of gridding is able to accurately represent the complicated geometrical features of reservoirs, the connection line between two neighboring nodes is not necessarily orthogonal to the interface between them. The flux in

and out of such grids should be corrected or projected to the primary axes (W-E, S-N). Thus, the flux in or out of the gridblock boundaries cannot be accurately calculated³.

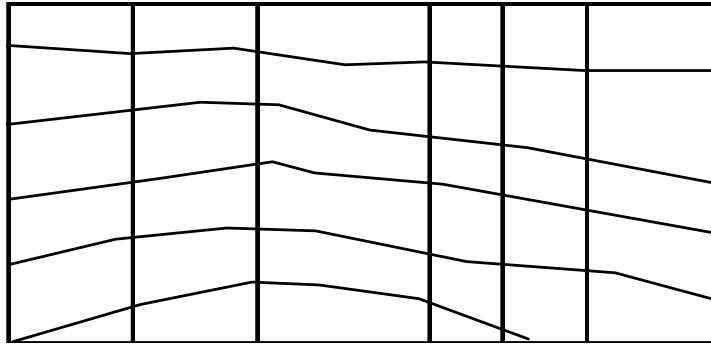


Fig. 1.3-Corner point grid

1.2.2.3 Locally Orthogonal Grid

The locally orthogonal grid is also known as the Voronoi grid. It has property that the connection line between two neighboring nodes is orthogonal to the interface between them (**Fig. 1.4**).

It was first applied by Heinrich in a reservoir simulation⁷ model. Heinemann named this grid a PEBI grid⁸, since a grid block consists of perpendicular bisectors of the triangle which have the common vertices (known as Delaunay triangle). He presented a k-orthogonal PEBI grid which has not been widely applied. Furthermore, Palagi also studied the PEBI grid generation method, applied the grid model into black-oil reservoir simulations¹³, and demonstrated the use of PEBI grid to reduce grid orientation effect, modelling horizontal well and etc. Economides applied PEBI grid to model horizontal wells¹⁴. Research results have shown that PEBI is a flexible grid that better handles complicated reservoirs. Recently, Chong et al.¹⁵ has shown that a kind of PEBI grid (hybrid grid) effectively reduces grid orientation effects. However, the structure of the matrix coefficients used to solve for the unknowns at nodes becomes quite complicated, and so it needs to use more efficient linear equation solution techniques.

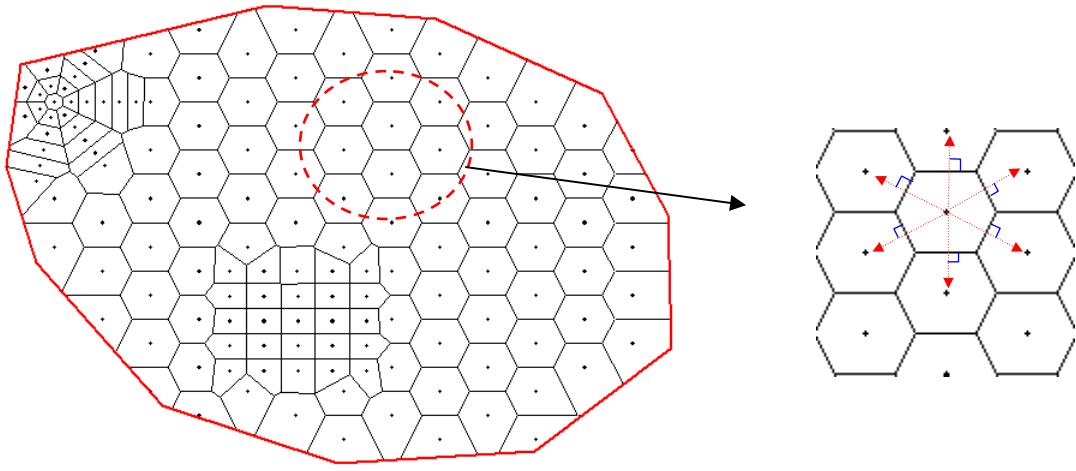


Fig. 1.4-Voronoi grid (locally orthogonal grid)

1.3 Introduction to Discrete Fracture Network Simulation

DFN was mainly used in attempts to directly model the fractures as an integrated media, not as an additional porous media in reservoirs as with Warrant and Root's dual-porosity concepts. The rock properties are the only factors to distinguish between fractures and matrix blocks. This model allows us to conduct simulations without coupling matrix and fracture media as was done in previous models. In addition, it makes it possible to directly model both matrix-fracture interactions and inter-fracture flow in porous media.

Studies on DFN can be traced back to the early 1980's. Researchers such as Noorishad et al.¹⁶ applied the technique. They investigated the pressure distribution along fractures using upstream Finite Element Method (FEM). Further enhancements for general petroleum engineering applications were made by Karimi-Fard and Firoozabadi². They used a Finite Element approach to avoid problems due to very small volumes of fractures compared to matrix blocks. Their DFN grid model used a Delaunay tessellation to align the block edges on the fractures. Meanwhile, Aziz et al.³ aggressively worked on a general

framework to apply finite difference discretization techniques to model the DFN more widely. He called the approach the Control Volume Finite Difference (CVFD). A few years earlier, Pruess¹⁷ used a similar concept for geothermal applications and called the method Integration of Finite Difference (IFD).

1.4 Introduction to Fracture Aperture Measurement Using X-Ray CT Scanner

Computed tomography (CT) is a medical imaging method employing X-Ray tomography. Digital processing is used to generate a three-dimensional image of the inside of an object from a large series of two-dimensional X-ray images taken around a single axis of rotation¹.

In the field of petroleum engineering, one of the applications of X-ray CT scanner is to measure variation of fracture apertures. Since there is no direct calculation from the images of fracture aperture data extracted from the CT scanner, a calibration curve needs to be established. This method was introduced by Muralidharan¹⁸. Initially, a rock is artificially fractured and different sizes of feeler gauges placed inside the fractures. Based on the known sizes of fillers, a graph of CT number vs. aperture along the perpendicular to the fracture was calibrated (**Fig. 1.5**). Images were taken every 1 mm up to 60 mm.

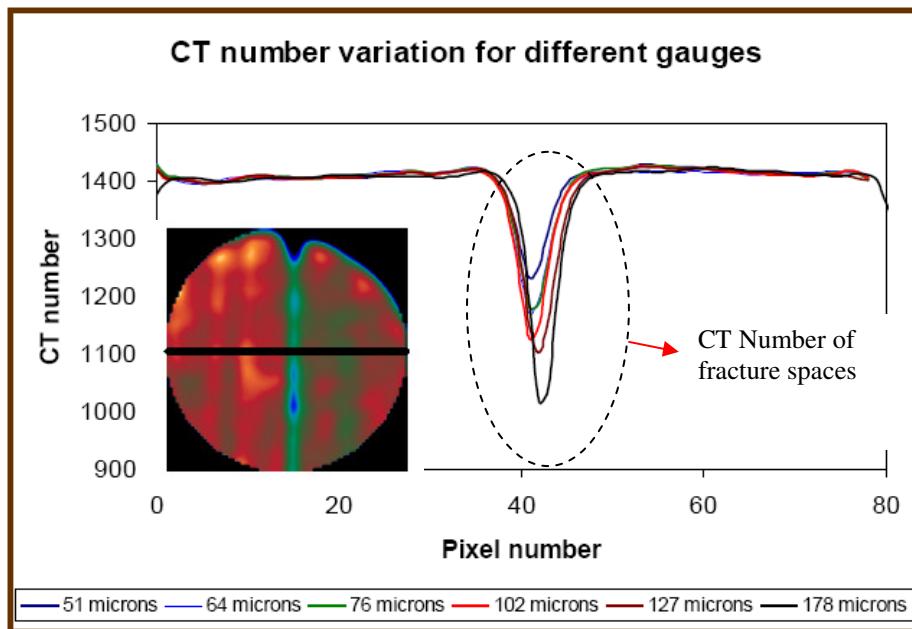


Fig. 1.5: CT Number from different feeler gauges (after Muralidharan et al.¹⁸)

The calibration curve is basically the width used to keep the fracture open vs. the area under the curves (**Fig. 1.6**). Based on the calibration curve, one could determine the relation between fracture aperture and the integration of the CT signals along the fracture.

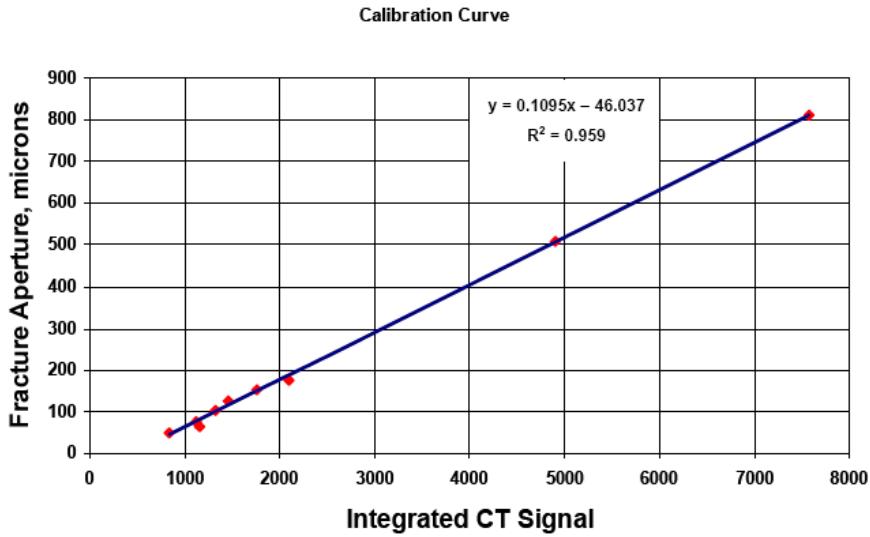


Fig. 1.6-Calibration curve to measure fracture apertures (after Muralidharan et al.¹⁸)

With the extensive work done on the fracture aperture measurements, the ability to couple the information on fracture geometry derived with the X-Ray CT scanner and numerical flow simulation has not yet been honored in any reservoir simulation studies.

1.5 Research Objectives

The main objective of this research is to develop methodology to model vigorously fluid flow in complex reservoir geometry with or without fractures in the system. The term “vigorously” here means that the fractures are represented explicitly as an integrated porous media, not a separate or virtual media as in the dual-porosity model. In order to achieve this main goal, the following steps have to be conducted in this research:

1. Developing a general flexible mesh generation technique based on Voronoi diagram algorithm.

2. Developing a 3D, three-phase black-oil reservoir simulator that is capable of modeling fractured and unfractured systems using control volume finite difference approach.
3. Comparing and benchmarking the developed DFN simulator against various simulators (commercial and academic simulators) and analytical solutions.
4. Honoring experimental work by incorporating fracture aperture distribution as determined by X-Ray CT scanning.
5. Performing simulation of a system with complex intersecting fractures and fracture networks generated using fractal approach¹⁹.

CHAPTER II

VORONOI DIAGRAM AND DISCRETE FRACTURE NETWORKS

2.1 Voronoi Diagram and Delaunay Triangulation

Simple Voronoi diagrams were initially employed as early as 1644 by Descartes. First comprehensive formulations of Voronoi diagrams were developed by Peter Dirichlet and Georgy Fedoseevich Voronoi. These diagrams consist of a polygon with all edges equidistant between the center point and neighboring points. Voronoi proposed the general case of the Voronoi diagram in 1908²⁰.

The Voronoi grid is considered to be the dual structure of the Delaunay triangles (DTs) formed by a given set of nodes in a plane. For a given set of nodes, Delaunay triangles are constructed by connecting the nodes in close proximity into triangles.

The *Delaunay triangulation* is a collection of edges satisfying an "empty circle" property²¹: a unique circle passing through three vertices of a triangle that does not contain any other points in the system. **Fig. 2.1** shows an example of the correct DTs with an "empty circle" property and incorrect triangles.

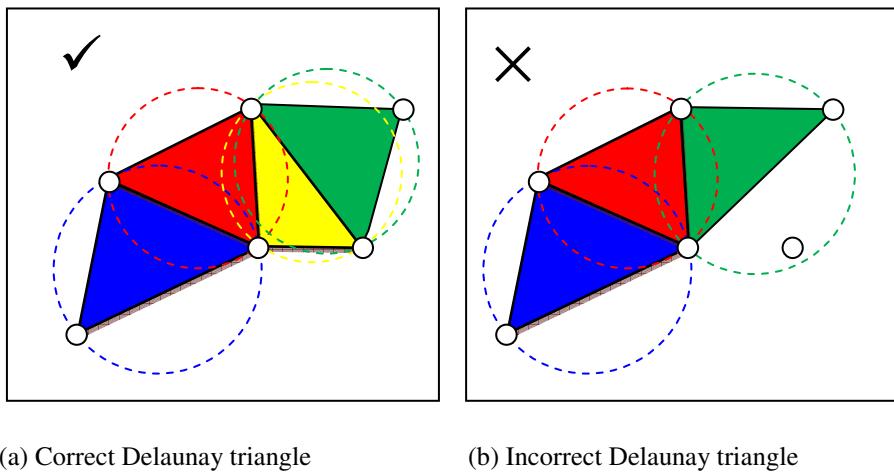


Fig. 2.1-Delaunay triangulation and “empty circle” property

The Voronoi grid is formed by the perpendicular-bisectors of the edges of the DTs. Due to this property, the Voronoi grid is also called perpendicular-bisector (PEBI) grid⁹.

2.1.1 Delaunay Tessellation Algorithm

Many Voronoi algorithms exist abundantly in the literature²²⁻²⁴ which mostly include the Delaunay tessellation algorithms. In general, the initial step to generate Voronoi polygon is essentially to build a Delaunay tessellation. A simple procedure in this study has been implemented to build DTs. The procedure contains the following steps:

1. Store nodes/points in 2D Cartesian coordinate, (X_i, Y_i) , (X_{i+1}, Y_{i+1}) , ..., (X_N, Y_N) . N is total number of nodes in the system.
 2. Select a node/point arbitrarily, (X_j, Y_j) , where $j \in \{i, N\}$
 3. Find the closest point to the point selected from step-2, (X_{j+1}, Y_{j+1}) .
 4. Draw a line from (X_j, Y_j) to (X_{j+1}, Y_{j+1}) . This line will be the first DT's edge/vertex.
 5. Search for a point (X_k, Y_k) , where $k \neq j$, $k \neq j+1$ and $k \in \{i, N\}$ such that the triangle satisfy the “empty circle” property of DT.
 6. Repeat step 4 and step 5 until no unique DT found in the system.

In order to determine whether the “empty-circle” property is satisfied, first we need to determine the center, (X_c, Y_c) and the radius, r of a circle by given three points $P_1(x_1,y_1)$, $P_2(x_2,y_2)$ and $P_3(x_3,y_3)$ on a plane (**Fig. 2.2**).

Two lines are formed; the first line, L_1 passes P_1 and P_2 . The second line, L_2 passes P_2 and P_3 . The equations of those lines are:

where, m_{L1} and m_{L2} are the slopes of L_1 and L_2 respectively.

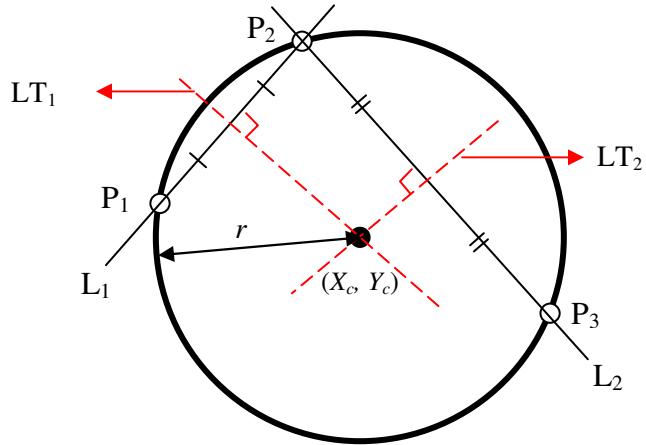


Fig. 2.2- A circle that passing through three points, P_1 , P_2 and P_3 on a plane

The centre of the circle basically is the intersection of the two lines perpendicular to and passing through the midpoints of the lines L_1 and L_2 . These lines are named LT_1 and LT_2 and expressed by the following equations:

$$y_{LT_1} = -\frac{1}{m_{L_1}} \left(x - \frac{1}{2}(x_1 + x_2) \right) + \frac{1}{2}(y_1 + y_2) \dots \quad (2.3)$$

$$y_{LT_2} = -\frac{1}{m_{L_2}} \left(x - \frac{1}{2}(x_2 + x_3) \right) + \frac{1}{2}(y_2 + y_3) \dots \quad (2.4)$$

The center of the circle is obtained by solving x or substituting Eq. 2.3 into Eq. 2.4.

$$X_c = \frac{1}{2(m_{L_2} - m_{L_1})} [m_{L_1} m_{L_2} (y_1 - y_3) + m_{L_2} (x_1 + x_2) - m_{L_1} (x_2 + x_3)] \dots \quad (2.5)$$

Y_c is obtained by substituting Eq. 2.5 into Eq. 2.3 or Eq. 2.4.

$$Y_c = -\frac{1}{m_{L1}} \left(X_c - \frac{1}{2}(x_1 + x_2) \right) + \frac{1}{2}(y_1 + y_2) \quad \dots \dots \dots \quad (2.6)$$

The radius of the circle is solved by the following equation:

$$r = \sqrt{(X_c - x_1)^2 + (Y_c - y_1)^2} \quad \dots \dots \dots \quad (2.7)$$

With the known attributes of a circle (radius and center), we can construct a complete equation of a circle:

Given an arbitrary point in a plane (x_{test} , y_{test}), the “empty circle” property is determined by the following conditions:

1. False, if $(x_{test} - X_c)^2 + (y_{test} - Y_c)^2 - r^2 \leq 0$
 2. True, if $(x_{test} - X_c)^2 + (y_{test} - Y_c)^2 - r^2 > 0$

2.1.2 Voronoi Algorithm

After performing the Delaunay tessellation algorithm, each vertex of DTs is bisected perpendicular by passing through their midpoints. The intersections of all perpendicular lines are connected to form a Voronoi polygon. The Voronoi polygon is created based on the shortest path of the connected intersections (**Fig. 2.3**). This procedure is repeated for all DTs in the system. This method, shortest-path Voronoi diagram generation²⁵, is the method applied in this study.

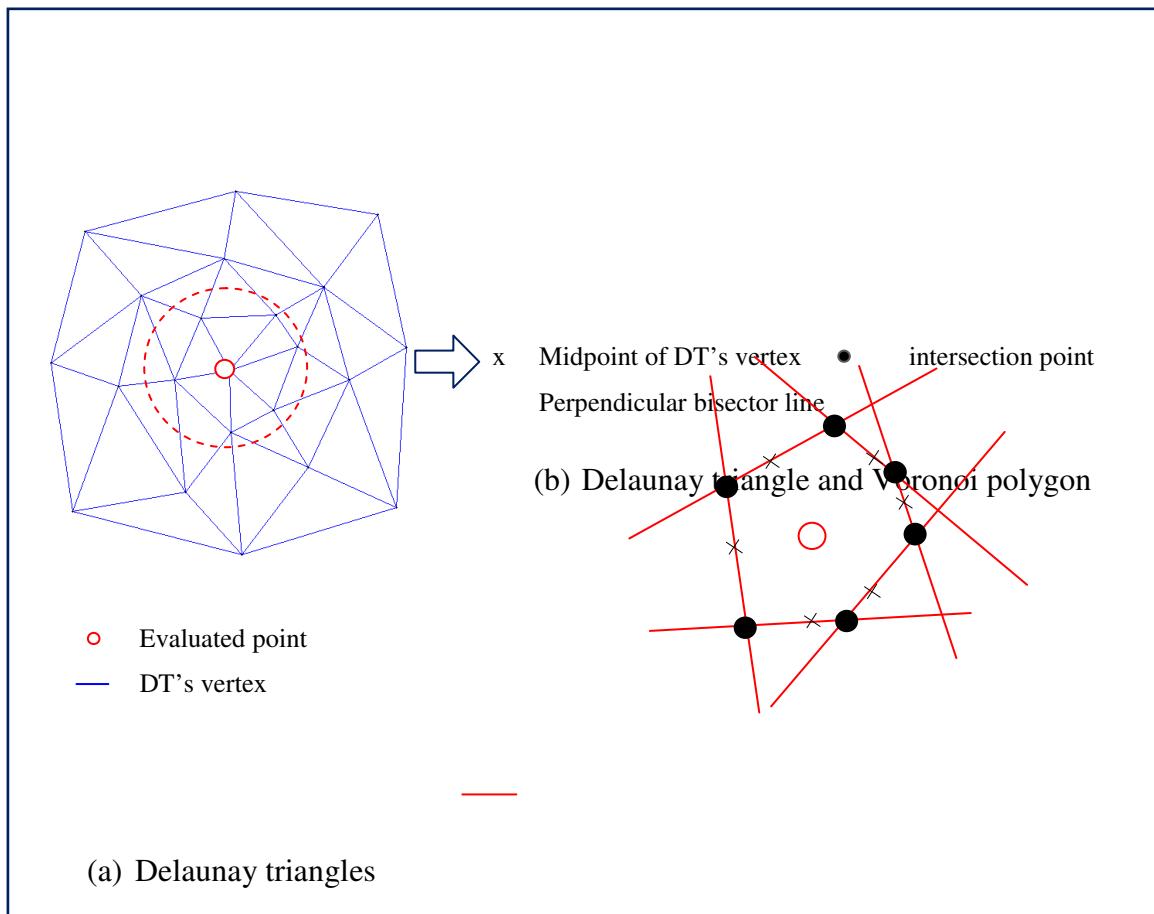


Fig. 2.3-Voronoi algorithm based on the shortest-path of connected intersection

Fig. 2.4 shows the correlations between DTs and Voronoi polygons. The dashed lines and solid lines are the DTs and Voronoi edges respectively.

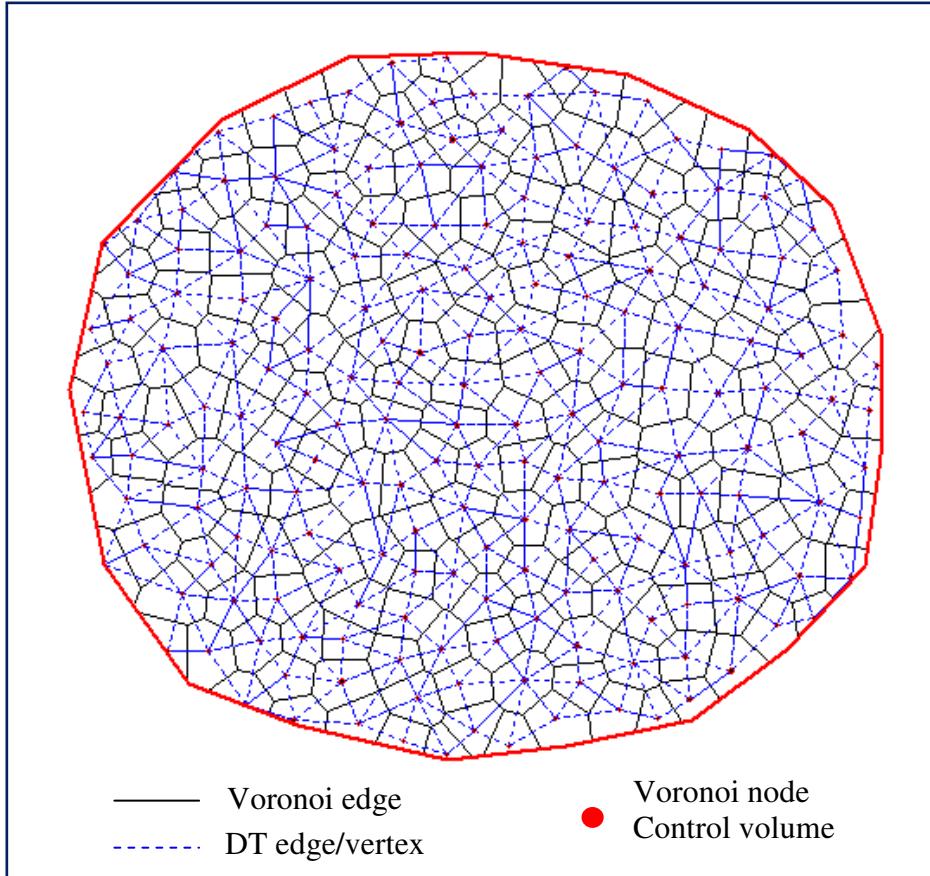


Fig. 2.4-Voronoi and Delaunay triangles

2.2 Discrete Fracture and Voronoi Diagram

Discrete fracture networks are formed by multiple fracture sets. Some of the fracture sets may intersect with the other fracture sets. In the case of fracture sets that do not intersect other fracture sets, they can be treated as a single fracture set, or otherwise it is treated as multiple-intersecting fracture sets.

This section will introduce techniques employed to populate Voronoi nodes needed to grid fracture network for both single fracture and multiple intersecting fracture sets. The techniques contain simple procedures or operations such as determining intersection of two straight lines and intersections of a straight line with a circle.

2.2.1 Single Fracture

For a single fracture set, technique to populate nodes such that Voronoi edges are aligned with the fracture is very simple. The fracture is represented as a straight line. A pair of nodes is simply distributed parallel along the fracture and another pair of nodes is distributed perpendicular and equidistant (emphasized by the circles) with the fracture (**Fig. 2.5**).

The detailed step by step procedures to populate nodes for a single fracture set are as follows (shown in **Fig. 2.5**):

1. Determine number of segments or blocks, N for a single fracture represented by a straight line equation.

2. Determine coordinates (X_i, Y_i) of each segment on the fracture.
 3. Draw N virtual small circles (radius of r). The center of the circle is X_i, Y_i .

The equation of each circle is:

$$(x-X_i)^2 + (y-Y_i)^2 = r^2 \quad \dots \dots \dots \quad (2.10)$$

4. Draw lines perpendicular to the fracture that passing through each center of the circle. Since these lines are passing through the center of each circle, each line equation becomes:

5. The Voronoi nodes can be obtained by substituting the **Eq. 2.11** into **Eq. 2.10**.

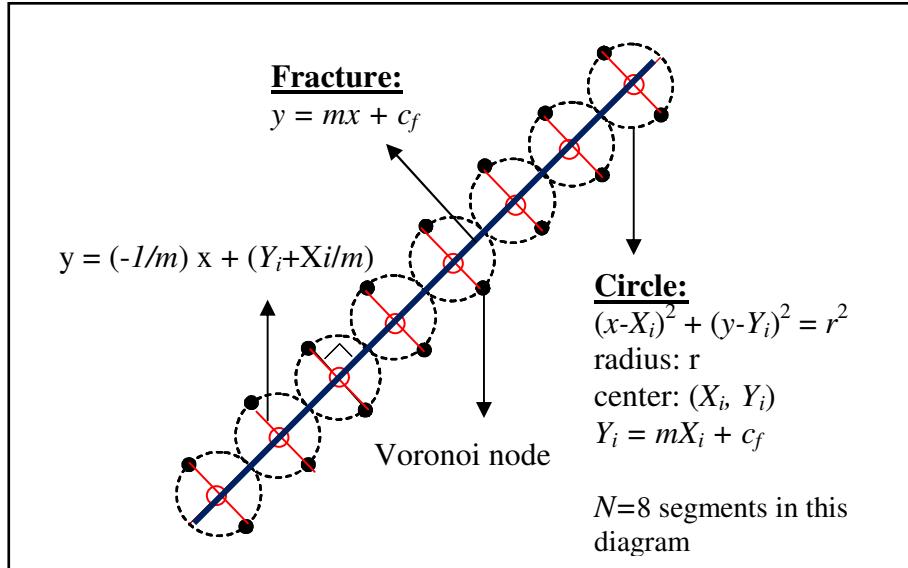


Fig. 2.5-Voronoi nodes for single fracture in the geometrical domain

2.2.2 Multiple Intersecting Fracture Sets

A more complex problem arises from discrete fracture networks formed by multiple-intersecting fracture sets. Each of line segments is treated as a single fracture. Away from intersecting points, nodes can be distributed similar to a single fracture set as discussed in the previous section. A different technique should be performed to grid the fractures near intersection points. The nodes should be populated on the virtual circle in which the pairs of nodes are equidistant to the associated fracture set.

Fig. 2.6 shows a technique to populate points around multiple-intersecting fractures. F(1,2) and F(2,1) are virtual lines which divide fracture sets into the same angles. Points 1 to 8 are the control volumes. Point 1 and point 2 are equidistant points to fracture Set 2. In the case of Fracture Set 2, the line is symmetrical with points 1 and 2 being a mirror image of each other. The rest of the points are equidistant to Fracture Set 1 or Fracture Set 2 as well. In order to maintain or avoid the distortion of Voronoi edges, the points which are

sited on the region between two fractures (e.g. point 1 and 8, 2 and 3, 4 and 5, 6 and 7) have to be pairs of mirror images with respect to $F(1,2)$ or $F(2,1)$. **Fig. 2.7** shows an example of the geometrical domain of a discrete fracture model with two perpendicular intersecting fracture sets.

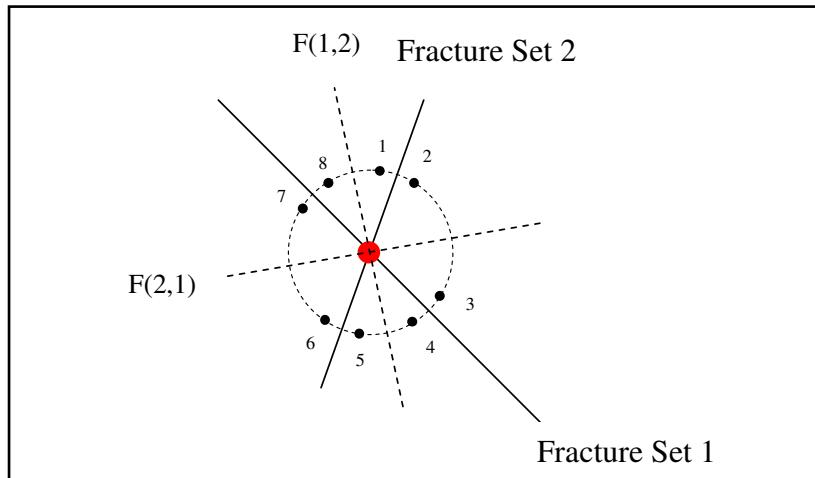


Fig. 2.6-Voronoi nodes for multiple fractures

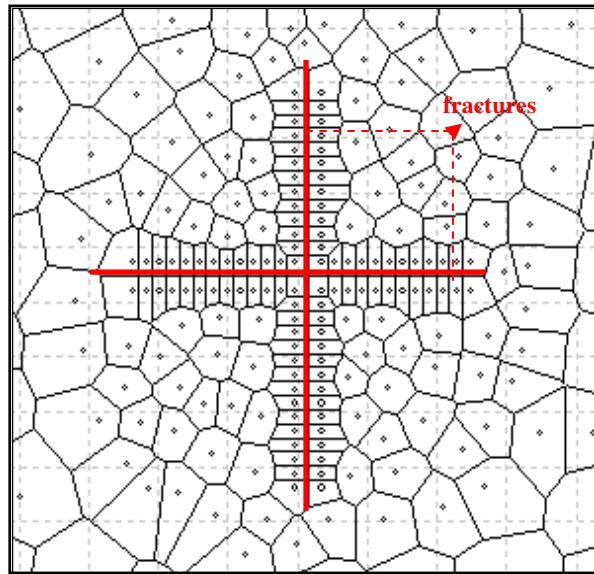


Fig. 2.7-Multiple fractures for hypothetical N/S – E/S fracture set in the geometrical domain

2.3 Treatment of Fracture Tips

Voronoi edges are formed by node population in plane. In the previous section, by populating nodes in the correct location, we were able to execute the Voronoi algorithm in order to build a single fracture and more complex fracture networks. However, the techniques previously discussed did not include the treatment of the fracture tips.

Without treating fracture tips, the fracture length generated by the Voronoi algorithm may not be accurate. The Voronoi edges may be extended and as consequence the volume of fracture will not be accurate. **Fig. 2.8** shows a single fracture set with and without fracture tips treatment.

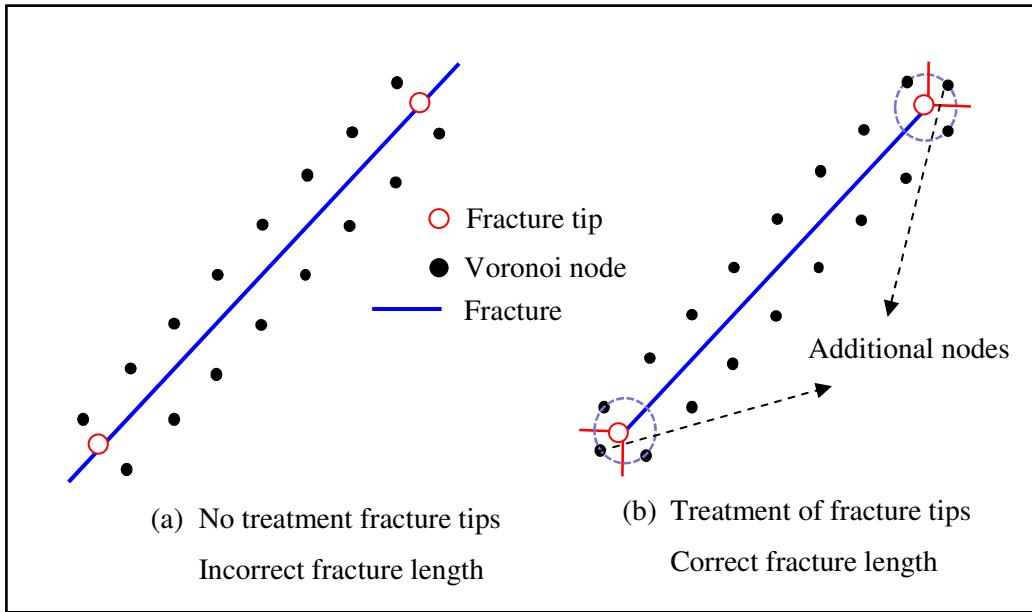


Fig. 2.8-Treatment of fracture tips

As depicted in the **Fig. 2.8**, an additional node for each fracture tip is required in order to terminate the Voronoi edges at the correct location. Each additional node is located on the extension of the fracture. The additional node should be passing through a virtual circle centered at the fracture tip.

2.4 Volume Correction on Discrete Fracture Network

The above description is merely a representation of the geometrical domain of a discrete fracture model. The computational domain treats and creates the fracture segments as additional or virtual control volumes. Each of the fracture grid blocks is given the required properties such as porosity, permeability, and etc. Moreover, the known distribution of fracture aperture (e.g. log-normally distributed¹⁸), thickness and fracture roughness can be easily incorporated into the computational domain. **Fig. 2.9** shows an example of the computational domain for two fracture sets. Additional nodes are added along the fracture lines. Since the computational domain is now honoring fracture characterization data, the numerical model can be applied as if the fractures are absent.

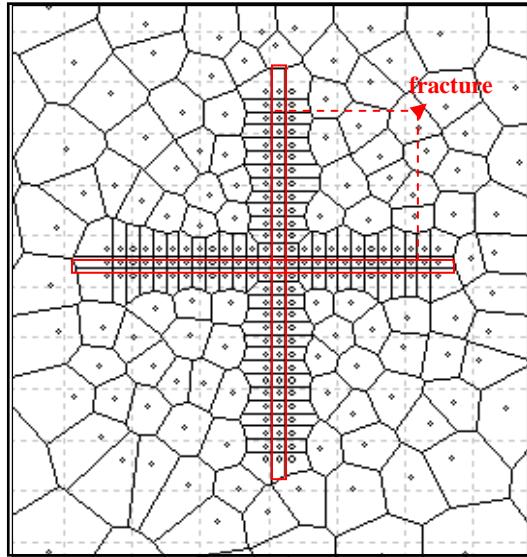


Fig. 2.9-Multiple fractures – computational domain

Furthermore, since the fractures in the geometrical domain are represented as lines, thus the bulk volumes of both fracture and the adjoining matrix blocks have to be corrected in the computational domain. The bulk volume of fracture segments can be computed based

on given fracture apertures. Thus the bulk volume of the matrix adjoining with the fracture should be corrected due to the volume taken by the fractures.

Fig. 2.10 shows the volume correction comparison of the geometrical domain and the computational domain. Bulk volumes of the matrix blocks directly connected to fracture segments are decreased by half the bulk volume of the fracture segments.

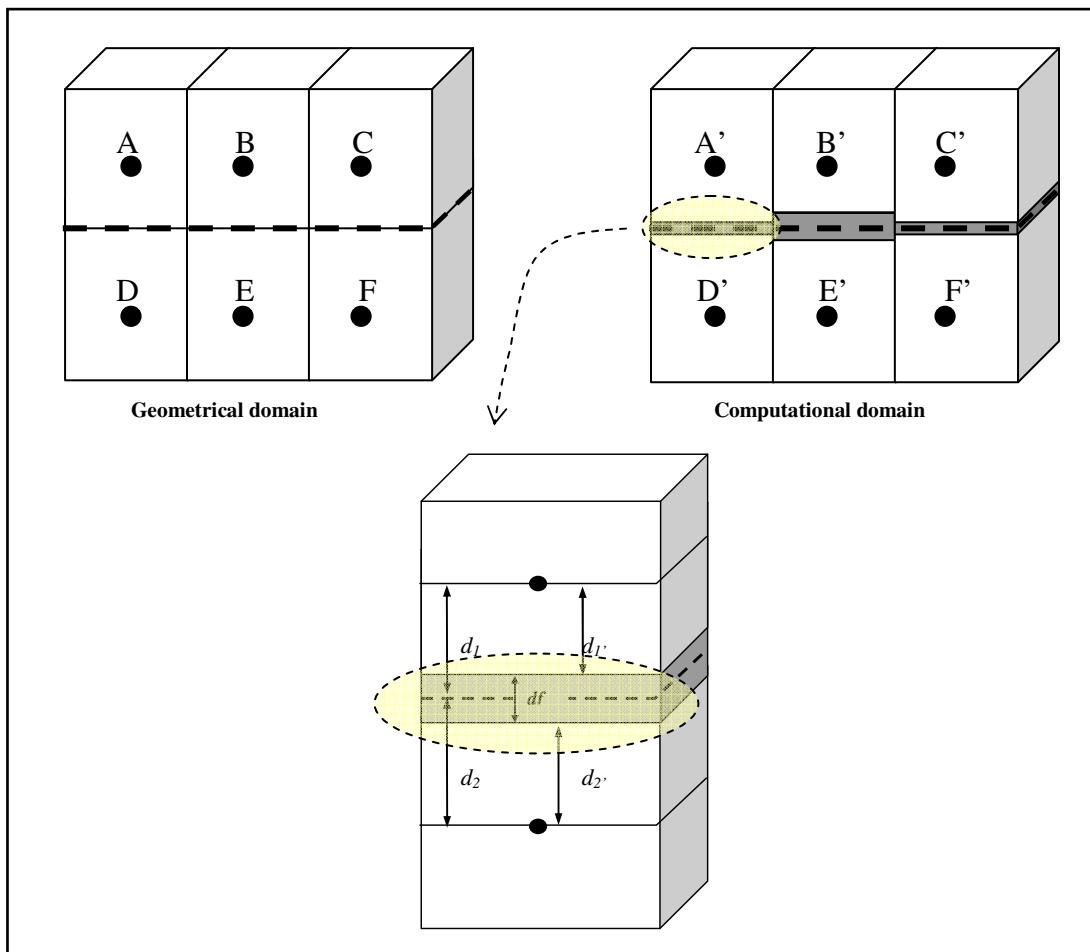


Fig. 2.10- Control Volume correction (computational domain)

d_1 and d_2 are the distances from the block A and D in the geometrical domain. After the volume correction, due to the aperture of the fracture (d_f), the distances become d_1' and d_2' in the computational domain.

The relationship between the original volume, V and the corrected volume, V' of a particular gridblock is expressed by the following equation:

$$V' = \left(1 - \frac{1}{2} \frac{d_f}{d}\right) V \quad \dots \dots \dots \quad (2.12)$$

Based on the above equation, it is important to have a refined grid blocks near fractures. Otherwise the volume correction is not necessarily performed in the computational domain, due to insignificant difference between V' and V .

2.5 Workflow of Grid Generation Technique

This workflow will describe the methodology on building a grid model using Voronoi algorithm. Besides the procedures to grid the matrix, the workflow will include the techniques to grid systems with fracture networks.

For this purpose, we assume that the fracture network and the fracture aperture distribution are provided prior to this work. The fracture network can be obtained by any approach, e.g. fractal geometry¹⁹, outcrop²⁶ studies and others. The fracture aperture distribution can be obtained from X-Ray CT scan experiments^{18,27}.

To start building a grid model, we extract the fracture network as sets of X and Y coordinates. The fracture aperture distribution is applied for each fracture following the log-normal distribution or can be assigned manually. As previously noted, all the fracture sets are represented as line(s) in the geometrical domain.

A pair of nodes which later become the control volume should be populated as such to construct the Voronoi edges perfectly aligned onto the line of fractures. Therefore, one set of nodes should have a mirror effect on another set as seen in **Fig. 2.5**.

However, additional procedures are needed to grid a more complex fracture network (intersecting fractures). **Fig. 2.6** illustrates how we populate the nodes around the intersection.

Once we have populated the nodes (control volumes) for the fractures and their intersections, we can continue to add nodes to grid up the matrix. This can be done manually or use other options (random, rectangular, hexagonal, radial or hybrid).

Finally, we can execute the Voronoi algorithm with all the nodes of fractures and matrix blocks. Additional nodes to represent control volume of fracture blocks are added and the volumes of matrix blocks should be corrected (**Fig. 2.10**).

Fig. 2.11 illustrates the steps in building a grid model using the Voronoi algorithm as we just discussed.

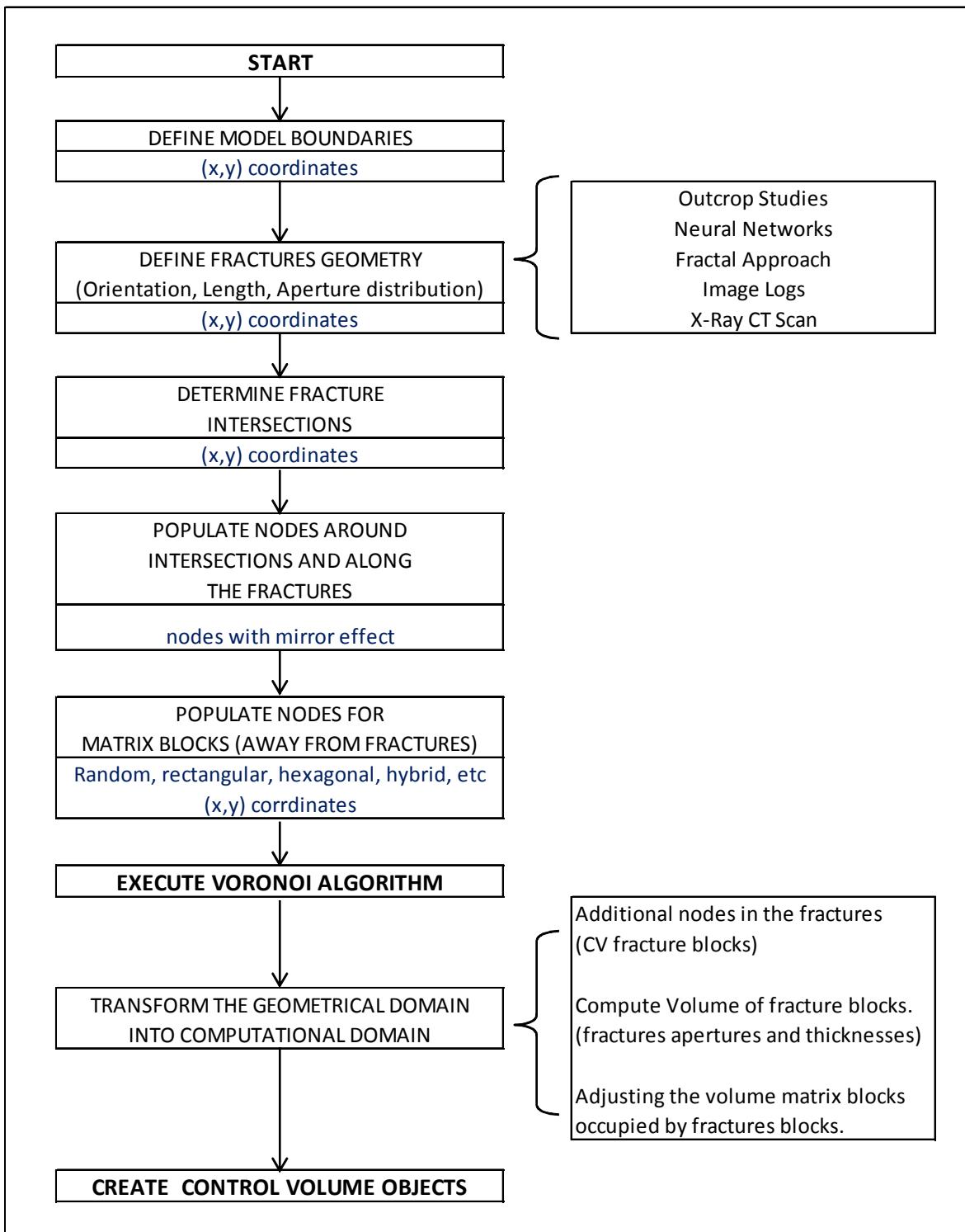


Fig. 2.11-Workflow of grid generation technique

CHAPTER III

DEVELOPMENT OF DISCRETE FRACTURE RESERVOIR SIMULATOR (DFN SIMULATOR)

3.1 Conservation of Mass Equations

The basic laws of reservoir simulation are the conservation of mass, energy and momentum. Mass balance in a grid block is achieved by equating the accumulation of mass in the block with the difference between the mass leaving and entering the block. Many derivations of the oil, water, and gas fluid flow equations exist abundantly in the literature^{6,28-33}. Therefore, only a brief discussion will be presented here, especially related to discretization for Voronoi gridblock.

3.2 Governing Equations

To simplify the derivation of flow equations, we derived the flow equation and material equation on a block/grid/cell basis. This approach is called the discrete approach and is commonly used in the industry rather than discretizing partial differential equations.

3.2.1 Material Balance Equation

We begin with the material balance definition that the net flow rate in a cell is equal to the rate of accumulation of the cell. This statement is true if at this moment the production/injection term is ignored.

The accumulation term can be expressed as the following equation:

$$\text{Rate of accumulation} = \frac{1}{\Delta t} \left[\left(\frac{V_p S}{B} \right)_e^{(n+1)} - \left(\frac{V_p S}{B} \right)_e^n \right] \dots \quad (3.1)$$

V_p = pore volume

S = phase saturation, *fraction*

B = formation volume factor

e = evaluated cell

Δt = time interval

The superscripts n and $n+1$ are corresponding to beginning and end of the time interval, Δt . the net flow rate into the evaluated cell, e is defined as:

$$\text{Net Flow Rate} = \sum_{i=1}^N q_{i \rightarrow e},_{e \neq i} \dots \quad (3.2)$$

Subscript i is assigned for cells connected to the evaluated cell, e . $i \rightarrow e$ is the flux direction from i to e .

For an explicit finite difference scheme, the net flow rate of **Eq. 3.2** can be written as:

$$\sum_{i=1}^N q_{i \rightarrow e} = \sum_{i=1}^N T_{i \rightarrow e} M_{i \rightarrow e}^n \Delta \Phi_{i \rightarrow e}^{n+1} \dots \quad (3.3)$$

And in fully implicit form the above equation becomes:

$$\sum_{i=1}^N q_{i \rightarrow e} = \sum_{i=1}^N T_{i \rightarrow e} M_{i \rightarrow e}^{n+1} \Delta \Phi_{i \rightarrow e}^{n+1}$$

where,

- T = Transmissibility term, $md\text{-}ft$
 M = Mobility term, $1/cp$
 $\Delta\Phi$ = Potential difference, $psia$
 N = Connection list (member of neighboring blocks)

The gradient or the potential difference $\Delta\Phi$ is calculated using the following formula:

$$\Delta\Phi_{i \rightarrow e} = \Delta p_{i \rightarrow e} + \gamma\Delta Z - \Delta p_c \quad \dots \dots \dots \quad (3.4)$$

where,

- γ = Average specific gravity, psi/ft
 ΔZ = Elevation difference, ft
 P_c = Capillary pressure, $psia$

The mobility term, M is calculated with respect to standard conditions, thus the formation volume factor is included. Upstream relative permeability, $k_{r\ upstream}$ is used to calculate the fluid mobility.

$$M_{i \rightarrow e} = \frac{k_{r_{upstream}}}{B_{i \rightarrow e} \mu_{i \rightarrow e}} \quad \dots \dots \dots \quad (3.5)$$

where,

$k_{rupstream}$ = Upstream relative permeability, fraction

$$k_{\text{upstream}} = \begin{cases} k_{ri} & \text{if } \Phi_i > \Phi_e \\ \frac{k_{ri} + k_{re}}{2} & \text{if } \Phi_i = \Phi_e \\ k_{re} & \text{if } \Phi_i < \Phi_e \end{cases} \quad (3.6)$$

The fluid formation volume factor and viscosity are the average values of the connected cells.

$$B_{i \rightarrow e} = \frac{B_i + B_e}{2} \quad (3.7)$$

$$\mu_{i \rightarrow e} = \frac{\mu_i + \mu_e}{2} \quad (3.8)$$

T is defined as transmissibility that describes the flow from one block to another block. **Fig. 3.1** illustrates the transmissibility of two blocks, block ① and block ②.

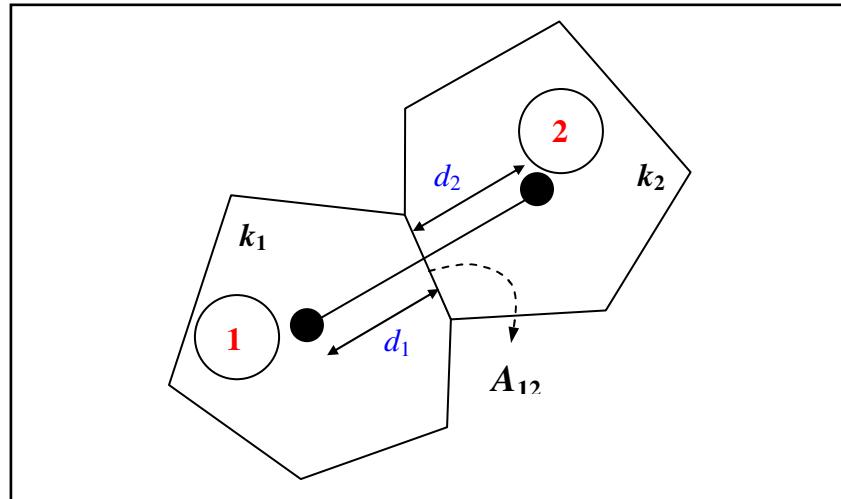


Fig. 3.1-Transmissibility description of two blocks; block ① and block ②

The transmissibility of two connected blocks is calculated using geometric average.

$$T_{12} = \frac{\alpha_1 \alpha_2}{\alpha_1 + \alpha_2} \quad \dots \quad (3.9)$$

where,

$$\alpha_1 = \frac{k_1 A_{1-2}}{d_1} \text{ and } \alpha_2 = \frac{k_2 A_{2-1}}{d_2} \quad \dots \quad (3.10)$$

where,

- A_{1-2} = Area of interface to the flow from *cell*₁ to *cell*₂
- A_{2-1} = Area of interface to the flow from *cell*₂ to *cell*₁
- d = Distance from control volume to area of interface

The material balance equation of an evaluated cell, *e*, can be obtained by simple algebraic operation from the above equations.

$$\Delta a_{i \rightarrow e}^m \Delta \Phi_{i \rightarrow e}^{n+1} = \frac{1}{\Delta t} \left[\left(\frac{V_p S}{B} \right)_e^{(n+1)} - \left(\frac{V_p S}{B} \right)_e^n \right] \quad \dots \quad (3.11)$$

where,

$$\Delta a_{i \rightarrow e}^m \Delta \Phi_{i \rightarrow e}^{n+1} = \sum_{i=1}^N T_{i \rightarrow e} M_{i \rightarrow e}^n \Delta \Phi_{i \rightarrow e}^{n+1} \quad \dots \quad (3.12)$$

The material balance equation for the entire gridblocks is:

$$\sum_{i=1}^N T_{i \rightarrow e} M_{i \rightarrow e}^n \Delta \Phi_{i \rightarrow e}^{n+1} = \frac{1}{\Delta t} \left[\left(\frac{V_p S}{B} \right)_e^{(n+1)} - \left(\frac{V_p S}{B} \right)_e^n \right], \quad e \in \{1, N_{cells}\} \quad \dots \quad (3.13)$$

where, N_{Cells} is number of blocks in the system.

The left-hand side of **Eq. 3.13** is evaluated at the beginning of specified time interval (Δt). The entire pressure and saturation dependent variables on the left-hand side are evaluated at the end and beginning of time interval, Δt respectively. The pressure dependent variables are fluid and rock properties, and the saturation dependent variables are relative permeability and capillary pressure. Thus, **Eq. 3.13** is just applied for the IMPES method.

Since the implicit method evaluates pressure and saturation dependent variables at the end of the time interval, **Eq. 3.13** now becomes:

3.2.2 Fracture Discretization

As mentioned in the previous chapter, the DFN is represented explicitly as lines in the geometrical domain. The fracture volume, in the computational domain is given by the fracture aperture distribution. **Fig. 3.2** shows the difference in fracture representation between the geometrical and computational domains.

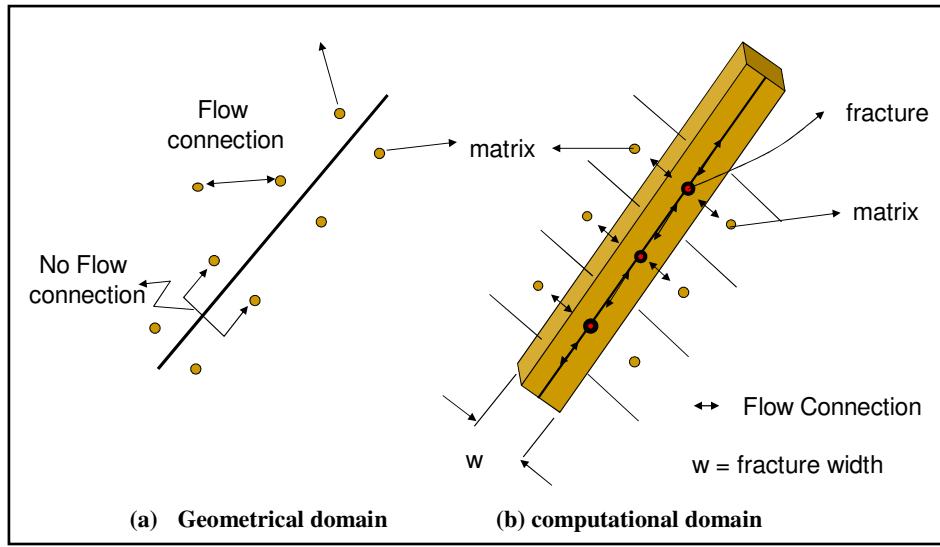


Fig. 3.2–Matrix-fracture and fracture-fracture connections in the computational and geometrical domains

As discussed in the previous chapter, the fracture aperture is not described as a smooth parallel plate in the DFN model. The fracture surfaces are naturally not uniform and the aperture follows a log-normal distribution^{18,27}.

Probability density function, *PDF* of log-normal distribution is expressed by the following equation³⁴:

$$PDF = \frac{1}{x\sigma\sqrt{2\pi}} e^{-\frac{(\ln(x)-\mu)^2}{2\sigma^2}} \dots \quad (3.15)$$

And the cumulative distribution function, *CDF* is:

$$CDF = \int_0^x \frac{1}{x\sigma\sqrt{2\pi}} e^{-\frac{(\ln(x)-\mu)^2}{2\sigma^2}} dx = \frac{1}{2} + \frac{1}{2} \operatorname{erf} \left[\frac{\ln(x)-\mu}{\sigma\sqrt{2}} \right] \dots \quad (3.16).$$

where,

μ = mean of fracture aperture.

σ = standard deviation.

x = fracture aperture.

With a given mean, standard deviation of fracture aperture, the fracture aperture, x along the line can be calculated using the inverse of **Eq. 3.16**. **Fig. 3.2** and **Fig. 3.4** are the example graphs of probability and cumulative density functions respectively.

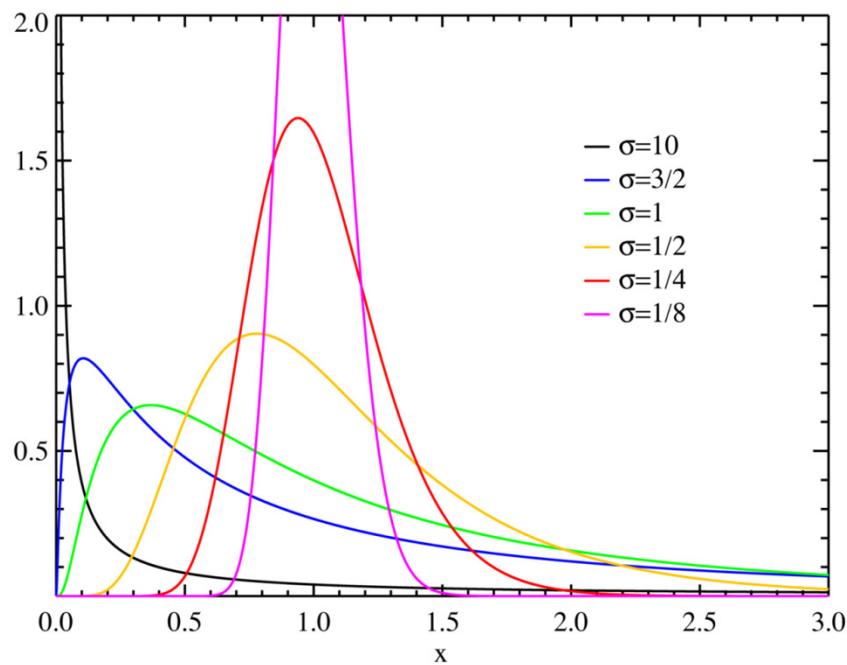


Fig. 3.3–Probability density function of a log-normal distribution³⁴

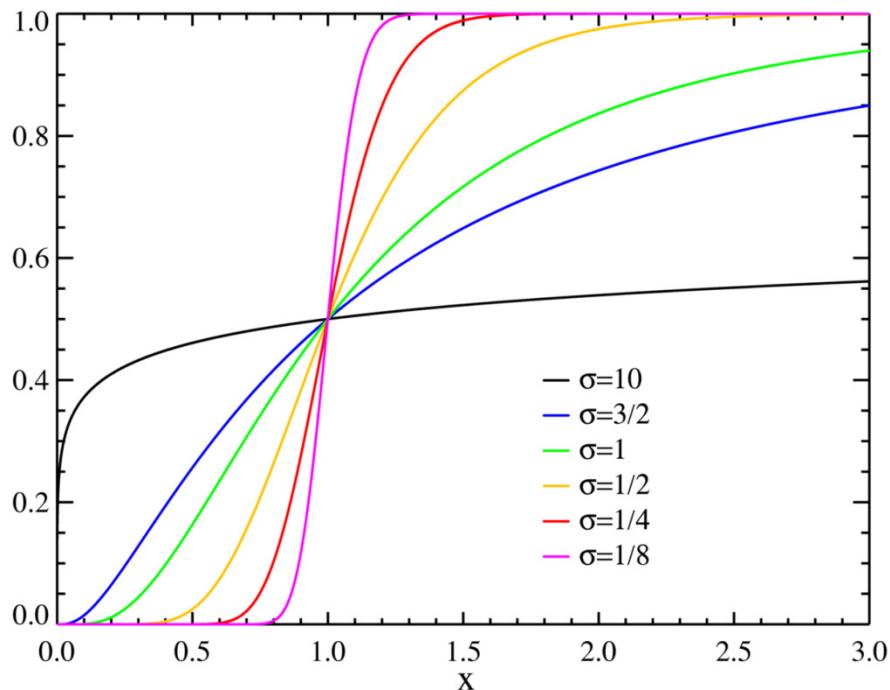


Fig. 3.4—Cumulative distribution function of a log-normal distribution³⁴

In order to discretize the fracture, it is important to fragment the fracture into several segments prior to building the grid model. The number of fracture segments depends on the heterogeneity of the apertures or the fracture openings. This could be determined based on standard deviation of the log-normal distribution. A smaller standard deviation means less variation of fracture apertures and requires less number of fracture segments.

For the sake of simplicity, an adequate number of fracture segments in this research are predetermined by user prior to building the grid model. The number of gridblocks per-fracture is proportional to the fracture length. The longer the fracture the more number of gridblocks per-fracture is required. Despite the value of standard deviation of log-normal distribution, the typical number of gridblock per-fracture used in this study is 20 gridblocks per-fracture.

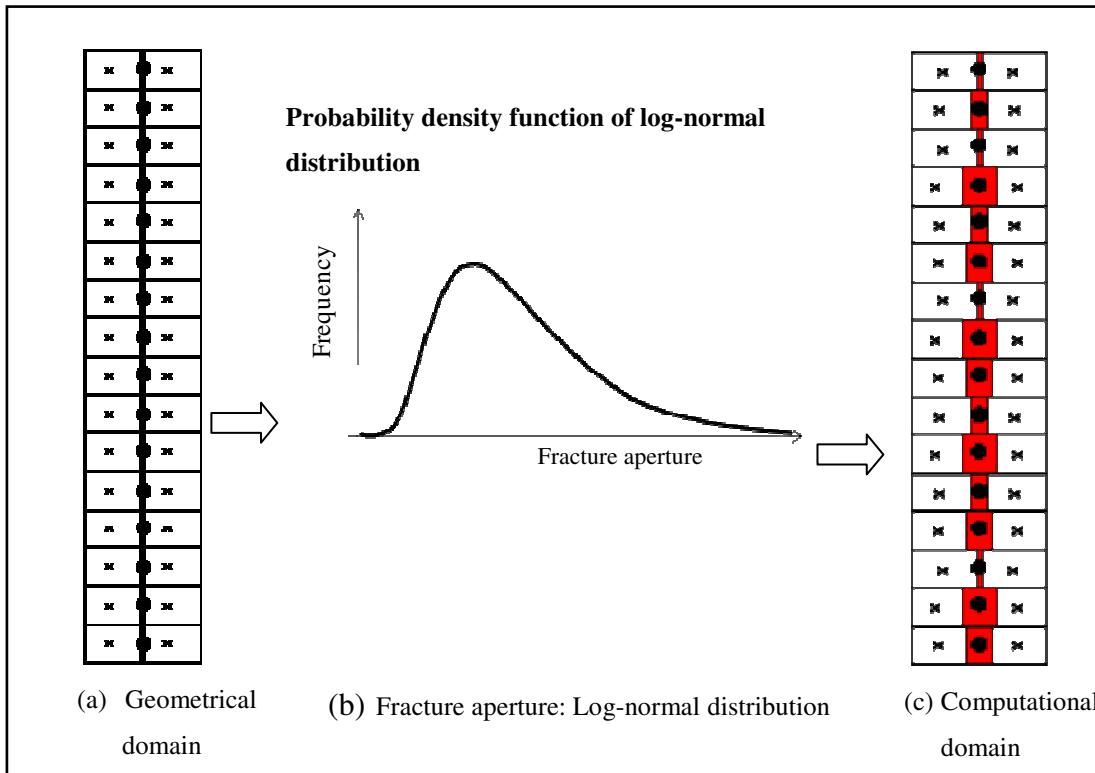


Fig. 3.5–Fracture aperture distribution

With a given fracture apertures, permeability of the fracture segments are calculated using the cubic-law formulation³⁵. Based on the cubic law, the permeability can be presented as a function of fracture width or fracture aperture (**Eq. 3.17**). It is worth being noted that the cubic-law formulation is using several assumptions such as the fracture surface is smooth and laminar flow occurs inside the fracture.

The permeability of the fracture is calculated by:

where,

w = fracture width

k_f = fracture permeability

Some researches introduced fracture roughness into the cubic-law relationship to account for the fact that smooth fracture surfaces are not likely found in nature. They believe that there should be a factor in the cubic-law which inhibits the flow through the fractures^{36,37}. However, in this case we assume the cubic law applies to individual point on the fracture face, as determined by CT scanning of fracture aperture or other methods.

If the fracture blocks are magnified as depicted in the dashed circle of **Fig. 3.5**, the flow connection will look like **Fig. 3.6**.

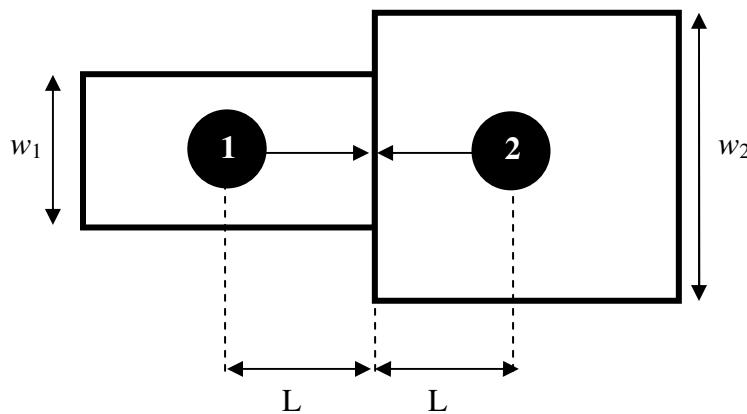


Fig. 3.6–Flow connection between two segments in the fracture where w_1 and w_2 represent two fracture grid cells with different aperture

3.2.3 Well Modeling

The pressure in the wellblock is not the same as the bottomhole flowing pressure at the well, p_{wf} . The reason is that the gridblock where the wells located are significantly larger than the wellbore radius. The pressure difference between the block pressure and bottomhole pressure, p_{wf} is proportional to the coefficient, the *productivity* or *injectivity index*. The geometric factor is commonly named the *well index*.

3.2.3.1 Peaceman's Well Model

Peaceman³⁸ found that the pressure calculated for a well block is the same as the flowing pressure at an equivalent radius, r_o , where he defined r_o as “the radius at which the steady-state flowing pressure for the actual well is equal to the numerically calculated pressure for the well block”. The relationship between r_o and bottomhole pressure is expressed in the following equation.

$$p_{wf} - p(r) = \frac{q\mu}{2\pi} \ln \left(\frac{r_w}{r_o} \right) \dots \dots \dots \quad (3.18)$$

where,

- p_{wf} = bottomhole well flowing pressure
 $p(r)$ = pressure at grid block containing the well
 q = production rate of well
 r_w = wellbore radius
 r_o = radius at which steady-state flowing pressure for the actual well is equal to the numerically calculated pressure for the well block.

Using uniform, square Cartesian grid blocks ($\Delta x = \Delta y$), Peaceman showed that if $\Delta x = \Delta y$ and $k_x = k_y$ then:

In another paper, Peaceman³⁹ derived an expression for r_o for an isotropic reservoir with non-square grid blocks:

Furthermore, he derived for an anisotropic reservoir:

$$r_o = \frac{0.28 \left[\sqrt{k_y/k_x} (\Delta x)^2 + \sqrt{k_x/k_y} (\Delta y)^2 \right]^{1/2}}{(k_y/k_x)^{1/4} + (k_x/k_y)^{1/4}}, \dots \quad (3.21)$$

3.2.3.2 Well Model for Voronoi Grid

In using Voronoi grid model, we need a different well model from Peaceman's well model originally formulated for radial and Cartesian square grid blocks. Aziz and Palagi¹³ presented an analytical well model based on Peaceman's work which can be applied to grids of any geometry. This model assumes that the pressure in all grid blocks that are neighbors of the wellblock can be evaluated by the radial flow equation around the well. Also, flow is assumed to be radial around the well block despite of the location of the well. Their well model (**Fig. 3.7**) is shown in **Eq. 3.22**.

$$r_o = \exp \left(\frac{\sum_j \left(\frac{b}{d} \right)_{ij} \ln(d_{ij}) - \theta_{ij}}{\sum_j \left(\frac{b}{d} \right)_{ij}} \right), \dots \quad (3.22)$$

where,

- j = grid block that is neighbor of well block i
- b_{ij} = length of side of polygon
- d_{ij} = distance between the centers of grid block i and j
- θ_{ij} = angle open to flow ($\theta = 2\pi$ for an internal well, i.e. well located in the center of the block)

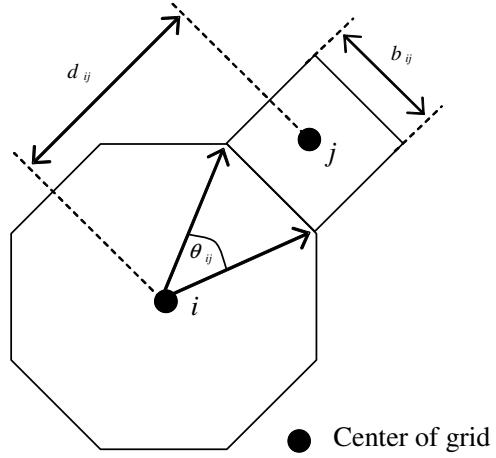


Fig. 3.7–Well model for a polygon (after Palagi et al.¹³)

Palagi derived a special case for Eq. 3.22 when the polygon of interest has equal sides, where:

$$(b/d)_{ij} = \tan(\pi/N), \dots \quad (3.23)$$

Substituting Eq. 3.23 into Eq. 3.22 (with $\theta = 2\pi$) and solving for r_o gives:

$$r_o = d_{ij} \exp\left(\frac{-2\pi}{N \tan(\pi/N)}\right), \dots \quad (3.24)$$

where, N is number of sides of the polygonal grid block containing the well.

Once we have the effective radius of the well, the well productivity index and the bottom-hole pressure can be calculated using the following formulas:

$$WI = \frac{2\pi k h}{\ln(\frac{r_o}{r_w}) + S}, \dots \quad (3.25)$$

$$P_{wf} = p(r) - \frac{q}{\lambda WI}, \dots \quad (3.26)$$

λ is the fluid mobility ($\lambda = k_r/\mu$).

3.2.3.4 Well Constraints

Producers are operated by the following constraints:

1. Constant flow rate of any one phase

If the rate of any one phase is specified, then the rate of the other phase(s) can be calculated as follows:

$$P_{wf}^{n+1} = p(r)^{n+1} + \frac{q_\alpha}{WI \lambda_\alpha^{n+1}} \dots \quad (3.27)$$

where,

α = fluid phase (oil, gas and water)

2. Constant bottom hole pressure

If the well bottomhole pressure is specified, then the rate of any phase can be obtained as follows:

$$q_\alpha^{n+1} = WI \lambda_\alpha^{n+1} (p(r)^{n+1} - p_{wf}) \dots \quad (3.28)$$

Injectors are usually operated at two constraints – either constant injection rate or constant injection pressure.

3. Constant Injection Rate

If the injection rate of any one phase is specified, then the flowing bottomhole pressure is computed as follows:

4. Constant Injection Pressure

If the injection pressure is specified, then the rate of the injected phase can be obtained as follows:

$$q_\alpha = J\lambda_\alpha(P_{wf} - P_i) \quad \dots \quad (3.30)$$

3.3 Solution Technique

Eq. 3.14 is the equation that we are going to solve in order to obtain the pressure and saturation distribution throughout the model. Residual functions will be used to construct a series of linear equations. The residual function is basically the difference of the net flow rate and the rate of accumulation (**Eq. 3.31**)

The residual equation implemented in the DFN Simulator is expressed by the following equations³³:

$$r_{o,g,w}^{n+1} = \sum_{i=1}^N T_{i \rightarrow e} M_{i \rightarrow e}^{n+1} \Delta \Phi_{i \rightarrow e}^{n+1} - \frac{1}{\Delta t} \left[\left(\frac{V_p S}{B} \right)_e^{(n+1)} - \left(\frac{V_p S}{B} \right)_e^n \right] + q_{sc}, \quad e \in \{1, Ncells\} \dots (3.31)$$

For black oil model, the equation should be expanded into all forms of residual functions of oil, gas as water phase.

Oil Phase:

$$r_o^{n+1} = \sum_{i=1}^N T_{i \rightarrow e} M_{o i \rightarrow e}^{n+1} \Delta \Phi_{o i \rightarrow e}^{n+1} - \frac{1}{\Delta t} \left[\left(\frac{V_p S_o}{B_o} \right)_e^{(n+1)} - \left(\frac{V_p S_o}{B_o} \right)_e^n \right] + q_{osc}, \quad e \in \{1, Ncells\}. \quad (3.32)$$

Gas Phase:

$$\begin{aligned} r_g^{n+1} = & \sum_{i=1}^N T_{i \rightarrow e} M_{g i \rightarrow e}^{n+1} \Delta \Phi_{g i \rightarrow e}^{n+1} - \frac{1}{\Delta t} \left[\left(\frac{V_p S_g}{B_g} \right)_e^{(n+1)} + R_{so}^{n+1} \left(\frac{V_p S_o}{B_o} \right)_e^{(n+1)} + R_{sw}^{n+1} \left(\frac{V_p S_w}{B_w} \right)_e^{(n+1)} - \dots \right. \\ & \left. \dots \left(\frac{V_p S_G}{B_G} \right)_e^n - R_{so}^n \left(\frac{V_p S_o}{B_o} \right)_e^n - R_{sw}^n \left(\frac{V_p S_w}{B_w} \right)_e^n \right] + q_{g sc}, \quad e \in \{1, Ncells\}, \dots \end{aligned} \quad (3.33)$$

Water Phase:

$$r_w^{n+1} = \sum_{i=1}^N T_{i \rightarrow e} M_{wi \rightarrow e}^{n+1} \Delta \Phi_{wi \rightarrow e}^{n+1} - \frac{1}{\Delta t} \left[\left(\frac{V_p S_w}{B_w} \right)_e^{(n+1)} - \left(\frac{V_p S_w}{B_w} \right)_e^n \right] + q_{wsc}, \quad e \in \{1, Ncells\} .. \quad (3.34)$$

Eq. 3. 31, Eq. 3.32 and Eq. 3.33 contain gravity terms. Now, we will add the capillary terms:

$$P_{cow} = P_o - P_w \quad \therefore P_w = P_o - P_{cow}, \dots \quad (3.35)$$

$$P_{cog} = P_g - P_o \quad \therefore P_g = P_{cog} + P_o, \dots \quad (3.36)$$

Thus, the potential terms of $\Delta \Phi_g$ and $\Delta \Phi_w$ in the **Eq. 3.33** and **Eq. 3.34** can be expressed with one unknown variable of oil pressure, P_o . The P_{cow} and P_{cog} are the rock properties provided in the form of tables as function of fluid saturations.

Another equation that we need is the saturation equation:

$$S_o^{n+1} + S_w^{n+1} + S_g^{n+1} = 1 \quad \therefore \quad S_o^{n+1} = 1 - S_g^{n+1} - S_w^{n+1}, \dots \quad (3.37)$$

Finally, we can solve the three unknown variables (P_o , S_g and S_w) with the three Equations (Eq. 3.32, 3.33 and 3.34). Another remaining unknown, S_o can be computed by simply using **Eq. 3.37**.

3.3.1 Linear Equations

We will simplify the flow equations in term of residual functions and all the unknown variables. We can rewrite the residual functions for all phases as follows,

$$r_o = f(p, s_w, s_g) \dots \quad (3.38)$$

$$r_g = f(P, s_w, s_g) \dots \quad (3.39)$$

$$r_w = f(P, s_w, s_g) \dots \quad (3.40)$$

In more common terms, we may also express those equations as:

$$r_o = OIP^{n+1} - (OIP^n + Q_o) \dots \quad (3.41)$$

$$r_g = GIP^{n+1} - (GIP^n + Q_g) \dots \quad (3.42)$$

$$r_w = WIP^{n+1} - (WIP^n + Q_w) \dots \quad (3.43)$$

where,

OIP , GIP and WIP are oil, gas and water in place at standard conditions.

Q_o , Q_g and Q_w are oil, gas and water produced or injected from wells into the reservoir during the period from n to $n+1$ (Δt) at standard conditions.

Since our objective functions are to satisfy $r_o = 0$, $r_g = 0$ and $r_w = 0$, we can consider our problem similar to a root-finding problem. We can use any iterative method to solve all the equations. Newton-Raphson and Quasi-Newton iterative methods are used due to their general application in petroleum industry and simple implementation. **Fig. 3.8** and **Fig. 3.9** illustrate the iteration procedures of those two methods.

In order to solve the equations iteratively, we should compute the Jacobian matrix, J of those equations.

$$J = \begin{bmatrix} \frac{\partial r_o}{\partial p} & \frac{\partial r_o}{\partial s_w} & \frac{\partial r_o}{\partial s_g} \\ \frac{\partial r_g}{\partial p} & \frac{\partial r_g}{\partial s_w} & \frac{\partial r_g}{\partial s_g} \\ \frac{\partial r_w}{\partial p} & \frac{\partial r_w}{\partial s_w} & \frac{\partial r_w}{\partial s_g} \end{bmatrix} \dots \quad (3.44)$$

The overall Newton-Raphson and Quasi-Newton iteration schemes form a linear equation of:

$$J^k [\Delta m]^{k+1} = -[r]^k \dots \quad (3.45)$$

The superscript of k indicates the iteration k^{th} and $\Delta m = \begin{bmatrix} dp \\ ds_w \\ ds_g \end{bmatrix}$.

p^{k+1} , s_w^{k+1} and s_g^{k+1} are updated using the following equation.

$$\begin{bmatrix} p \\ s_w \\ s_g \end{bmatrix}^{k+1} = \begin{bmatrix} p \\ s_w \\ s_g \end{bmatrix}^k - \begin{bmatrix} dp \\ ds_w \\ ds_g \end{bmatrix}^{k+1} \dots \quad (3.36)$$

The iteration is continued until our objective functions satisfied, or the residual functions of oil, gas and water (Eq. 3.41, 3.42 and 3.43) are closed to specific tolerance. In addition to Quasi-Newton method, it doesn't need to update the Jacobian matrix for each iteration. It uses the first Jacobian for the entire iterations ($J^{k+1} = J^k = J^0$).

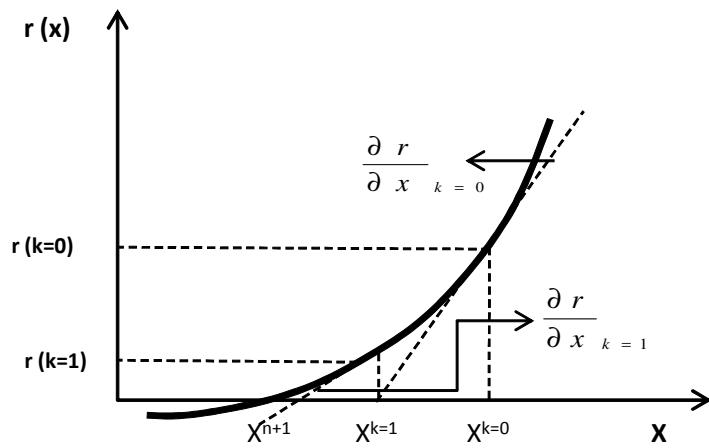


Fig. 3.8-Newton iteration method

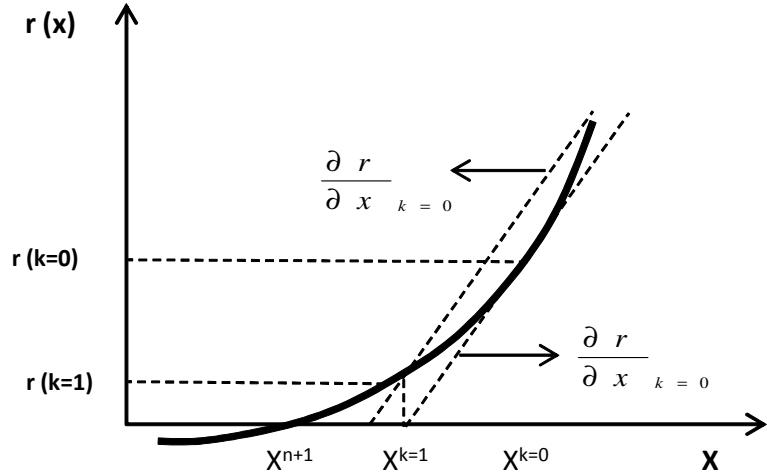


Fig. 3.9-Quasi Newton iteration method

3.3.2 Matrix Solvers

The final equation (**Eq. 3.45**) can be expressed in more compact form using matrix notation as $A\mathbf{x} = \mathbf{B}$, where A is the co-efficient of the Jacobian matrix, and \mathbf{x} and \mathbf{B} are column of vectors.

There are various methods available for solving such a system of linear equations, but generally these methods fall into two groups, direct methods and iterative methods. In DFN simulator developed, the solvers that we implemented were provided by SparseLib++ which was developed by Bertolazzi⁴⁰.

SparseLib++ contains many libraries of matrix and vector operations, such as matrix multiplication, transpose, and inversion. SparseLib++ is structurally implemented using C++. Thus, it is quite simple to couple the codes from SparseLib++ with any C++ code, such as the DFN simulator.

SparseLib++ is equipped with various iterative solver and pre-conditioners. The solvers are GMRES, Conjugate Gradient, Bi-Conjugate Gradient, Stabilized Bi-Conjugate Gradient, QMR, CHEBY and Richardson Iterations. The pre-conditioners are ILU, Diagonal, and ICP pre-conditioners.

The technical discussion of the matrix solver and the pre-conditioners in details is beyond the scope of this study. Most importantly, despite the matrix solver used, all methods should yield similar results and should be accurate as long as the specified tolerance can be satisfied.

3.4 Data Structure

DFN simulator has been developed using an object oriented programming language, Visual Basic 6.0 and Microsoft Visual C++. Visual Basic was used to implement the pre and post-processor while C++ was the processor of the simulator.

In order to simplify the implementation, several important objects were created. Most of the objects are recognizable by users as common terms in the reservoir simulators, e.g. fluid properties, rock properties, numerical controls, etc.

In general, the DFN Simulator uses common data structures as found in many commercial simulators. The main differences between commercial and DFN simulator are the static model structure. In models with Cartesian grid systems, the grid blocks are usually defined using the terms DX, DY and DZ for 2D and 3D models. The standard indexing system of i, j and k are no longer applicable in Voronoi grid system, due to the variation of block shapes.

The following data structures of the DFN simulator are reported in the form of tables. The explanation of keywords used in the DFN simulation is described in the second column of the tables.

3.4.1 Data Structure - Static Model

The static model consists of the dimensions of the model and the control volume (block) objects which include the rock properties assigned for each object:

1. Model dimensions

NXNY : number of control volumes/layer

NZ : number of layers

START_CV [NCELLS]: initial block of control volume connections and their properties

{Control Volume Connection and their Properties}

END_CV : end of control volume connections and their properties

2. Control volume object (**Table 3.1**)

This section is arranged in column format. Each column is separated by space(s) or tab characters. There are more than 10 columns (sub sections) associated for each control volume property. Additional columns depend on the number of neighboring blocks.

Table 3.1 Control volume (CV) Object

Column	Properties
1	Number of connections
2	Connection lists
3	The depth of control volume
4	Surface area (X-Y cross section)
5	Porosity
6	Lateral permeability
7	Vertical permeability
8	Pore volume multiplier
9	Net pay
10	PVT type or ID
11	Rock type or ID
12	The distance from CV centroid to the interface of connected cell-(i)
.	The distance from CV centroid to the interface of connected cell-(i+1)
.	
.	
n	The distance from CV centroid to interface of connected cell-(n)

More details regarding the control volume object is reported in the Appendix B.

3.4.2 Data Structure - Fluid Properties

NPVT : number of PVT table

The DFN simulator uses three-phase fluid properties as shown in the following table (**Table 3.2**).

Table 3.2 Fluid properties object

Column	Properties
1	Pressure (psia)
2	Oil formation volume factor, B_o (RB/STB)
3	Oil viscosity, μ_o (cp)
4	Gas solution in oil phase, R_{so} (SCF/STB)
5	Gas formation volume factor, B_g (RB/SCF)
6	Gas viscosity, μ_g (cp)
7	Water formation volume factor, B_w (RB/STB)
8	Water viscosity, μ_w (cp)
9	Gas solution in water phase, R_{sw} (SCF/STB)

3.4.3 Data Structure – Relative Permeabilities

Since the DFN simulator uses three-phase relative permeability, it requires two relative permeability tables, oil-water (Table 3.3) and gas-water (Table 3.4) relative permeability.

Table 3.3 Oil-water relative permeability curve

Column	Properties
1	Water saturation, S_w (fraction)
2	Oil relative permeability, k_{row} (fraction)
3	Water relative permeability, k_{rw} (fraction)
4	Oil-water capillary pressure, $P_{c_{ow}}$ (psia)

Table 3.4 Gas-water relative permeability curve

Column	Properties
1	Liquid saturation, S_L (fraction)
2	Liquid relative permeability, k_{rwg} (fraction)
3	Gas relative permeability, k_{rg} (fraction)
4	Gas-liquid capillary pressure, pc_{wg} (psia)

3.4.4 Data Structure –Properties at Reference Condition

Table 3.5 shows fluid and rock properties at specified reference condition.

Table 3.5 Data at the reference condition

PB	Bubble point pressure, <i>psia</i>
PREF	Reference pressure, <i>psia</i>
ZREF	Reference depth, <i>ft</i>
CROCK	Rock compressibility, <i>l/psia</i>
DENOIL	Oil density, <i>lb/cu-ft</i>
DENWAT	Water density, <i>lb/cu-ft</i>
DENGAS	Gas density, <i>lb/cu-ft</i>

3.4.5 Data Structure – Numerical Controls

Numerical controls of the DFN simulator are depicted in Table 3.6.

Table 3.6-Numerical Control

RESIDERR	Residual Error
RESIDSOLVER	Solver Tolerance
ITMAX	Maximum Solver Iterations
ITSOLVER	Max. Newton Iterations
DELTIME	Time Step, days
MAXDP	Max. ΔP , psia
DTMAX	Maximum time step, days
DTMIN	Minimum time step, days
TMAX	TMAX, days
MASSW	MAX ΔS_w , fraction
MAXSG	MAX ΔS_g , fraction
MAXSO	Max. ΔS_o , fraction
DPPERT	Δp to calculate dr/dp , psia
DSWPERT	ΔS_w to calculate dr/ds_w , fraction
DSGPERT	Δs_g to calculate dr/dp , fraction

3.5 DFN Black Oil Simulator Work Flow

The following figures (Fig. 3.10 and Fig. 3.11) describe the detailed workflows of the developed reservoir simulator.

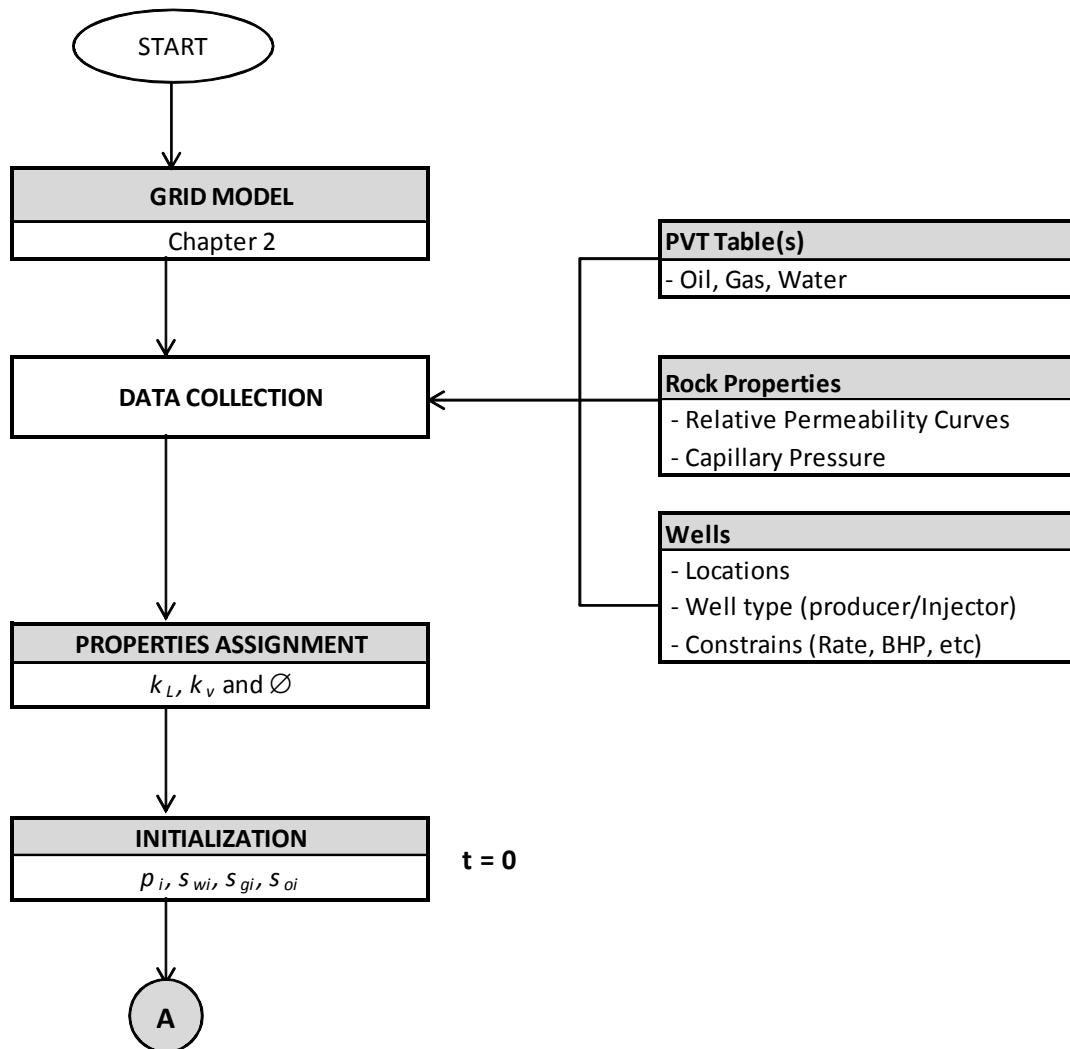


Fig. 3.10-Initialization workflow

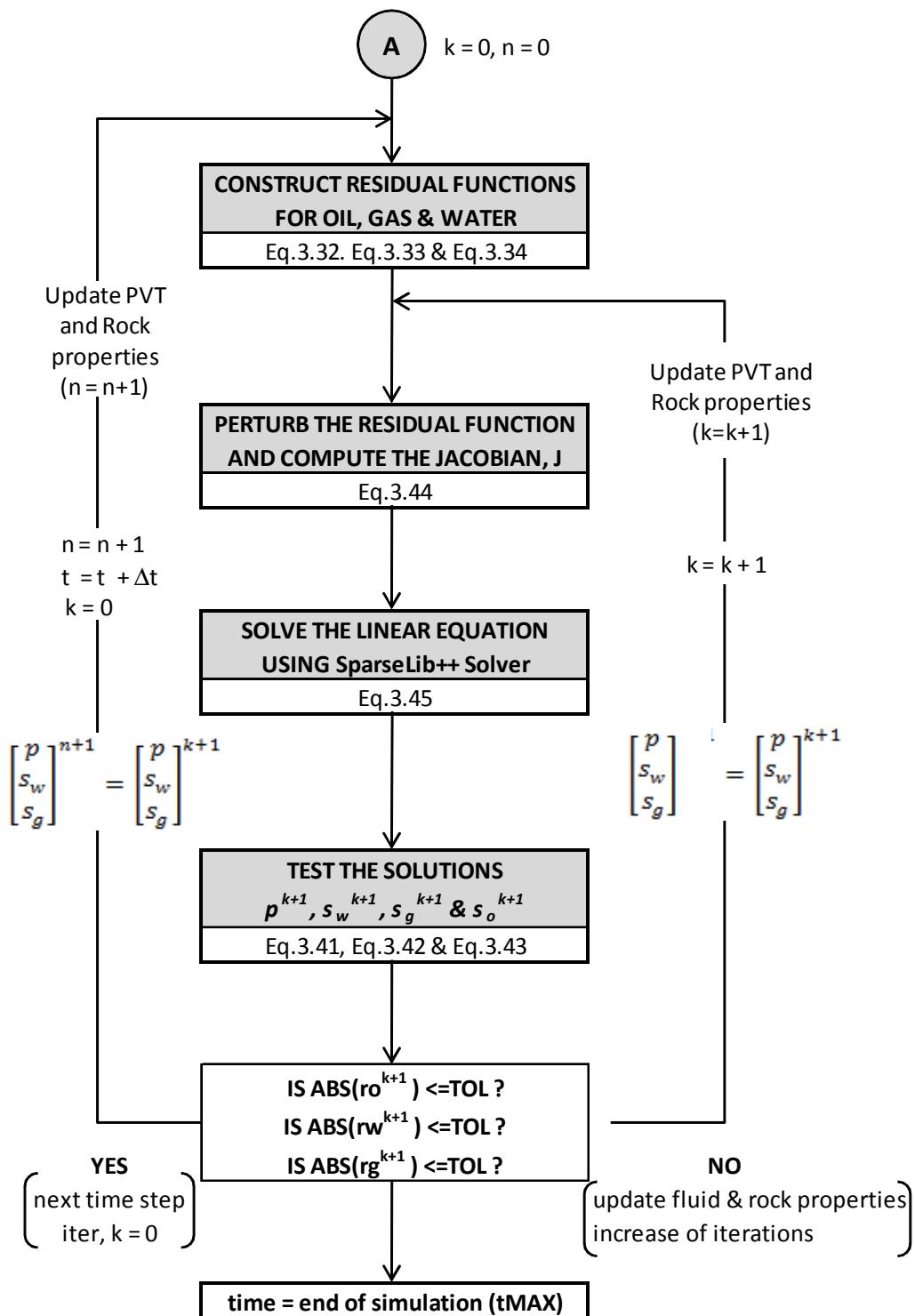


Fig. 3.11-Iteration workflow

CHAPTER IV

VALIDATION OF DFN SIMULATOR

Prior to using the developed DFN simulator to model complex geometry of reservoirs, we extensively validated the simulator against available commercial and academic simulators. Most importantly, we also compared the DFN simulator results against analytical solutions.

This section provides validation procedures of the DFN simulator against single-phase, analytical solutions for well testing and other black-oil academic and commercial reservoir simulators. Several test problems were built to validate the DFN simulator against existing commercial and academic simulators.

The welltest solutions were obtained from welltest software, KAPPA[®]. We used the Computer Modeling Group simulator, IMEX as a commercial black-oil simulator and RZ, which developed by Robert A Wattenbarger³³ as an academic simulator.

Various models were built, from 2D single-phase, to 3D 3-phase unstructured grid models. Block pressures, GOR, saturations and bottomhole pressures were the parameters that were compared in all the validation cases.

In addition to comparison of the results of the DFN and other simulators, one model was built to validate the shape factor formula in the Warren and Root¹ dual-porosity approach. Finally, we validated our simulator with six other simulators that participated in the first SPE comparative solution project⁴¹.

The following are the list of the validation cases:

1. Case I: single-phase DFN and analytical well testing solutions.
2. Case II: DFN to validate “*shape factor*” in dual-porosity approach.
3. Case III: DFN and commercial and academic simulators with rectangular grid model.

4. Case IV: DFN unstructured and structured grid models
5. DFN and first SPE comparative solution project.

4.1 Single-Phase DFN Simulation and Well Testing Solution

A welltest solution was used to validate the DFN simulator against analytical solutions. The analytical solutions can be obtained from any welltest or Pressure Transient Analysis (PTA) software. As mentioned earlier, the analytical solution for the following example was obtained from KAPPA® software.

In order to validate the DFN Simulator against the analytical solution, the DFN model was built to follow the basic assumptions applied in the analytical solution:

- (1) Single phase flow.
- (2) Homogeneous reservoir.

4.1.1 Model Description – Case I

A producer well is located in the center of a square model of 5000 ft x 5000 ft. Constant pressure was applied to all sides of the boundaries (**Fig. 4.1** and **Table 4.1**). The well was operated with the following drawdown and buildup sequences:

1. Drawdown or constant rate of 1000 bbl/day for 12 hours.
2. Build up or shut in the well for 12 hours.
3. Drawdown or constant rate of 1000 bbl/D for 24 hour.
4. Build up or shut in the well for 8 days.

Single phase oil flow behavior could be achieved by modifying the Stone's three-phase relative permeability curves in the black oil simulation model such that only oil dominates the flow (**Fig-4.2** and **Table 4.2**). Constant porosity and permeability values

were applied through the entire model to preserve the homogeneous assumption in the analytical solutions.

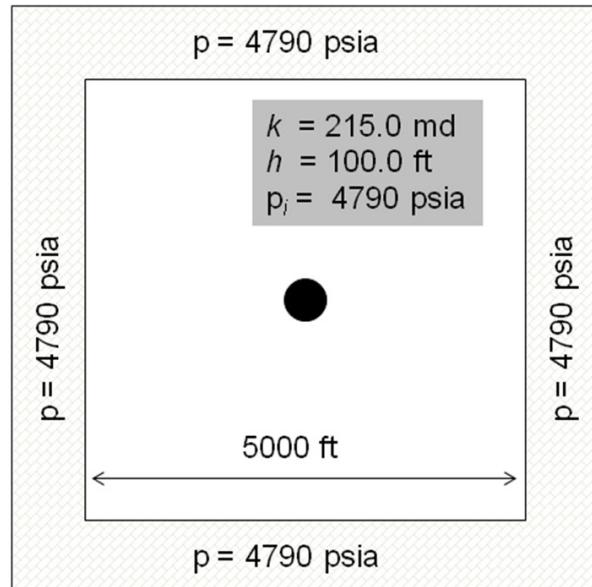


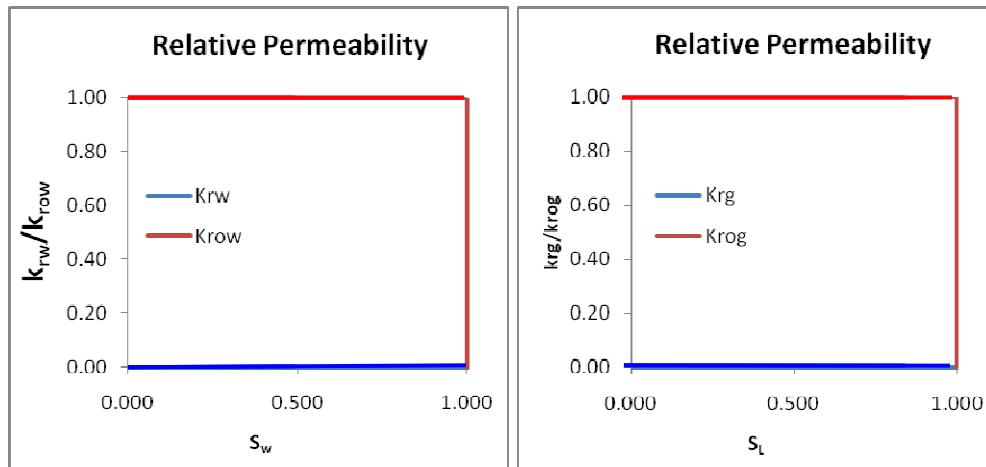
Fig. 4.1–Model description (homogeneous single-porosity model)

Table 4.1 Reservoir and wellbore model

Reservoir and wellbore	
Permeability	215 md
Thickness	100 ft
Porosity	20%
Model dimensions	5000 ft x 5000 ft
Closed-constant pressure boundaries	4790 psia
Initial pressure	4790 psia
Wellbore radius	0.25 ft
Formation volume factor	1.2 RB/STB

Table 4.2 Single-phase relative permeability

s_w	k_{rw}	k_{row}	s_L	k_{rg}	k_{rog}
0.000	0.00	1.00	0.000	0.00	1.00
0.999	0.00	1.00	0.999	0.00	1.00
1.000	1.00	0.00	1.000	1.00	0.00

**Fig4.2-Relative permeability curves for single-phase oil flow**

DFN Simulator was used to run the model and the result was compared to the analytical model provided by the welltest software. Small time step, Δt of 0.01 day was set in order to construct good pressures and derivatives vs. time plots.

There were two flow periods, the second drawdown and the last buildup period that was evaluated to validate results of the DFN simulation. We interpreted the results and expected to get exactly the same properties that were used in the DFN simulation model.

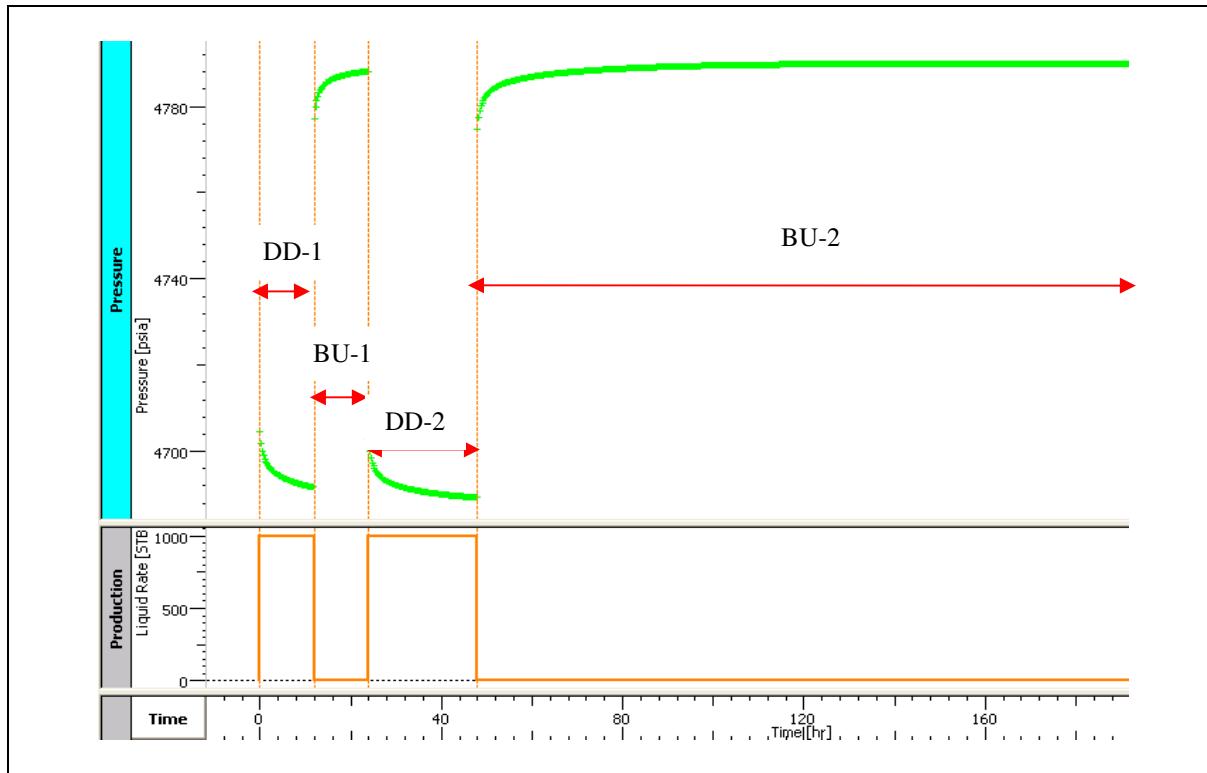


Fig. 4.3—Welltest design (rate and pressure profiles)

Fig. 4.3 shows the complete welltest period (10 days). It contains drawdown and build up periods. The figure shows rate and pressure profiles generated from DFN simulator results.

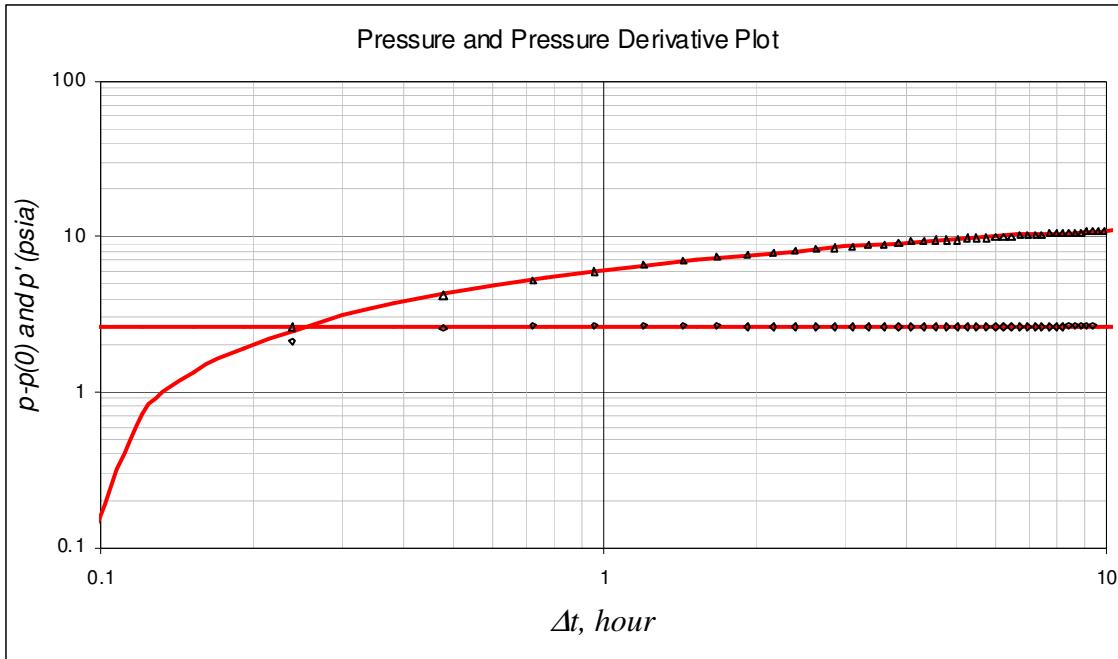


Fig. 4.4—Pressure and the derivative plot for second drawdown period (DD-2)

Fig. 4.4 shows the pressure and its derivative plots of the real data and the interpretation results. The interpretation results were forced using the given DFN model properties. The initial pressures, permeabilities and skin factors were identical between the DFN simulation and analytical solution.

Since we did not incorporate wellbore storage into the DFN model, we assumed the value the wellbore storage was negligible ($C_{wb} = 0$ bbl/psi). However in order to get reasonable matches on pressure and its derivative, the wellbore storage from the well test interpretation was also very small ($C_{wb} = 1.12 \times 10^{-6}$ bbl/psi).

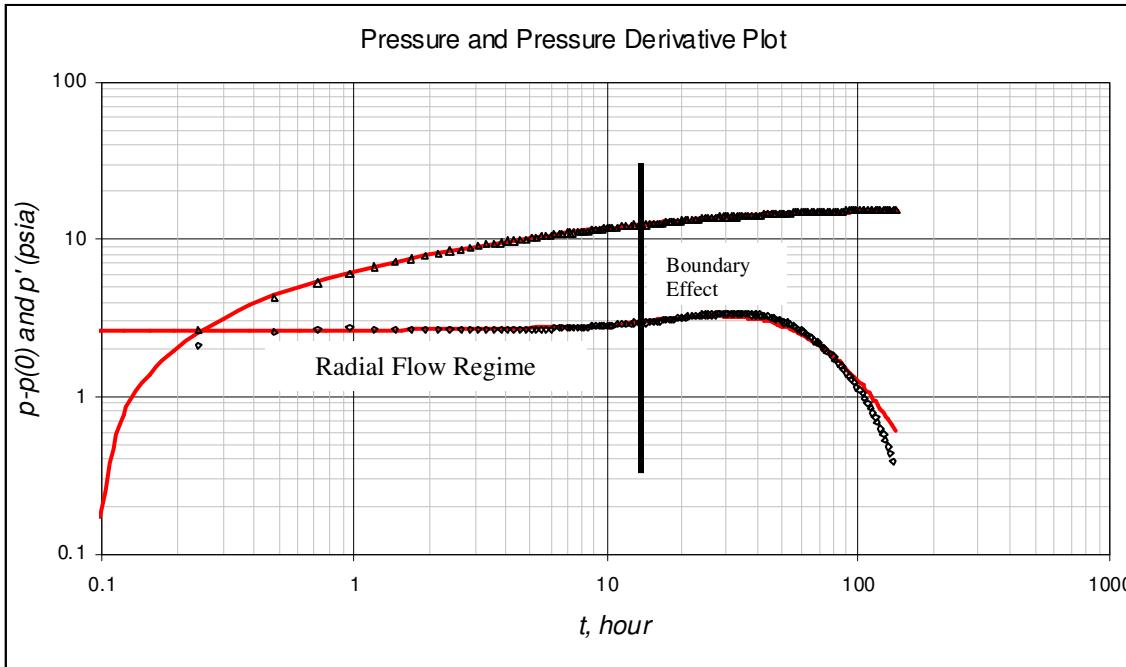


Fig. 4.5–Pressure and the derivative plot for second buildup period (BU-2)

In order to see the boundary effect, we used the second buildup period which was performed for a much longer period compared to the earlier drawdown and buildup periods. The second buildup period was performed for 8 days. The effect of the constant pressure boundary condition was clearly shown in the pressure derivative plot (**Fig.4.5**).

As expected, the DFN simulation was in excellent agreement with the welltest interpretation results. As it was shown in the DD-2 interpretation, the wellbore storage effect could be considered negligible for the BU-2 period as well ($C_{wb} = 1.65 \text{ E-6 bbl/psi}$).

In addition to the interpretation results provided from DD-2 and BU-2 periods, we could construct the pressure profile for the entire test periods as shown in **Fig. 4.6**. The difference between DFN simulator result and analytical solution is not noticeable.

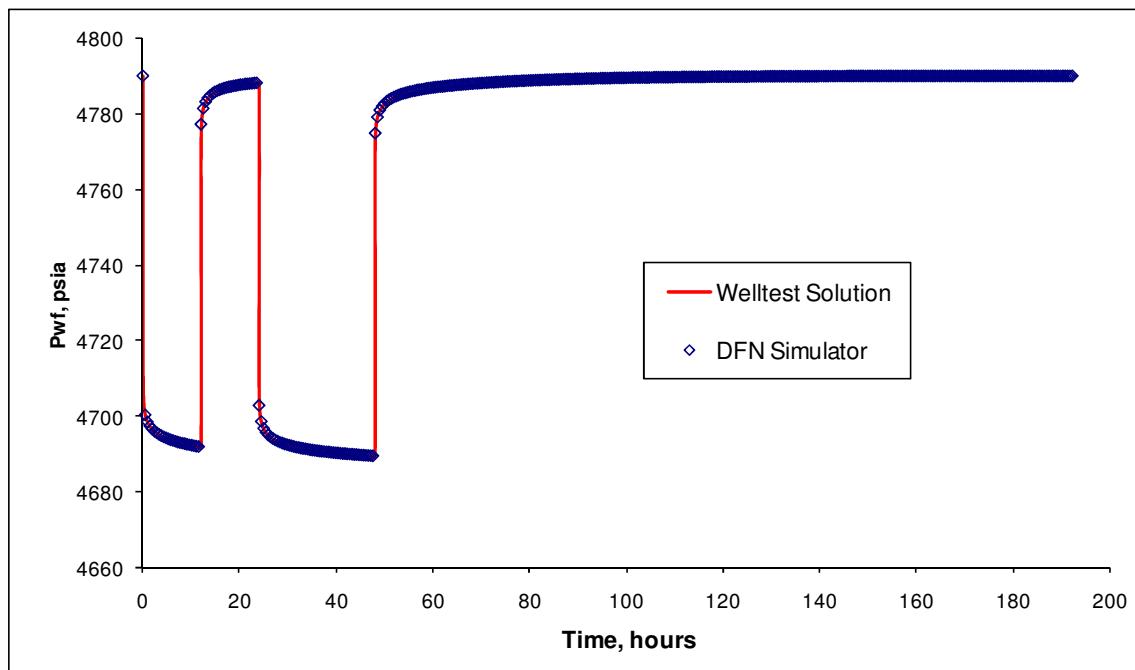


Fig. 4.6-Welltest and DFN Simulator (All test periods)

4.2 DFN Simulator and Dual-Porosity Model

This particular test case demonstrates the use of the DFN simulator to investigate the “shape factor” (σ), the value to quantify the matrix-fracture drainage in the dual-porosity model.

Matrix-fracture drainage in the dual-porosity model was idealized by Warren and Root¹ and expressed using the following equation.

$$q^* = \frac{q}{V_b} = \sigma \frac{k_m}{\mu} (p_m - p_f) \quad \dots \dots \dots \quad (4.1)$$

where,

q^* = drainage rate per bulk volume.

V_b = bulk volume.

k_m = matrix permeability.

μ = fluid viscosity.

p_m = pressure of matrix block.

p_f = pressure of fracture.

σ = dual-porosity shape factor.

Eq.4.1 is applied for pseudo-steady state flow which means that the drainage rate, q^* from matrix to fracture is constant.

4.2.1 Model Description – Case II

Fig. 4.7 represents one quarter of a full 2D model to represent a single matrix block in dual-porosity model. The distances between fractures are the same along x and y directions. High permeability and low permeability are applied for fractures and matrix blocks respectively. Parameters for Case II are shown in **Table 4.3**.

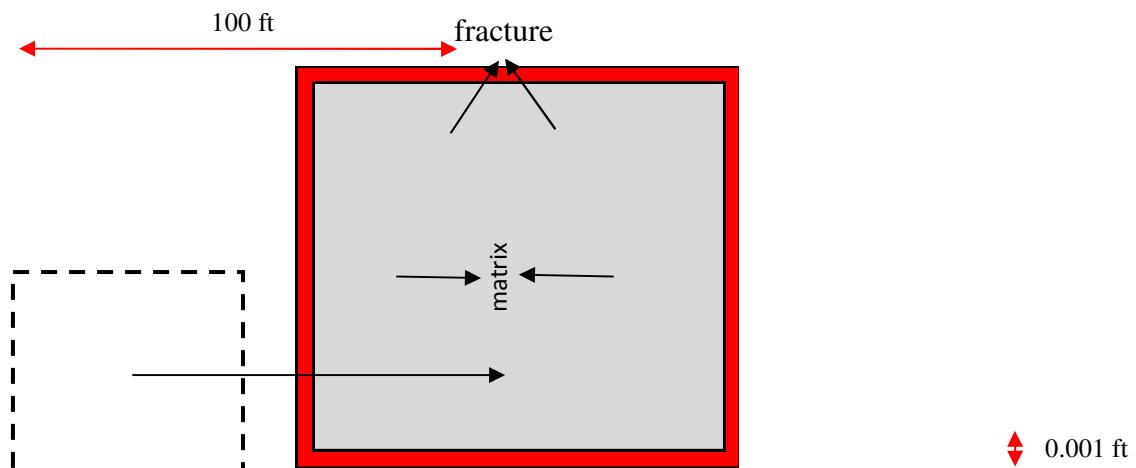


Fig. 4.7-“Shape factor” dual-porosity model

Table 4.3-Model description (Case II)

Fracture width, w	0.001 ft
Fracture spacing, $L_x=L_y$	100 ft
Fracture permeability, k_f	10,000 md
Matrix Permeability, k_m	0.0001 md
Formation Volume Factor, B_o	1.0 RB/STB
Viscosity, μ_o	0.7 cp
Bulk Volume, V_b	100x100x20 = 200,000 cu-ft

Small and constant drainage rate ($q = 0.001$ cu-ft/day) from matrix and fracture are applied along the fractures. The simulation was run for several days. At the early time, transient flow occurred followed by stabilized flow regime (pseudo-steady state flow).

The following steps were used to investigate dual-porosity shape factor under constant drainage condition:

1. Record the value of $\Delta p/q$ after the occurrence of pseudo-steady state flow.

From **Fig. 4.8**, the $\Delta p/q = 0.31442$ psi/cu-ft/D

2. Calculate $\Delta p/q^*$.

If $q^* = q/V_b$, the value of $\Delta p/q^*$ is $0.31442 \times V_b = 0.31442 \times 2.0E+5 = 62,884$

3. In order to represent a full model (a single matrix block model), the $\Delta p/q^*$ from a quarter model should be divided by 4. Therefore, the $\Delta p/q^* = 62,884 / 4 = 15,721$.
4. Calculate the shape factor by using **Eq. 4.1**.

$$\sigma = 0.00282$$

5. With $\sigma = 0.00282$ and fracture spacing of 100 ft, we can express the shape factor with the following formula:

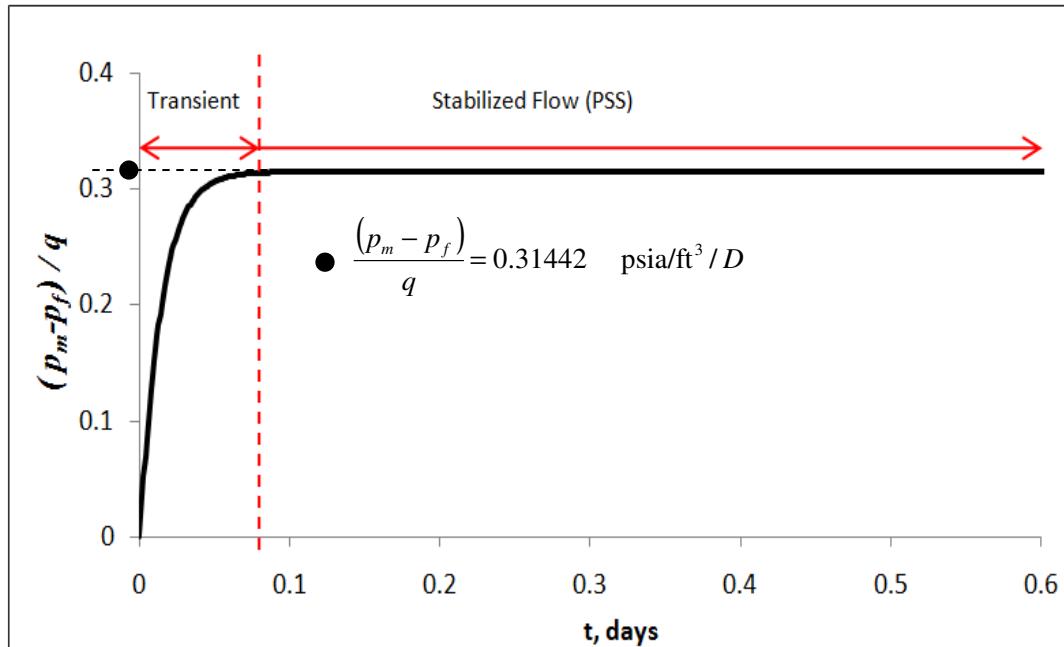
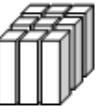
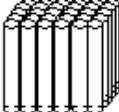
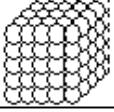


Fig. 4.8-Plot of $\frac{(P_m - P_f)}{q}$ vs. time (transient & pseudo-steady states)

The shape factors as function of fracture spacing from other researchers with a constant drainage rate are depicted in the **Table 4.4**.

For the same geometry, this expression is consistent with several authors. Mora et al.⁴² and Coats⁴³ obtained 28.43 and 28.5 respectively.

Table 4.4-Shape factors from different authors (after Mora et al.⁴²)

Geometry	Constant Fracture Pressure			Constant Rate (ps)			This study
	W & R¹	Kazemi⁴⁴	Zimmerman /Lim & Aziz^{45,46}	Mora⁴²	Coats⁴³	Mora⁴²	
	12	4*	$\pi^2 = 9.87$	$\pi^2 = 9.87$	12	12	
	32*	8*	$2\pi^2 = 19.74$	$2\pi^2 = 19.74$	28.5	28.43	28.2
	60*	12*	$3\pi^2 = 29.61$	$3\pi^2 = 29.61$	49.6	49.48	
			$18.17 \left(-L^2 \frac{23.11}{D^2} \right)$	$18.17 \left(-L^2 \frac{23.11}{D^2} \right)$		$25.13 \left(= L^2 \cdot \frac{32}{D^2} \right)$	
			$25.67 \left(= L^2 \frac{4\pi^2}{D^2} \right)$	$25.67 \left(= L^2 \frac{4\pi^2}{D^2} \right)$		$38.98 \left(= L^2 \cdot \frac{60}{D^2} \right)$	

4.3 DFN Simulator and Commercial Reservoir Simulators

This section will describe the validation procedures and present the results of the DFN simulator against commercial simulator. As previously mentioned, the commercial simulator used for this validation was the black oil simulator, IMEX as part of package from Computer Modeling Group (CMG). A 3-D, three-phase black oil model was simulated using both IMEX and DFN simulator.

4.3.1 Model Description – Case III

A simple example case was created based on a regular Cartesian 3-D reservoir model grid of 5x5x3 (**Fig. 4.9**). The dimension of each block is 1,200 ft x 1,200 ft x 100 ft. The three-phase model contains one producer located in the one corner of the model. The producer is perforated on the corner top layer and operated with constant oil rate (1000 stb/d) under the constraint of minimum bottom-hole pressure (1000 psia). The reservoir is homogeneous. Lateral permeabilities of 215 md and vertical permeability of 21.5 md were applied to each layer. The detailed data of the model is provided in the **Table 4.3**, **Table 4.4** and **Table 4.5**.

Table 4.3- Three-phase fluid properties

<i>p</i> (psi)	<i>Rs</i> (SCF/STB)	<i>Bo</i> (RB/STB)	<i>Bg</i> (RB/SCF)	<i>Viso</i> (cp)	<i>Visg</i> (cp)	<i>Co</i> (1/psi)
14.7	1.0	1.062	0.9358	1.040	0.0080	1.581E-05
264.7	90.5	1.150	0.0679	0.975	0.0096	1.575E-05
514.7	180.0	1.207	0.0352	0.910	0.0112	1.569E-05
1014.7	371.0	1.295	0.0180	0.830	0.0140	1.556E-05
2014.7	636.0	1.435	0.0091	0.695	0.0189	1.533E-05
2514.7	775.0	1.500	0.0073	0.641	0.0208	1.521E-05
3014.7	930.0	1.565	0.0061	0.594	0.0228	1.509E-05
4014.7	1270.0	1.695	0.0046	0.510	0.0268	1.487E-05
5014.7	1618.0	1.827	0.0036	0.449	0.0329	1.465E-05
9014.7	2984.0	2.357	0.0022	0.203	0.0470	1.384E-05

Table 4.4 provides additional data at the reference pressure:

Table 4.4 Fluid properties at reference pressure

$B_w = 1.03 \text{ RB/STB}$
$c_w = 3 \times 10^{-6} \text{ psia}^{-1}$
$\rho_w = 63.24 \text{ lb/cu-ft}$
$\mu_w = 0.31 \text{ cp}$
$\rho_o = 46.24 \text{ lb/cu-ft}$
$\rho_g = 0.0647 \text{ lb/cu-ft}$
$p_{\text{ref}} = 4790.0 \text{ psia}$
$p_b = 4017.7 \text{ psia}$

Table 4.5 Three-phase relative permeability data

Water-Oil Saturation

SWT	KRW	KRNW
0.0000	0.0000	1.0000
0.3996	0.0000	1.0000
0.5994	0.0000	1.0000
0.9990	0.0000	1.0000
0.9992	0.2000	0.8000
0.9998	0.8000	0.2000
1.0000	1.0000	0.0000

Gas-Oil Saturation

SLT	KRG	KRNG
0.0000	1.0000	0.0000
0.1500	1.0000	0.0000
0.3000	0.9970	0.0000
0.4000	0.9800	0.0050
0.5000	0.7000	0.0250
0.5500	0.3500	0.0750
0.6000	0.2000	0.1250
0.7000	0.0900	0.1900
0.7500	0.0210	0.4100
0.8000	0.0100	0.6000
0.8800	0.0010	0.7200
0.9500	0.0001	0.8700
0.9800	0.0000	0.9400
0.9990	0.0000	0.9800
1.0000	0.0000	1.0000

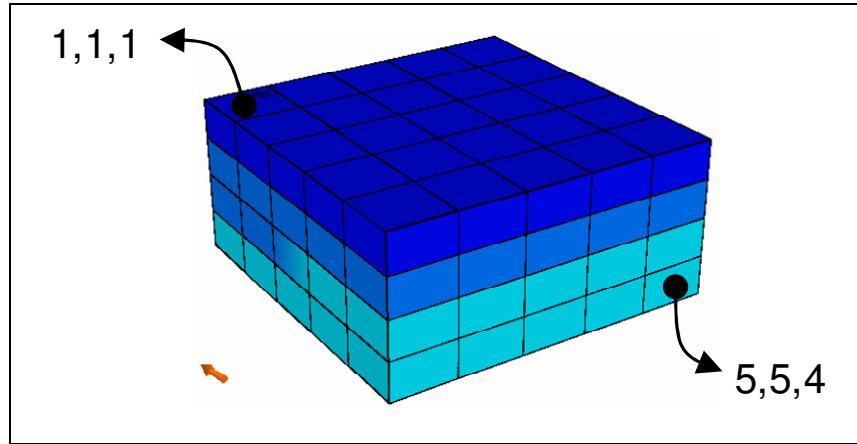


Fig. 4.9–Grid model of Case III (5 x 5 x 3)

The simulation was run for a short period (100 days). Both simulations were run using a fully-implicit scheme. The maximum residual errors in each time step were kept at 1×10^{-6} . We compared the pressure and oil saturation from both simulators.

We selected two different locations in the model to compare the pressures. One was at the well block (block 1,1,1) and another one was at the furthest distance from the well (block 5,5,4). The oil saturation at the well block was also observed.

The results of the two simulators were as expected. The pressures at the well block and at block 5,5,4 from DFN simulator were in good agreement with CMG results (**Fig. 4.10**). The match was also followed by the oil saturation at the well block (**Fig. 4.11**).

The relative error in pressure between the two simulators was less than 0.01%. This error primarily occurred during the early time period (the first 5 days). This could be reduced by setting smaller time step sizes at the early time. However, since the validation results were extremely good, we decided not rerun the model.

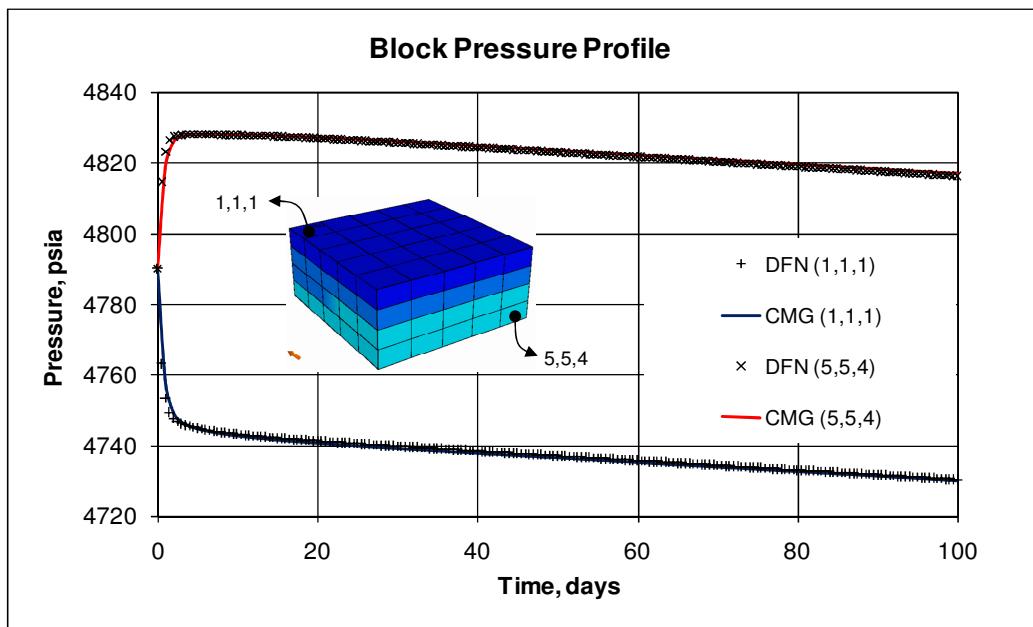


Fig. 4.10—Pressure profiles at the well block and furthest location from the well

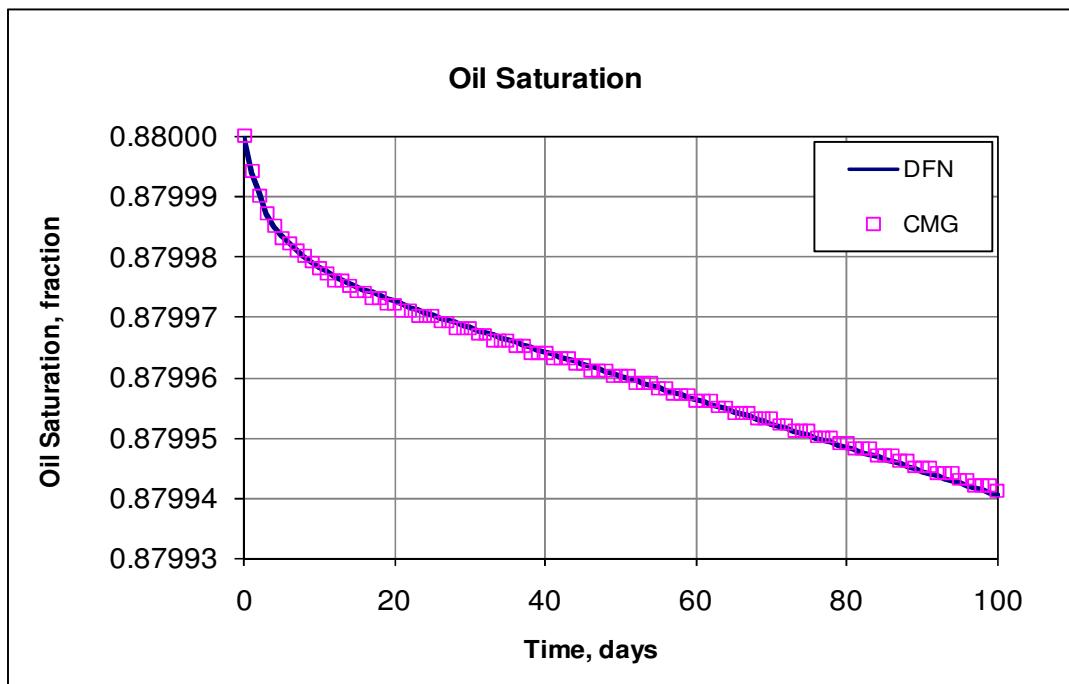


Fig. 4.11—Oil saturation at the well block

4.4 DFN Simulator Validation against RZ and Commercial Reservoir Simulators – Voronoi and Regular Grid Systems

The following section will present several example cases to validate the regular Cartesian grid and Voronoi grid system of the DFN simulator against IMEX and academic simulator (RZ).

In previous chapters, we have discussed how Voronoi algorithm can be used to generate various grid shapes. Thus, the purpose of this validation is to show the flexibility of Voronoi grid system in the DFN simulator compared with the academic and commercial simulators. In order to achieve this goal, a 2D black oil and unfractured model with no fractures should be created using all three simulators (IMEX, RZ and DFN simulator).

4.4.1 Model Description – Case IV

There were six different models tested in this exercise. They are:

1. CMG or IMEX with Cartesian regular grid system (CMG) – **Fig. 4.12a**
2. RZ with Cartesian regular grid (RZ-Regular) – **Fig. 4.12a**
3. DFN with Cartesian regular grid (REGULAR) – **Fig. 4.12a**
4. DFN with combination of regular and hexagonal grid (HEXA) – **Fig. 4.12b**
5. DFN with combination of regular and triangle grid (TRIANGLE) – **Fig. 4.12c**
6. DFN with irregular Voronoi grid (IRREGULAR) – **Fig. 4.12d**

The only difference between Case III and Case IV is the number of layers. The layer thickness is 100 ft. The fluid and rock properties were kept identical with the previous validation case. The numerical controls, e.g. time step, maximum saturations change, maximum pressures change and residual errors were also kept the same. All the runs utilized a fully-implicit finite difference scheme.

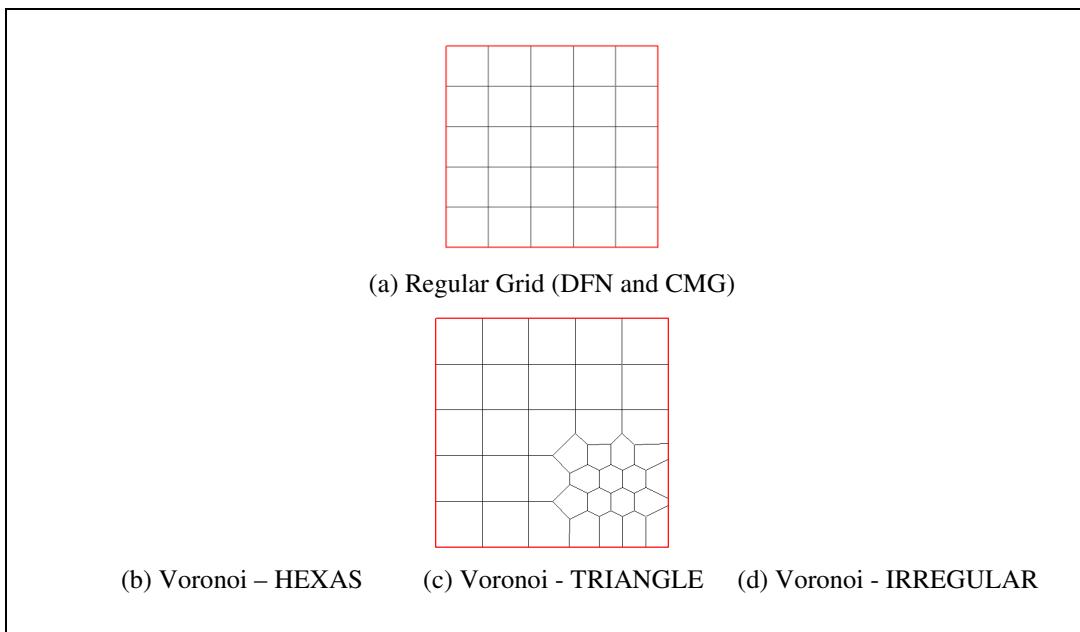


Fig. 4.12–CMG, RZ and DFN grid models (CASE 4)

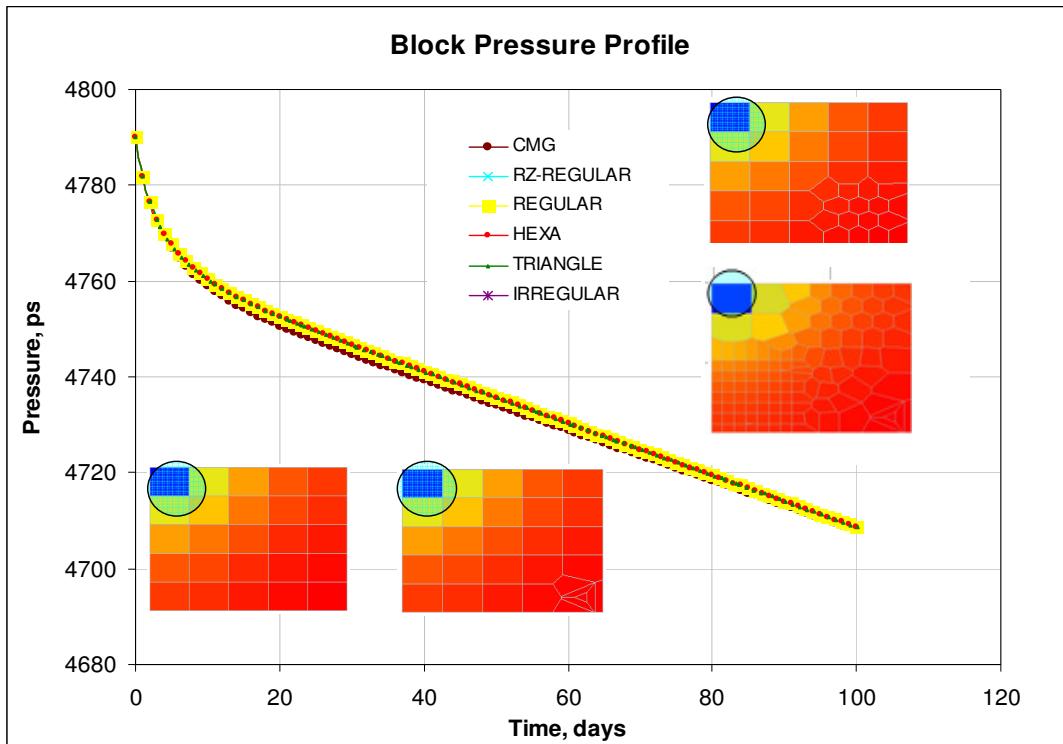


Fig. 4.13 – Block pressure profile of CMG, RZ and DFN with various grid systems

Fig. 4.13 shows the pressure profile of all six models using different simulators and various grid designs. It is clear that the DFN simulator with the Voronoi grid were in good agreement with the commercial and academic simulator for all grid designs.

4.5 DFN Simulator and First SPE Comparative Study

Similarly with other simulators, we also compared the results our DFN simulator with other simulators (commercial and in-house simulators) presented in the first SPE comparative study⁴¹.

The first SPE comparative study was published in 1981. The model was a black-oil, 3-layer gas injection/oil production problem. The grid size was 10 x 10 x 3. The initialization and recurrent data were reported in detail in the original paper, and these data were used to setup the case for DFN Simulator. The grid dimension and well completions are depicted in **Fig. 4.14** and **Fig. 4.15** respectively.

The original study tested two different cases; the first case had constant saturation pressure (4014.7 psia), and the second case had a variable bubble-point pressure due to the variation of gas saturation. Only Case 1 results will be compared with DFN Simulator.

Fig. 4.16 and **Fig. 4.17** present the comparison of the well response in plots of oil rate vs. time and Gas-Oil Ratio vs. time for Case 1. The problem does not pose any major numerical difficulties and all the results are close. The results of the DFN simulator are well within the group for both IMPES and fully implicit methods of solution that were used by other simulators at the time. **Fig.4.18** and **Fig. 4.19** present the comparision of block pressure at the producer well and pressure across the diagonal from the producer to the injector respectively.

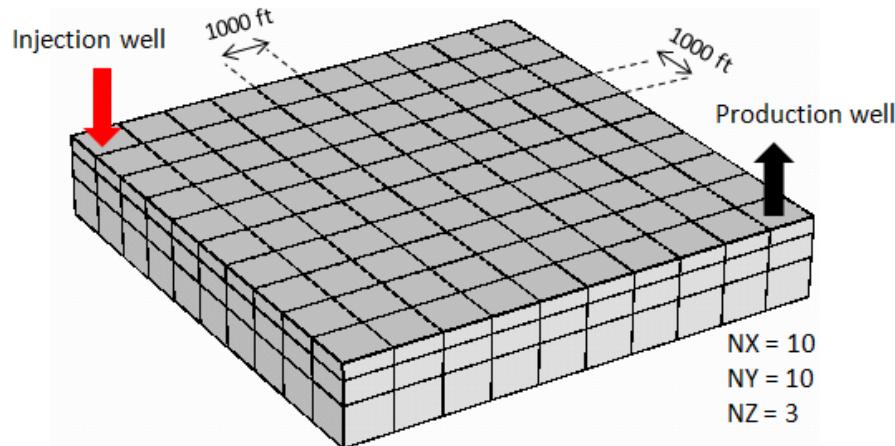


Fig. 4.14-2D grid model of first SPE comparative study (after Odeh et al.⁴¹)

Gas injection well Flow rate = 100 MMSCF/D		Oil production well Minimum BHP = 1000 psia						
\emptyset	H, ft	k _x , md	k _y , md	k _z , md	sw	so	Depth	
0.3	20	500	500	50	0.12	0.88	8335	
0.3	30	50	50		0.12	0.88	8360	
0.3	50	300	300	25	0.12	0.88	8400	

Fig. 4.15-Well completion data and layer properties (after Odeh et al.⁴¹)

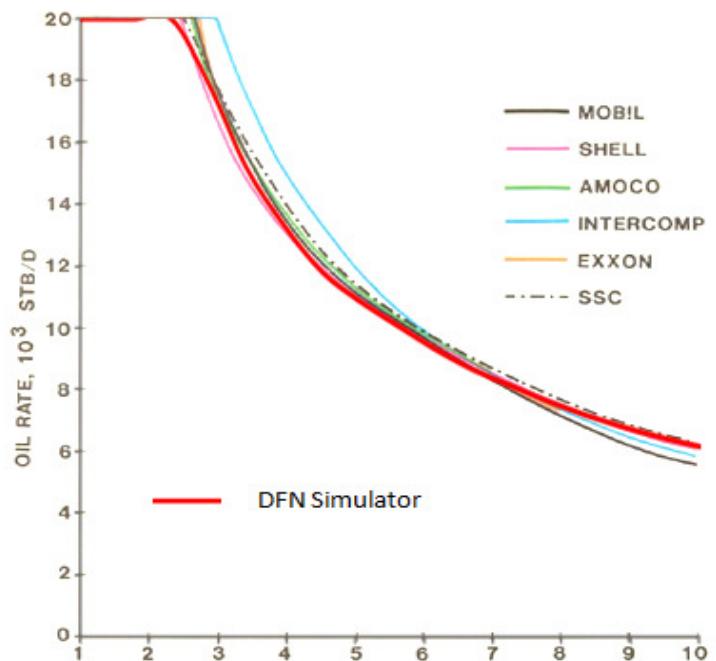


Fig. 4.16-Oil rate (after Odeh et al.⁴¹)

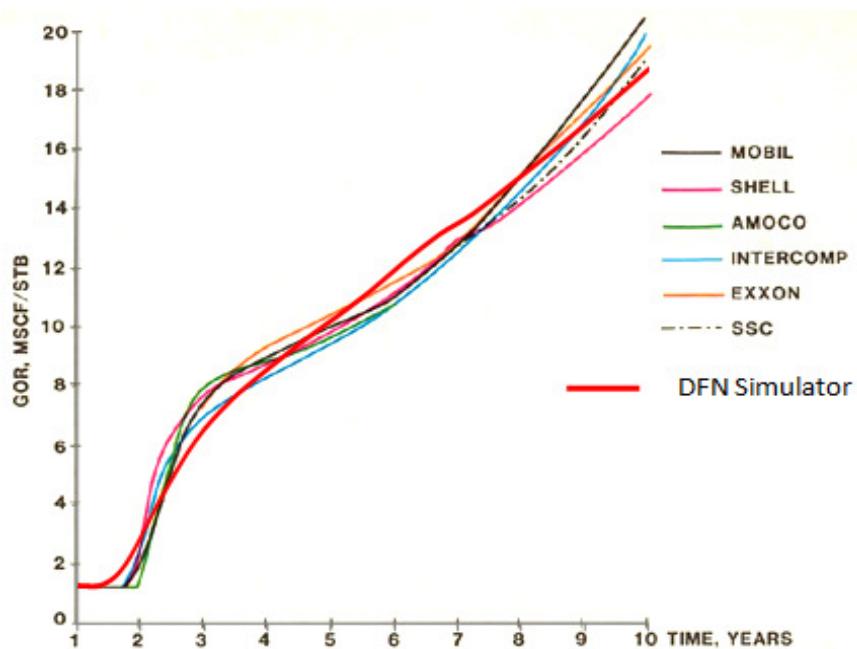


Fig. 4.17-Gas-oil ratio (after Odeh et al.⁴¹)

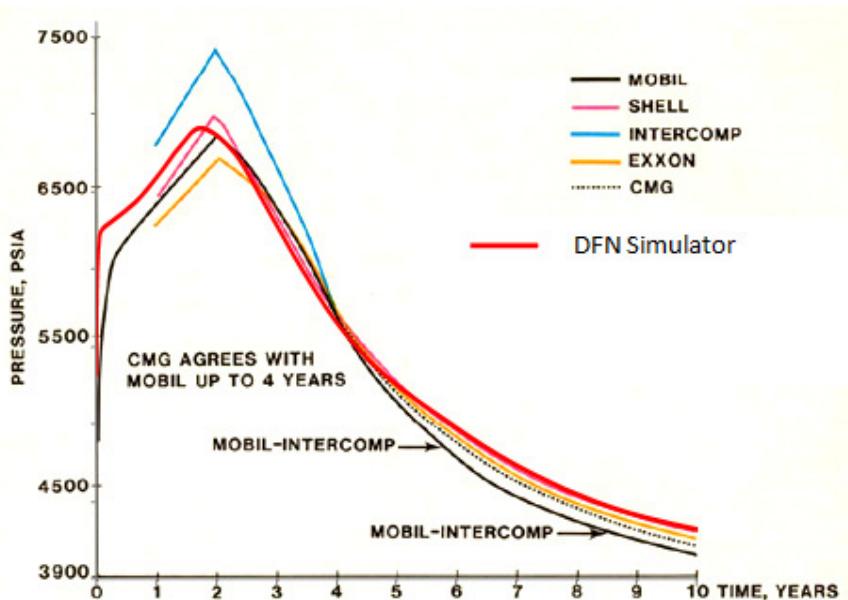


Fig. 4.18- Producer wellblock pressures (after Odeh et al.⁴¹)

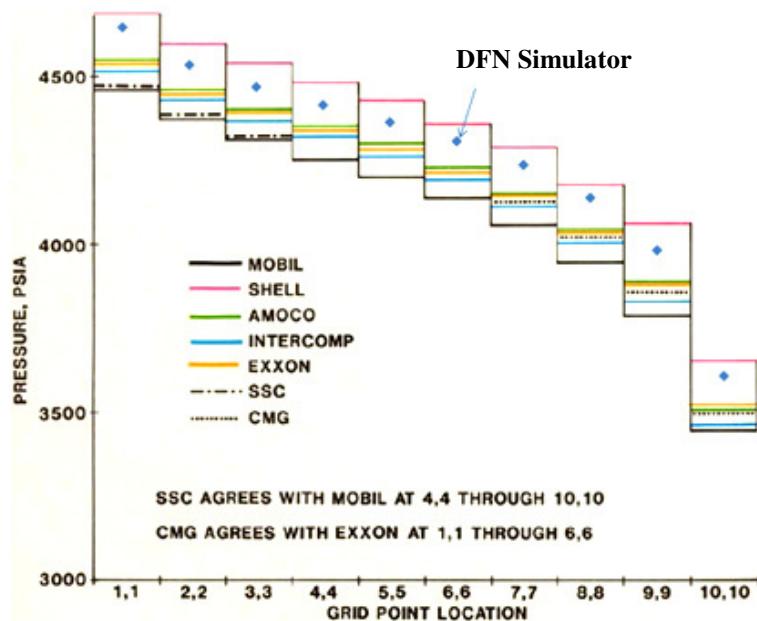


Fig. 4.19 – Block pressure at time = 8 years (after Odeh et al.⁴¹)

CHAPTER V

SIMULATION OF DISCRETE FRACTURE NETWORKS USING VORONOI GRID SYSTEM

The previous chapter discussed the validation procedures of the DFN simulator that we have developed. The validation results have confirmed that the DFN simulator is comparable with other reservoir simulators and excellent agreement with welltest analytical solutions.

In this chapter, we mainly use the simulator to demonstrate various capabilities to model complex reservoir geometries, especially for fractured systems. Several simulations such as models of regular fracture spacing, multiple-fracture (isolated and connected fractures) geometries were performed to demonstrate the capabilities of the developed simulator.

The first model of regular fracture spacing was chosen to show the effects of aperture distribution on reservoir performance. Some other exercises are solely intended to show the unique features of the simulator. The unique features here are the gridding techniques, capability to incorporate fracture apertures distribution into reservoir model and etc.

Besides the capability to model complex geometry of fractures, an additional neat feature of our DFN simulator to run multiple-model simulations simultaneously is also reported in this section.

The simulation datasets of the entire exercises reported in this chapter are attached in the APPENDIX C.

5.1. DFN Simulation of 2D Regular Fracture Spacing

The following test cases were intended to show the effects of fractures and their aperture distribution on reservoir performance. Two models were built. One case was reservoir with uniform fracture apertures (CASE 5.A1) and the other one with log-normally distributed apertures (CASE 5.A2).

The matrix and fracture porosities are 0.25 and 0.5 respectively. The permeabilities of fractures were calculated using cubic law formulation based on the apertures of the fractures. Fracture permeability for CASE 5.A1 is 9,055 md (fracture width = 0.1 ft) and fractures permeabilities for CASE 5.A2 were in the range of 25 md to 300,000 md with mean of 9,055 md. The fluids and other rock properties were identical with the first SPE comparative study.

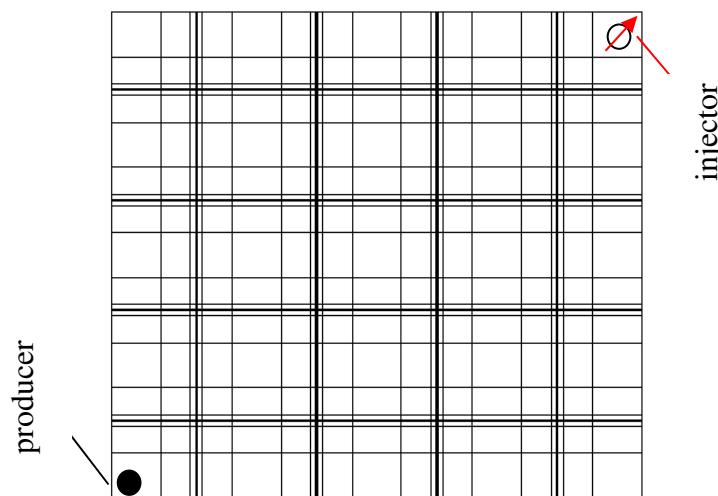
Fig. 5.1 shows the squared grid model (33 x 33 x 1) applied for both cases. We used variable grid sizes, with finer grids near the fractures. The largest grid blocks are 500 ft x 500ft and the smallest blocks are 0.1 ft x 0.1 ft. The model dimension is 5,380.4 ft x 5,380.4 ft. It is a single-layer model with thickness of 100 ft.

A producer well is located in the bottom left corner and the injector well is located at the top right corner of the model. The producer well was operated with a constant oil rate of 15,000 STB/D and minimum bottomhole pressure of 1,000 psia was set as constrain. Gas was injected constantly at 50 MMSCF/D until end of simulation (10 years).

Table 5.1 is the summary of the model descriptions and **Fig. 5.1** shows the grid model of these two cases.

Table 5.1-Model descriptions (CASE A1 and CASE A2)

Descriptions	CASE 5.A1	CASE 5.A2
Grid dimension	33x33x1	33x33x1
Fracture spacing	1,220 ft	1,220 ft
Model width/ Length	5,380.4 ft	5,380.4 ft
Model thickness	100 ft	100 ft
Matrix permeability	50 md	50 md
Fracture permeability	Constant 9,055 md	Log-normally distributed 24 md – 300 D (mean = 9,055 md)
Matrix porosity	0.25	0.25
Fracture porosity	0.5	0.5
Fluid properties	SPE-1	SPE-1
Initial conditions	SPE-1	SPE-1
Other rock properties	SPE-1	SPE-1
Producing rate	Oil, 15,000 STB/D	Oil, 15,000 STB/D
Minimum produce BHP	1,000 psia	1,000 psia
Injection rate	Gas, 50 MMSCF/D	Gas, 50 MMSCF/D

**Fig. 5.1–CASE 5.A1 and CASE 5.A2 grid model (33 x 33 x 1)**

With fully implicit scheme, both simulations ran relatively smooth, especially for CASE 5.A1. There were no serious numerical problems occurred during the simulations except for several times in CASE 5.A2 the simulation performed time step cuts and reached the maximum linear solver iteration. The detailed numerical performances of these simulations are presented in **Table 5.2**. The material balance error vs. time plot is depicted in **Fig. 5.2**.

Table 5.2-Numerical information and simulation time of CASE 5.A1 and CASE 5.A2

Numerical Performances	CASE 5.A1	CASE 5.A2
Maximum residual error	1.0E-3	1.0E-3
Max. Newton iteration	20	20
Max. linear solver iteration	30	30
Linear solver tolerance	1.0E-3	1.0E-3
Newton iteration	956	1,150
Solver iteration	11,703	29,061
Time step cut	0	10
Simulation time	475 sec.	873 sec.

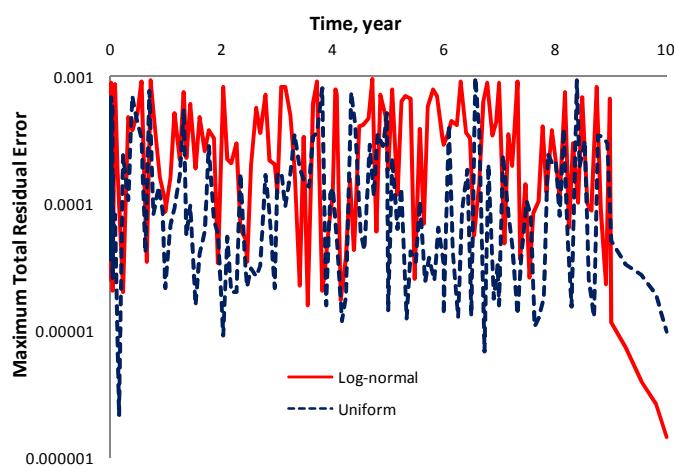


Fig. 5.2-Maximum total material balance error (CASE 5.A1 and CASE 5.A2)

Fig. 5.3, Fig. 5.4, Fig. 5.5 and Fig. 5.6 are the 2D visualizations of pressures and gas saturation after 90, 365, 900 and 3,650 days respectively. At the early time until end of simulation the constant fracture permeability case shows more uniform streamlines compared to the log-normally distributed fracture permeabilities case.

The gas front was moving relatively faster, more sporadic and some oil trapped behind the gas region due to the permeability field in the CASE 5.A2 model. The impacts of the permeability distributions can be clearly noticed on the recovery (**Fig. 5.7**), gas-oil ratio (**Fig. 5.8**), oil rate performances (**Fig. 5.9**), bottomhole pressure (**Fig. 5.10**) and wellblock pressure at the producer location (**Fig. 5.11**).

The recovery factors are 45% for CASE 5.A1 and 41.5% for CASE 5.A2. The gas breakthrough occurred after 3.5 and 4 years for CASE 5.A1 and CASE 5.A2 respectively.

These small differences of the recovery factors and breakthrough times were due to small number of fractures introduced in the model. We might be able to see more significant differences due to the fracture distributions if we had more extensive number of fractures in the models. In our model, the fractures are just occupied approximately 0.05% of the total pore volume.

Hopefully, from these exercises is able to convince many of us that besides fracture spacing, fracture aperture distribution plays very important role to the performances of reservoirs.

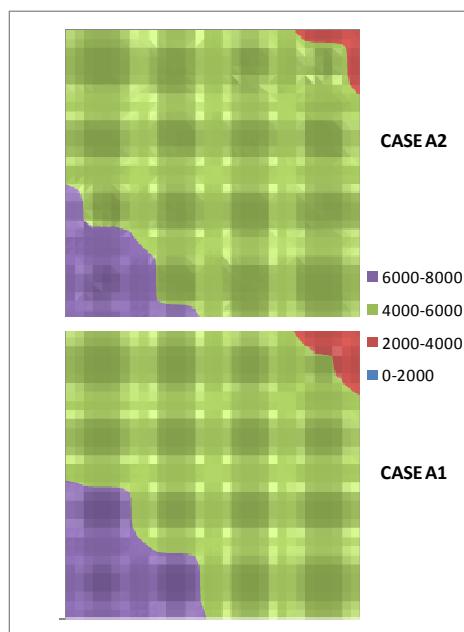


Fig. 5.3-Pressures and gas saturation at time = 90 days

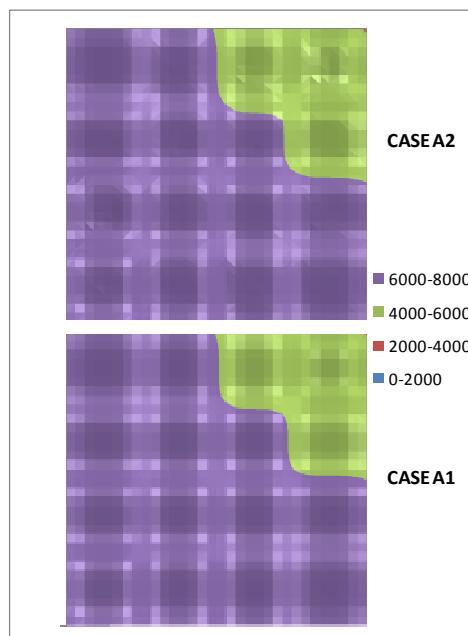


Fig. 5.4-Pressures and gas saturation at time = 365 days

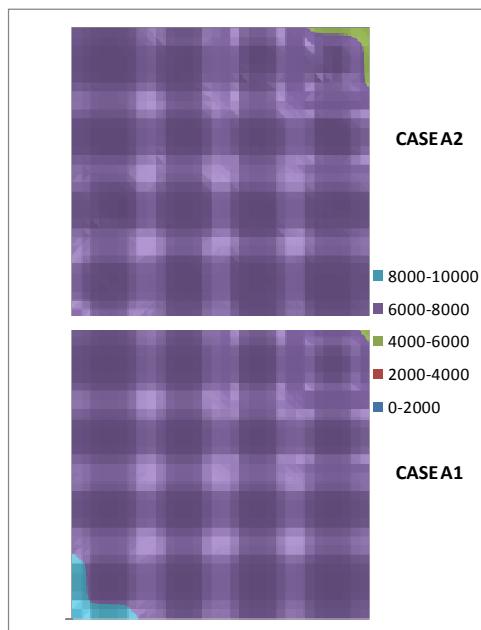


Fig. 5.5-Pressure and gas saturation at time = 900 days

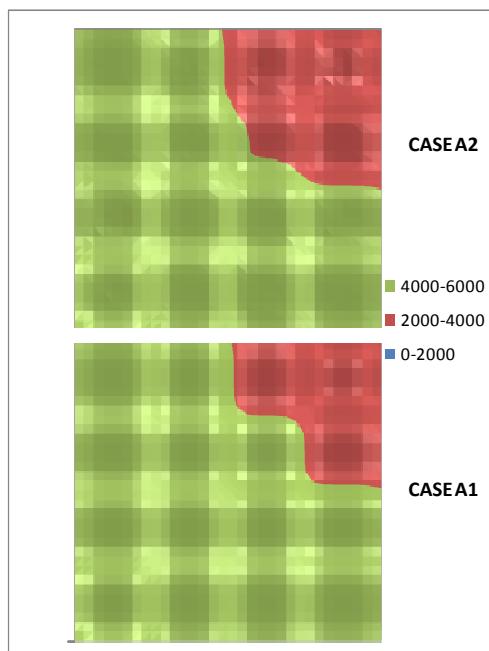


Fig. 5.6 Pressure and gas saturation at the end of simulation (time = 3650 days)

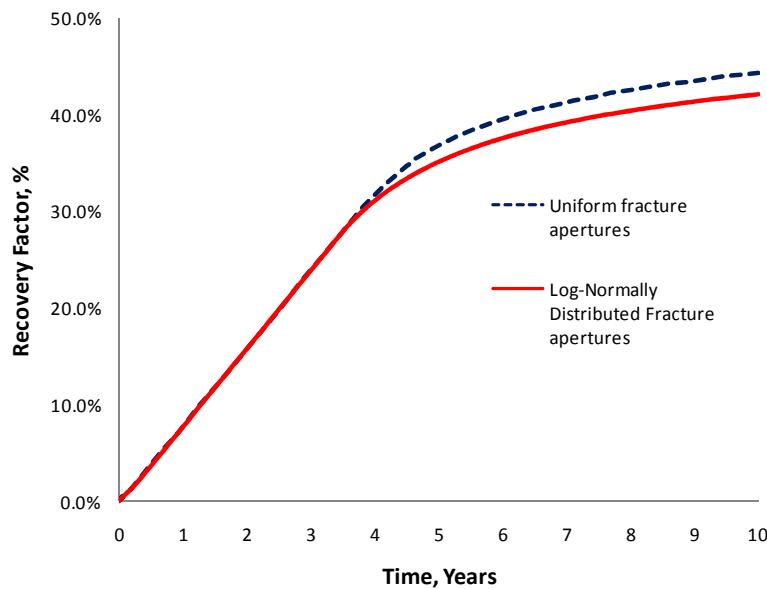


Fig. 5.7-Recovery factor (CASE 5.A1 and CASE 5.A2)

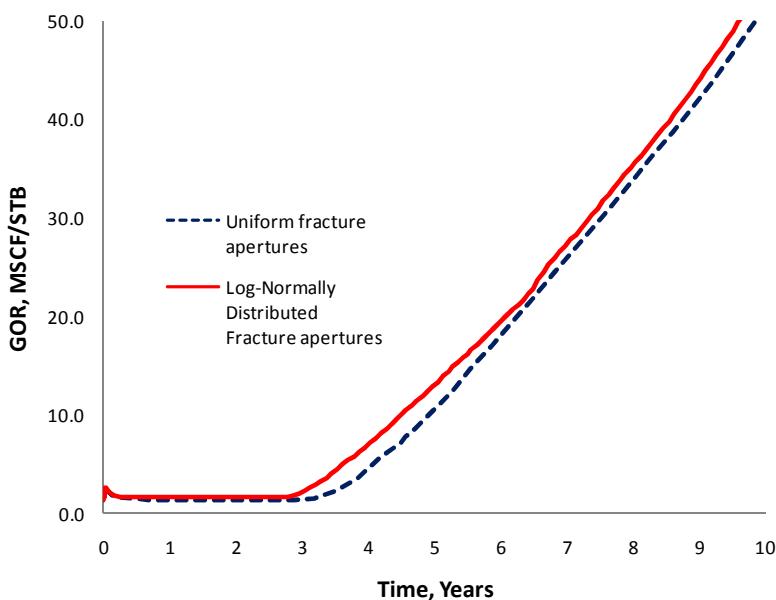


Fig. 5.8-Produce gas-oil ratio (CASE 5.A1 and CASE 5.A2)

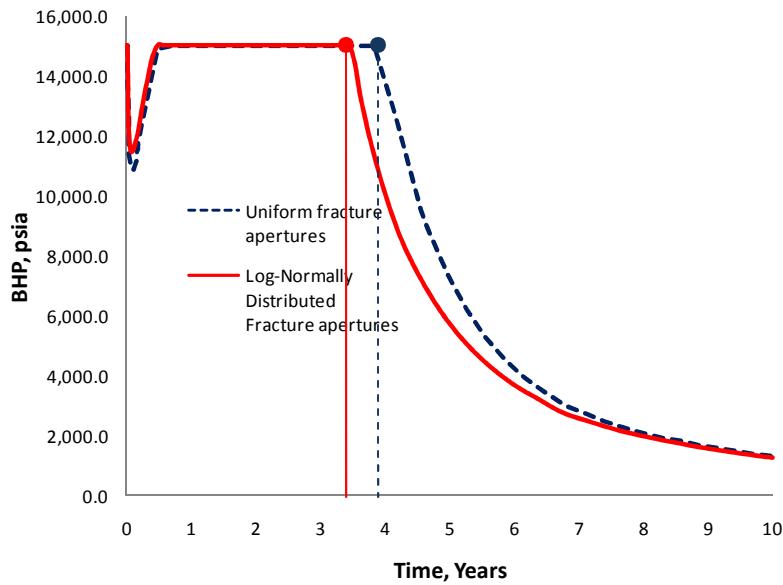


Fig. 5.9-Produced oil rate (CASE 5.A1 and CASE 5.A2)

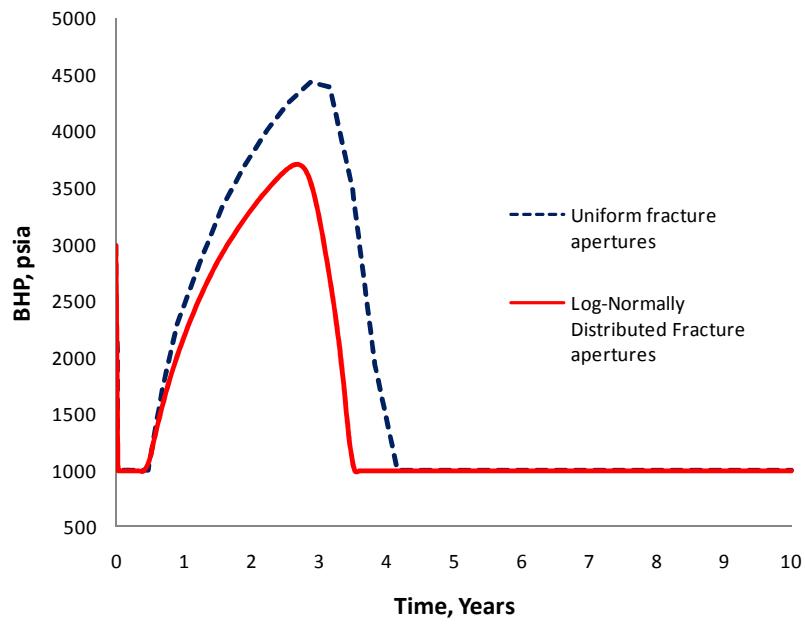


Fig. 5.10-Bottomhole pressures (CASE 5.A1 and CASE 5.A2)

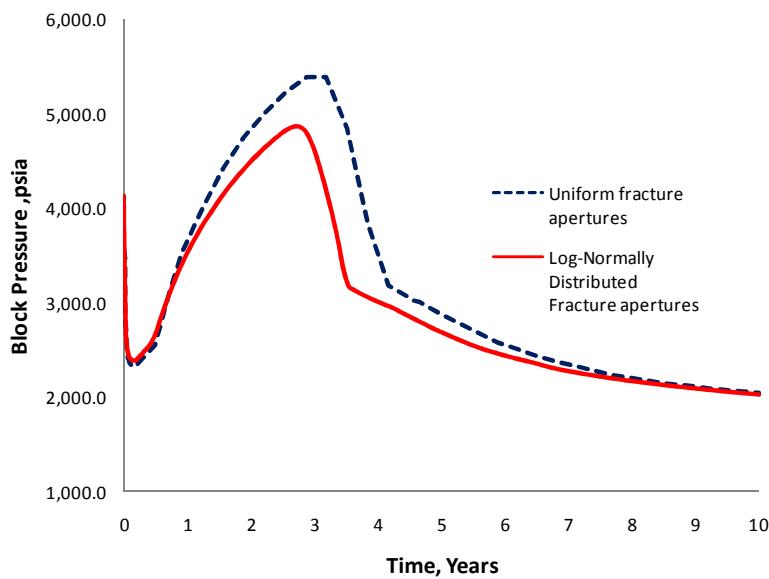


Fig. 5.11-Block pressures at the producer location (CASE 5.A1 and CASE 5.A2)

5.2 DFN Simulation of Multiple Fractures – Isolated Fractures

A relatively small 2D model was built with six vertical fractures. The model dimension is 100 ft x 100 ft x 20 ft. Each fracture has different length and orientation and they are not intersecting each other (isolated fractures). The fracture apertures is log-normally distributed with the mean of 0.01 ft and $\sigma^2 = 1.0$ (**Fig. 5.12**). we named this case as CASE 5.2.

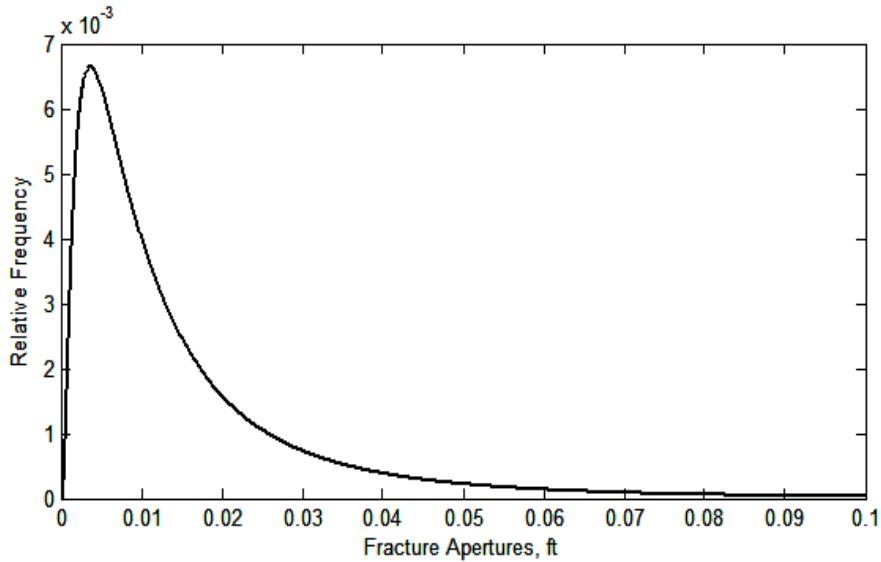


Fig. 5.12-Fracture apertures (log normal distribution)

Prior to building the grids for CASE 5.2, firstly we need to determine the number Control Volumes that we want to place in the computational domain to represent the fractures (there is no CV in the geometrical domain for fractures). The number of CV in this exercise is proportional to the length of each fracture. The longer the fracture the more CVs are needed to be placed in the computational domain.

The nodes population technique to grid up the fractures was described in the previous chapter. Initially, nodes should be populated such that the Voronoi edges are aligned with the fractures. These nodes later are going to be the CVs of the matrix blocks. The initial grid model of CASE 5.2 is depicted in Fig. 5.13.

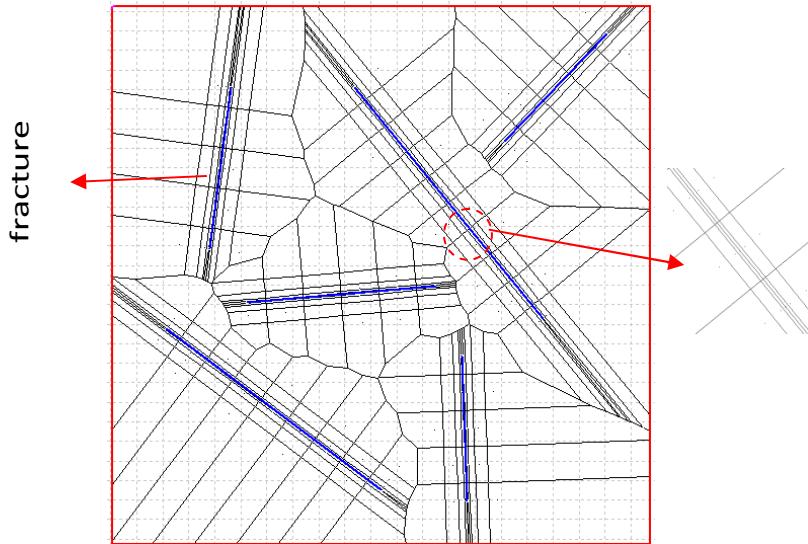


Fig. 5.13-Grids model of disconnected fracture (initial grid model = 504 blocks)

This initial model (**Fig. 5.13**) is quite coarse due to insufficient nodes in the matrix region. However, the initial grid model has 504 nodes (matrix blocks) caused by the grid refinement near the fractures. The number of grids to represent the fracture blocks in the computational domain is 40 blocks. Thus, the total number of blocks both in the geometrical and computational domains of the initial grid model is $504 + 40 = 544$ blocks.

Manually, more nodes were added to refine the matrix region and the final grid number of the model becomes 640. **Fig. 5.14** shows the final grid model of this exercise.

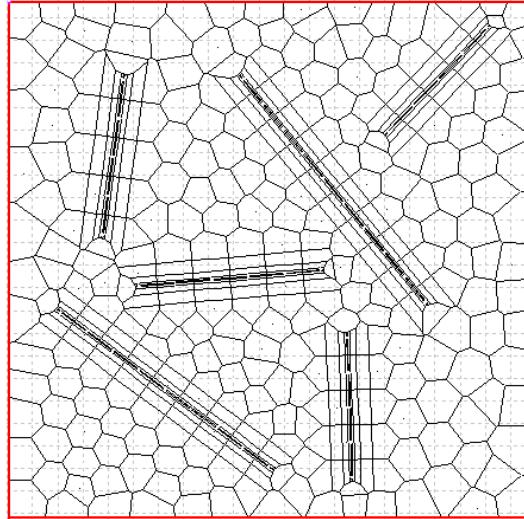


Fig. 5.14 CASE 5.2 final grid model (640 blocks)

The matrix permeability of the model is 100 md and log-normally distributed permeabilities applied for the fractures. The fractures permeabilities are in the range of 0.25 md to 1,500 md. SPE-1 fluid properties were used as the other previous exercises.

A producer is located in the bottom-left corner, while the gas injector is located in the top-right corner of the model. The oil was withdrawn constantly from the producer with the rate of 2 STB/D. 3,000 SCF/D of gas was injected constantly through the injector well. In this exercise, the simulation was run for 2 years or 730 days.

For a comparison, a similar model with no fracture was built to show the different of the pressures and saturations profiles due to the isolated fracture network introduced in the system. The model with no fracture contains 275 control volumes.

The simulation of the no fracture model was running smoothly without any numerical difficulties. There was no time step cut and the residual error set (1.0E-4) was reach after few Newton iterations.

Contrary to the isolated fracture system, the simulation was posing serious numerical challenge. Frequently the simulation could not satisfy the linear solver tolerance

(1.0E-2). Although we have doubled (from 20 to 40) the number of iteration, the tolerance yet could not be satisfied. Both models were using the same linear solver method, GMRES.

This difficulty occurred was most likely due to the volume contrast of the fracture blocks and matrix blocks. In this model, the minimum volume ratio between the fracture and matrix blocks could be as small as 0.0001. However, after cutting the time step for many times and performed more Newton iterations, the simulation finally could achieve the residual error of 1.0E-4.

The numerical performances of these two models are provided in **Table 5.3** and the plot of material balance error is depicted in **Fig. 5.15**.

Table 5.3-Numerical information and simulation time of CASE 5.2

Numerical Controls	No Fracture	Isolated Fractures (No intersections) Case 5.2
Maximum residual error	1.0E-4	1.0E-4
Max. Newton iteration	25	25
Max. linear solver iteration	40	40
Linear solver tolerance	1.0E-5	1.0E-5
Total time steps	152	324
Newton iterations	976	6,576
Solver iterations	28,315	216,445
Solver failures	0	5
Time step cuts	7	183
Simulation time	458 sec.	8,009 sec.

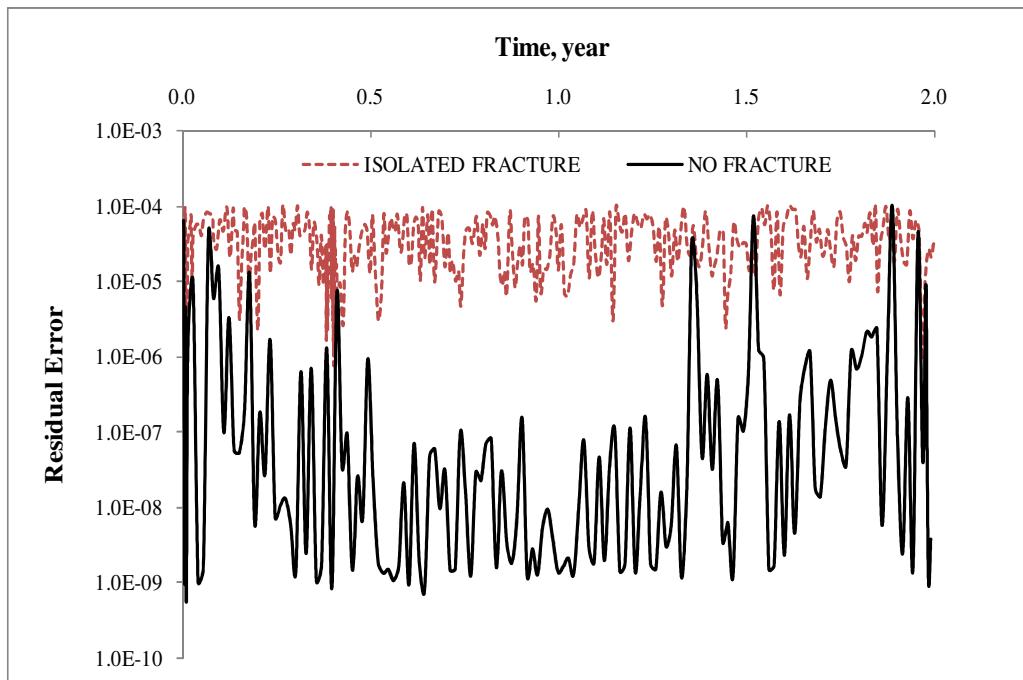
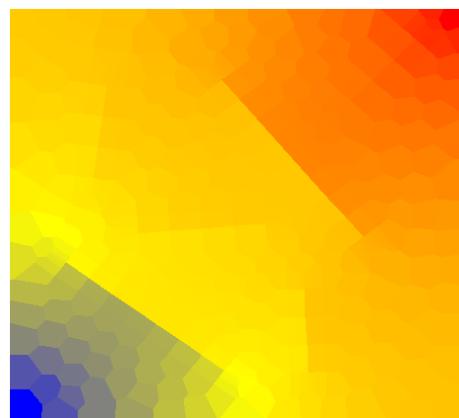
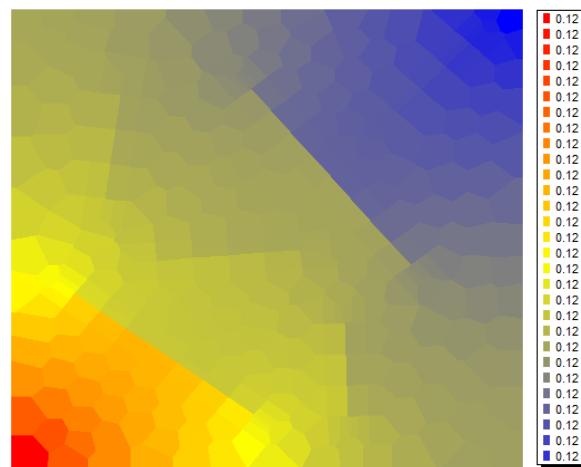


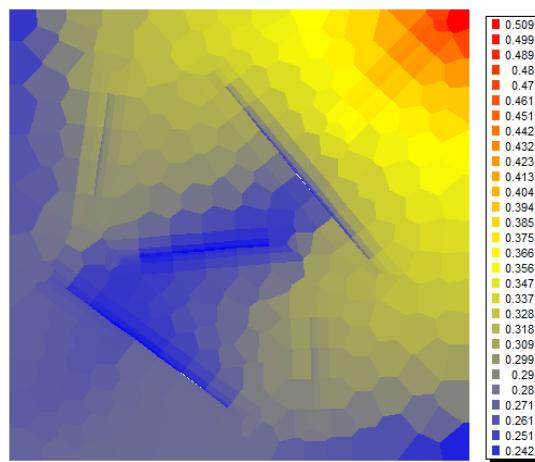
Fig. 5.15- Residual errors (Isolated fractures and no fracture)



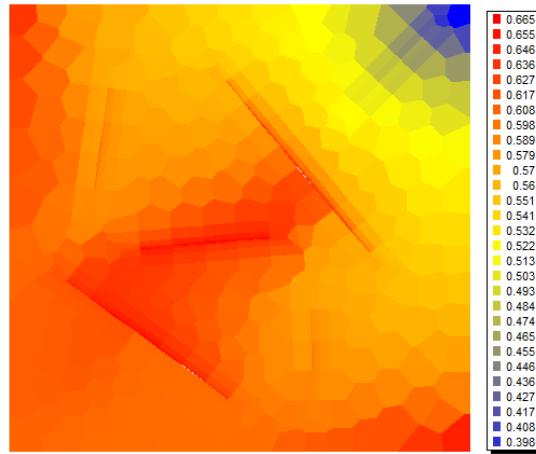
**Fig. 5.16- Pressure field of CASE 5.2 at t = 1 day
(Isolated fractures and no fracture)**



**Fig. 5.17- Water saturation of CASE 5.2 at time = 1 day
(Isolated fractures and no fracture)**



**Fig. 5.18- Gas saturation of CASE 5.2 at time = 730 days
(Isolated fractures and no fracture)**



**Fig. 5.19- Oil saturation of CASE 5.2 at time = 730 days
(Isolated fractures and no fracture)**

From the simulation results (**Fig. 5.16-5.17**), from early time (time = 1 day), it is clearly seen that the fractures in particular condition could be an excellent conduit for hydrocarbon. However, when the aperture is very small, the fracture behavior could be the opposite of its definitions. In the later condition, we can interpret that the more fracture segments are closing (apertures ≈ 0) and acting as flow barrier rather than excellent flow conduit.

Additional 2D visualizations of Oil and gas saturations at the end of simulation (time = 730 days) and GOR, block pressures, oil and water saturation are depicted in **Fig. 5.18 -Fig. 5.23** respectively.

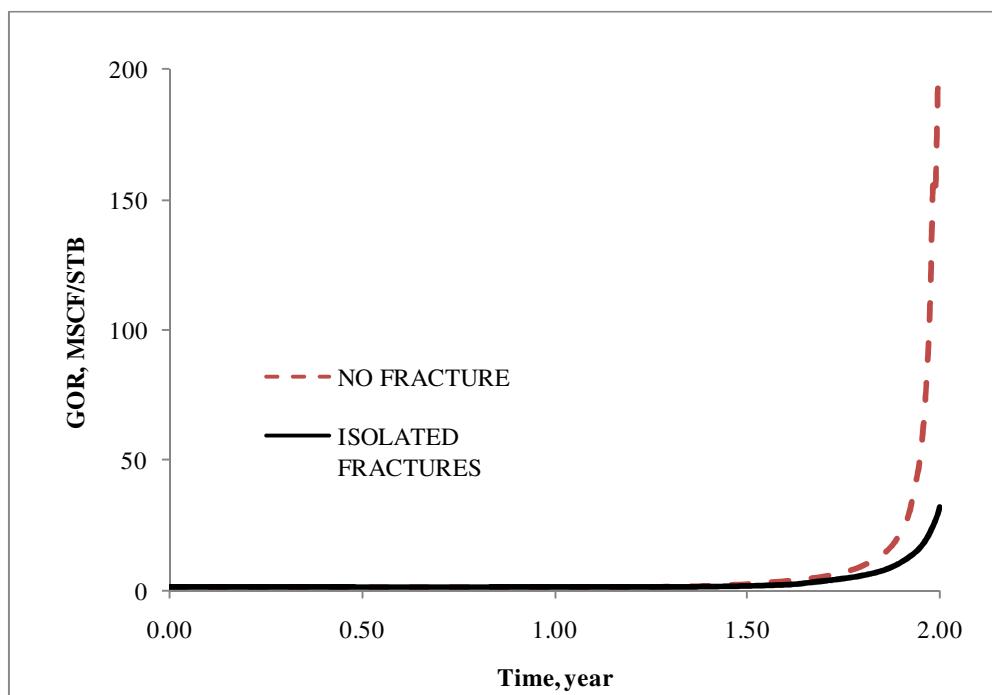
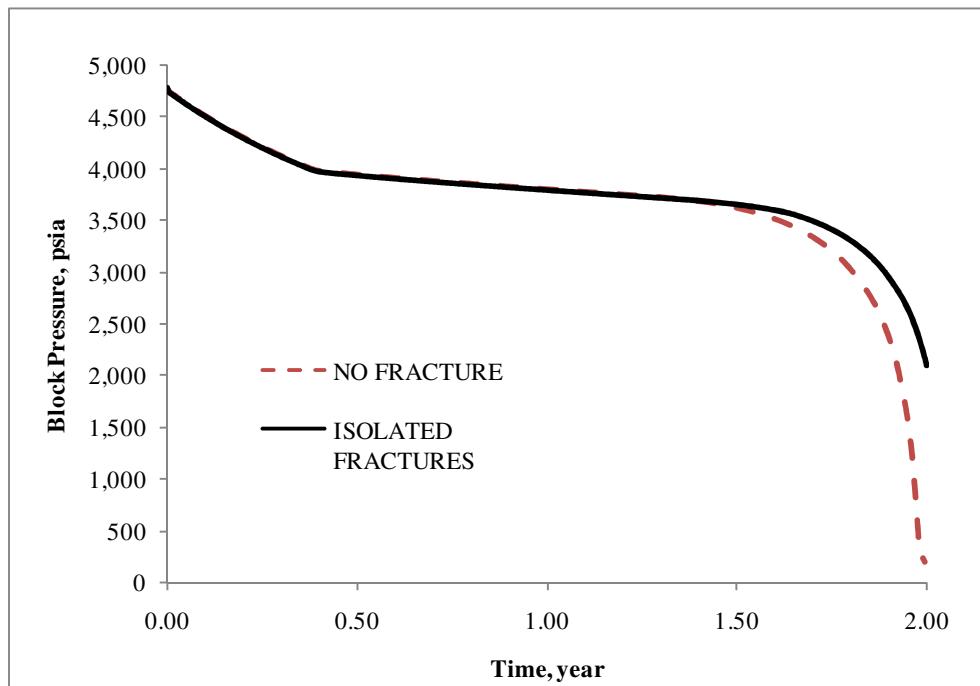
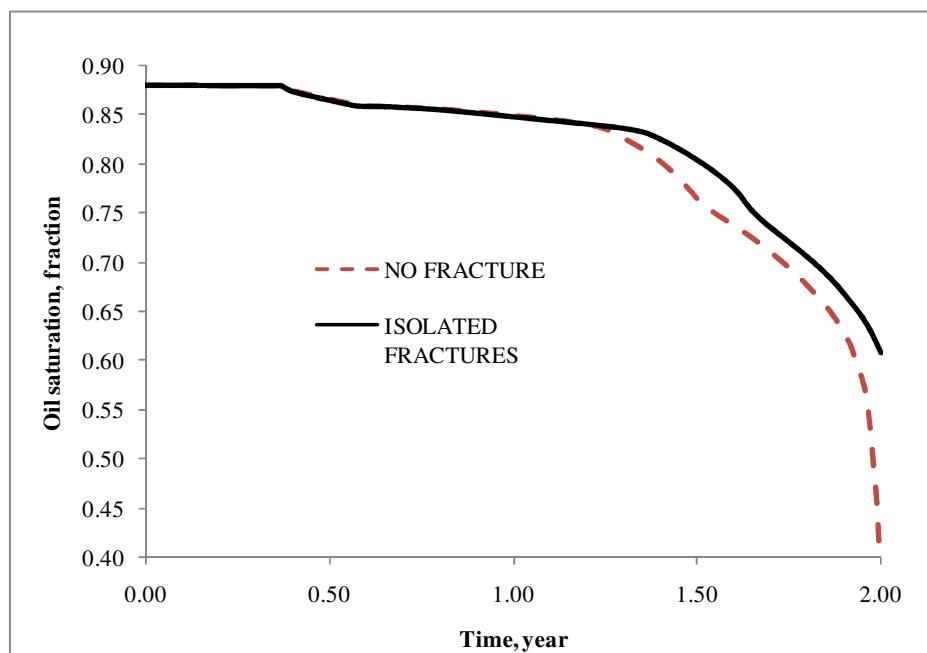


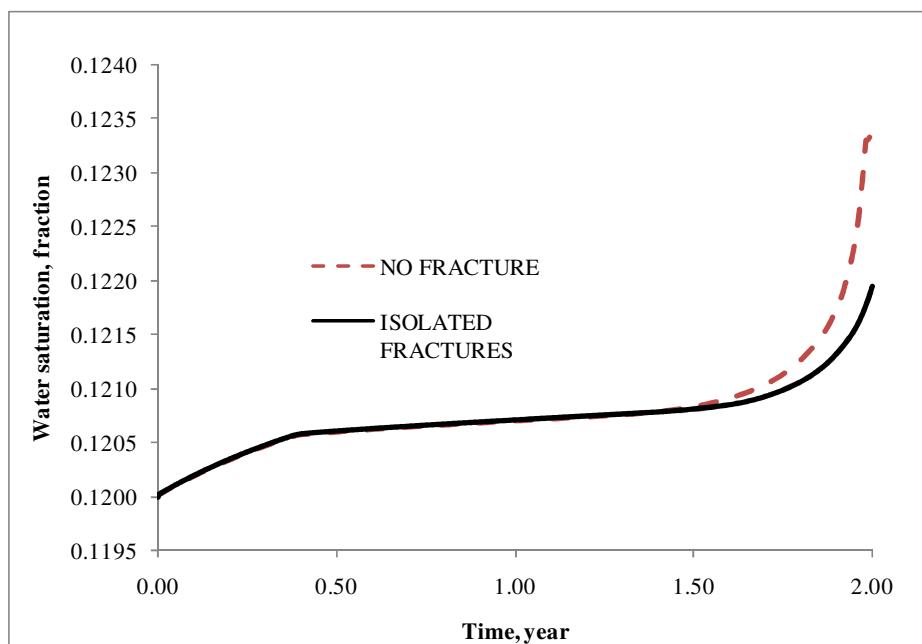
Fig. 5.20- GOR of CASE 5.2 (Isolated fractures and no fracture)



**Fig. 5.21- Block pressures at producer of CASE 5.2
(Isolated fractures and no fracture)**



**Fig. 5.22- Oil saturation at producer of CASE 5.2
(Isolated fractures and no fracture)**



**Fig. 5.23- Water saturation at producer of CASE 5.2
(Isolated fractures and no fracture)**

5.3 DFN Simulation of Complex Fracture Networks

The fracture network model presented in this section was provided by the work of KIM et al. (2007). The network was simulated using fractal geometry by a given fracture length, fracture distribution and fractal dimension. We will not discuss how the geometry created in detail. We simply created the grid model based on the provided network. The detailed procedures of the fracture network were presented by KIM et al.¹⁹.

5.3.1 2D Fracture Network Generation Based on Fractal Geometry

Kim et al.¹⁹ had developed a methodology to construct DFN using a fractal approach (FDFN). The fracture length and orientation are randomly generated using Monte Carlo simulation. The basic characteristics of fractal geometry, *self affine* and *self similar* are maintained during the process.

2D fractal codes developed by KIM were used to generate the fracture networks used in this study. The fracture network created by the code is named Fractal Discrete Fracture Network (FDFN). The network was set up using a synthetic dataset as follows:

- Fractal dimension of fracture center, $F_{Dc} = 1.3125$
- Fractal dimension of length, $F_{Dl} = 0.655$
- Side Length of the Domain, $L = 100$ ft
- Boundary Effect Flag, $b_{Flag} = 5$;
- Fracture Density, $\alpha = 1.5$
- Min. Fracture Length, $l_{min} = 5$ ft

The specific definition of these parameters can be found in Kim¹⁹.

Below is the rose diagram (**Fig. 5.24**) to describe the distribution of fractures, including their lengths and orientations. This diagram is determined by analysis of outcrop in Briger Gap, Wyoming²⁶. **Fig. 5.25** illustrates the DFN model (Case 5.3) produced by the code.

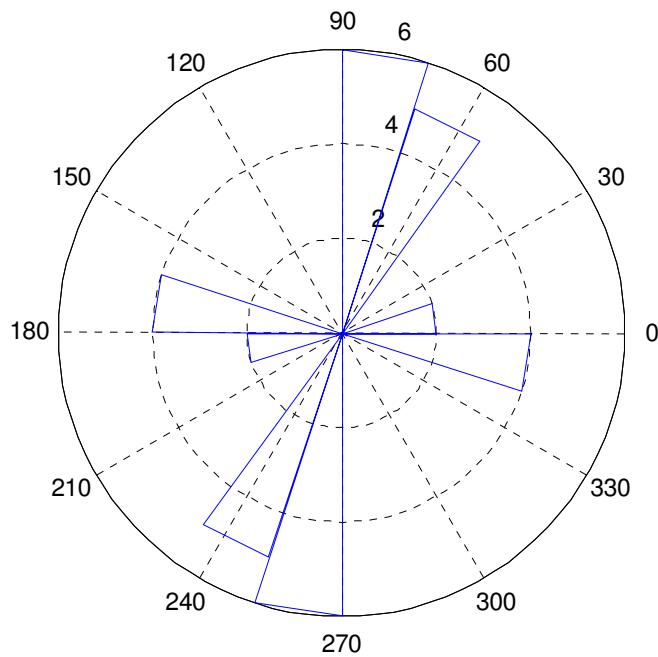


Fig. 5.24-FDFN rose diagram of connected fracture network

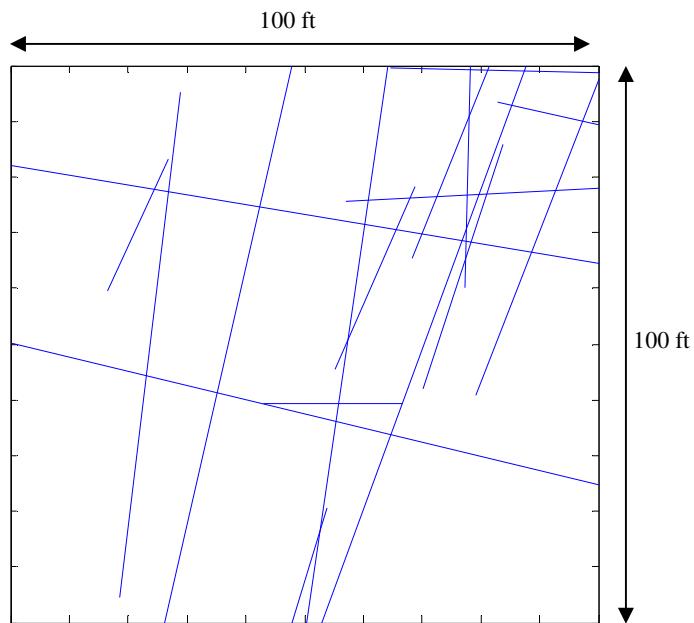


Fig. 5.25- Fracture network generated based on fractal geometry

As illustrated in **Fig. 5.25** the fractures are intersecting in many places inside the model. Prior to gridding the fractures, we need to determine the coordinates of all intersections.

To find the intersection of two straight lines: first we need the equations of the two lines. We will assume the following equations:

$$\text{Fracture-1 (Line-1): } y = m_1 x + c_1$$

$$\text{Fracture-2 (Line-2): } y = m_2 x + c_2$$

where, m and c are the slope and intercept of a line.

The point of intersection of the two lines is (X_{int} , Y_{int}).

$$Y_{\text{int}} = m_1 X_{\text{int}} + c_1 = m_2 X_{\text{int}} + c_2$$

$$\text{Thus, } X_{\text{int}} = \frac{c_2 - c_1}{m_1 - m_2} \text{ and } Y_{\text{int}} = m_1 X_{\text{int}} + c_1$$

All the points of the intersecting fractures are shown in **Fig. 5.26**.

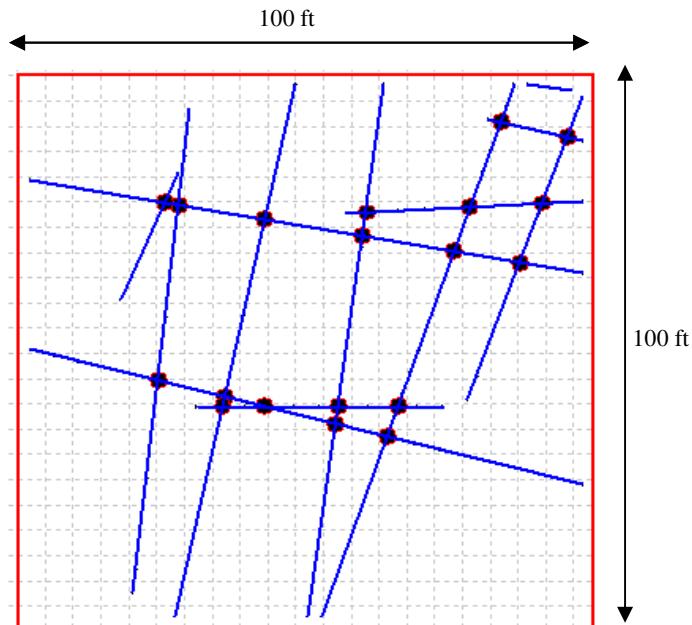


Fig. 5.26-19 Fracture intersections from the FDFN model

Once we had determined the intersecting points of the fractures, we can populate nodes surrounding the fractures and their intersections. The main concern here is to ensure that the edges of Voronoi grids are still aligned with the fracture. Gridding on intersection creates additional nodes. Once Voronoi polygons are created, the edge of the polygon may not be aligned with the fracture. Lack of alignment results in the need to re-grid the system. The process of these procedures is depicted in the **Fig. 5.27**. The initial number of control volumes in the model in Fig. 5.27 is 784.

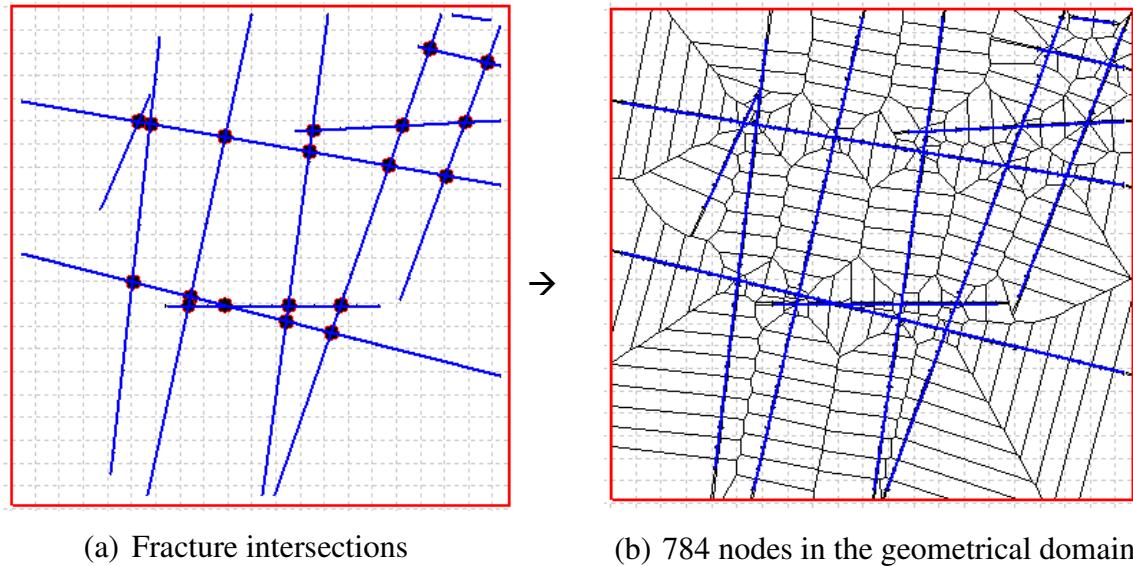


Fig. 5.27-Fracture nodes and Voronoi grid (initial model = 784 blocks)

Furthermore, blocks refinement should be addressed for the matrix blocks by adding nodes into the initial grid model as we did in the previous exercise. We should remember that the additional nodes in the system should not deform the perfect alignment of the fracture lines and Voronoi edges constructed in the earlier steps. Deformation of the fracture grid will result in restarting the entire gridding processes.

In order to avoid the deformation, additional nodes were populated further away from the nodes used to shape the fracture lines after executing the Voronoi algorithm. **Fig. 5.28** illustrates the grid model for both fractures and matrix blocks. The final model contains 1,403 control volumes in the geometrical domain and an additional 190 control volumes in the computational domain to represent the fracture segments. Thus, the total number of control volumes is 1,593 (computational domain + geometrical domain).

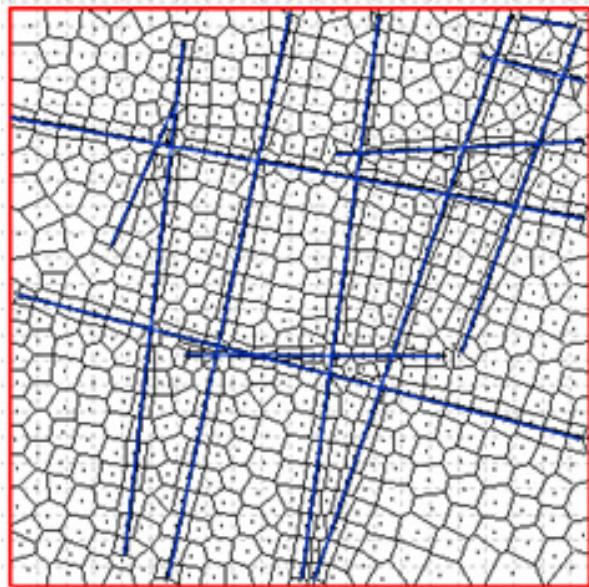


Fig. 5.28-Final grid model of the FDFN fracture network (1,593 grids)

The last step of building the grid model is to add control volumes to represent the fracture blocks. There are two steps that are needed to proceed; (1) volume corrections of the adjacent matrix blocks with fractures and (2) adjusting the connection properties for all the blocks (matrix and fractures) in the computational domain. All these aspects were discussed in Chapter II.

The fracture permeabilities are calculated using the cubic law and the same procedure as in the previous cases. In this model, the permeability of fractures is within the range of 0.1 md to 3000 md.

The simulation of this model was very challenging. As observed in the previous exercise with the disconnected fractures, this FDFN model poses very serious numerical challenges. The linear solver faced difficulty to satisfy the given tolerance, even though the number of iteration was increased to three times more than that of the disconnected fracture case.

Several other attempts were undertaken to tackle this highly non-linear problem by fine tuning the numerical controls, such as reducing the time step size, increasing the number of Newton iterations, or loosening the maximum pressure and saturation tolerance per-time step.

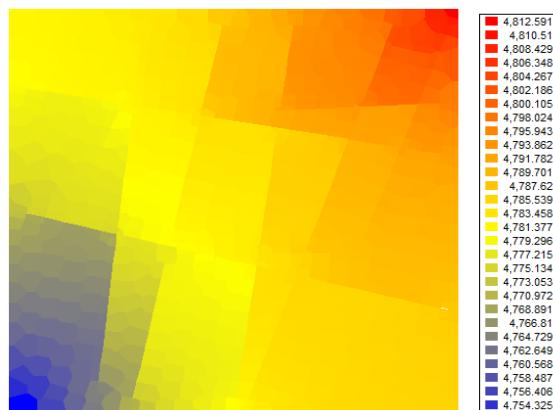
The simulation was successfully terminated after 730 days. The results of the simulation were extremely accurate. Throughout the simulation, the residual errors were kept at a maximum of 1.0E-4. The numerical performance of this case and the previous two cases are reported in the **Table 5.4**.

Table 5.4-Numerical information and simulation time of CASE 5.3

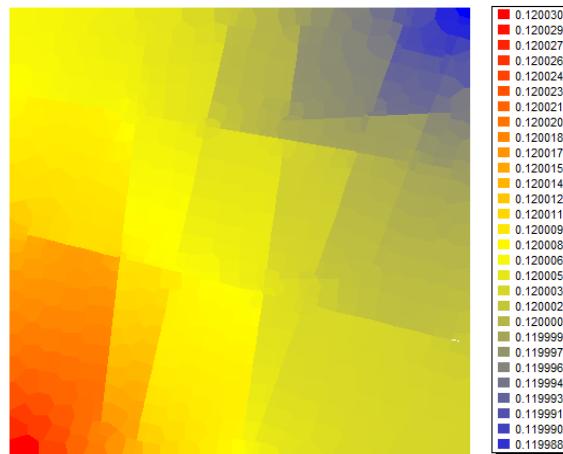
Numerical Controls	No Fracture Case 5.2 & 5.3	Isolated Fractures (No intersections), Case 5.2	FDFN Fracture Network, Case 5.3
Maximum residual error	1.0E-4	1.0E-4	1.0E-4
Max. Newton iteration	25	25	25
Max. linear solver iteration	40	40	140
Linear solver tolerance	1.0E-5	1.0E-5	1E-5
Total time steps	152	324	2,045
Newton iterations	976	6,576	34,285
Solver iterations	28,315	216,445	1,420,171
Solver failures	0	5	103
Time step cuts	7	183	228
Simulation time	458 sec.	8,009 sec.	56,125 sec.

The effect of fractures in this model is more pronounced compared to the unfractured or the isolated fractures models. The gas displacement during the injection is more sporadic due to the variation of conductivity along the fracture segments. The stream lines are more distorted compared to the previous cases. These behaviors can be clearly seen from the 2D visualization of pressures and saturations profiles from the early until the end time of simulation (**Fig. 5.29 – Fig. 5.32**).

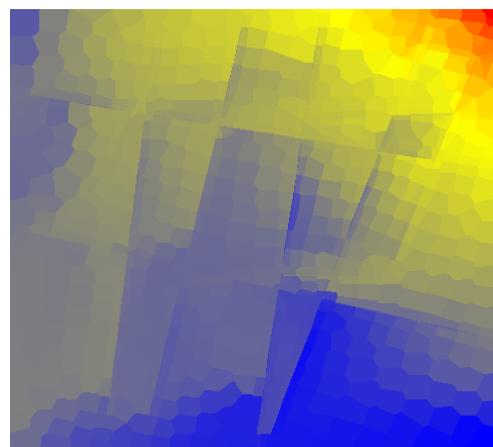
Plots of fluids saturations and block pressures at the producers vs. time (**Fig. 5.33 – Fig. 5.36**) were also observed. There was no significant difference of the disconnected fractures and connected fractures profiles. However, based on the pressure and saturation 2D visualizations, if we continued the simulation, we should be able to see more significant differences of those three cases (no fracture, isolated and connected fractures).



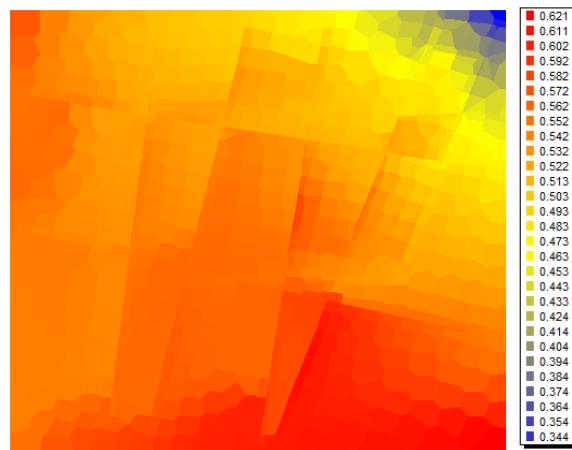
**Fig. 5.29-Pressure profile of at time = 1 day
(connected fractures and no fracture)**



**Fig. 5.30-Water saturation at time = 1 day
(Connected fractures and no fracture)**



**Fig. 5.31- Gas saturation of CASE 5.3 at time = 730 days
(Connected fractures and no fracture)**



**Fig. 5.32- Oil saturation of CASE 5.3 at time = 730 days
(Connected fractures and no fracture)**

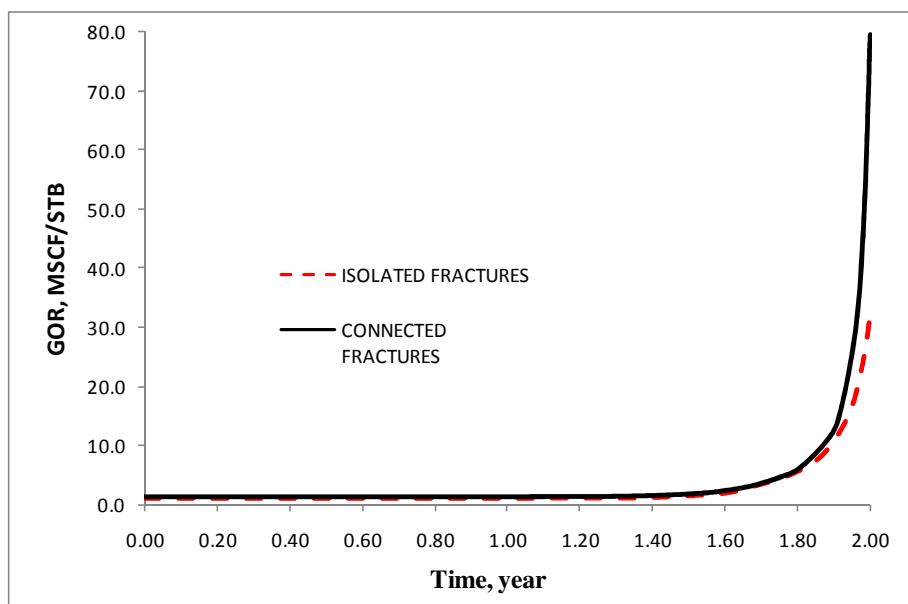
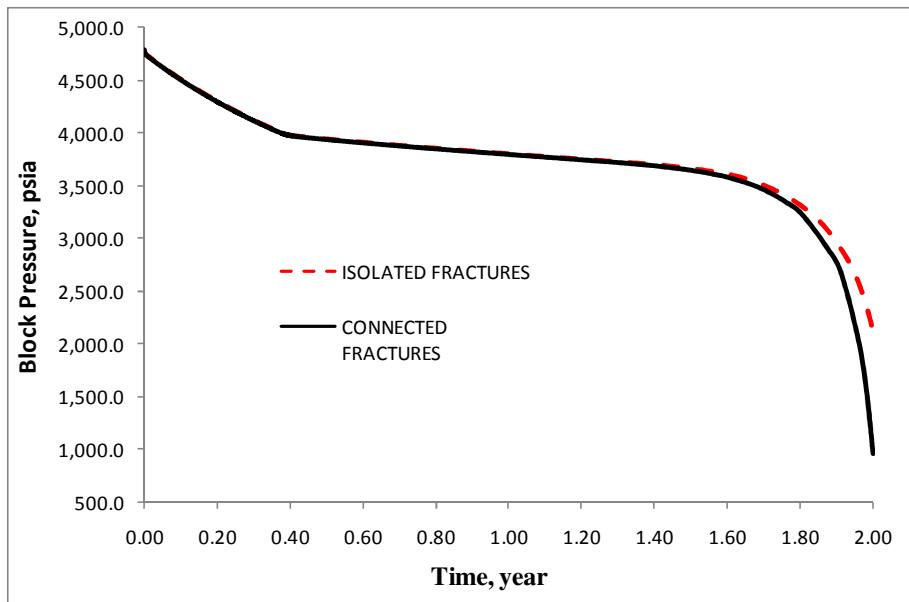
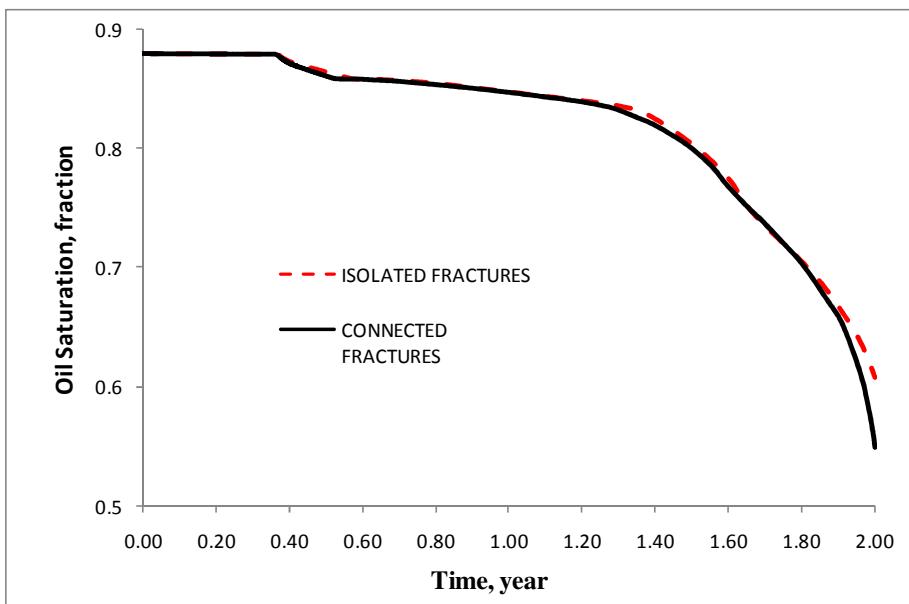


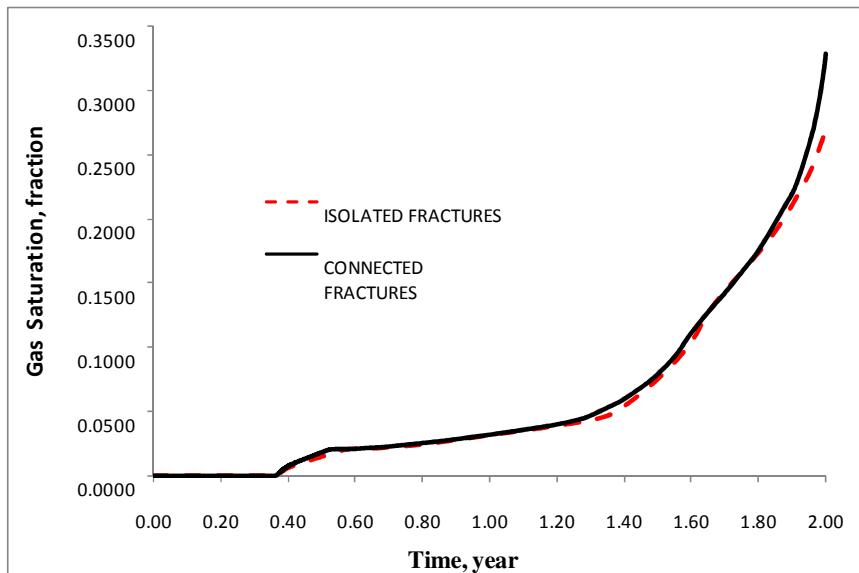
Fig. 5.33- GOR of CASE 5.3 (Connected and isolated fractures)



**Fig. 5.34- Block pressures at the producer of CASE 5.3
(Connected and isolated fractures)**



**Fig. 5.35- Oil Saturations at the producer of CASE 5.3
(Connected and isolated fractures)**



**Fig. 5.36- Gas saturations at the producer of CASE 5.3
(Connected and isolated fractures)**

5.4 DFN Simulator and Multi-Reservoir Simulation

Another unique feature in the DFN simulator is its capability to simulate multiple reservoir models simultaneously. This feature is enabled due to the control volume object implemented in the DFN simulator. Each grid block in the DFN is defined as a control volume object (Chapter II and Chapter III). The control volume object implemented in the DFN simulator has properties such as area, volume, thickness, porosity, permeability and most importantly each control volume can recognize its neighboring control volumes and their properties.

With its CV properties, DFN is capable of simulating multiple models with different grid systems, either structured or unstructured grids. Furthermore, the models may contain a fracture network or no fractures.

For the sake of simplicity, two simple 2D models were built to demonstrate the multi-reservoir simulation capability implemented in the DFN simulator. The grid dimensions of those models were identical, 6,000 ft x 6,000 ft x 100 ft. The lateral

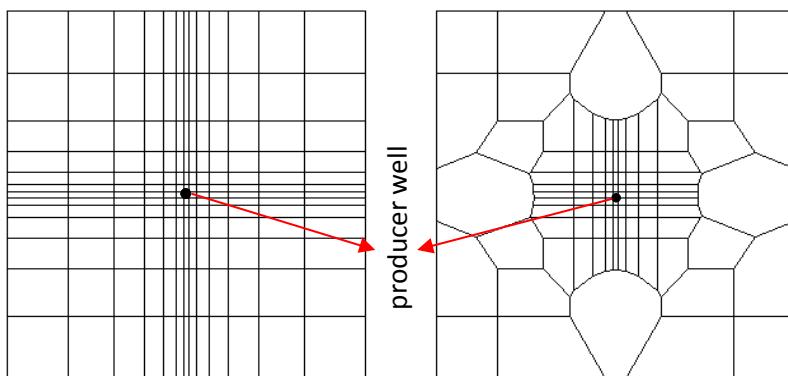
permeability was 215 md. All other rock, fluid properties and initial conditions remained identical with the first SPE comparative solution project. **Fig. 5.37** shows the two reservoir systems (Reservoir A and Reservoir B) that were built for this exercise.

Reservoir A was built using a regular Cartesian grid system (169 blocks). A producer well was located in the center of Reservoir A. The oil rate was set constant at 1,000 STB/D with minimum bottomhole pressure of 1,000 psia. Voronoi grid system of reservoir B (105 blocks) was built similar to Reservoir A with less number of grid blocks. Similar well location and operating conditions were used for Reservoir A. The simulation was run for ten years.

Since the size of the model, rock and fluid properties are identical; we may consider this exercise as a grid sensitivity study. Oil rates, bottomhole pressures, GORs and block pressure profiles are depicted in **Fig. 5.38**, **Fig. 5.39**, **Fig. 5.40** and **Fig. 5.41** respectively.

In addition to multiple reservoir simulations, the current stage of the DFN simulator is applying single numerical controls (residual error, number of iterations, time steps) for the entire model to get the solutions. Thus, we should consider the degree of difficulty of each sub-model prior to utilizing this capability in our studies. It is reasonable to suggest using this feature for sensitivity studies due to the similarity of the difficulty.

Total material balance error is depicted in **Fig. 5.42**. The material balance error was applied for the entire model (Reservoir A and Reservoir B).



Reservoir A (Number of grids: 169)

Reservoir B (Number of grids: 105)

Fig. 5.37-Grid models of multi-field application (Reservoir A and B)

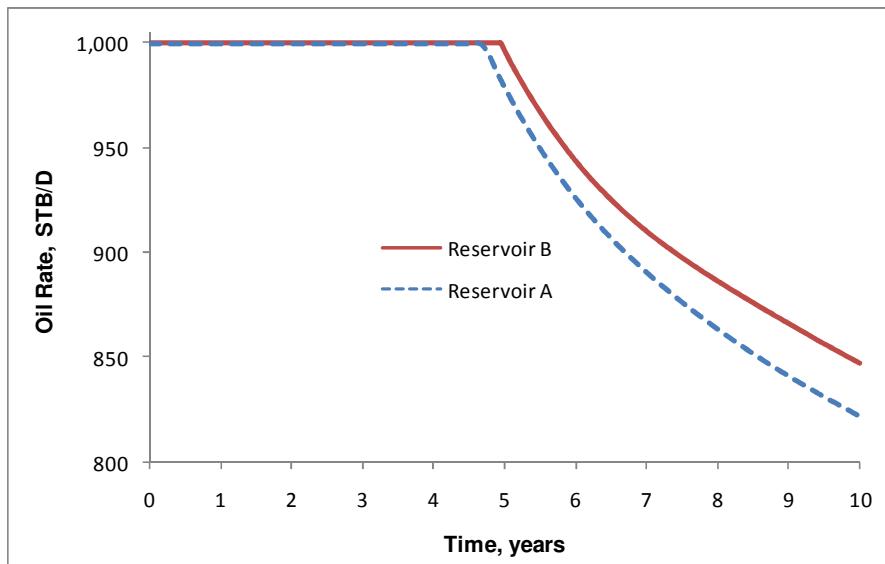


Fig. 5.38-Oil rate profiles (Reservoir A and Reservoir B)

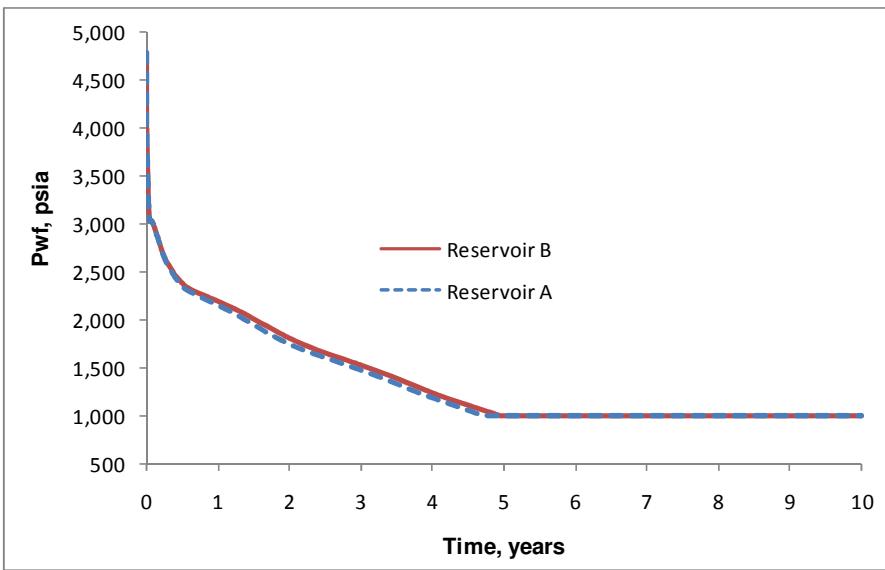


Fig. 5.39-Bottomhole pressure profiles (Reservoir A and Reservoir B)

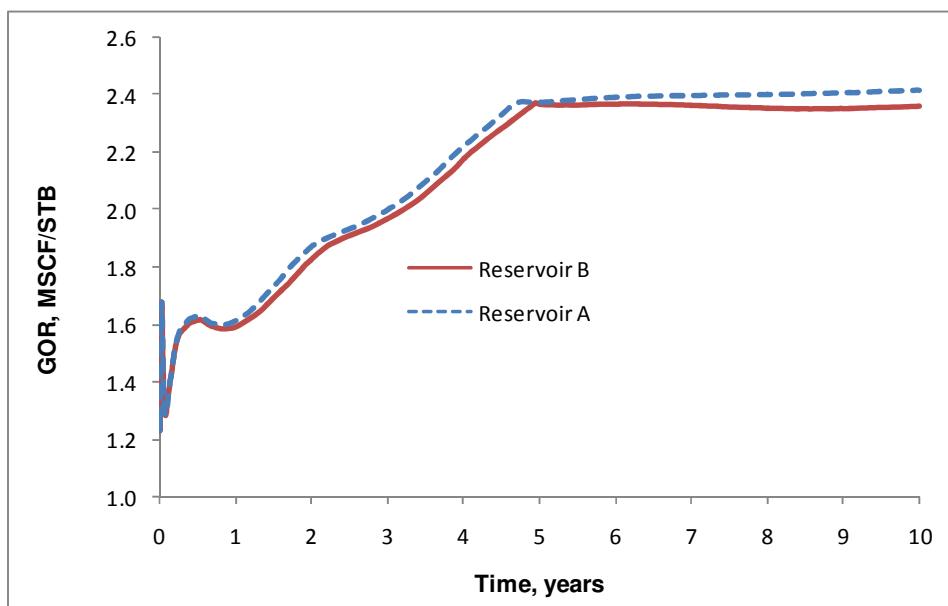


Fig. 5.40: GOR profiles (Reservoir A and Reservoir B)

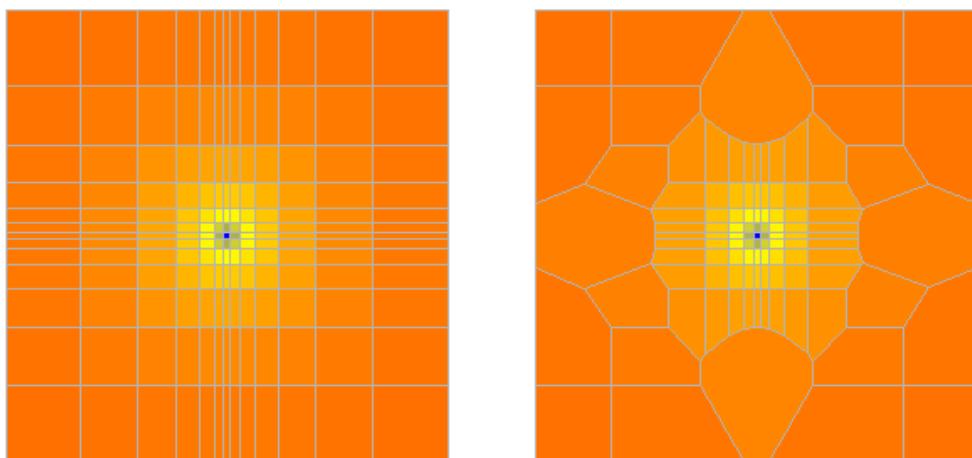


Fig. 5-41-Block pressure at time=10 year (Reservoir A and Reservoir B)

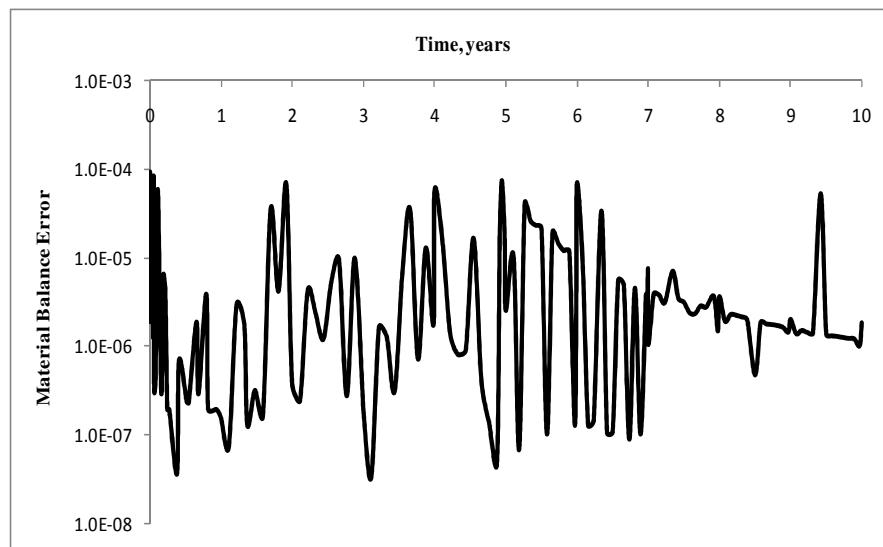


Fig. 5.42-Total material balance error (multi-reservoir simulation)

CHAPTER VI

CONCLUSIONS AND RECOMMENDATIONS

6.1 Conclusions

Two major works have been accomplished in this research, the development of flexible gridding technique based on Voronoi grid system and the implementation of a new DFN simulator. Therefore, the following conclusions will be associated based on those two works.

The main conclusions of the generation of Voronoi grid system to model DFN are as follows:

1. Voronoi grid system is one of most general gridding technique compared to conventional gridding technique. Voronoi algorithm can be used to generate many other grid models, e.g. rectangular, rectilinear, hexagonal, and hybrid grid.
2. The Voronoi algorithm is capable and flexible to build grid model for both fractured and unfractured systems, structured and unstructured grid models.
3. The proposed mesh generation technique has demonstrated the range of capabilities from building the simplest unfractured, regular Cartesian grids until gridding of complex fracture networks generated based on fractal geometry.

The conclusions of the development of DFN simulator are as follows:

1. DFN simulator has been developed using Object Oriented Programming languages (Visual Basic and C++).
2. DFN simulator was satisfactorily validated against analytical solutions, a commercial simulator and an academic reservoir simulator.
3. DFN simulator is able to simulate model based on structured and unstructured grid systems.

4. DFN simulator capabilities were tested to obtain the dual-porosity shape factor under a constant draining rate conditions. As a function of fracture spacing, the shape factor obtained from DFN simulator is similar with the works done by Mora et al.⁴² and Coats⁴³.
5. DFN simulator demonstrated the capabilities to model systems with fractures, isolated/disconnected and connected fracture network.
6. We have enabled the simulation to include the fracture apertures distribution that might be collected from X-Ray CT scanning experiment or other possible methods.
7. Based on the simulation conducted in this research, the aperture distribution plays very important role to the performance of a reservoir. In the gas injection model, the recovery could be as much as 4.5 % different between the model with uniform and log-normally distributed fracture apertures.
8. Numerically, simulation on fractured systems, disconnected or connected fractures model are very challenging. It requires an extensive amount of time to build the grid model and runs the simulation.
9. DFN simulator capability for multiple-reservoir simulation has been tested and it can be a potential tool for sensitivity studies.

6.2 Recommendations

The following are some recommendations of this research:

1. The current stage of our mesh generator is not so robust in term of the execution speed. It requires a massive amount of time to build grid model for a large system and containing complex fracture networks. It could be much faster if it was implemented using a more robust programming languages, such as C++ or .NET rather than Visual Basic 6.0.
2. DFN Simulator and its mesh generator are supposed to be one integrated package. Currently, the communication between those two applications needs manual works from user and some mistakes might be occurred during the process.

3. The developed mesh generator is not equipped with capabilities to read the grid properties from maps. An idea of adding a geostatistical module will give multiplicative values into the overall package of the simulator.
4. The simulations of fractured system conducted in this report have raised serious numerical challenges compared to the simulations of unfractured systems, especially for intersecting fractures and log-normally distributed fracture apertures. The linear solvers implemented in the DFN were frequently failed to get the solutions, even though the number of iteration was three times more compared to the simulations of uniform fracture apertures or unfractured cases.

We haven't tried to tackle this challenge with other methods, such as high-order discretization of the flow equations or implementing linear solvers other than the solvers available in the DFN simulator (SparseLib++ library).

5. The large scale model with an extensive number of intersecting fractures has always been a great challenge in the DFN simulation. Besides upscaling techniques, enabling the simulation run with multi or parallel processors will open opportunities to better understanding the flow behavior of large scale fractured systems.

NOMENCLATURE

Variables

A	= Area, ft ²
B	= Formation volume factor, BBL/STB
d	= fracture width, ft
k	= Permeability, md
L	= Fracture spacing, ft
M	= Mobility term, 1/cp
μ	= Fluid viscosity, cp
p	= fluid pressure, psia
q	= Flow rate, ft ³
s	= Fluid saturation, fraction
T	= Transmissibility, md-ft
V	= Bulk volume, ft ³
w	= fracture aperture, ft
\emptyset	= porosity, fraction
γ	= specific gravity, air =1.0
r	= <i>residual error</i>

Subscripts

b	= bulk.
e	= Evaluated cell/block.
f	= Fracture.
m	= matrix.
o,g,w	= oil, gas and water phase.
sc	= Standard condition.

int = intersection.

Superscripts

n = previous time step.

$n+1$ = next time step.

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APPENDIX A

DFN SIMULATOR INTERFACES

A.1 Pre-processor

The pre-processor of DFN simulator includes features to build 2D or 3D grid model, fluids, rock properties and well modeling. Currently, all these features are not fully integrated with the processor of the simulator. The grid and well modeling features are what we currently used in the DFN simulator. The remaining features are not fully integrated as one simulator package. This integration effort considered minor and less important than all the works done in this dissertation.

The following appendix shows the screen captured to show the features of the package. The implementation of DFN simulator's pre-processor is very user-friendly and relatively similar compared to other simulators. Thus, it is not necessary to explain how to use this package.

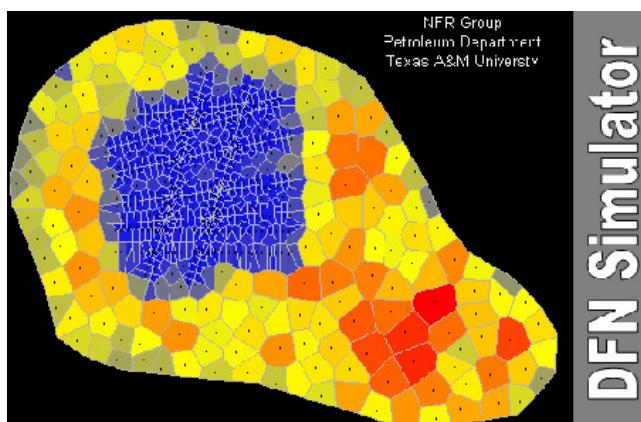


Fig. A.1-DFN simulator splash screen

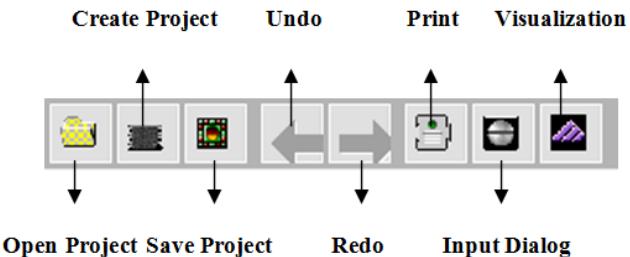
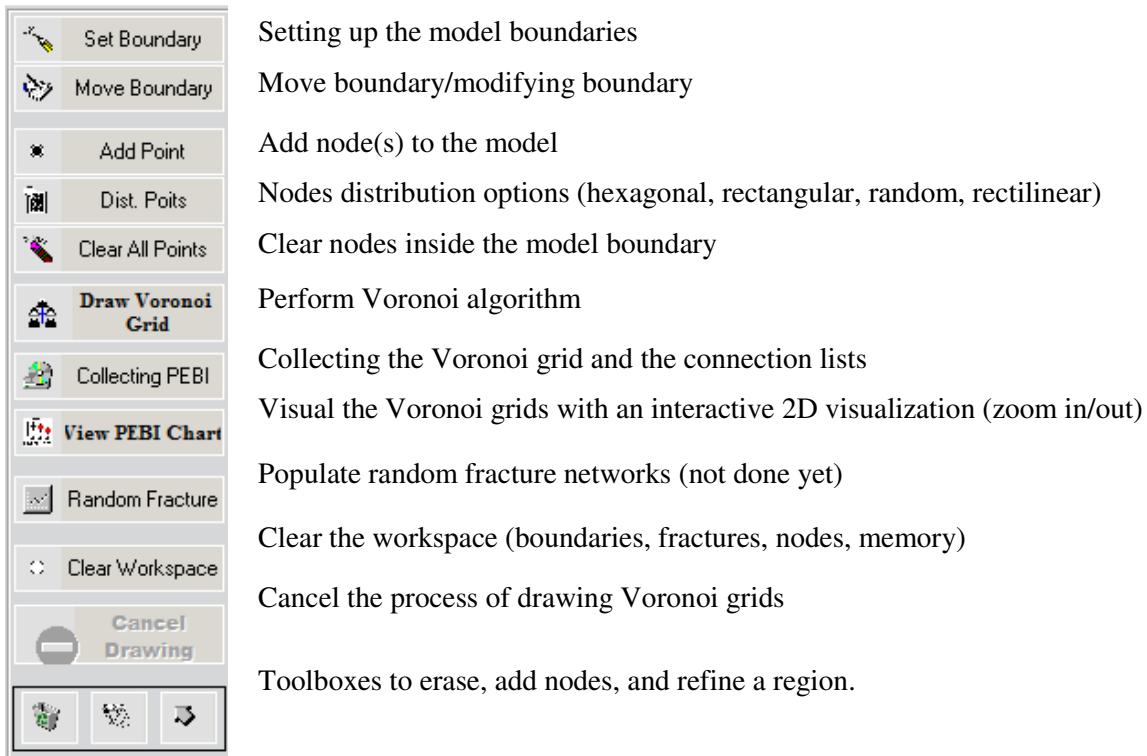


Fig. A.2-DFN simulator toolbar



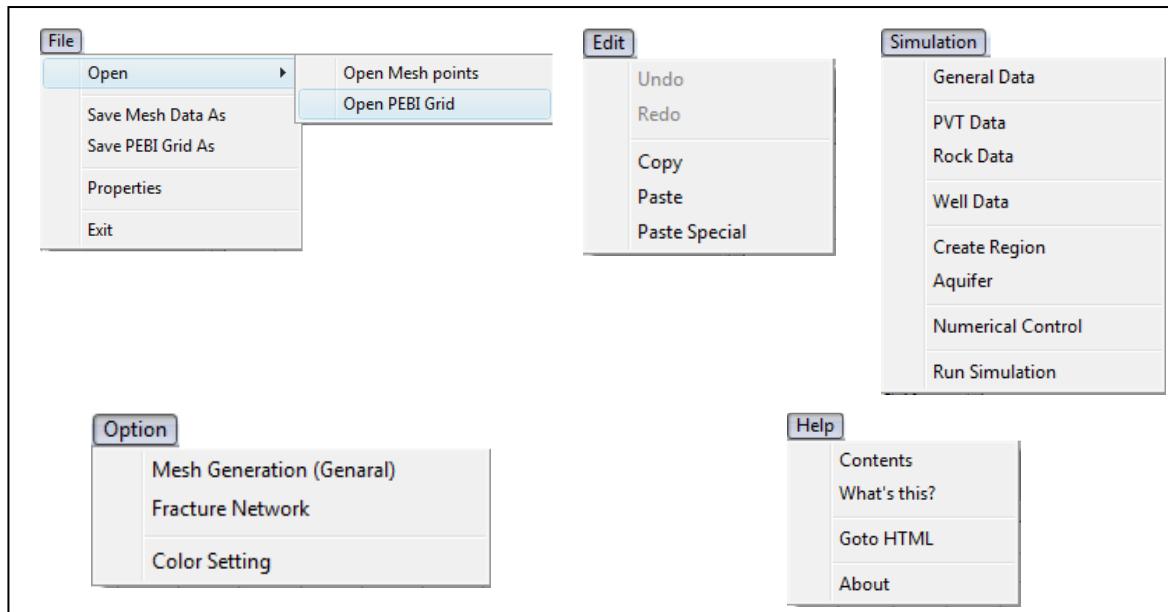


Fig. A.3-DFN simulator menu structure

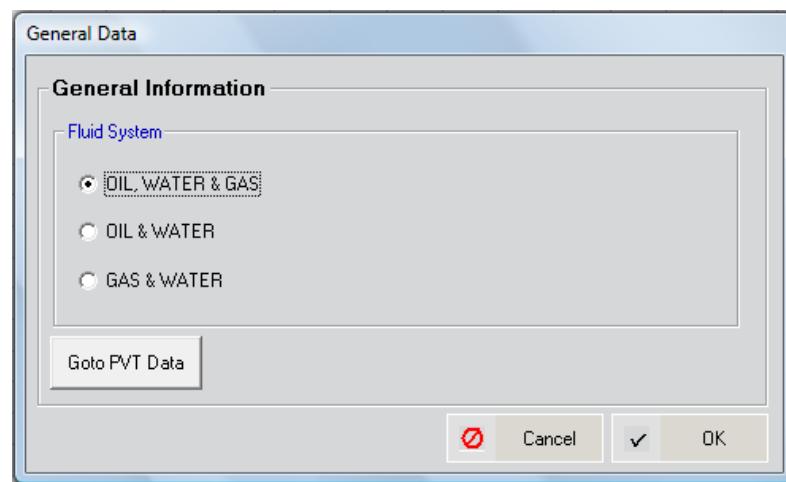


Fig. A.4- General data dialog

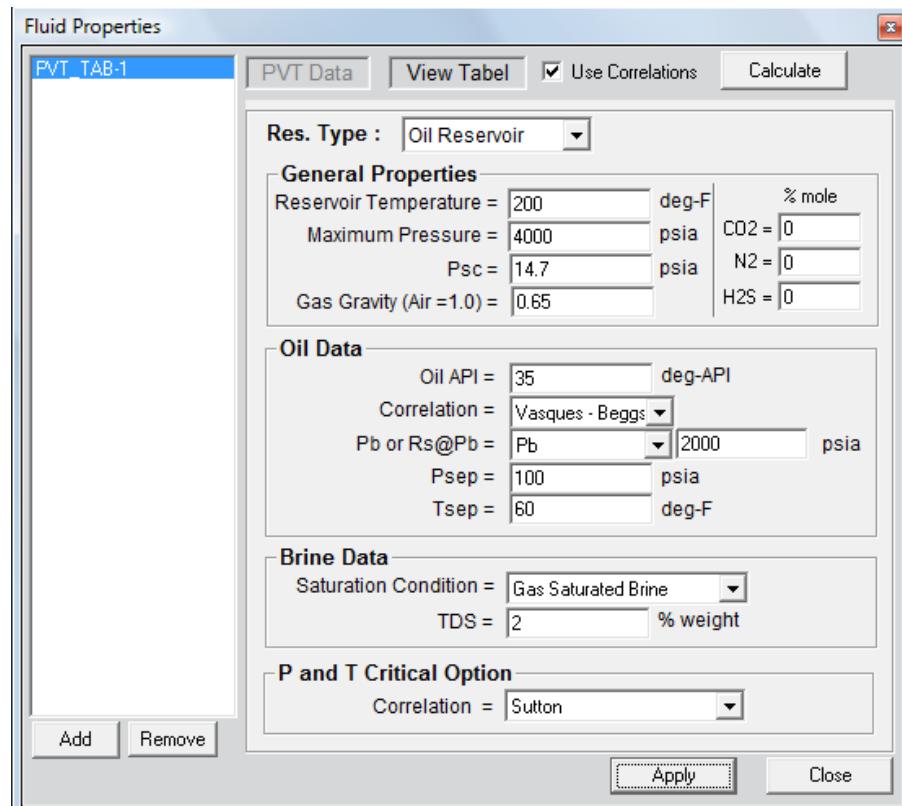


Fig. A.5-Fluid properties dialog (a)

Fluid Properties

PVT TAB-1 PVT Data View Table

P(psia)	Bo(RB/Mscf)	Rs(Mscf/BB)	miuO(cp)	rhoO(lb/cu-ft)
4000.00	1.224169	0.3385181	0.9672	45.7412
3790.25	1.225316	0.3385181	0.9404	45.6984
3580.49	1.226599	0.3385181	0.9147	45.6506
3370.74	1.228044	0.3385181	0.8902	45.5969
3160.99	1.229681	0.3385181	0.8669	45.5361
2951.24	1.231555	0.3385181	0.8448	45.4669
2741.48	1.233718	0.3385181	0.8241	45.3871
2531.73	1.236245	0.3385181	0.8048	45.2944
2321.98	1.239235	0.3385181	0.7870	45.1851
2112.23	1.242829	0.3385181	0.7708	45.0544
1902.47	1.235760	0.3190145	0.7863	45.1727
1692.72	1.216051	0.2777091	0.8426	45.6047
1482.97	1.196794	0.2373520	0.9089	46.0404
1273.22	1.178042	0.1980514	0.9878	46.4785
1063.46	1.159861	0.1599480	1.0835	46.9168
853.71	1.142342	0.1232324	1.2014	47.3523
643.96	1.125617	0.0881806	1.3497	47.7807
434.21	1.109896	0.0552336	1.5392	48.1951
224.45	1.095563	0.0352274	1.7022	49.5820

Add Remove View Chart Apply Close

Fig. A.6-Fluid properties dialog (b)

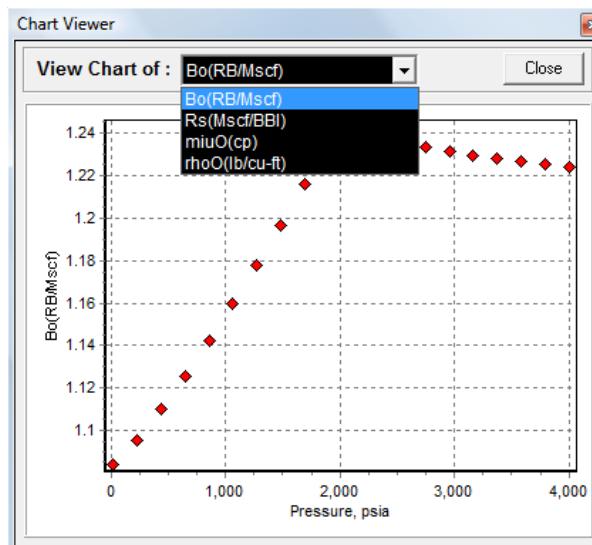


Fig. A.7-Fluid Properties Dialog (c)

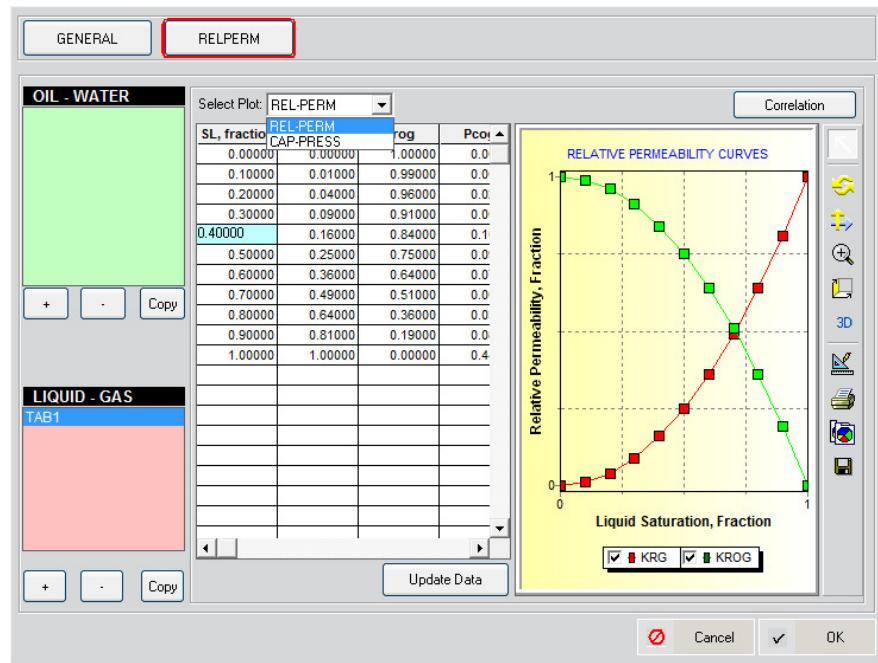


Fig. A.8-Rock properties dialog

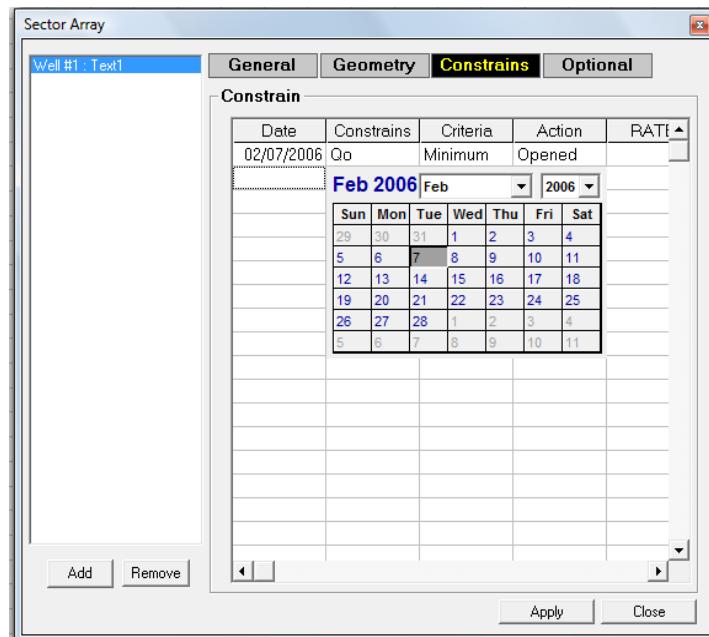


Fig. A.9-Well and recurrent data dialog

A.1.2 Voronoi Grid Examples from the DFN Simulator

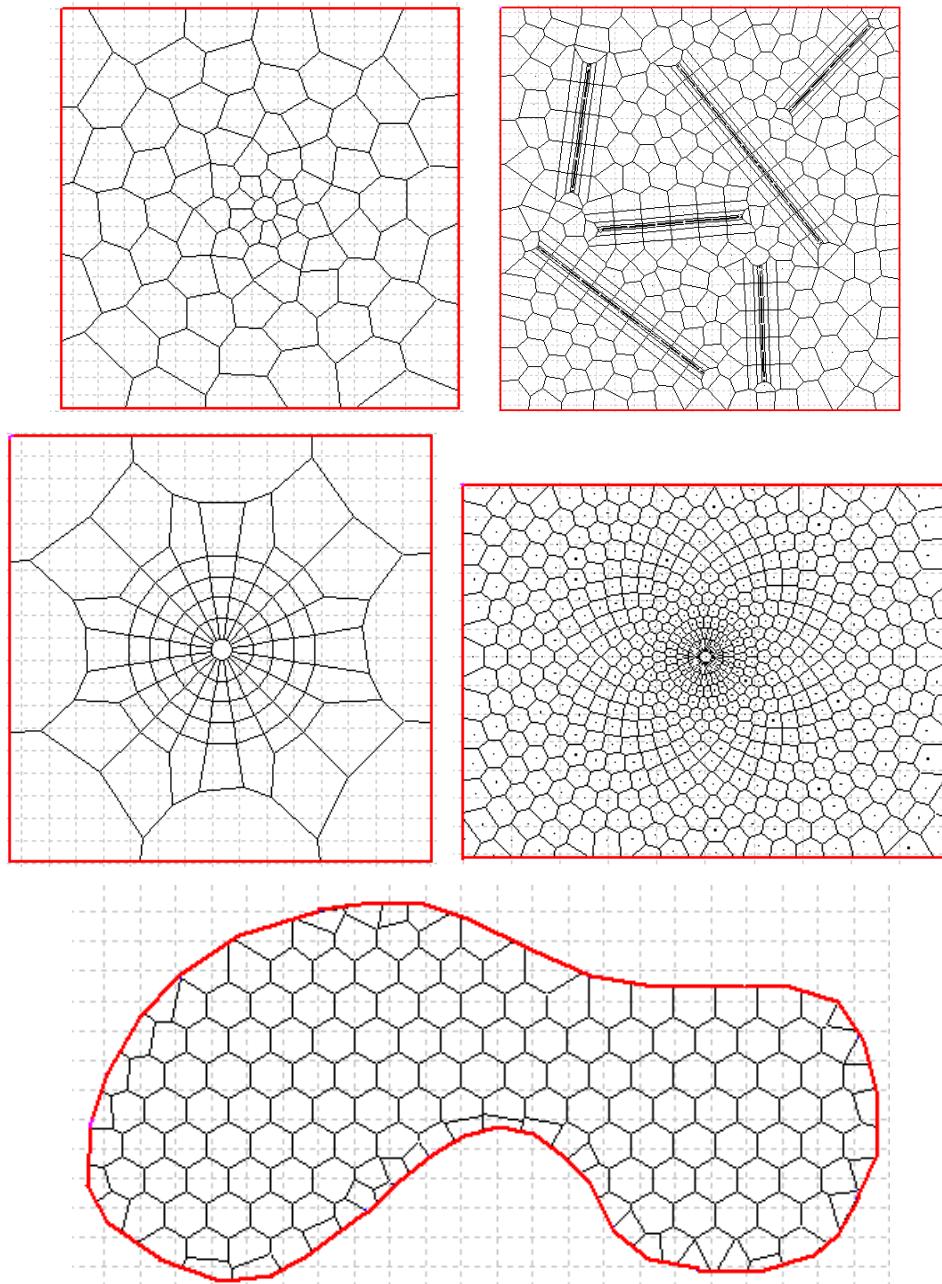


Fig. A.10-Examples of voronoi grids generated by the simulator's pre-processor

A.2 Processor

The simulator engine or processor was implemented using Microsoft Visual studio 2008 with C++ as the programming language. Several library/Header files (*.h) and source file were created as follows:

Header Files:

```
#include "stdafx.h"
#include <string>
#include <cstdlib>
#include <iostream>
#include "compcol_double.h"      // column matrix
#include "comprox_double.h"     // row matrix
#include "coord_double.h"       // I,J matrix
#include "ilupre_double.h"      // ILU(0) pre-conditioner
#include "icpre_double.h"
#include "diagpre_double.h"      // diagonal pre-conditioner
#include "gmres.h"              // GMRES solver
#include "bicg.h"                // Bi-Conjugate gradient solver
#include "cg.h"                  // Conjugate gradient solver
#include "ir.h"                   // Richardson Iteration solver
#include "cgs.h"                  // Square conjugate gradient
#include "cheby.h"                // Cheby solver
#include "qmr.h"                  // QMR solver
#include "bicgstab.h"             // Stabilized conjugate
gradient
#include <time.h>                // Read CPU time
#include "mvm.h"                  // Solver data structure/class
#include <cstdlib>
#include <iostream>
#include <stdio.h>
#include <stdlib.h>
#include <string.h>
#include "prepareLib.h"           // Library to read data from
file
#include "publicParamLib.h"        // parameter declarations
#include "allocMemoryLib.h"        // dynamic memory allocation
#include "publicFunctionLib.h"      // general function of the
simulator
#include "matbalLib.h"             // material balances
```

```
#include "wellLib.h" // sink & source term of the
equations
#include "pvtPropertiesLib.h" // PVT properties (table
lookup)
#include "rockPropertiesLib.h" // Rock properties
#include "perturbationLib.h" // Perturbation to construct
the elements of Jacobian matrix
#include "BICG_STABLib.h" // Linear Solver (partially
not used anymore)
```

Source Files:

DFNSIM.cpp // Main Code

Processor Screen Captured:

```
Warning!!! Reached maximum solver iteration, but could not satisfy the tolerance !!!
TOL<4.98518E-002 | Time = 11.859 | dp=1.6E-005 | dsu=1.2E-011 | dsg=2.0E-008 | I=10 | C=0
Warning!!! Reached maximum solver iteration, but could not satisfy the tolerance !!!
TOL<3.03165E-002 | Time = 11.859 | dp=9.4E-007 | dsu=6.8E-013 | dsg=4.2E-009 | I=11 | C=0
Warning!!! Reached maximum solver iteration, but could not satisfy the tolerance !!!
TOL<1.24941E-003 | Time = 11.859 | dp=2.9E-007 | dsu=2.1E-013 | dsg=2.2E-009 | I=12 | C=0
=====
Time = 11.85909 MBERROR(Total)=1.715E-003 Iteration=12 nCut = 0 MBERROR(Local)=8.537E-005
Puf Qsia Qg (STB/D) Qg (SSTB/D) Qg (MSCF/D) Qg (STD) Qw(STB) Qw(MSCF)
L-1 11.8591 4031.6746 2.0000 9.0000 2.0000 3.2124 0.0000 38.1224 Qw(STD)
L-2 11.8591 4731.1145 0.0000 0.0000 -3.0000 0.0000 0.0000 -35.5723
TOL<4.02360E+003 | Time = 12.758 | dp=2.9E-007 | dsu=2.1E-013 | dsg=2.2E-009 | I=1 | C=0
Warning!!! Reached maximum solver iteration, but could not satisfy the tolerance !!!
TOL<2.51296E+003 | Time = 12.758 | dp=3.2E-002 | dsu=2.8E-001 | dsg=2.8E-001 | I=2 | C=0
Warning!!! Reached maximum solver iteration, but could not satisfy the tolerance !!!
TOL<1.11109E+005 | Time = 12.758 | dp=1.6E+001 | dsu=2.3E-001 | dsg=1.8E-001 | I=3 | C=0
Warning!!! Reached maximum solver iteration, but could not satisfy the tolerance !!!
TOL<2.55462E+003 | Time = 12.758 | dp=6.4E+000 | dsu=8.1E-004 | dsg=2.8E-001 | I=4 | C=0
Warning!!! Reached maximum solver iteration, but could not satisfy the tolerance !!!
TOL<4.93408E+004 | Time = 12.758 | dp=2.6E+000 | dsu=4.1E-004 | dsg=3.7E-002 | I=5 | C=0
Warning!!! Reached maximum solver iteration, but could not satisfy the tolerance !!!
TOL<1.79755E+004 | Time = 12.758 | dp=1.5E+000 | dsu=1.3E-006 | dsg=8.7E-002 | I=6 | C=0
Warning!!! Reached maximum solver iteration, but could not satisfy the tolerance !!!
TOL<5.67309E+004 | Time = 12.758 | dp=7.0E-001 | dsu=8.5E-007 | dsg=3.3E-002 | I=7 | C=0
Warning!!! Reached maximum solver iteration, but could not satisfy the tolerance !!!
TOL<4.47232E+003 | Time = 12.758 | dp=2.7E-001 | dsu=1.9E-007 | dsg=1.7E-002 | I=8 | C=0
Warning!!! Reached maximum solver iteration, but could not satisfy the tolerance !!!
TOL<2.50792E+003 | Time = 12.758 | dp=1.3E-001 | dsu=9.6E-008 | dsg=4.7E-003 | I=9 | C=0
```

Fig. A.11-DFN simulator processor

A.3 Post-processor

From the pre-processor interface, we can easily activate the post-processor of the DFN simulator.

The main feature of this interface is to show the 2D visualization of pressures, saturation pressures and saturations of each layer for 3D simulation model and every time step and. The post-processor displays the

Voronoi grid system directly from the pre-processor and extracts the simulation results from the output files of the simulation.

The output file of the simulation contains the pressures, bubble-point pressures and saturation of each phase. The following is an example of the DFN simulation results:

NBLOCK 25

NLayer 1

NCols 5

TIME=0.2000000

BLOCK PRESSURE

4787.7072701	4789.8460889	4789.9896280	4789.9992984	4789.9999492
4789.8460889	4789.9806327	4789.9981266	4789.9998375	4789.9999857
4789.9896280	4789.9981266	4789.9997640	4789.9999749	4789.9999974
4789.9992984	4789.9998375	4789.9999749	4789.9999968	4789.9999996
4789.9999492	4789.9999857	4789.9999974	4789.9999996	4789.9999999

SATURATION PRESSURE

4014.7000000	4014.7000000	4014.7000000	4014.7000000	4014.7000000
4014.7000000	4014.7000000	4014.7000000	4014.7000000	4014.7000000
4014.7000000	4014.7000000	4014.7000000	4014.7000000	4014.7000000
4014.7000000	4014.7000000	4014.7000000	4014.7000000	4014.7000000
4014.7000000	4014.7000000	4014.7000000	4014.7000000	4014.7000000

WATER SATURATION

0.1200017	0.1200001	0.1200000	0.1200000	0.1200000
0.1200001	0.1200000	0.1200000	0.1200000	0.1200000
0.1200000	0.1200000	0.1200000	0.1200000	0.1200000
0.1200000	0.1200000	0.1200000	0.1200000	0.1200000
0.1200000	0.1200000	0.1200000	0.1200000	0.1200000

OIL SATURATION

0.8799983	0.8799999	0.8800000	0.8800000	0.8800000
0.8799999	0.8800000	0.8800000	0.8800000	0.8800000
0.8800000	0.8800000	0.8800000	0.8800000	0.8800000
0.8800000	0.8800000	0.8800000	0.8800000	0.8800000
0.8800000	0.8800000	0.8800000	0.8800000	0.8800000

GAS SATURATION

0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000

TIME=0.4

BLOCK PRESSURE

Post-Processor Interface

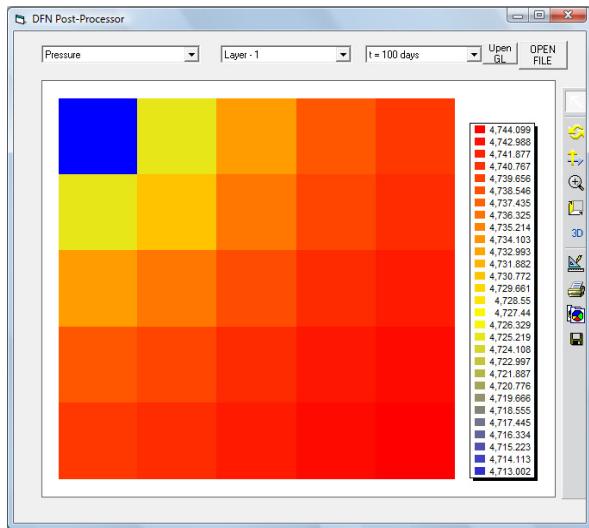


Fig. A.12-DFN simulator post-processor (no values displayed)

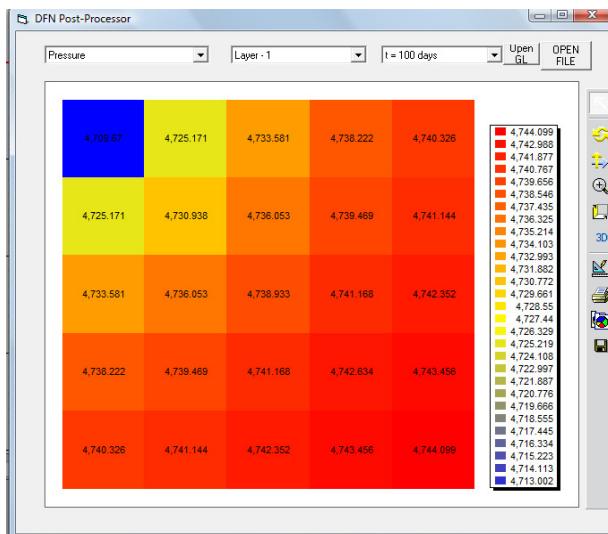


Fig. A.13-DFN simulator post-processor (values displayed)

APPENDIX B

OBJECTS AND DATA STRUCTURES OF DFN SIMULATOR

B.1 OBJECTS IMPLEMENTED IN THE DFN SIMULATOR

There are many objects or data types implemented in the DFN simulator. The following are the list of most important objects in the simulator.

B.1.1 Control Volume Object

```

typedef struct CV_type {
    int activeCV;           // active CV=1, Null =0
(default=active)
    int nconne;            // number of connection
    double zTop;             // grid top (ft)
    double area;              // X-Y block area (sq-ft)
    double pvMult;            // pore volume multiplier

    double por;                // porosity, fraction
    double kL;                  // Lateral permeability, md
    double kV;                  // Veritical permeability , md

    double thickness;          // grid thickness
    int rockID;               // rock ID, integer (default=0)
    int pvtID;                 // pvt ID, integer (default=0)
    long *indexconne;        // lists of the adjacent CVs
    long *indexTo; // array of CVs connected to the
evaluated CV
    double *areaInt; // Area of interface
}

```

```

    double *transMult;      // transmissibility multiplier
    double *LCV1, *LCV2;   // dist. Of CV to areaInt (to &
from)
} CVol;

```

B.1.2. Relative Permeabilities Object

```

typedef struct rockData {
    int      nRowSW, nRowSG;           // number of sw/sg in the
table
    double *swTable                  // array of water
saturation
    double *kro_sw, *krw_sw, *pcow_sw; // krows, krws &
pcows

    double *sgTable;                 // array of gas saturation
    double *krg_sg, *krw_sg, *pcgw_sg; // krgs, krwgs, pcgws

} rockTable;

```

B.1.3. Fluid Properties Object

```

typedef struct pvtData {
    int      nRow;
    double *pTable; // Pressure Table
// Oil data
    double *rsoTable; // rso
    double *moTable;  // oil viscosity, cp
    double *boTable;  // Oil FVF (Vol/std Vol)

```

```

//Water data

double *rswTable; // solution gas in water phase
double *mwTable; // water viscosity, cp
double *bwTable; // water FVF, vol/std. vol

//Gas data

double *mgTable; // gas viscosity, cp
double *bgTable; // Gas FVF, vol/std. vol
} pvtTable;

```

B.1.4. Well Object

```

typedef struct well_type {
    double st_time; // well schedule
    double qo, qw, qg, qt, pwf, PI, BHPmin, qginj, qwinj;
    // PI = productivity Index → calculated from the mesh
    generator
    double qoMAX, qoMIN, qgMAX, qgMIN, qwMAX, qwMIN;
    long IDCell; // well position

    int dir; //0 vertical ; 1=horizontal
    int prod_inj; // 0=prod // 1= inj
    int operate; // 0= oil rate, 1 = g rate 2 = wrate , 3
    pwf
    // injection (-), production (+)
    // all rate units are in std. condition (cu-ft)

} wellType;

```

B.2 DATA STRUCTURES OF DFN SIMULATOR

The data structures implemented in the DFN simulator, more or less similar to the data structure in many reservoir simulators. In order to keep the familiarity of users, DFN has been developed using “keyword” system. Each keyword represents a part or a section in the reservoir simulator dataset (grids, rocks, fluids, initialization, and well sections).

Since DFN simulator grid system is based on Voronoi grid, automatically, in the grid section keywords (DX, DY, DZ, NX, NY, NZ) as in many reservoir simulators are no longer applicable. Those keywords are replaced with a new structure of Control Volume object as discussed in some chapters of this dissertation.

Fig.B.1 will be used to explain how the data structure of grid section in the DFN Simulator. Each hexagonal grid is a CV object and has its own properties. The properties are listed in the data structure of CV (see section B.1.1).

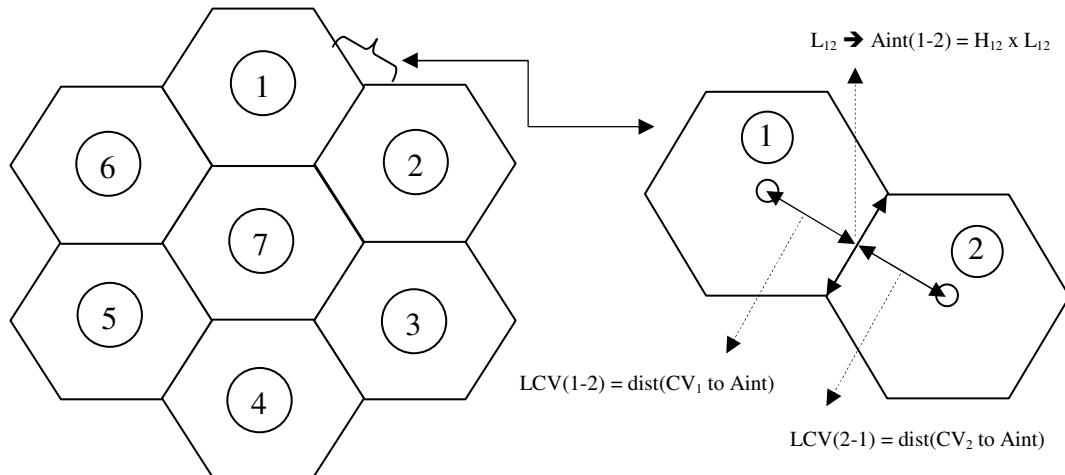


Fig.B.1-Control volume object (DFN grid system)

In orderly manner the grid section of DFN simulator begins with:

1. Keyword “**NXNY**” : number of CV in each layer
2. Keyword “**NZ**” : number of layer followed by array of thickness for each layer

3. Keyword “START_CV” : total number of CV and followed by CV object properties

This part contains of CV properties from grid #1 until grid #NXNY*NZ. Thus, the number of lines should be as many as total number of CV in the model.

Number of columns in every line depends on the number of connection of each CV. Total number of column in each line should be (10+4*Number of connection).

First column must be the number of connection +1 of the evaluated CV and column 11th contains array of connected CVs.

For an example, CV #1:

- Number of connection = 3 → Column #1 = **4**
- Array of connected CVs = {2,6,7}

Another example, CV #7:

- Number of connection = 6 → Column #1 = **7**
- Array of connected CVs = {1,2,3,4,5,6}

The grid section of the model illustrated in Fig.B.1 is as follows:

	Grid Section
1	4 Top ₁ A ₁ por ₁ kL ₁ kv ₁ pvMult ₁ H ₁ RockID ₁ pvtID ₁ 2 6 7 Aint(1-2) Aint(1-6) Aint(1-7) LCV(1-2) LCV(2-1) LCV(1-6) LCV(6-1) LCV(1-7) LCV(7-1)
2	4 Top ₂ A ₂ por ₂ kL ₂ kv ₂ pvMult ₂ H ₁ RockID ₂ pvtID ₂ 1 3 7 Aint(2-1) Aint(2-3) Aint(2-7) LCV(2-1) LCV(1-2) LCV(2-3) LCV(3-2) LCV(2-7) LCV(7-2)
3	4 Top ₃ A ₃ por ₃ kL ₃ kv ₃ pvMult ₃ H ₁ RockID ₃ pvtID ₃ 2 4 7 ...
4	4 Top ₄ A ₄ por ₄ kL ₄ kv ₄ pvMult ₄ H ₁ RockID ₄ pvtID ₄ 3 5 7 ...
5	4 Top ₅ A ₅ por ₅ kL ₅ kv ₅ pvMult ₅ H ₁ RockID ₅ pvtID ₅ 4 6 7 ...

6	4 Top ₆ A ₆ por ₆ kL ₆ kv ₆ pvMult ₆ H ₁ RockID ₆ pvtID ₆ 1 5 7 ...
7	7 Top ₇ A ₇ por ₇ kL ₇ kv ₇ pvMult ₇ H ₁ RockID ₇ pvtID ₇ 1 2 3 4 5 6 ...

4. Keyword “END_CV : end of grid section

Note on symbols:

- Top_I : grid top of CV_I, *ft*
- A_I : Area of CV_I, *ft*²
- por_I : porosity of CV_I, fraction
- kL_I and kv_I : Lateral and vertical permeability of CV_I, *md*
- H_I : Thickness of CV_I, *ft*
- RockID_I : Rock ID of CV_I, integer
- pvtID_I : pvt ID of CV_I, integer
- Aint (I –J) : area of interface of CV_I and CV_J, *ft*²
- LCV(I-J) : distance from CV_I to Aint(I-J), *ft*

The data structure of rocks, fluids and other sections are relatively similar with other simulators and specifically discussed in Chapter III of this dissertation.

APPENDIX C

SIMULATION DATASETS

Regular Fracture Spacing

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Disconnected Fracture Network

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7 2000 0.15313 0.3 100 10 1 20 1 1 22 27 165 166 499 590 0.14306 0.143 0.68303 0.67171 0.21977 0.0071 1.77E-03 1.77E-03 0.10000801 0.100005751 0.77478604 3.026648533 0.00177 0.00177 0.10001 0.10001 0.77479 3.02665

4 2000 0.38554 0.3 100 10 1 20 1 1 21 23 165 0.14306 0.09985 3.88438 1.77E-03 3.783308368 9.88E-02 0.00177 3.78331 0.09875

4 2000 0.75445 0.3 100 10 1 20 1 1 22 24 167 0.09985 0.09952 756662 3.783311864 3.783313198 9.88E-02 3.78331 3.78331 0.09875

4 2000 0.76499 0.3 100 10 1 20 1 1 23 25 169 0.09952 0.10265 756662 3.783310819 3.783309641 9.87E-02 3.78331 3.78331 0.09875

4 2000 0.76612 0.3 100 10 1 20 1 1 24 26 171 0.10265 756662 3.783310342 3.783310218 9.88E-02 3.78331 3.78331 0.09875

5 2000 0.38554 0.3 100 10 1 20 1 1 25 31 32 173 0.09985 756662 3.783310342 3.78331027 2.50E-03 1.77E-03 9.87E-02 3.78331 0.0025 0.00177 0.09875

4 2000 0.39074 0.3 100 10 1 20 1 1 26 28 166 0.143 0.09985 3.88429 1.77E-03 3.783311864 0.098749206 0.00177 3.78331 0.09875

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4 2000 0.76601 0.3 100 10 1 20 1 1 29 31 172 0.09956 0.10204 756662 3.78331181 3.78330923 9.88E-02 3.78331 3.78331 0.09875

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7 2000 0.22004 0.3 100 10 1 20 1 1 26 31 173 174 519 594 0.14301 0.14304 0.97118 0.98297 0.22731 0.0071 1.77E-03 1.77E-03 0.100006846 0.100008478 1.07405539 3.026648533 0.00177 0.00177 0.10001 0.107406 3.02665

7 2000 0.13405 0.3 100 10 1 20 1 1 34 40 205 206 414 595 0.14329 0.14331 0.58237 0.59732 0.21777 0.00374 1.77E-03 1.77E-03 0.100004358 0.100006738 0.687062055 2.927335242 0.00177 0.00177 0.10001 0.10001 0.68706 2.92734

4 2000 0.3609 0.3 100 10 1 20 1 1 33 35 205 0.14329 0.10119 3.61419 1.77E-03 3.512801201 9.87E-02 0.00177 3.5128 0.09875

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5 2000 0.3607 0.3 100 10 1 20 1 1 38 45 210 0.10119 3.61419 3.512799993 2.50E-03 1.77E-03 9.87E-02 3.5128 0.0025 0.00177 0.09875

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7 2000 0.11171 0.3 100 10 1 20 1 1 39 45 215 216 422 600 0.14343 0.14339 0.49941 0.47325 0.21624 0.00374 1.77E-03 1.77E-03 0.100006241 0.100007836 0.581009453 2.927335242 0.00177 0.00177 0.10001 0.1058101 2.92734

7 2000 0.27147 0.3 100 10 1 20 1 1 48 58 253 254 523 601 0.14311 0.14312 1.1936 1.20848 0.23301 0.00525 0.001767694 1.77E-03 0.100009082 0.100008509 1.296929818 2.772041717 0.00177 0.00177 0.10001 0.10001 1.29693 2.77204

4 2000 0.31684 0.3 100 10 1 20 1 1 47 49 254 0.14311 0.10116 3.61818 1.77E-03 3.080046445 9.88E-02 0.00177 3.08005 0.09875

4 2000 0.62316 0.3 100 10 1 20 1 1 48 50 256 0.10116 0.10116 6.16009 3.080046435 3.080046452 9.88E-02 3.08005 3.08005 0.09875

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4 2000 0.62318 0.3 100 10 1 20 1 1 52 54 264 0.10115 0.10118 6.16009 3.080049338 3.080050433 9.88E-02 3.08004 3.08004 0.09875

4 2000 0.62316 0.3 100 10 1 20 1 1 53 55 266 0.10118 0.10114 6.16009 3.080043573 3.080042851 9.88E-02 3.08005 3.08005 0.09875

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 0.10001 0.98014 2.75913
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 5 2000 2.72653 0.3 100 10 1 20 1 1 14 97 101 117 625 0.43618 0.43625 6.25 0.098748398 3.125003912 3.125001847 0.337500381 0.09875 3.125 0.3375
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5 2000 7.84626 0.3 100 10 1 20 1 1 336 344 348 356 6.89783 1.1375 1.13749 6.89783 0.337499513 3.448916063 3.448913966 0.800000701 0.3375 3.44892 3.44891 0.8
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 6 2000 19.04833 03 100 10 1 20 1 1 151 153 241 243 430 0.72363 4.17841 4.59323 4.71311 3.20706 3.036525289 1.859805389 2.373232099 2.219409068 2.110097034 3.03652 1.8598 2.37323 2.21941
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 6 2000 29.31496 03 100 10 1 20 1 1 401 411 444 445 453 1.15402 4.06876 0.36425 4.57813 2.52476 3.1.57036731 2.873153285 3.213380698 2.554275048 3.04012881 3.15704 2.87316 3.21338 2.55428
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 5 2000 33.15196 03 100 10 1 20 1 1 416 164 436 467 1.02001 6.29203 1.06996 7.23959 3.213158552 2.829287806 3.25817542 2.58754813 3.21315 2.82928 3.25817 2.58754
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6 2000 55.94909 03 100 10 1 20 1 1 503 505 507 508 573 3.69208 3.07997 1.01662 4.6634 7.18065 5.37727978 5.652994334 4.936352685 4.09099974 2.909137994 5.37728 5.65299 4.93636 4.0991 2.90914
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6 2000 50.83524 03 100 10 1 20 1 1 196 198 502 503 507 4.79866 5.48383 8.17539 7.37297 2.3971 3.9175642 3.468200433 3.502082779 3.40577844 4.21794061 3.91756 3.4682 3.50208 3.40578 4.21794
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7 2000 43.15515 03 100 10 1 20 1 1 199 201 509 511 512 518 4.38522 5.34548 2.98116 3.17088 3.23886 5.62814 3.454819068 3.174971401 3.875650618 4.001724827 3.9249915 3.06193481 3.45482 3.17497
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7 2000 41.95059 03 100 10 1 20 1 1 201 203 314 510 512 522 3.83158 2.93461 3.77771 3.17088 5.02272 6.20851 3.767638204 3.27685079 3.84364976 4.001726433 3.253792806 2.624922348 3.76764
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7 2000 37.34128 03 100 10 1 20 1 1 314 316 510 511 513 518 5.07343 3.08042 3.23886 5.02272 3.49027 3.05912 2.635309706 3.146405246 3.924991907 3.253791771 3.253793836 3.663882683 2.63531
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7 2000 34.37016 03 100 10 1 20 1 1 316 318 512 514 517 518 4.21105 3.24839 3.49027 3.76964 1.96314 5.45855 2.848739632 3.165962952 3.253793811 3.198559004 3.796995326 2.856389558 2.84874
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7 2000 31.57312 03 100 10 1 20 1 1 318 320 418 513 515 517 3.94296 2.79133 1.25148 3.76964 3.8497 5.89952 3.00174788 3.193867816 3.596470325 3.198557777 2.924615123 2.471062558 3.00175 3.19387
3.59647 3.19856 2.92461 2.47106
6 2000 24.75672 03 100 10 1 20 1 1 320 322 418 419 514 514 4.25447 2.03101 5.71282 3.63488 3.8497 2.658665939 3.051267695 1.952177508 2.639362132 2.924614876 2.65867 3.05127 1.95218 2.63937
2.92462
6 2000 32.03897 03 100 10 1 20 1 1 416 417 509 517 518 4.92096 3.78581 4.60278 4.79207 3.58737 2.829647933 2.633956195 3.367189907 2.463358116 3.587209199 2.82965 2.63396 3.36719 2.46336
3.58721
7 2000 31.86928 03 100 10 1 20 1 1 417 418 513 514 516 518 4.02127 2.42155 1.96314 5.89952 4.79207 2.64538 2.74439852 3.681995521 3.796994166 2.471062848 2.463361177 3.761161211 2.7444
3.68199 3.797 2.47106 2.46336 3.76116
7 2000 40.01168 03 100 10 1 20 1 1 509 510 512 513 516 517 3.57881 5.62814 3.05912 5.45855 3.58737 2.64538 3.736441788 3.061931974 3.66388266 2.856390411 3.587208513 3.761159338 3.73644
3.06193 3.66388 2.85639 3.58721 3.76116
12 2000 21.26469 03 100 10 1 20 1 1 32 173 174 183 184 193 194 203 204 520 571 0.22731 0.04243 0.42837 1.20718 1.25183 3.51267 3.69845 0.37918 0.73866 84561 0.10226 1.07405271 1.074756889
1.085111168 1.139631841 1.181787818 1.596650767 1.681097412 2.94671118 3.05112949 2.69195135 3.6536336894 1.07406 1.07476 1.08511 1.13963 1.18179 1.59665 1.6811 2.94672 3.05114 2.69195 3.65364
7 2000 46.29413 03 100 10 1 20 1 1 203 519 521 526 571 572 0.54356 8.4561 7.03608 5.74118 4.49178 1.0238 4.495672632 2.691951976 3.003174018 3.516300941 4.66656436 4.987113892 4.49567 2.69195
3.00317 3.5163 4.66656 4.98711
5 2000 42.47879 03 100 10 1 20 1 1 520 525 526 527 703608 2.05346 4.32949 4.04684 3.008174125 5.489227547 4.193081744 4.282782544 3.00817 5.48923 4.19308 4.28278
6 2000 43.10633 03 100 10 1 20 1 1 203 314 511 524 526 6.28798 2.25517 6.20851 4.23288 6.85534 2.235237706 4.928176415 2.624921508 5.028392095 3.422479821 2.23524 4.92818 2.62492 5.02839
3.42248
11 2000 21.5274 03 100 10 1 20 1 1 47 253 254 273 274 293 294 314 524 528 0.23301 0.42136 0.42531 1.17937 1.2258 2.17875 3.37314 1.14658 6.45848 1.25048 2.96930454 1.295650769 1.308367601
1.343219294 1.396104517 1.735452872 1.849745811 3.16506433 2.648352004 2.948454366 1.29693 1.29565 1.30837 1.34322 1.3961 1.73545 1.84974 3.16502 2.64835 2.94485
8 2000 48.18071 03 100 10 1 20 1 1 314 522 523 525 526 527 528 0.69977 4.23288 6.54581 5.16276 2.36576 2.69522 4.78793 4.898379089 5.028390858 2.648350085 3.671650619 4.796722805 3.977905444
2.775388347 4.89838 5.02839 2.64835 3.67166 4.79673 3.97791 2.77539
5 2000 47.26893 03 100 10 1 20 1 1 521 524 526 527 205346 5.16276 7.9433 4.9124 5.489228028 3.67165615 3.269091372 3.162702105 5.48923 3.67166 3.26909 3.1627
7 2000 52.0085 03 100 10 1 20 1 1 203 520 521 522 524 525 124569 5.74118 4.32949 6.85534 2.36576 7.9433 4.401233842 3.516300596 4.193080055 3.42247985 4.796725155 3.269091044 4.40124 3.5163
4.19308 3.42248 4.79672 3.26909
5 2000 29.70111 03 100 10 1 20 1 1 524 525 528 564 2.69522 4.9124 3.78618 2.9891 3.977905407 3.162702138 3.843641361 3.931645858 3.97791 3.1627 3.84364 3.93165
8 2000 34.1847 03 100 10 1 20 1 1 293 313 523 524 527 564 565 0.8226 2.94402 2.50428 4.78793 3.78618 3.22263 3.75813 3.108266765 2.78661881 2.94485363 2.77539 3.843641187 3.617547768
2.77539 3.84364 3.61755 2.85639
7 2000 32.06948 03 100 10 1 20 1 1 313 315 530 562 565 566 2.71955 2.89609 3.50074 3.09964 4.58159 4.51358 3.322014888 3.670802644 3.35021184 3.03872333 2.601282442 2.530912105 3.32202
3.6708 3.335021 3.03837 2.60128 2.53091
5 2000 37.15153 03 100 10 1 20 1 1 315 317 529 531 556 562 4.09531 3.2266 3.50074 4.39148 2.80531 4.85054 3.289902892 3.408524944 3.350212635 3.089742327 3.654143864 2.94485481 3.2899 3.40852
3.35021 3.08974 3.65414 2.94486
7 2000 33.3374 03 100 10 1 20 1 1 317 319 364 530 532 556 3.71564 2.71945 3.42983 4.39148 3.05957 4.33476 3.270368965 3.3380955925 2.847229301 3.089740611 2.908321768 3.021315648 3.27037
3.38096 2.84723 3.08974 2.90832 3.02132
8 2000 26.18938 03 100 10 1 20 1 1 319 312 351 364 531 533 534 4.20229 3.08824 1.62053 3.6017 3.05957 2.14906 1.41132 2.832594104 3.158989234 2.415080591 2.05623673 2.908319719 2.727028653
2.388657544 2.8326 3.15899 2.41503 2.05624 2.90832 2.72703 3.28866
10 2000 12.2747 03 100 10 1 20 1 1 69 33 343 344 353 524 532 534 0.22462 0.42827 0.4267 1.25432 1.23688 1.79773 1.58608 2.14906 4.93363 0.980135178 0.988340032 0.98459381 1.081986435
1.0693805 1.593820778 1.56486354 2.727029011 1.946085208 0.98013 0.98834 0.98459 1.08198 1.06949 1.59381 1.56486 2.72703 1.94609
8 2000 27.39142 03 100 10 1 20 1 1 321 323 353 363 532 533 535 4.34934 3.97374 1.28154 1.24385 1.41132 4.93363 2.94746 2.618091099 2.764151313 2.86030464 3.522350981 3.288656987 1.946085335
3.434260881 2.61809 2.76415 2.80624 3.52234 3.28866 1.94609 3.43426
7 2000 35.79613 03 100 10 1 20 1 1 323 325 363 534 536 539 3.86058 4.21667 5.46978 2.94746 5.73687 0.8028 2.793782466 2.53194893 3.515822525 3.434264447 2.931102377 4.934909107 2.79378
2.53195 3.51582 3.43426 2.93111 4.93491

5 2000 0.08458 0.99 2098.809029 2098.809029 1 20 1 1 587 589 9 18 001522 001522 2.77778 2.77778 2.77779444 2.77779444 7.61E-03 7.61E-03 2.77778 2.77778 0.00761 0.00761
 5 2000 0.09055 0.99 2405.764031 2405.764031 1 20 1 1 588 20 10 19 00163 00163 2.77778 2.77778 2.77779444 8.15E-03 8.15E-03 2.77778 2.77778 0.00815 0.00815
 5 2000 0.0859 0.99 1823.474282 1823.474282 1 20 1 1 591 21 22 27 001419 001419 3.02665 3.02665 3.026648533 3.026648533 7.10E-03 7.10E-03 3.02665 3.02665 0.0071 0.0071
 5 2000 0.00555 0.99 7.615165618 7.615165618 1 20 1 1 590 592 23 28 0.00092 0.00092 3.02665 3.02665 3.026648533 3.026648533 4.15E-03 4.15E-03 3.02665 3.02665 0.00046 0.00046
 5 2000 0.05019 0.99 6223949087 6223949087 1 20 1 1 591 593 24 29 0.00829 0.00829 3.02665 3.02665 3.026648533 3.026648533 8.63E-03 8.63E-03 3.02665 3.02665 0.00863 0.00863
 5 2000 0.10449 0.99 2698.299435 2698.299435 1 20 1 1 592 594 25 30 0.01726 0.01726 3.02665 3.02665 3.026648533 3.026648533 7.91E-03 7.91E-03 3.02665 3.02665 0.00791 0.00791
 5 2000 0.00976 0.99 2266.102085 2266.102085 1 20 1 1 593 12 26 31 001582 001582 3.01726 3.02665 3.026648533 3.026648533 7.91E-03 7.91E-03 3.02665 3.02665 0.00791 0.00791
 5 2000 0.0438 0.99 506.7288693 506.7288693 1 20 1 1 596 33 34 40 0.00748 0.00748 292734 292734 2927335242 2927335242 3.74E-03 3.74E-03 292734 292734 0.00374 0.00374
 5 2000 0.1127 0.99 3355.116883 3355.116883 1 20 1 1 595 597 35 41 0.01925 0.01925 292734 292734 2927335242 2927335242 9.62E-03 9.62E-03 292734 292734 0.00962 0.00962
 5 2000 0.1021 0.99 2753.768709 2753.768709 1 20 1 1 596 598 36 42 0.01744 0.01744 292734 292734 2927335242 2927335242 8.72E-03 8.72E-03 292734 292734 0.00872 0.00872
 5 2000 0.00664 0.99 11.65947747 11.65947747 1 20 1 1 597 599 37 43 0.00113 0.00113 292734 292734 2927335242 2927335242 5.67E-04 5.67E-04 292734 292734 0.00057 0.00057
 5 2000 0.11125 0.99 3269.244857 3269.244857 1 20 1 1 598 600 38 44 0.019 0.019 292734 292734 2927335242 2927335242 9.50E-03 9.50E-03 292734 292734 0.0095 0.0095
 5 2000 0.04268 0.99 4812691466 4812691466 1 20 1 1 599 14 39 45 0.00729 0.00729 292734 292734 2927335242 2927335242 3.65E-03 3.65E-03 292734 292734 0.00365 0.00365
 5 2000 0.05825 0.99 9997154129 9997154129 1 20 1 1 600 47 48 58 0.01051 0.01051 2.77204 2.77204 2.772041717 2.772041717 5.25E-03 5.25E-03 2.77204 2.77204 0.00525 0.00525
 5 2000 0.08511 0.99 2134.182581 2134.182581 1 20 1 1 601 603 49 59 0.01535 0.01535 2.77204 2.77204 2.772041717 2.772041717 7.68E-03 7.68E-03 2.77204 2.77204 0.00768 0.00768
 5 2000 0.00599 0.99 10.56352278 10.56352278 1 20 1 1 602 604 50 50 0.00108 0.00108 2.77204 2.77204 2.772041717 2.772041717 5.40E-04 5.40E-04 2.77204 2.77204 0.00054 0.00054
 5 2000 0.06575 0.99 1273.49331 1273.49331 1 20 1 1 603 605 51 51 0.01186 0.01186 2.77204 2.77204 2.772041717 2.772041717 5.93E-03 5.93E-03 2.77204 2.77204 0.00593 0.00593
 5 2000 0.05203 0.99 7973787511 7973787511 1 20 1 1 604 606 52 52 0.00938 0.00938 2.77204 2.77204 2.772041717 2.772041717 4.69E-03 4.69E-03 2.77204 2.77204 0.00469 0.00469
 5 2000 0.0312 0.99 323.0861864 323.0861864 1 20 1 1 605 607 53 53 0.00597 0.00597 2.77204 2.77204 2.772041717 2.772041717 2.99E-03 2.99E-03 2.77204 2.77204 0.00299 0.00299
 5 2000 0.0691 0.99 1406691077 1406691077 1 20 1 1 606 608 54 54 0.01246 0.01246 2.77204 2.77204 2.772041717 2.772041717 6.23E-03 6.23E-03 2.77204 2.77204 0.00623 0.00623
 5 2000 0.07189 0.99 1522.400354 1522.400354 1 20 1 1 607 609 55 55 0.01297 0.01297 2.77204 2.77204 2.772041717 2.772041717 6.48E-03 6.48E-03 2.77204 2.77204 0.00648 0.00648
 5 2000 0.02931 0.99 2529994307 2529994307 1 20 1 1 608 610 56 56 0.00529 0.00529 2.77204 2.77204 2.772041717 2.772041717 2.64E-03 2.64E-03 2.77204 2.77204 0.00264 0.00264
 5 2000 0.03103 0.99 283.644528 283.644528 1 20 1 1 609 22 57 57 0.0056 0.0056 2.77204 2.77204 2.772041717 2.772041717 2.80E-03 2.80E-03 2.77204 2.77204 0.0028 0.0028
 5 2000 0.09164 0.99 2497.00962 2497.00962 1 20 1 1 612 60 70 70 0.0166 0.0166 2.75913 2.75913 2.759131919 2.759131919 8.30E-03 8.30E-03 2.75913 2.75913 0.0083 0.0083
 5 2000 0.09106 0.99 2465.83413 2465.83413 1 20 1 1 611 613 71 76 0.0165 0.0165 2.75913 2.75913 2.759131919 2.759131919 8.25E-03 8.25E-03 2.75913 2.75913 0.00825 0.00825
 5 2000 0.006508 0.99 1259.37831 1259.37831 1 20 1 1 612 614 72 77 0.01179 0.01179 2.75913 2.75913 2.759131919 2.759131919 5.90E-03 5.90E-03 2.75913 2.75913 0.0059 0.0059
 5 2000 0.10889 0.99 3525.531906 3525.531906 1 20 1 1 613 615 73 78 0.01973 0.01973 2.75913 2.75913 2.759131919 2.759131919 9.87E-03 9.87E-03 2.75913 2.75913 0.00987 0.00987
 5 2000 0.10059 0.99 3009.038758 3009.038758 1 20 1 1 614 12 74 79 0.01823 0.01823 2.75913 2.75913 2.759131919 2.759131919 9.11E-03 9.11E-03 2.75913 2.75913 0.00911 0.00911
 5 2000 0.02458 0.99 1872403805 1872403805 1 20 1 1 617 81 82 87 0.00455 0.00455 2.70222 2.70222 2.702215967 2.702215967 2.27E-03 2.27E-03 2.70222 2.70222 0.00227 0.00227
 5 2000 0.07519 0.99 175261674 175261674 1 20 1 1 616 618 83 88 0.01391 0.01391 2.70222 2.70222 2.702215967 2.702215967 6.96E-03 6.96E-03 2.70222 2.70222 0.00696 0.00696
 5 2000 0.10598 0.99 3482.142262 3482.142262 1 20 1 1 617 619 84 89 0.01961 0.01961 2.70222 2.70222 2.702215967 2.702215967 9.81E-03 9.81E-03 2.70222 2.70222 0.00981 0.00981
 5 2000 0.02642 0.99 216402498 216402498 1 20 1 1 618 620 85 90 0.00489 0.00489 2.70222 2.70222 2.702215967 2.702215967 24.4E-03 24.4E-03 2.70222 2.70222 0.00244 0.00244
 5 2000 0.05776 0.99 1034.278725 1034.278725 1 20 1 1 619 12 86 91 0.01069 0.01069 2.70222 2.70222 2.702215967 2.702215967 5.34E-03 5.34E-03 2.70222 2.70222 0.00534 0.00534
 END_CV

Multiple Reservoir Model

NXNY274
 NZ1
 100
 START_CV274
 32000 102491.90033 0.3 215.21.5 100 1 1 214 101 25000 462.5 462.5 50000 462.5 50000
 42000 784690.4327403 215.21.5 100 1 1 13 15 101 250760 101 24925 775.00000 462.5 312.5 462.499999992945 462.5 50000 312.5 50000 462.5 50000
 42000 518904.279303 215.21.5 100 1 1 12 4 101 24929 101 24929 50000 312.5 50000 312.5 50000 200.00000 462.5 50000
 42000 329078.8054 0.3 215.21.5 100 1 1 13 5 17 101 260034 101 249548 325.00000 200 125 462.49999999466 312.5 50000 200.00000 125.00000 462.5 50000
 42000 208827.6592303 215.21.5 100 1 1 14 6 18 101 249548 101 225293 206.25000 125 81.25 462.499999997104 125.00000 81.25000 462.5 50000
 42000 126547.0581103 215.21.5 100 1 1 15 7 19 101 225293 101 249962 125.00000 81.25 43.75 462.49999999698 81.25000 43.75000 462.5 50000
 42000 88593.7339803 215.21.5 100 1 1 16 8 201 249962 101 249808 37.50000 43.75 43.75 462.499999992253 43.75000 43.75000 462.5 50000
 42000 126562.3779303 215.21.5 100 1 1 17 9 21 101 249981 101 249981 125.00000 43.75 81.25 462.4999999986 43.75000 81.25000 462.5 50000
 42000 208827.4829903 215.21.5 100 1 1 18 10 22 101 249381 101 264478 206.25000 81.25 125 462.49999999293 81.25000 125.00000 462.5 50000
 42000 329086.0260003 215.21.5 100 1 1 19 11 23 101 264478 101 249993 325.00000 125 200 462.499999991855 125.00000 200.00000 462.5 50000
 42000 518906.093603 215.21.5 100 1 1 11 12 24 101 249939 101 248346 512.5 50000 203 462.49999999291 203.00000 312.5 50000 462.5 50000
 42000 784681.1142003 215.21.5 100 1 1 11 13 25 39 101 249939 101 248346 101 253308 77.5 50000 312.5 462.5 462.49999999546 312.5 50000 462.5 50000 462.5 50000
 32000 102504890671 0.3 215.21.5 100 1 1 12 26 101 253308 101 25000 462.5 462.49999999586 462.5 50000 462.5 50000
 42000 784681.5673803 215.21.5 100 1 1 11 15 27 101 25000 77.4 77.4 77.4 462.5 50000 462.5 50000 462.5 50000 312.5 50000
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 52000 397190.37781 0.3 215.21.5 100 1 1 13 15 17 29 51 50000 77.4 77.4 77.4 462.5 50000 77.4 77.4 77.4 462.5 50000 312.5 50000
 52000 251876.11084 0.3 215.21.5 100 1 1 14 16 18 30 325.00000 77.5 00272 77.5 00000 462.5 50000 373.5 200 125 312.49999999265 462.5 50000 200.00000 125.00000 312.5 50000
 52000 159841.66031 0.3 215.21.5 100 1 1 15 17 19 31 206.25000 77.5 00000 77.4 95605 206.25000 462.5 50000 00962 125 81.25 312.49999999038 462.5 50000 125.00000 81.25000 312.5 50000
 52000 968748.87793 0.3 215.21.5 100 1 1 16 18 20 32 125.00000 77.4 95605 77.4 95605 125.00000 462.5 50000 008714 81.25 43.75 312.499999991286 462.5 50000 81.25000 43.75000 312.5 50000
 52000 67812521360 0.3 215.21.5 100 1 1 17 19 21 33 78.75000 77.4 99930 77.5 00127 87.50000 462.5 50000 00563 43.75 43.75 312.49999999437 462.5 50000 43.75000 43.75000 312.5 50000
 52000 96875.3967303 0.3 215.21.5 100 1 1 18 20 22 34 125.00000 77.5 00127 77.5 00174 125.00000 462.5 50000 00946 43.75 81.25 312.49999999504 462.5 50000 43.75000 81.25000 312.5 50000
 52000 159840.8294703 0.3 215.21.5 100 1 1 19 21 35 206.25000 77.5 01747 77.4 95050 206.25000 462.5 50000 00364 81.25 125 312.49999999636 462.5 50000 81.25000 125.00000 312.5 50000
 52000 251879.60205 0.3 215.21.5 100 1 1 10 22 24 36 325.00000 77.4 95050 073 325.00000 462.5 50000 005249 125 200 312.499999994751 462.5 50000 125.00000 200.00000 312.5 50000
 52000 397187.06207 0.3 215.21.5 100 1 1 11 23 25 37 51 50000 77.5 07037 77.4 99680 512.5 50000 462.5 50000 007671 200 301 312.5 312.49999999239 462.5 50000 200.00000 312.5 50000 312.5 50000
 52000 600637.4877903 0.3 215.21.5 100 1 1 12 24 26 38 77.5 00000 77.4 99680 77.5 06122 77.5 00000 462.5 50000 00535 312.5 462.5 312.49999999465 462.5 50000 312.5 50000 462.5 50000 312.5 50000
 42000 784703.8147003 0.3 215.21.5 100 1 1 11 13 25 39 101 25000 77.5 06122 101 25000 462.5 50000 005924 462.5 312.499999994076 462.5 50000 462.5 50000 312.5 50000
 42000 518917.373660 0.3 215.21.5 100 1 1 14 28 40 101 25000 512.5 5275 101 25000 312.5 462.5 200 312.5 50000 462.5 50000 200.00000
 52000 397181.6345203 0.3 215.21.5 100 1 1 15 27 29 41 77.5 00000 512.5 5275 512.49994 77.5 00000 312.5 50000 004687 462.5 312.5 199.999999995313 312.5 50000 462.5 50000 312.5 50000
 52000 262649.6185303 0.3 215.21.5 100 1 1 16 28 30 42 512.5 50000 512.49994 512.5 50000 312.5 50000 002982 312.5 200 199.999999997018312.5 50000 200.00000 200.00000

Connected Fracture Networks

NXNY 1593
NZ 1
20

START CV 1503

STAR1_CV_159
7 2000 022341 03 100 10 1 20 1 2 27 405 406 986 1214 022824 0.2282 0.6022 0.60421 0.33192 0.00706 1.77E-03 1.77E-03 0.160004259 0.160005645 0.762183882 2036158209 0.00177 0.00177 0.160016 0.076218 203616
4 2000 03546 03 100 10 1 20 1 1 1 3 406 022824 0.16084 0.228253 1.77E-03 2.12099876 0.158750145 0.00177 2.121 0.15875
4 2000 068311 03 100 10 1 20 1 2 4 408 0.16084 0.16084 0.16084 4.24199 2.120997561 2.12099875 0.158752626 2.121 2.121 0.15875
4 2000 06839 03 100 10 1 20 1 1 3 5 410 0.16084 0.16159 0.16159 4.24199 2.120998471 2.12099756 0.158748083 2.121 2.121 0.15875
4 2000 068392 03 100 10 1 20 1 1 4 6 412 0.16159 0.16086 4.24199 2.12099696 2.120997888 0.158752626 2.121 2.121 0.15875
4 2000 068232 03 100 10 1 20 1 1 5 7 414 0.16086 0.16086 0.16084 4.24199 2.120998433 2.120999636 0.158749023 2.121 2.121 0.15875
4 2000 068391 03 100 10 1 20 1 1 6 8 416 0.16084 0.16161 0.16161 4.24199 2.12099739 2.120997502 0.158748083 2.121 2.121 0.15875
4 2000 068232 03 100 10 1 20 1 1 7 9 418 0.16161 0.16009 0.16009 4.24199 2.120997017 2.120999279 0.15875294 2.121 2.121 0.15875
4 2000 068232 03 100 10 1 20 1 1 8 10 420 0.16009 0.16161 0.16161 4.24199 2.120998844 2.120997502 0.15874871 2.121 2.121 0.15875
4 2000 046474 03 100 10 1 20 1 1 9 422 485 0.16161 2.95737 0.022006 2.120997017 0.158752367 0.508156471 2.121 0.15875 0.50317
4 2000 042266 03 100 10 1 20 1 1 10 424 485 775 2.60309 0.1695 0.17633 0.158745241 1.786429667 0.751962108 0.15875 1.78642 0.75197
4 2000 054246 03 100 10 1 20 1 1 13 426 776 0.16088 3.34188 0.17118 2.120999666 0.158751201 1.202170264 2.121 0.15875 1.20217
4 2000 068395 03 100 10 1 20 1 1 14 12 428 0.16086 0.16084 4.24199 2.120998457 2.120999603 0.15874871 2.121 2.12099 0.15875
4 2000 06839 03 100 10 1 20 1 1 13 15 430 0.16084 0.1593 0.1593 4.24199 2.120994915 2.121001387 0.158752313 2.121 2.121 0.15875
4 2000 068386 03 100 10 1 20 1 1 14 16 432 0.1593 0.16235 0.16235 4.24199 2.120996735 2.12099796 0.158747456 2.121 2.121 0.15875
4 2000 068382 03 100 10 1 20 1 1 15 17 434 0.16235 0.15929 0.15929 4.24199 2.120996559 2.120999671 0.158752313 2.121 2.121 0.15875
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7 2000 0.14322 0.3 100 10 1 20 1 1 352 356 739 740 940 1381 02282 0.22857 0.36503 0.35515 0.32827 0.00483 1.77E-03 1.77E-03 0.15998836 0.16004712 0.519087929 2.11703457 0.00177 0.00177
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4 2000 0.22172 0.3 100 10 1 20 1 1 351 450 739 0.2282 0.19292 1.50598 1.77E-03 1.04126059 0.158742093 0.00177 1.04125 0.15875
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0.16 0.65007 2.07233

4 2000 0.04125 0.3 100 10 1 20 1 1 361 363 748 0.2282 0.16006 2.6482 1.77E-03 2.486796243 0.158751194 0.00177 2.4868 0.15875
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4 2000 0.79606 0.3 100 10 1 20 1 1 363 365 752 0.16006 0.16006 4.97346 2.48679139 2.486796243 0.158751327 2.4868 2.4868 0.15875
5 2000 0.78298 0.3 100 10 1 20 1 1 364 514 516 754 0.16006 0.1802 0.01611 4.84377 2.486796756 1.9844884 2.26837327 0.158750732 2.4868 1.98442 2.2677 0.15875
5 2000 0.7265 0.3 100 10 1 20 1 1 354 516 712 756 0.20664 0.08579 0.16457 4.42779 1.485705043 0.096129712 2.122744699 0.158748396 1.48573 0.9616 2.12274 0.15875
5 2000 0.13221 0.3 100 10 1 20 1 1 373 374 712 758 0.06916 0.22809 0.021233 0.966 2.50E+03 1.77E-03 0.511783462 0.158749444 0.0025 0.00177 0.51179 0.15875
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5 2000 0.10986 0.3 100 10 1 20 1 1 367 374 712 757 0.066916 0.22831 0.021029 0.69518 2.50E+03 1.77E-03 0.510179163 0.158749624 0.0025 0.00176 0.51017 0.15875
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7 2000 0.11347 0.3 100 10 1 20 1 1 376 387 759 760 828 1391 0.20352 0.20359 0.2959 0.28045 0.32681 0.00411 1.58E-03 1.58E-03 0.160006797 0.160003801 0.410293911 1.948342957 0.00158 0.00158 0.16
0.16 0.41029 1.94834

4 2000 0.34598 0.3 100 10 1 20 1 1 375 618 760 0.20352 0.16095 2.21471 1.58E-03 2.083894487 0.159032096 0.00158 2.08389 0.15903
5 2000 0.07774 0.3 100 10 1 20 1 1 213 237 618 762 0.0745 0.1543 0.23333 0.64839 0.13574757 0.13784264 8.73E-02 0.159032921 0.13575 0.13784 0.08732 0.15903
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 6 2000 8.821302 03 100 10 1 20 1 1 149 548 657 659 1008 3.30339 2.15688 0.09452 1.90242 3.1541 0.158756286 2.122141454 2.391691112 1.174485274 2.165085725 0.15875 2.12214 2.39169 1.17448
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 6 2000 7.62086 03 100 10 1 20 1 1 126 545 549 1107 1110 4.24428 1.61153 1.80888 0.26224 4.05322 0.158751158 2.12213803 2.122141931 2.511910682 1.640816556 0.15875 2.12214 2.12214 2.5119
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 7 2000 9.960176 03 100 10 1 20 1 1 150 546 550 1008 1009 1010 4.24428 2.15688 2.11698 0.07339 3.94252 0.32506 0.158756232 2.122137734 2.122141198 2.905029778 2.109208652 2.86411937 0.15875
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 7 2000 5.9151 03 100 10 1 20 1 1 127 547 943 1110 1111 2.28458 0.52654 1.80888 1.88562 0.20253 3.37256 0.158747919 0.160008023 2.122139809 0.698431061 2.688185225 1.685123319 0.15875
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 6 2000 6.6672 03 100 10 1 20 1 1 151 552 548 943 1010 2.28413 0.48055 2.11698 2.51561 3.0528 0.158745039 0.160008067 2.122140623 0.655211808 2.212429497 0.15874 0.16 2.12214 0.65521 2.21243
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 7 2000 5.40742 03 100 10 1 20 1 1 153 154 554 985 1159 1160 0.49857 2.27098 1.82619 1.74093 0.18857 2.95202 0.160002858 0.158749095 2.110191692 0.675773616 2.688343832 1.638718144 0.16001
 0.15875 2.11019 0.67577 2.68834 1.63872
 6 2000 3.40405 03 100 10 1 20 1 1 179 406 551 555 984 4.22036 0.040792 0.611 0.63264 0.406487 0.158750427 2.106091788 2.110191985 2.110189834 0.653422879 0.15875 2.10609 2.11019 0.65342
 6 2000 7.43581 03 100 10 1 20 1 1 155 552 556 1158 1159 4.22036 1.82619 1.58973 0.13694 4.14346 0.158750753 2.110191573 2.110191862 2.54932773 1.603434563 0.15875 2.11019 2.11019 2.54933
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 6 2000 3.98115 03 100 10 1 20 1 1 180 553 557 983 984 4.22036 0.63264 0.099202 4.13613 0.28215 0.158750819 2.110189652 2.110191501 0.787076269 2.154792091 0.15875 2.11019 2.11019 0.78708
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 6 2000 5.63278 03 100 10 1 20 1 1 181 555 559 982 983 4.22036 0.099202 0.0571 4.02589 0.76526 0.158750558 2.110191764 2.110190793 1.178918401 2.268260521 0.15875 2.11019 2.11019 1.17892 2.26826
 6 2000 6.99981 03 100 10 1 20 1 1 157 556 560 1157 1158 4.22036 1.66203 1.53609 4.14753 0.14118 0.158748538 2.110191116 2.110191968 1.49841167 2.590600405 0.15875 2.11019 2.11019 1.49841
 2.5906
 6 2000 5.80671 03 100 10 1 20 1 1 182 557 561 981 982 4.22036 0.09571 1.27915 3.89528 0.63391 0.158750558 2.110191949 2.110191244 1.237115753 2.1216435693 0.15875 2.11019 2.11019 1.23712 2.21643
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 2.51569
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 2.11019 2.11019 2.530569707 1.507686499 2.385491897 0.15875
 6 2000 7.12905 03 100 10 1 20 1 1 159 560 564 1155 1156 4.22036 1.66211 1.54242 4.10051 0.021401 0.158750949 2.110191403 2.110187806 1.529380909 2.58948726 0.15875 2.11019 2.11019 1.52938
 2.58949

5	2000	7.04646	03	100	10	1	20	1	1	184	561	565	979	422036	1.56135	1.77762	4.22592	0.158750819	2.110188584	2.110191678	1.508899856	0.15875	2.11019	2.11019	1.5089																																																																																															
6	2000	7.53359	03	100	10	1	20	1	1	160	562	566	1154	1155	422036	1.54242	1.53428	3.87763	0.61907	0.158750558	2.11019168	2.110192356	1.63654092	2.517145616	0.15875	2.11019	2.11019	1.6365																																																																																												
6	2000	9.64112	03	100	10	1	20	1	1	185	563	567	978	979	422036	1.77762	2.01235	3.70747	0.98315	0.158752447	2.11019211	2.110188233	2.158525456	2.656234173	0.15875	2.11019	2.11019	2.15853																																																																																												
6	2000	7.49081	03	100	10	1	20	1	1	161	564	568	1146	1154	422036	1.53428	1.63615	3.9	0.50921	0.158748929	2.110191432	2.110188693	1.627918523	2.497934292	0.15875	2.11019	2.11019	1.62792																																																																																												
6	2000	4.19204	03	100	10	1	20	1	1	191	186	482	565	978	0.0873	3.19432	3.56008	2.01235	0.53143	0.711508444	0.158754213	0.588132343	2.110191254	2.774795133	0.71149	0.15875	0.58813	2.11019	2.77479																																																																																											
10	2000	6.99806	03	100	10	1	20	1	1	166	90	162	479	480	481	566	570	1146	0.17575	0.17574	3.52566	0.7246	2.90827	0.087678	1.63615	0.10089	1.05976	1.562177412	1.561182053	0.158748189	1.631936903																																																																																									
1.505210718	2000	1.06507899	2.110190793	2.110187079	2.569147274	1.56217	1.56118	1.5875	1.63193	1.50521	1.06507	2.11019	2.1102	2.56915	2	7	2000	1.19194	03	100	10	1	20	1	1	187	382	393	481	771	772	224645	0.17174	0.17141	0.68674	1.58524	0.49512	0.158749382	0.399372714	0.398710387	1.495663717	0.375032398	0.478562484	0.15875	0.39938	0.39871	1.49567	0.37505	0.47857																																																																							
12	2000	5.81281	03	100	10	1	20	1	1	163	381	392	479	481	568	572	769	770	772	803	3.0484	0.16174	0.16185	1.096	0.65962	0.10089	0.79664	1.13063	1.47886	0.095854	0.58655	0.158747038	1.455030781	1.454843865	1.779601934	1.628071507	2.110196186	2.110188646	1.453381396	1.473964282	0.736363909	2087516578	0.15875	1.45503	1.45485	1.7796	1.62807	2.11019	2.11019	1.45338	1.47397	0.73636																																																																				
208752	7	2000	5.01014	03	100	10	1	20	1	1	188	573	772	973	3.96433	1.20326	1.42794	3.70754	0.158750521	2.110190662	1.793494033	1.517172032	0.15875	2.11019	1.7935	1.51717	5	7	2000	6.58568	03	100	10	1	20	1	1	164	570	574	772	802	803	4.05382	0.079644	1.35217	0.48189	3.21476	1.81719	0.158746472	2.110194619	2.110191616	1.878757403	1.483254664	1.964447434	0.15875	2.11019	2.11019	1.87876	1.48326	1.96445																																																											
6	2000	4.06836	03	100	10	1	20	1	1	189	571	575	970	973	4.22036	1.20326	0.62045	4.22096	0.11076	0.158748407	2.110191558	2.110190988	0.795409062	2.351166989	0.15875	2.11019	2.11019	0.79541	2.35117	7	7	2000	8.16589	03	100	10	1	20	1	1	165	572	576	796	799	802	4.22036	1.35217	1.94709	0.29512	3.74323	0.5028	0.158748929	2.110190604	2.110188509	2.765992518	1.783607202	2.399399424	0.15875	2.11019	2.11019	1.76599	2.76599	1.78361																																																								
2.3994	2.3994	6	2000	4.91386	03	100	10	1	20	1	1	190	573	577	967	970	4.22036	0.62045	1.3235	4.06784	0.44267	0.158748929	2.110188498	2.110194232	1.010688075	2.131984323	0.15875	2.11019	2.11019	1.01068	2.13198	5	6	2000	5.83105	03	100	10	1	20	1	1	166	574	578	796	4.22036	1.94707	1.99211	4.22062	0.158748146	2.110190977	2.110195313	1.810892613	0.15875	2.11019	2.11019	1.81089	7	7	2000	5.95821	03	100	10	1	20	1	1	191	575	579	961	965	967	4.22036	1.3235	1.02773	0.41822	3.9889	0.12416	0.158748407	2.110191766	2.110190752	2.2278956276	1.261690816	2.404717471	0.15875	2.11019	2.11019	2.227896	1.26169	2.40407																											
1.27318	6	2000	10.60202	03	100	10	1	20	1	1	167	576	580	793	796	4.22037	1.99211	2.63767	3.83991	0.59479	0.158752708	2.110190686	2.110190748	2.370171196	2.795309497	0.15875	2.1102	2.11019	2.37017	0.279531	6	5	2000	4.81076	03	100	10	1	20	1	1	192	577	581	961	963	4.22036	1.02773	1.25177	4.22632	0.158748407	2.110192513	2.110190104	0.979762351	0.15875	2.11019	2.11019	0.97976	5	6	2000	12.0331	03	100	10	1	20	1	1	168	578	582	790	793	4.22036	2.63767	274	3.87351	0.48589	0.158752323	2.110192517	2.110190669	2.7042799	3.251437648	0.15875	2.11019	2.11019	2.70248	3.25143	6	6	2000	6.54209	03	100	10	1	20	1	1	193	579	583	960	961	4.22036	1.25177	1.68455	4.15095	0.18837	0.158748929	2.110188567	2.110191174	1.390148936	2.373193261	0.15875	2.11019	2.11019	1.39015	2.37318
6	2000	12.73854	03	100	10	1	20	1	1	169	580	584	787	790	4.22036	274	2504	3.34651	1.25591	0.158752186	2.110185038	2.110191959	2.856978157	3.328180628	0.15875	2.11019	2.11019	2.85698	3.32818	6	6	2000	5.7893	03	100	10	1	20	1	1	194	532	581	955	960	2.93161	2.5717	1.68455	2.20603	0.28622	0.158749708	0.755231779	2.110192091	2.208661751	2.598950501	0.15875	2.11019	2.11019	2.20866	2.59896	7	8	2000	8.04461	03	100	10	1	20	1	1	194	532	581	955	960	4.22036	1.02405	0.26236	3.08588	3.42172	1.24704	2.504	0.82917	1.873696985	1.802167911	0.891165643	2.110191306	3.01905724	1.87373	1.82818	0.15875	1.80217	0.89116	2.11019	3.0191																								
6	2000	3.89742	03	100	10	1	20	1	1	195	531	532	921	921	2.92367	2.78792	0.05432	2.99688	0.51791	0.158750864	1.078291465	2.584849289	0.982397938	2.596470252	0.15875	1.07829	2.58482	0.9824	2.59648	12	6	2000	5.57227	03	100	10	1	20	1	1	171	530	531	921	922	2.56854	0.19164	0.23424	0.19099	1.02345	1.50498	1.37089	2.10485	0.298	0.051484	0.38106	0.158753502	1.698710192	1.258295638	1.697360698	1.256525636	1.877449274	1.18060197	1.6176	1.78919	1.14652	1.37799																																																					
5	2000	8.18547	03	100	10	1	20	1	1	196	589	592	924	924	3.1789	0.63329	0.06907	1.09718	0.158749328	2.110188554	0.949900328	0.81620943	0.15875	2.11019	0.9499	0.43162	5	6	2000	5.33187	03	100	10	1	20	1	1	172	590	720	722	724	3.03543	0.08864	0.94534	1.42016	3.54033	1.508751444	2.110188551	1.012329573	2.6257761	1.821075	0.15875	2.11019	2.08656	1.10124	1.26578	6	2000	4.71381	03	100	10	1	20	1	1	197	587	591	924	928	4.22037	0.63329	0.088501	0.73902	4.10021	0.158748929	2.110190114	2.110191842	2.162455667	0.96465361	0.15875	2.11019	2.11019	2.16246	0.96465																																	
6	2000	7.33233	03	100	10	1	20	1	1	173	588	592	940	943	4.22036	0.98864	1.80428	1.80208	0.09469	3.69191	0.158752186	2.110190176	2.110191992	2.224131987	1.62751694	0.15875	2.11019	2.11019	2.162752	6	6	2000	5.75839	03	100	10	1	20	1	1	198	589	593	928	932	4.22037	0.88501	1.17661	0.76501	3.91004	0.158748929	2.110191423	2.110190753	2.216837314	1.227613384	0.15875	2.11019	2.11019	2.21684	1.22761																																																												
1.22761	7	2000	5.53112	03	100	10	1	20	1	1	201	202	2595	854	938	939	2.27135	0.34121	1.69595	1.87809	0.35138	3.08785	0.158747462	0.160001651	2.110192336	0.524687266	2.608673187	1.673086005	0.15875	0.16001	2.11019	2.11019	2.67461	6	7	2000	7.67876	03	100	10	1	20	1	1	174	590	594	843	846	4.22036	1.80208	1.69329	0.177	4.12023	0.158752186	2.110192128	2.674640851	1.659530257	0.15875	2.11019	2.11019	2.67461	1.65953																																																									
1.65953	8	2000	6.32495	03	100	10	1	20	1	1	199	591	593	937	4.22036	1.17661	1.12948	0.08057	3.86838	0.158748407	2.110192512	2.110191654	2.330733146	1.53324604	0.15875	2.11019	2.11019	2.33073	1.53323	9	10	2000	5.58811	03	100	10	1	20	1	1	175	592	596	846	849	4.22036	1.69329	1.02239	0.08184	1.42369	1.5288	0.158752186	2.110192475	2.6046167	1.216497407	0.15875	2.11019	2.11019	2.60467	1.216497407																																																												
1.216497407	10	2000	7.32929	03	100	10	1	20	1	1	200	593	597	937	938	4.22036	1.12948	1.69595	0.08161	3.70977	0.158748407	2.110190929	2.2208696232	1.621438389	0.15875	2.11019	2.11019	2.22087	1.621438389	0.15875	2.11019	2.11019	2.22087	1.621438389																																																																																						
1.621438389	11	2000	7.00032	03	100	10	1	20	1	1	203	228	601	987	1135	0.51798	2.22972	1.42594	0.20866	0.12546	3.28179	0.160006962	0.158752617	2.138799618	0.69586309	2.466942962	1.619544019	0.15875	2.11019	2.11019	2.466942962	1.619544019	0.15875	2.110																																																																																						

7 2000 8.62091 03 100 10 1 20 1 1 236 613 617 761 1128 1129 4.20446 1.92765 1.00347 0.63014 3.96453 0.59846 0.158750403 2.138799228 2.138800958 2.070144081 1.851363855 2.775461464 0.15875
 2.1388 2.1388 2.07014 1.85136 2.77546
 7 2000 10.66633 03 100 10 1 20 1 1 212 614 759 761 1116 1127 4.19189 1.53623 2.02363 1.75887 1.22669 2.04304 0.158750291 2.138798579 2.571126984 2.05772014 2.543563209 2.661962456 0.15875
 2.1388 2.57113 2.05772 2.54356 2.66196
 11 2000 631403 03 100 10 1 20 1 1 237 378 389 472 615 761 762 763 764 1128 0.75074 0.16144 0.16126 1.18352 1.00347 1.92375 0.85452 1.92675 0.80095 1.05515 0.158752227 1.895374001 1.895241962
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 6 2000 821383 03 100 10 1 20 1 1 239 619 623 797 800 4.27758 1.99455 1.75217 0.12151 4.20758 0.158750698 2.138801744 2.138798084 2.667192256 1.761 2.0886 0.15875 2.1388 2.1388 2.66719 1.76121
 5 2000 531163 03 100 10 1 20 1 1 215 620 624 824 427758 1.26164 1.22156 4.27779 0.158751101 2.138798065 2.138799615 1.08293539 0.15875 2.1388 2.1388 1.08294
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 6 2000 5.54672 03 100 10 1 20 1 1 216 622 625 821 824 427758 1.22156 1.31375 4.27018 0.001788 0.158751505 2.138800154 2.138799469 1.116738659 2.388261275 0.15875 2.1388 2.1388 1.11674 2.38826
 7 2000 8.54578 03 100 10 1 20 1 1 241 623 627 791 794 797 427757 1.74852 2.03619 0.01186 4.11251 0.26485 0.158751101 2.13879671 2.138803125 2.845942218 1.842543236 2.665024394 0.15875 2.1388
 2.1388 2.8459 1.84254 2.66502
 7 2000 6.89694 03 100 10 1 20 1 1 217 624 628 815 818 821 427758 1.31375 1.22256 0.30458 3.93259 0.4918 0.158751101 2.1388003 2.138799286 2.387652533 1.46650013 2.430406882 0.15875 2.1388
 2.1388 2.38765 1.4665 2.43041
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 5 2000 4.94533 03 100 10 1 20 1 1 218 626 630 815 427758 1.22256 1.0894 4.27967 0.158751101 2.138800484 2.138798921 0.996868929 0.15875 2.1388 2.1388 0.99687
 5 2000 8.2941 03 100 10 1 20 1 1 243 627 631 788 427757 1.82078 2.05686 4.2841 0.158751101 2.138796872 2.138793101 1.777513327 0.15875 2.1388 2.1388 1.77751
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7 2000 19.69948 0.3 100 10 1 20 1 1 526 528 785 787 788 789 2.00195 2.39543 3.88273 4.15126 0.05291 4.18901 2.41085 5758 2.37548 4053 2.11459 5485 2.09654 1.348 3.17762 927 2.46046 4695 2.41086
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8 2000 23.10594 0.3 100 10 1 20 1 1 528 530 582 584 786 789 790 2.33227 3.06943 3.34651 0.82917 4.15126 0.48661 3.96189 2.38371 3054 2.3710 2.635 2.85698 3567 3.01909 731 2.09654 2.17 3.28359 6295
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8 2000 17.73136 0.3 100 10 1 20 1 1 627 629 631 785 786 789 791 0.24403 4.2841 0.61774 2.62398 0.52291 4.51846 3.73995 2.70464 5451 1.77751 0074 2.85532 607 2.7882 00971 3.17768 7855 1.96079 964
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7 2000 20.21608 0.3 100 10 1 20 1 1 786 787 788 790 791 792 4.18901 0.48661 4.51846 4.18292 0.65178 3.58397 2.46045 9487 3.28359 2448 1.96067 9523 2.31108 4322 2.81280 3935 2.27898 9126 2.46046
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 6 2000 12.43121 0.3 100 10 1 20 1 1 626 815 817 820 821 3.93259 2.80771 4.29395 0.95343 2.16482 1.466501222 2.128034218 1.373495249 2.400836358 2.278990757 1.4665 2.12803 1.3735 2.40084 2.27899
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7	2000 16.27197 03 100 10 1 20 1 1 639 641 841 842 845 847 053827 4.22492 3.31045 0.10697 4.59748 3.26545 2.567348604 1.530901265 2.2232647006 2.982532415 201806203 23.59916993 2.56735 1.5309 223265 2.98253 201801 23.5991
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8	2000 16.68044 03 100 10 1 20 1 1 641 643 645 844 845 848 850 0.11655 4.30012 0.29239 3.26545 0.42328 3.75542 3.93882 2.619229432 1.309043967 2.390771252 2.359910662 3.135538166 2.624920623 1.989550351 2.61922 1.30905 2.39077 2.35992 3.13554 2.62492 1.98955
6	2000 21.86299 03 100 10 1 20 1 1 845 847 849 850 851 4.88989 3.75542 4.49136 0.34573 5.19989 2.163466962 2.624920478 2.509230573 3.283592226 2093136481 2.16347 2.62492 2.50923 3.2836 209314
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7	2000 19.63932 03 100 10 1 20 1 1 596 848 849 850 852 1105 0.79404 5.19989 0.99176 2.29487 3.74124 4.56427 3.382043692 2093140363 3.369307578 2.744397307 2.397866094 1.55521854 3.38205 209314 3.3693 2.7444 2.39787 1.55522
6	2000 15.9911 03 100 10 1 20 1 1 596 598 851 854 854 1105 3.23458 3.13463 3.74124 0.84504 1.75687 2.13328227 1.194507998 2.397865787 1.511830885 2.727026183 2.13324 1.19451 2.39787 1.51184 2.72703
5	2000 4.50309 03 100 10 1 20 1 1 252 645 646 850 0.33505 1.53422 2.12439 1.93069 0.67150163 0.666021598 0.716079906 1.571933917 0.6715 0.66602 0.71608 1.57193
6	2000 4.7444 03 100 10 1 20 1 1 202 597 598 852 939 0.32836 1.87809 1.7001 0.84504 1.067 0.48824776 0.524681195 0.150509537 1.511843388 1.896622508 0.48825 0.52469 0.5051 1.51183 1.89661 7
7	2000 3.12326 03 100 10 1 20 1 1 52 399 453 454 781 782 0.48096 0.33498 1.41336 1.0281 1.65559 0.6241 0.511239732 0.731593996 0.411543543 0.63749802 0.727572868 0.771961881 0.51124 0.7316 0.41154 0.63743 0.72758 0.77196
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8	2000 10.65579 03 100 10 1 20 1 1 328 717 718 867 870 907 919 0.33369 1.60251 1.75939 1.29164 1.94068 3.58374 2.36392 0.809049339 0.813902789 0.837808176 1.723345947 2.104455101 2009747355 2009749063 0.80905 0.8139 0.83781 1.72334 2.10446 200975 200975
8	2000 13.22132 03 100 10 1 20 1 1 711 713 757 831 832 859 861 2.79072 0.34067 0.19576 3.61676 0.21705 3.55984 3.64144 1.667717492 2.451587596 201836156 1.473634679 2.691951175 2.138060034 1.931379589 1.66771 2.45159 201834 1.47364 2.69195 2.13806 1.93138
7	2000 16.50126 03 100 10 1 20 1 1 832 833 858 860 861 862 4.49915 0.35716 3.55984 3.53935 0.19879 3.96253 1.655847842 2.876288173 2.138061992 2.300780192 2.876283051 2069160788 1.65585 2.87628 2.13806 2.30078 2.87628 206916
7	2000 16.93614 03 100 10 1 20 1 1 636 638 833 859 862 863 0.78977 3.67494 2.80505 3.53935 1.45315 3.51956 2.520536459 1.651285919 2.352855637 2.300779163 2.799257967 1.98549256 2.52054 1.65129 2.35286 2.30078 2.79925 1.98955
7	2000 14.28619 03 100 10 1 20 1 1 713 715 858 859 862 864 3.92826 0.10149 3.64144 0.19879 3.73044 3.41708 1.499965737 2.484775308 1.931379815 2.876283673 2.13805993 2.003830178 1.49997 2.48477 1.93138 2.87628 2.13806 200383
7	2000 19.39682 03 100 10 1 20 1 1 859 860 861 863 864 865 3.96253 1.45315 3.73044 2.75845 0.82522 4.22755 2.069160823 2.799252785 2.138058284 2.696361581 2.77881275 2086315817 206916 2.79926 2.13806 2.69636 2.77881 208632
7	2000 17.32487 03 100 10 1 20 1 1 638 640 860 862 865 866 0.09562 3.75428 3.51956 2.75845 1.3625 3.58554 2.365949959 1.616804345 1.989547142 2.696361581 3.047154558 2.154663096 2.36595 1.6168 1.98955 2.69636 3.04716 2.15466
6	2000 14.64577 03 100 10 1 20 1 1 715 861 862 865 867 4.06277 3.41708 0.82522 3.34095 3.39196 1.407962362 2.003827881 2.778812261 2.278989356 2.009747453 1.40796 2.00383 2.77881 2.27899 200975
7	2000 20.26054 03 100 10 1 20 1 1 862 863 864 866 867 868 4.22755 1.3625 3.34095 2.75191 1.38672 4.16637 2.086319156 3.047156883 2.278991544 2.702521734 2.782230535 2.073753211 208632 3.04715 2.27899 2.70252 2.78223 207375
7	2000 17.59237 03 100 10 1 20 1 1 640 642 863 865 868 869 0.88712 3.63979 3.58554 2.75191 1.5177 3.67503 2.497146741 1.793744177 2.154663715 2.702519436 2.745264793 1.935066492 2.49715 1.79375 2.15466 2.70252 2.74526 1.93507
8	2000 15.82091 03 100 10 1 20 1 1 715 717 857 864 865 868 870 0.10631 3.08981 1.29164 3.39196 1.38672 2.90207 3.02005 2.425721206 1.389590385 1.723344421 2.009749982 2.782230542 2.623112192 2.176603841 2.45272 1.38959 1.72335 200975 2.78223 2.62311 2.45272 2.17661
7	2000 23.56578 03 100 10 1 20 1 1 865 866 867 869 870 871 4.16637 1.5177 2.90207 3.4105 3.26681 3.20591 2.073748408 2.745261253 2.623110619 2.284196663 2.976950865 2.868841295 2.07375 2.74526 2.62311 2.28242 2.97695 2.86884
6	2000 18.25237 03 100 10 1 20 1 1 642 644 866 868 871 0.89797 4.35306 3.67503 3.4105 4.54242 2.555501601 2.113582416 1.935066991 2.284197973 2.225185775 2.5555 2.11358 1.93507 2.2842 2.22518
6	2000 24.207693 03 100 10 1 20 1 1 857 867 868 871 907 1.94068 3.02005 3.26681 2.87752 3.51509 2.104457938 2.176607608 2.976953199 3.875651198 1.82121092 2.10446 2.1766 2.97695 3.87565 1.82121 3.87565 2.17661
6	2000 28.13751 03 100 10 1 20 1 1 644 646 868 869 870 0.10481 3.36536 3.20591 4.54242 2.87752 3.379434129 3.183458329 2.86883798 2.225184003 3.875650464 3.37945 3.18346 2.86884 2.22519 3.87565
6	2000 23.82816 03 100 10 1 20 1 1 503 505 873 909 910 4.42655 0.92908 3.48106 4.55683 1.14667 1.462215442 2.49121304 2.347800938 3.32028654 3.288655058 1.46222 2.49121 2.3478 3.32029 3.28866
6	2000 16.49378 03 100 10 1 20 1 1 505 507 872 874 910 3.7605 0.099382 3.48106 3.24709 4.54884 1.755374921 2.501418645 2.347800889 207832946 1.97396024 1.75538 2.50142 2.3478 207833 1.97396
7	2000 17.93438 03 100 10 1 20 1 1 507 509 873 875 910 911 3.59276 0.83016 3.24709 3.16084 1.9674 3.34932 1.8988068 2.644086341 2.078329614 2.164565963 2.702519331 2.37196655 1.89881 2.64408 2.07833 2.16457 2.70252 2.37197
7	2000 17.44938 03 100 10 1 20 1 1 509 511 874 876 911 912 3.70035 0.82694 3.16084 3.36171 2.50643 2.29428 1.934036237 2.635707849 2.16456615 2.096540505 2.397868825 2.46817677 1.93403 2.6357 2.09654 2.39787 2.46818
7	2000 16.38509 03 100 10 1 20 1 1 511 513 875 877 912 913 3.68336 0.57798 3.36171 3.76866 2.53784 1.63388 1.947343091 2.66600468 2.09653925 1.797575104 2.424474364 2.497843598 1.94734 2.09654 1.79757 2.42447 2.49784
7	2000 15.03651 03 100 10 1 20 1 1 513 712 756 758 876 913 2.45218 0.41402 1.77164 3.32045 3.76866 3.29972 2.101290503 2.236452514 2.192224525 1.950983739 1.797574745 2.078329678 2.10128 2.23646 2.19222 1.95098 1.79758 2.07833
8	2000 17.80254 03 100 10 1 20 1 1 512 514 752 754 879 883 903 3.64437 1.86327 0.078432 3.53093 2.4829 2.76665 1.01019 2.079617443 2.147281927 2.648271528 1.751552559 2.6012818 2.291468081 3.139328756 2.07962 2.14728 2.64827 1.75155 2.60128 2.29147 3.13933
7	2000 20.082642 03 100 10 1 20 1 1 878 880 883 884 903 904 2.4829 1.22846 4.33582 2.74804 2.89172 3.8543 2.6012818 3.175448343 1.788297721 2.84722273 2.529036353 2.179878995 2.60128 3.17545 1.7883 2.84723 2.52904 2.17988
7	2000 25.98542 03 100 10 1 20 1 1 879 881 884 885 899 904 1.22846 4.03379 4.39916 2.00244 4.37513 3.39869 3.175446398 2.992873746 2.838866798 3.731349121 1.906615315 2.267494186 3.17545 2.99287 3.73135 1.90661 2.26749
7	2000 26.48378 03 100 10 1 20 1 1 880 882 885 898 899 906 4.03379 4.88446 0.8515 5.41794 0.56954 4.79726 2.992870209 2.444966338 3.582566261 2.471063824 3.228872974 2.227321575 2.99287 2.44497 3.58257 2.47106 3.22887 2.22732
6	2000 27.78749 03 100 10 1 20 1 1 881 886 887 898 906 4.88446 0.48949 3.32718 1.1566 3.92869 2.44496642 3.94852413 4.082837004 3.962944397 2.73138063 2.44497 3.94853 4.08284 3.96295 2.73138
6	2000 15.7214 03 100 10 1 20 1 1 750 752 878 879 884 1.90597 4.53578 2.67665 4.33582 2.22249 2.642048098 1.398670037 2.291466061 1.788297946 2.778810887 2.64204 1.39867 2.29147 1.7883 2.77881 2.078329678 2.237461 2.84722 2.83887 2.77881 2.28538911 3.17474

9 2000 32.76518 0.3 100 10 1 20 1 1 748 830 880 881 884 886 897 906 2.02431 2.00271 2.00244 0.8515 4.51807 2.4024 2.70524 5.33498 3.084956271 3.086666718 3.731352492 3.582571577 2.85389379
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 8 2000 23.55791 0.3 100 10 1 20 1 1 882 885 887 888 889 897 906 4.04894 2.4024 3.83488 4.34983 2.16647 0.68123 5.79661 3.948534523 3.327439957 2.352856858 1.449249863 2.729637081 4.019496419
 2.278989591 3.94852 3.32744 2.35286 1.44925 2.72964 4.0195 2.27899
 7 2000 23.48171 0.3 100 10 1 20 1 1 455 457 829 882 886 888 3.03565 0.8698 2.15462 3.32718 3.83488 2.46946 1.421857118 2.403607591 1.70672073 4.08283845 2.352857038 2.07832882 1.42186 2.40361
 1.70672 4.08284 2.35286 207833
 5 2000 12.76183 0.3 100 10 1 20 1 1 457 886 887 889 3.78127 4.34983 2.46946 3.9464 1.718832859 1.449252514 2.078328927 1.922745738 1.71883 1.44925 2.07833 1.92275
 7 2000 19.45663 0.3 100 10 1 20 1 1 457 459 886 888 890 897 0.04729 2.42823 2.16647 3.9464 2.76835 4.34338 2.651044462 1.71109441 2.729642183 1.92274724 2.463359593 2.564485347 2.65103
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 8 2000 17.24018 0.3 100 10 1 20 1 1 459 461 463 889 891 896 897 0.07703 4.34055 0.60009 2.76835 3.38163 1.20215 3.73943 2.798132862 1.558407943 2.516113225 2.4633597 2.10897008 2.887003591
 2.291463666 2.79814 1.55841 2.51611 2.46336 2.10897 2.887 2.29147
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 6 2000 6.40069 0.3 100 10 1 20 1 1 516 706 708 753 893 1.20781 1.70128 3.70229 4.47882 0.31593 1.854484017 2.06906118 0.7192449 0.806608206 2.424472148 1.85449 2.06906 0.71925 0.80661 2.42447
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 1.1497 1.18589 2.44045 2.42447 2.62493
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 5 2000 27.24599 0.3 100 10 1 20 1 1 881 882 889 905 5.41794 1.1566 4.29514 4.38868 2.471060624 3.962947003 2.036758297 2.352853738 2.47106 3.96294 2.03676 2.35286
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 5 2000 12.41454 0.3 100 10 1 20 1 1 504 506 901 905 3.78479 0.21621 2.84678 3.08565 1.316118213 2.484421289 2.027404748 2.311086063 1.31612 2.48442 2.0274 2.31108
 6 2000 16.83605 0.3 100 10 1 20 1 1 506 889 900 902 905 4.04986 1.36562 2.84678 3.84534 3.92151 1.59711234 3.210424824 2.027403925 2.359914048 2.013295341 1.59711 3.21042 2.0274 2.35991 2.01329
 8 2000 16.25993 0.3 100 10 1 20 1 1 506 508 510 899 901 903 904 0.07116 4.26237 0.08737 1.13504 3.84534 2.74744 3.7186 2.688867677 1.467407952 2.466480267 3.207465214 2.359913607 2.009748886
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 7 2000 16.02336 0.3 100 10 1 20 1 1 510 512 878 879 902 904 4.1929 1.9627 1.01019 2.89172 2.74744 2.60108 1.320008628 2.484107484 3.1393281 2.52903739 2.009748942 2.164566629 1.32 2.48411
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 6 2000 18.32986 0.3 100 10 1 20 1 1 879 880 899 902 903 3.8543 3.39369 3.07059 3.7186 2.60108 2.17987938 3.2267490012 2.380961539 2.049551671 2.164567428 2.17988 2.226749 2.38096 2.04955 2.16457
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 4 2000 37.54318 0.3 100 10 1 20 1 1 909 914 922 4.66829 2.10375 4.96984 3.173951181 3.17105492 2.623110871 3.17395 3.17172 2.62311
 5 2000 34.83517 0.3 100 10 1 20 1 1 872 908 910 914 4.55683 4.68289 3.03096 4.22279 3.320294742 3.173951568 2.908322808 2.420548203 3.33209 3.17395 2.90832 2.42055
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 6 2000 12.24366 0.3 100 10 1 20 1 1 444 728 926 930 931 3.0185 4.33803 1.39504 2.58871 2.48794 1.688603947 1.058260133 2.551479358 2.291468509 2.138059061 1.68861 1.05825 2.55148 2.29147
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7 2000 18.06785 03 100 10 1 20 1 1 925 926 928 930 932 933 274543 281325 275221 242444 244157 271557 2009745791 1906616707 2206961969 2210190253 2702525259 26599904 200975
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 6 2000 18.64656 03 100 10 1 20 1 1 926 927 929 931 933 3.27749 258871 242444 401506 4542 18561014 2.291466495 2210184518 2368955991 2.291464489 18561 229147 221019 236896 229147
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 7 2000 18.60407 03 100 10 1 20 1 1 932 933 935 937 944 945 1.28434 5.37112 1.62287 3.81078 4.32027 0.80835 2.909140386 1.728850161 3.239891052 1.989554783 2.003827542 3.326726198 2.90913
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 7 2000 13.69562 03 100 10 1 20 1 1 593 595 932 936 938 944 3.86838 0.88161 2.70583 3.81078 2.95995 0.29055 1.353319835 2.28069546 2.244318775 1.989549017 1.94119822 2.564490235 1.35332
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 6 2000 13.12701 03 100 10 1 20 1 1 595 597 937 939 944 3.70977 0.35138 2.95995 3.17269 4.31376 1.621434971 2.608670417 1.94119586 2.164572297 1.555218186 1.62144 2.60867 1.94119 2.16457
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 5 2000 0.03549 0.99 709.1469948 71.4095187 1 20 1 1 1363 1365 299 321 0.00889 0.00889 1.99672 1.99672 1.996716105 1.996716105 4.44E-03 4.44E-03 1.99672 1.99672 0.00444 0.00444
 5 2000 0.002184 0.99 269.8980794 26.292907641 1 20 1 1 1364 1366 300 322 0.00547 0.00547 1.99672 1.99672 1.996716105 1.996716105 2.73E-03 2.73E-03 1.99672 1.99672 0.00273 0.00273
 5 2000 0.006973 0.99 2741.025292 274.3890049 1 20 1 1 1365 1367 301 323 0.01746 0.01746 1.99672 1.99672 1.996716105 1.996716105 8.73E-03 8.73E-03 1.99672 1.99672 0.00873 0.00873
 5 2000 0.006 0.99 2038.047486 202.745366 1 20 1 1 1366 1368 302 324 0.01502 0.01502 1.99672 1.99672 1.996716105 1.996716105 7.51E-03 7.51E-03 1.99672 1.99672 0.00751 0.00751
 5 2000 0.02184 0.99 269.7594321 264.8747455 1 20 1 1 1367 1369 303 325 0.00547 0.00547 1.99672 1.99672 1.996716105 1.996716105 2.73E-03 2.73E-03 1.99672 1.99672 0.00273 0.00273
 5 2000 0.005384 0.99 164.1673724 163.1481773 1 20 1 1 1368 1370 304 326 0.01348 0.01348 1.99672 1.99672 1.996716105 1.996716105 6.74E-03 6.74E-03 1.99672 1.99672 0.00674 0.00674
 5 2000 0.002054 0.99 238.9369067 238.1181348 1 20 1 1 1369 46 305 327 0.00514 0.00514 1.99672 1.99672 1.996716105 1.996716105 2.36E-03 2.36E-03 1.99672 1.99672 0.00257 0.00257
 5 2000 0.00747 0.99 29.4403956 29.37843423 1 20 1 1 1372 329 330 340 0.00181 0.00181 206642 206642 2066417074 2066417074 9.04E-04 9.04E-04 206642 206642 0.0009 0.0009
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 5 2000 0.002109 0.99 233.9659404 23.35501103 1 20 1 1 1377 1379 337 347 0.0051 0.0051 206642 206642 2066417074 2066417074 2.55E-03 2.55E-03 206642 206642 0.00255 0.00255
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 5 2000 0.00409 0.99 839.8809272 83.93375105 1 20 1 1 1381 351 352 356 0.00966 0.00966 2.11703 21.1703457 21.1703457 4.83E-03 4.83E-03 206642 206642 0.00483 0.00483
 5 2000 0.001749 0.99 1532.106927 1542.616988 1 20 1 1 1381 1383 353 357 0.00413 0.00413 2.11703 21.1703457 21.1703457 2.07E-03 207E-03 21.1703 21.1703 0.00207 0.00207
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 5 2000 0.004989 0.99 1248.8793125.5397705 1 20 1 1 1383 10 355 359 0.01178 0.01178 2.11703 21.1703 2.11703457 2.11703457 5.89E-03 5.89E-03 2.11703 2.11703 0.00589 0.00589
 5 2000 0.006262 0.99 2049.894935 2062.647371 1 20 1 1 1386 361 362 368 0.01511 0.01511 207233 207233 2072329718 2072329718 7.55E-03 7.55E-03 207233 207233 0.00755 0.00755
 5 2000 0.007696 0.99 3104.854038 31.7347623 1 20 1 1 1385 1387 363 369 0.01857 0.01857 207233 207233 2072329718 2072329718 9.28E-03 9.28E-03 207233 207233 0.00928 0.00928
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 5 2000 0.003199 0.99 606.1262863 605.1287804 1 20 1 1 1392 375 376 387 0.00821 0.00821 1.94834 1.94834 1.948342957 1.948342957 4.11E-03 4.11E-03 1.94834 1.94834 0.00411 0.00411
 5 2000 0.007489 0.99 332.0960888 331.4606883 1 20 1 1 1393 377 388 0.01922 0.01922 1.94834 1.94834 1.948342957 1.948342957 9.61E-03 9.61E-03 1.94834 1.94834 0.00961 0.00961
 5 2000 0.000897 0.99 47.96031921 4.75754

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5 2000 0.00229 0.99 3.124060694 0.309774447 1 20 1 1 1403 399 400 402 0.00059 0.00059 1.94553 1.94553 1.945528153 1.945528153 2.94E-04 2.94E-04 1.94553 1.94553 0.00029 0.00029
5 2000 0.02692 0.99 429.5995221 4293146976 1 20 1 1 1402 6 401 403 0.00692 0.00059 1.94553 1.94553 1.945528153 1.945528153 3.46E-03 3.46E-03 1.94553 1.94553 0.00346 0.00346
END_CV

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Rock and Fluid properties section

SWI 0.12

SGI 0.00

SWMAX 0.88

SGMAX 1.00

PB 4014.7

PREF 4790

ZREF 2000

CROCK 3.00E-06

DENOIL 4.6244

DENWAT 63.238

DENGAS 0.0647

KROW 3

0 1 0 0

0.999 1 0 0

1 0 1 0

NPVT1

PVTDATA 10

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14.7 1.062 1.04 1 0.9358295 0.008 1.04473539 0.31 0
264.7 1.15 0.975 905 0.0679021 0.0096 1.043962905 0.31 0
514.7 1.207 0.91 180 0.0352285 0.0112 1.04319042 0.31 0
1014.7 1.295 0.83 371 0.0179511 0.014 1.04164545 0.31 0
2014.7 1.435 0.695 636 0.0090626 0.0189 1.03855551 0.31 0
2514.7 1.5 0.641 775 0.0072658 0.0208 1.03701054 0.31 0
3014.7 1.565 0.594 930 0.0060642 0.0228 1.03546557 0.31 0
4014.7 1.695 0.51 1270 0.00455376 0.0268 1.03237563 0.31 0
5014.7 1.827 0.449 1600 0.003644 0.0329 1.02928569 0.31 0
9014.7 2.353 0.203 2984 0.00216739 0.047 1.01692593 0.31 0

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COREF 1.47E-05

CWREF 3.00E-06

CGREF 3.00E-04

CROCK 3.0E-6

Numerical Controls

DELT02

TMAX730

DTMIN02

DTMAX05

RESIDERR 1E-4

EPSSOLVER 1E-5

ITISOLVER 60

ITIMAX 20

NCUT 5

DPMAX50

DSWMAX0.10

DSGMAX0.10

DSOMAX0.10

DPPERT -5e-5

DSWPERT 5E-6

DSGPERT 5E-6

Schedule

TIME1

TIME2

TIME10

TIME15

TIME20

TIME90

TIME365

TIME500

TIME900
TIME1095
TIME1460
TIME1825
TIME2190
TIME2555
TIME2920
TIME3285
TIME3650

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