

A Quasi-Steady Model of
Blade/Vortex Interaction

by

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ABSTRACT

A steady state transonic airfoil analysis code has been modified to include the presence of a vortex near the airfoil. The objective was to provide quasi-steady analysis of blade/vortex interaction for studying or predicting impulsive rotor noise. Results of BVI in low speed flows compare well with the results of incompressible methods in both lift coefficients and pressure distributions. In high speed flows, the code breaks down in the fine grid near the center of the vortex because the program does not model a compressible vortex. The code must be altered to correctly model the flow near the center of the vortex before it will be useful in the study of impulsive rotor noise.

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NOMENCLATURE

a	local speed of sound or circle radius (App. D)
c	chord
c_l	lift coefficient
c_p	pressure coefficient
F	complex potential function
k	constant
l	panel length
M	Mach number
q	speed
R	complex variable
r	radius or distance
s	surface coordinate
T	vortex position angle
u	horizontal velocity
V	velocity
v	vertical velocity
W	complex variable
w	relaxation coefficient
x	horizontal flowfield coordinate
y	vertical flowfield coordinate
Z	complex variable
α	angle of attack
β	panel orientation angle
Γ	vortex circulation
γ	circulation density
ϵ	damping coefficient
η	vertical coordinate in computational grid
θ	angle measured from branch cut
λ	source strength
ξ	horizontal coordinate in computational grid
ϕ	potential

Superscripts:

*	old value or critical (Fig. 3)
-	complex conjugate
'	modified

Subscripts:

c	circulatory
i	counter
j	counter
L	lower
n	normal
o	zero-lift
s	streamwise
U	upper
v	vortex
∞	freestream

INTRODUCTION

To produce lift, helicopter blades must have a high pressure region beneath the blade and a region of lower pressure above the blade. This pressure difference causes air to be sucked around the tip of the blade, forming a vortex. The vortices from the blade tips of a forward-moving helicopter form an approximate epicycloid pattern, due to the combination of forward speed and blade rotation, when viewed from above¹. The vortices convect downward from the disc plane and distort from the epicycloid pattern under the influence of self-induced velocities.

During some flight regimes, a particular blade may pass near the vortex trailing from a previous blade or its own vortex from a previous passage. Such an occurrence of blade/vortex interaction, BVI, is governed by the advance ratio of the rotor and the helicopter's rate of descent¹. This interaction is negligible if the vortex center is more than 1.5 blade chords from the rotor plane². BVI typically occurs in low-power descending flight and in maneuvers³.

Surendraiah² measured tangential velocities in a straight line vortex and found magnitudes as high as 47% of the freestream velocity. The tangential velocity in the core increases outward exponentially from the center and then decreases inversely proportional to the distance from the vortex center.

*Style from AIAA Journal.

The vortex passage causes strong, unsteady velocity disturbances which rapidly alter local blade aerodynamics¹. The disturbances are generally irregular. The induced velocities of the vortex may generate regions of transonic flow on the blade. Transonic flow is characterized by shock waves, strong pressure gradients that decelerate the flow from supersonic to subsonic, that cause acoustic problems due to their motion relative to an observer.

The aerodynamic phenomenon is strongly dependent on the orientation and proximity of the vortex to the blade³. The aerodynamic loads fluctuate rapidly, building up faster than they decay. The magnitude of the change in lift coefficient, a nondimensional expression of the lift force, is greatest when the vortex axis is parallel to the blade chord. The rate of change of the lift coefficient is a maximum with the vortex axis about 70 degrees from the chord line of the rotor blade. The rate of change of the lift coefficient is about 75% of its maximum value when the vortex axis is parallel to the blade span². The rate of change of the lift coefficient increases as the blade passes closer to the center of the vortex. After BVI, an azimuth travel of about 50 degrees is required for the flow to return to a normal condition.

BVI is known to be a cause of impulsive rotor noise, or blade slap. This noise is characterized by a distinctive low-frequency nature, high intensity, and crispness and is annoying and undesirable for both military and civilian helicopters¹. The total sound energy per unit time varies with the square of the time rate of change of the blade loading², and the intensity can approach 90 dB¹. The sharpness of the disturbance increases the annoyance⁴. The acoustic radiation is usually a maximum ahead of the

rotor at approximately 30 degrees below the rotor plane¹.

The impulsive rotor noise is similar to a sonic boom. The mechanism responsible has not yet been determined. George⁵ suggests that the increased flow velocities during BVI cause shocks to form on the blade. As the vortex passes on by, the shocks move forward on the blade, eventually propagating off the front end of the blade. Schlieren techniques on small, Mach number scaled rotors have shown discrete bow shock waves during BVI¹. Isom⁶ suggests that the disturbances caused by the unsteady loading of the blade are so large that as they propagate, they steepen and break, forming shocks.

To investigate the aerodynamic cause of blade slap, an existing transonic airfoil analysis code, TRANDES⁷, has been modified to determine the flow field of blade/vortex interaction. TRANDES incorporates a finite difference solution to the full perturbation potential equation for irrotational, inviscid transonic flow. Second-order central differences are used in regions of subsonic flow and first-order backwards (upwind) differences are used in regions of supersonic flow to reflect the hyperbolic character of the equation for supersonic flow. A rotated finite difference scheme introduced by South and Jameson⁸ is used to simulate a local rotation to coordinates along and normal to the local velocity vector. This scheme not only has the correct zone of dependence for the upwind differencing used in regions of supersonic flow, but it also does not require alignment of the computational grid with the flow. In TRANDES, a coordinate transformation maps an infinite flowfield onto a finite computational grid described by Cartesian coordinates⁹.

TRANVOR, the modified version of TRANDES, has two primary

limitations. First, as in TRANDES, the flow is two-dimensional, so that the axis of the vortex is assumed to be parallel with the blade span. Secondly, the BVI is analyzed with a quasi-steady approach. A series of steady-state solutions for several positions of the vortex along a path are produced. This method may show the build-up of a shock, but it will probably not show the decay.

LTRAN2¹⁰ is an unsteady code that will solve the unsteady aerodynamic problem of BVI. It is a small disturbance code with a correction for flow at the leading edge of the airfoil. The primary drawback of LTRAN2 is the computer time required for a run.

The objective of the development of TRANVOR is to provide a quick, inexpensive method to approximately model BVI and determine if impulsive rotor noise is likely to result for any blade/vortex orientation. If the existence of a BVI problem is determined, the quasi-steady results of TRANVOR might suffice for further analysis, or an appeal to LTRAN2 might be necessary. In any case, the existence of the problem can be signalled cheaply by TRANVOR.

METHOD

The finite difference scheme and the formulation of the boundary conditions in TRANDES were examined to determine the alterations necessary to represent a vortex in the flow field.

The full potential equation in TRANDES is valid for the flow about a vortex, so the form of the finite difference scheme was not altered. The finite difference formulation incorporates a mixture of old and new values for the perturbation potential, providing a tridiagonal system of equations that can be implicitly solved for one column of new potential values at a time as the computational grid is traversed. Additional terms ensure stability and hasten convergence of the system of equations. The various forms of the finite difference equations are given in Appendix A.

The presence of the vortex in the flowfield does not alter the surface boundary condition of the airfoil; the flow must still be tangent to the airfoil surface.

The infinity boundary condition of the vortex is treated identically to the infinity boundary condition of the airfoil. The potential at infinity due to the circulation of the vortex is superimposed onto the potential at infinity due to the circulation of the airfoil. This is depicted for a general case in Figure 1.

The perturbation potential for a vortex is:

$$\phi = \frac{-\Gamma \theta}{2\pi} \quad (1)$$

For the perturbation potential of the flow to satisfy this equation, a branch cut in the potential field is necessary. A difference of potential equal to the strength of the vortex must exist across the branch cut which extends from the vortex center to infinity. The branch cut extends upward from the vortex center if the vortex is above the chordline of the airfoil and downward if the vortex is below the chordline. An example of this cut can be seen in Figure 1. To establish a vortex in the flowfield, this discontinuity of the potential across the cut must be established and maintained in the computational grid. To accomplish this, programming segments were added to TRANDES performing the following tasks:

- (1) Input the position and strength of the vortex.
- (2) Locate the center of the vortex in the computational grid.
- (3) At the infinity boundary, add the potential specified by the boundary conditions of the vortex to the potentials resulting from the airfoil's circulation.
- (4) Alter the horizontal difference in potential across the cut so that the velocities and other derivatives of the potential are continuous.
- (5) Correct the interpolated values of the potential near the cut when the grid mesh size is halved.

Changes in the program are referenced to the card numbers that occupy columns 73-80 of the original TRANDES code⁷. Line numbers refer to the listing of TRANVOR in Appendix E.

Task 1:

The strength and position of the vortex are entered as nondimensional values through the namelist for real variables. The vortex strength is divided by the freestream velocity and the chord length to

nondimensionalize it. A positive vortex strength (VORCIR) will induce clockwise rotation in the flowfield. The position of the vortex is described by a horizontal (XV) and a vertical (YV) distance from the midchord of the airfoil, as shown in Figure 2a. These distances are normalized by the airfoil chord since TRANDES assumes a unit chord. The addition of the variables VORCIR, XV, and YV to the namelist FINP follows card 31. These three variables are placed in a new common block, titled VORTEX, that contains only variables associated with the vortex. This addition follows card 28. The default value of the vortex strength is zero, specified following card 88.

Task 2:

The vortex position in the computational grid is determined in lines 144-154 following card 110. Line 144 checks for the existence of a vortex. Lines 145-148 and 149-152 determine the horizontal and vertical position of the vortex in the computational grid. IVOR is the number of horizontal grid lines below the vortex and JVOR is the number of vertical grid lines to the left of the vortex. The value of the variable IVLOC is determined in lines 153-154. Values of positive or negative one indicate the vortex is located above or below the chordline, respectively. The default vortex strength of zero indicates no vortex is present in the flowfield. Lines 180-181 print the vortex location in the computational grid and its strength.

Task 3:

The boundary conditions at infinity are altered for the circulation of the vortex in the subroutine VORBCI, placed in the code following the original TRANDES subroutines. This subroutine is called in line 299 following card 208. The increment of potential is calculated just like the original values for the airfoil alone, except the circulation is the vortex strength and the potential discontinuity does not extend horizontally from the trailing edge to infinity. The angle in the vortex potential equation is referenced to a line extending from the center of the vortex to infinity.

The potential at the corners of the computational grid are calculated in lines 3174-3177 and lines 3179-3182 for vortices located below and above the airfoil chordline, respectively. The values of the corner potentials are calculated to fall between the potentials on the adjacent sides, though the specific values are not critical to the numerical scheme.

TRANVOR handles angles of attack by rotating the freestream relative to the x-axis, keeping the airfoil chord on the x-axis. the freestream is rotated through the boundary condition at infinity. Since the vortex is located with respect to the airfoil chordline, the angle of attack affects the infinity boundary condition of the vortex in the same manner it affects the infinity boundary conditions of the airfoil. Therefore, the value of the potential at infinity for the vortex is given by equation (2).

$$\phi = \frac{-\Gamma_v}{2\pi} \text{Tan}^{-1}[\beta \tan(\theta - \alpha)] \quad (2)$$

Lines 3217-3223 and lines 3225-3231 adjust the infinity boundary potentials for vortices below or above the airfoil chordline, respectively, when the angle of attack is zero. In this case, it is easy to see that the boundary at infinity is treated like four sides of a rectangle. At infinity, four positions relative to the airfoil are considered: behind, above, in front of, and below the airfoil. Each of these positions is represented by the corresponding side of a rectangle. The values of the potential at infinity may be assigned by substituting the angle of the direction perpendicular to each side into equation (2). For example, all points on the top side of the rectangle are considered to be an infinite distance above the airfoil and their potential is calculated using 90 degrees as the directional angle. Thus the potential is constant along a side of the rectangle, though each side has a different value. A side intersected by a branch cut is an exception--the potential will have one value before the cut, and another value after the cut. The difference between the segments is the circulation about the airfoil or vortex that is connected to the infinity boundary by the cut.

The cases of positive and negative angles of attack must be treated separately because of the properties of the arctangent function. For a vortex below the chordline, the potentials at infinity are adjusted in lines 3186-3199. Lines 3201-3214 do the same for a vortex above the chordline.

Task4:

In TRANDES, the potential is incremented by the circulation of the airfoil when the branch cut of the airfoil is crossed in a

counter-clockwise manner. This convention was repeated in TRANVOR for the potential increment across a cut used to establish a vortex; so that when sweeping from left to right, the vortex circulation is added across the cut for a vortex below the chordline and subtracted across the cut for a vortex above the chordline. This change of sign is the reason the variable IVLOC, which indicates the vortex position relative to the chordline, has a value of positive or negative unity. When horizontal velocities are calculated near the cut, the vortex circulation must either be added to or subtracted from difference equations involving two grid points on opposite sides of the cut to maintain continuity of the horizontal velocity component.

The velocity field is calculated in the main program for the Mach chart and in subroutine SOLVE to determine the flow type and for use in the system of finite difference equations. The velocity correction, found in lines 432-433, 462-463, 482-483, and 1807-1808, is preceded by two statements that determine the necessity of the adjustment. This correction removes the circulation from the potential difference between two points on opposite sides of the cut.

Second derivatives of the potential should also be continuous. The tridiagonal matrix representing the finite difference equations of Appendix A is set up in subroutine SOLVE. On the right-hand side of the equations, differences between the values of the potential at various grid locations are calculated repeatedly. Each time a difference is calculated between potentials on opposite sides of a cut, the increment of potential across the cut (the circulation of the vortex) must be removed from the difference. Table 1 shows the various conditions for which the right side (RS) terms need adjustment and the proper adjustment for each case. Most

of the adjustments have opposite signs for vortices above and below the chordline, so the variable IVLOC is used to provide the proper sign. Lines 1905-1932 of TRANVOR, inserted in the subroutine SOLVE following card 1679, represent the conditions and statements listed in Table 1.

Table 1: Adjustments to the Finite Difference Scheme

Subsonic Points		
IF	AND IF	THEN
i=IVOR	IVLOC=1 and j>JVOR or IVLOC=-1 and j≤JVOR	$RS' = RS - IVLOC \left(1 - \frac{u^2}{a^2}\right) \left(\frac{d\xi}{dx}\right)_i \left(\frac{d\xi}{dx}\right)_{i-1} \frac{\Gamma_v}{(\Delta\xi)^2}$
i=IVOR	j=JVOR or j=JVOR+1	$RS' = RS + \frac{uv}{a^2} \left(\frac{d\xi}{dx}\right)_i \left(\frac{d\eta}{dy}\right)_j \frac{\Gamma_v}{2 \Delta\xi \Delta\eta}$
i=IVOR+1	IVLOC=1 and j>JVOR or IVLOC=-1 and j≤JVOR	$RS' = RS + IVLOC \left(1 - \frac{u^2}{a^2}\right) \left(\frac{d\xi}{dx}\right)_i \left(\frac{d\xi}{dx}\right)_{i-1} \frac{\Gamma_v}{(\Delta\xi)^2}$
i=IVOR+1	j=JVOR or j=JVOR+1	$RS' = RS + \frac{uv}{a^2} \left(\frac{d\xi}{dx}\right)_i \left(\frac{d\eta}{dy}\right)_j \frac{\Gamma_v}{2 \Delta\xi \Delta\eta}$

Table 1 (cont.)

Supersonic Points

IF	AND IF	THEN
$i=IVOR$	IVLOC=1 and $j>JVOR$ or IVLOC=-1 and $j\leq JVOR$	$RS' = RS - IVLOC \frac{v^2}{q^2} \left(\frac{d\xi}{dx} \right)_i \left(\frac{d\xi}{dx} \right)_{i+\frac{1}{2}} \frac{T_v}{(\Delta\xi)^2}$
$i=IVOR$	$j=JVOR$ or $j=JVOR+1$	$RS' = RS + \frac{uv}{2q^2} \left(\frac{d\xi}{dx} \right)_i \left(\frac{d\eta}{dy} \right)_j \frac{T_v}{\Delta\xi \Delta\eta}$
$i=IVOR+1$	IVLOC=1 and $j>JVOR$ or IVLOC=-1 and $j\leq JVOR$	$RS' = RS - IVLOC \left(1 - \frac{q^2}{a^2} \right) \frac{u^2}{q^2} \left(\frac{d\xi}{dx} \right)_i \left(\frac{d\xi}{dx} \right)_{i-\frac{1}{2}} \frac{T_v}{\Delta\xi \Delta\eta}$
$i=IVOR+1$	$j=JVOR+1$ and $v\geq 0.0$ or $j=JVOR$ and $v<0.0$	$RS' = RS - \left(1 - \frac{q^2}{a^2} \right) \frac{2uv}{q^2} \left(\frac{d\xi}{dx} \right)_i \left(\frac{d\eta}{dy} \right)_j \frac{T_v}{\Delta\xi \Delta\eta}$
$i=IVOR+1$	IVLOC=1 and $j>JVOR$ or IVLOC=-1 and $j\leq JVOR+1$	$RS' = RS + IVLOC \frac{v^2}{q^2} \left(\frac{d\xi}{dx} \right)_i \left(\frac{d\xi}{dx} \right)_{i-\frac{1}{2}} \frac{T_v}{(\Delta\xi)^2}$
$i=IVOR+1$	$j=JVOR$ or $j=JVOR+1$	$RS' = RS + \frac{uv}{2q^2} \left(\frac{d\xi}{dx} \right)_i \left(\frac{d\eta}{dy} \right)_j \frac{T_v}{\Delta\xi \Delta\eta}$
$i=IVOR+2$	IVLOC=1 and $j>JVOR$ or IVLOC=-1 and $j\leq JVOR$	$RS' = RS + IVLOC \left(1 - \frac{q^2}{a^2} \right) \frac{u^2}{q^2} \left(\frac{d\xi}{dx} \right)_i \left(\frac{d\xi}{dx} \right)_{i-\frac{3}{2}} \frac{T_v}{(\Delta\xi)^2}$

Task 5:

Lines 155-179 restore the proper increment of potential across the cut when the grid spacing is halved by subroutine HALVE to increase the detail of the solution. In this subroutine, each new grid point is assigned the average potential of adjacent grid points. When a new grid point is located beside the cut, it should be assigned the average potential of adjacent grid points as if they were both on the same side of the cut as the new grid point. To make the interpolation for the potential values of new grid points correct, the potential increment across the cut must be removed from the average of the potentials of adjacent grid points.

RESULTS

Six minutes of CPU time is typically required for TRANVOR to run on the AMDAHL 360.

Initially TRANVOR was tested to discover limitations on its use. Results were obtained for various positions of the vortex in the flow. Vortex positions very near the airfoil surface (less than .1c) have not been tested. The modifications did not hinder the viscous boundary layer analysis. The effect of vortices with strengths up to .6 has been analyzed successfully. Analysis with higher strengths has not been attempted.

High freestream velocities cause problems. For example, one case with a freestream Mach number of .6 broke down in the last grid because the square of the local speed of sound was calculated to be negative. This was the result of very high velocities encountered near the center of the vortex. Since the vortex is placed midway between grid lines, the maximum velocity measured near the vortex center increases as the grid becomes finer, doubling each time the mesh size is halved.

TRANVOR does not model the vortex correctly for compressible flow. The tangential velocity does not continually increase towards the center of a vortex in compressible flow. Rather, as shown in Figure 3, the Mach number becomes infinite at a certain radius, r_{min} . The region within r_{min} must be empty of flow or else contain a solid core.

Three incompressible methods for analyzing BVI were used to check the

accuracy of TRANVOR for low speed flows. A flat plate approximation, a source-panel method, and a conformal mapping technique are discussed in Appendices B, C, and D, respectively. Results at any subsonic flow speed may be scaled by the Prandtl-Glauert rule¹⁰ for comparison with results at another subsonic speed.

Each method was applied to the ten cases shown in Figure 4 with a zero angle of attack. TRANVOR and the source-panel method solved the flowfield around a NACA 0012 airfoil. The conformal mapping technique produced results for a Joukowski airfoil of comparable thickness. The airfoils are compared in Figure 5.

Lift coefficients were calculated in two ways: (1) directly from the circulation about the airfoil using the Kutta-Joukowski theorem¹¹ or (2) by integrating the pressure distribution on the surface of the airfoil. The lift coefficients obtained by both approaches are listed in Table 2 and compared in Figure 6.

Table 2: A Comparison of Results for Low Speed Flows

<u>Case</u>	<u>c_l from circulation</u>			<u>c_l from pressure</u>		
	<u>TRANVOR</u>	<u>Flat Plate</u>	<u>Conformal Mapping</u>	<u>TRANVOR</u>	<u>Source Panel</u>	<u>Conformal Mapping</u>
1	.3318	.3392	.3528	.2838	.3133	.2796
2	-.3332	-.3392	-.3528	-.3200	-.3651	-.3318
3	.3333	.3392	.3528	.3314	.3651	.3318
4	-.3319	-.3992	-.3528	-.2727	-.3133	-.2796
5	.1681	.1615	.1666	.1366	.1433	.1270
6	.6637	.6785	.7056	.5314	.5747	.5069
7	-.4134	-.3952	-.4149	-.5448	-.5359	-.4954
8	.4095	.3952	.4149	.3659	.3652	.3252
9	.5984	.6133	.6394	.5943	.6446	.5797
10	-.5991	-.6133	-.6394	-.5830	-.6446	-.5797

The lift coefficients calculated from the airfoil circulation differ by less than 7% in all cases. The maximum difference for the lift coefficients found by integration was 14.9%. Part of the significant disagreement is probably due to the inaccuracy of the numerical integration of the pressure distribution. Disagreement between the two groups of lift coefficients was largest when the vortex was near the airfoil surface or had a large strength.

Cases 1&4, 2&3, and 9&10 were symmetrical--the results for each pair should have been mirror images. The non-iterative codes showed exact symmetry. The lift coefficients of TRANVOR were within 4% of being symmetrical.

Pressure distributions obtained for three cases are compared in Figures 7, 8, and 9. The close agreement between TRANVOR and the source-panel method indicate that the conformal mapping technique is probably in error. The difference in the airfoil shapes is not really significant between the leading edge and about midchord, so the pressure distributions should be more similar. With the cusped trailing edge, the flow should not slow down as much on the Joukowski airfoil as on the NACA 0012. To determine if the conformal mapping technique was indeed wrong, the coordinates of the Joukowski airfoil were entered into TRANVOR and Case 1 was repeated. Figure 10 compares the results of TRANVOR and the conformal mapping technique with the same airfoil. The fairly proportional relationship between the pressure distributions suggests that the tangential velocities are too low in the conformal mapping technique. The results of TRANVOR with the Joukowski airfoil are believed to be valid because they agree with results with the NACA 0012 airfoil for this case until around the midchord.

The pressure distribution of Case 8 (see Figure 8) exhibits the influence of the vortex particularly well. The counter-clockwise flow of the vortex retards the velocity on the lower surface of the airfoil, while the flow on the upper surface is hardly affected. The increased pressure on the lower surface generates lift even though the airfoil is not inclined to the freestream flow.

CONCLUSIONS

The modifications made to TRANDES to model a vortex in the flowfield produce valid solutions for BVI in low speed flows and do not interfere with boundary layer calculations.

The code is not useful for indicating or analyzing the aerodynamic mechanism responsible for impulsive rotor noise because it will not iterate on the final computational grid with high speed flows. The flow around the center of the vortex must be modelled differently before accurate solutions will be obtained for high speed flows.

Fig. 1 Infinity Boundary Conditions

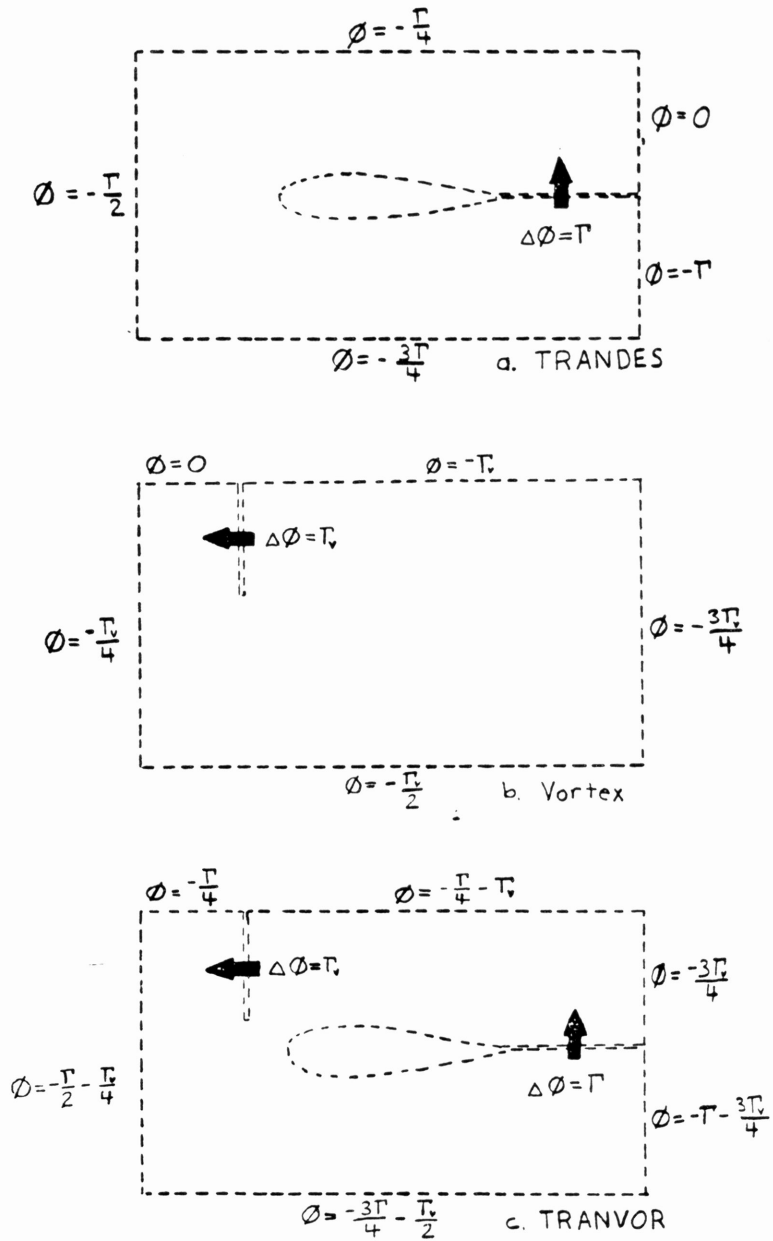
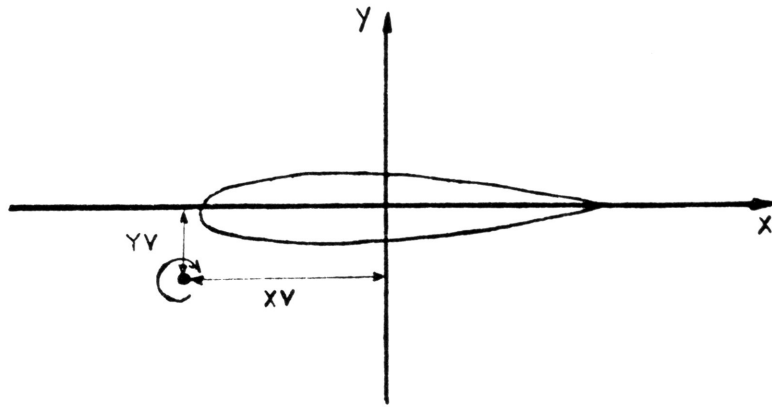
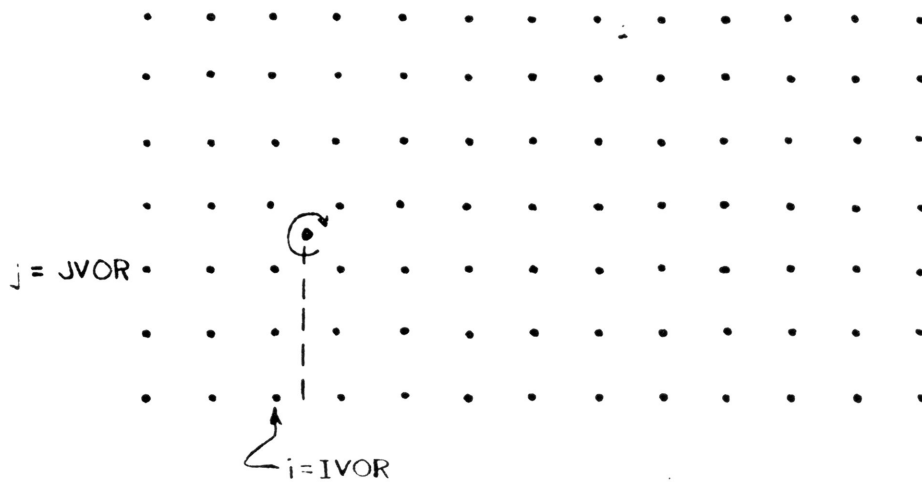


Fig 2. Vortex Position

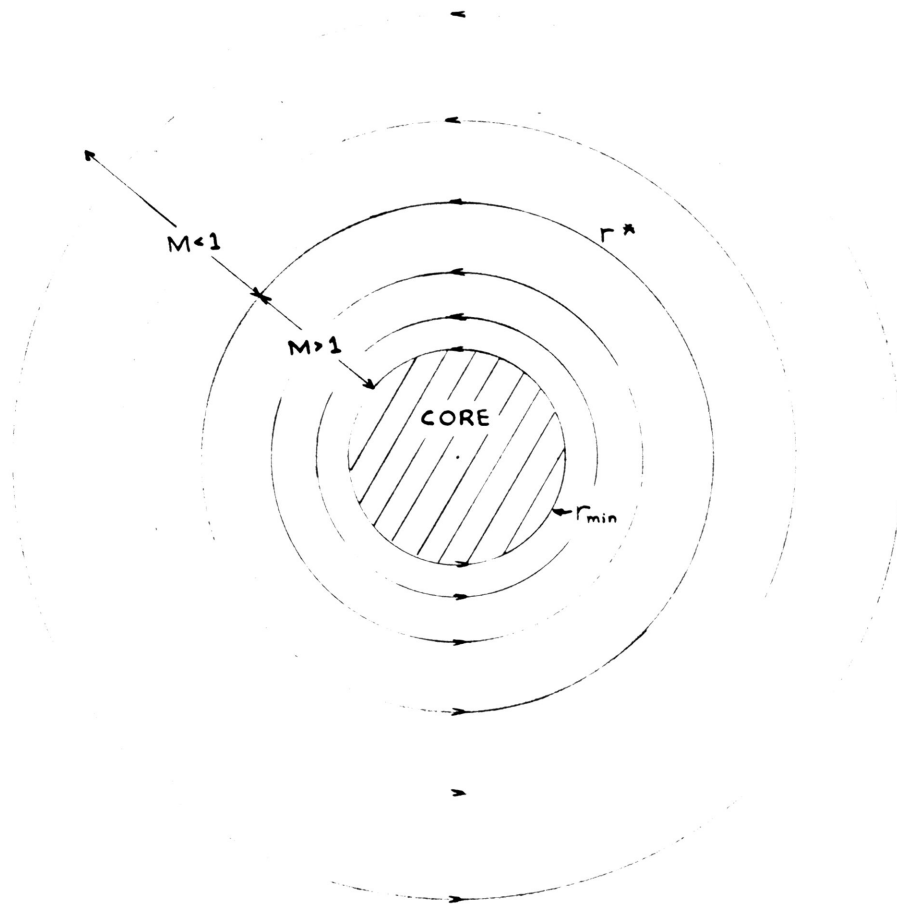


a. Flow field



b. Computational Grid

Figure 3 Compressible Vortex



(.7, .2)
CASE 9, $T_v = .3$

(.7, -.2)
CASE 10, $T_v = .3$

CASE 3, $T_v = .3$
CASE 4, $T_v = .3$
(-.7, .2)

(-.5, -.1) } CASE 5, $T_v = -.1$

(0, -.2) • CASE 7, $T_v = .3$
CASE 8, $T_v = .3$

CASE 1, $T_v = -.3$
CASE 2, $T_v = .3$
CASE 6, $T_v = -.6$
(-.7, -.2)



Figure 4 Test Cases

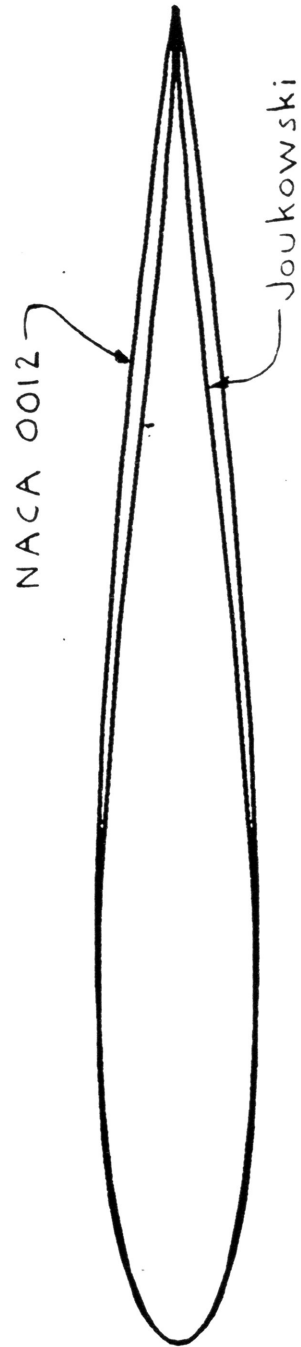


Figure 5 Airfoil Shape Comparison

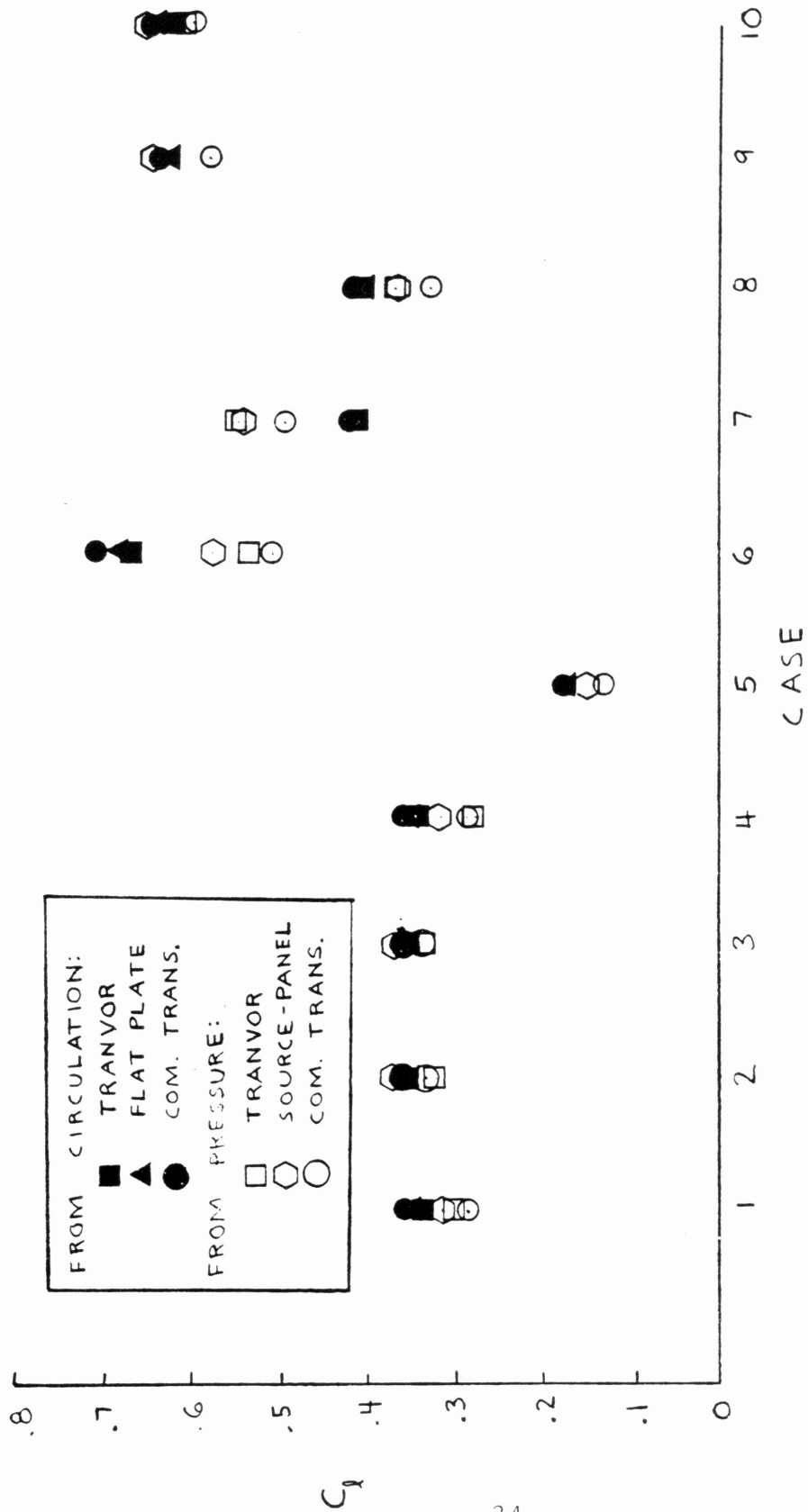


Figure 6 Comparison of Lift Coefficients

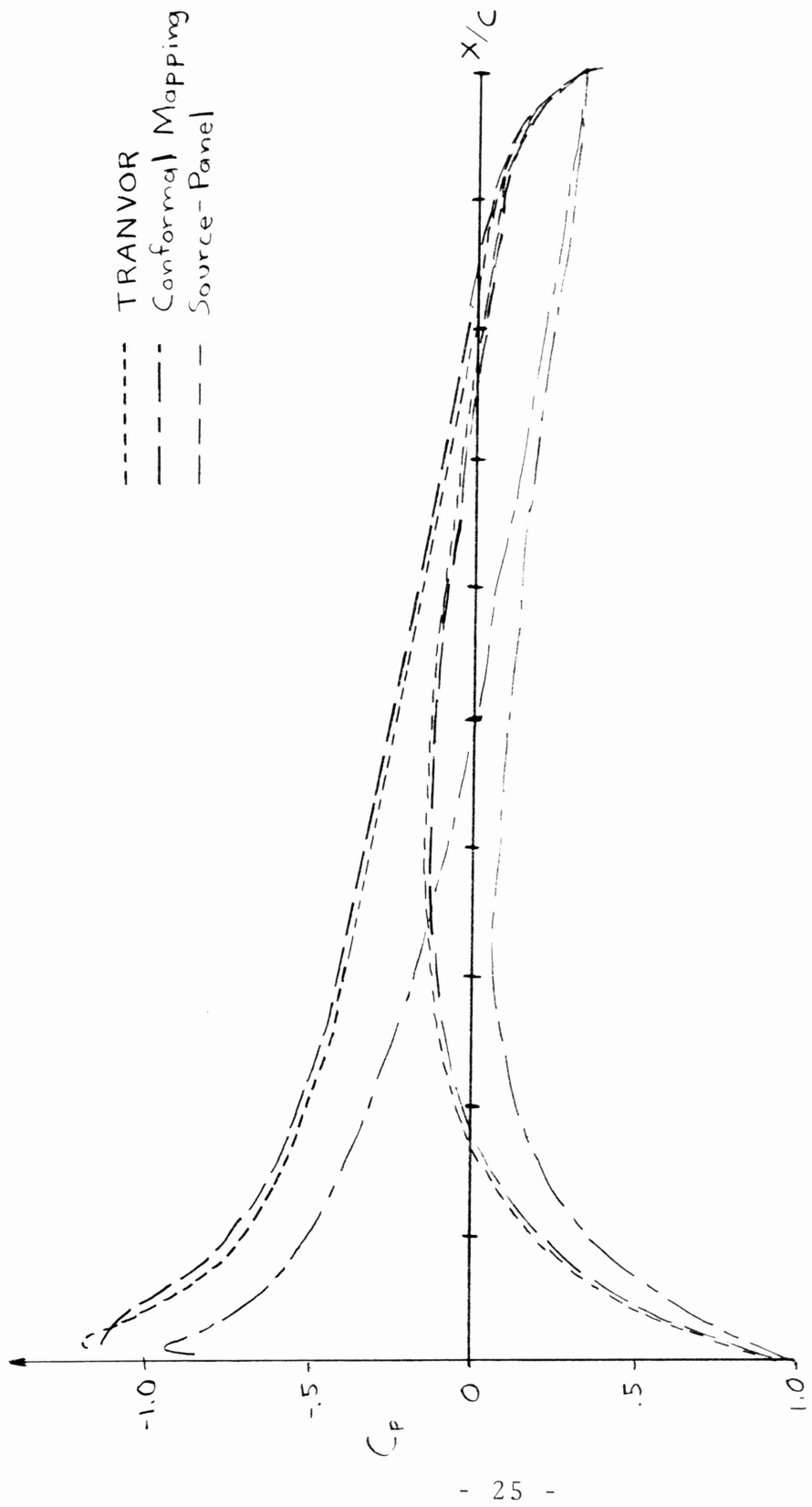


Figure 7 Case 1 Pressure Distribution

- TRANVOR
- Conformal Mapping
- Source - Panel

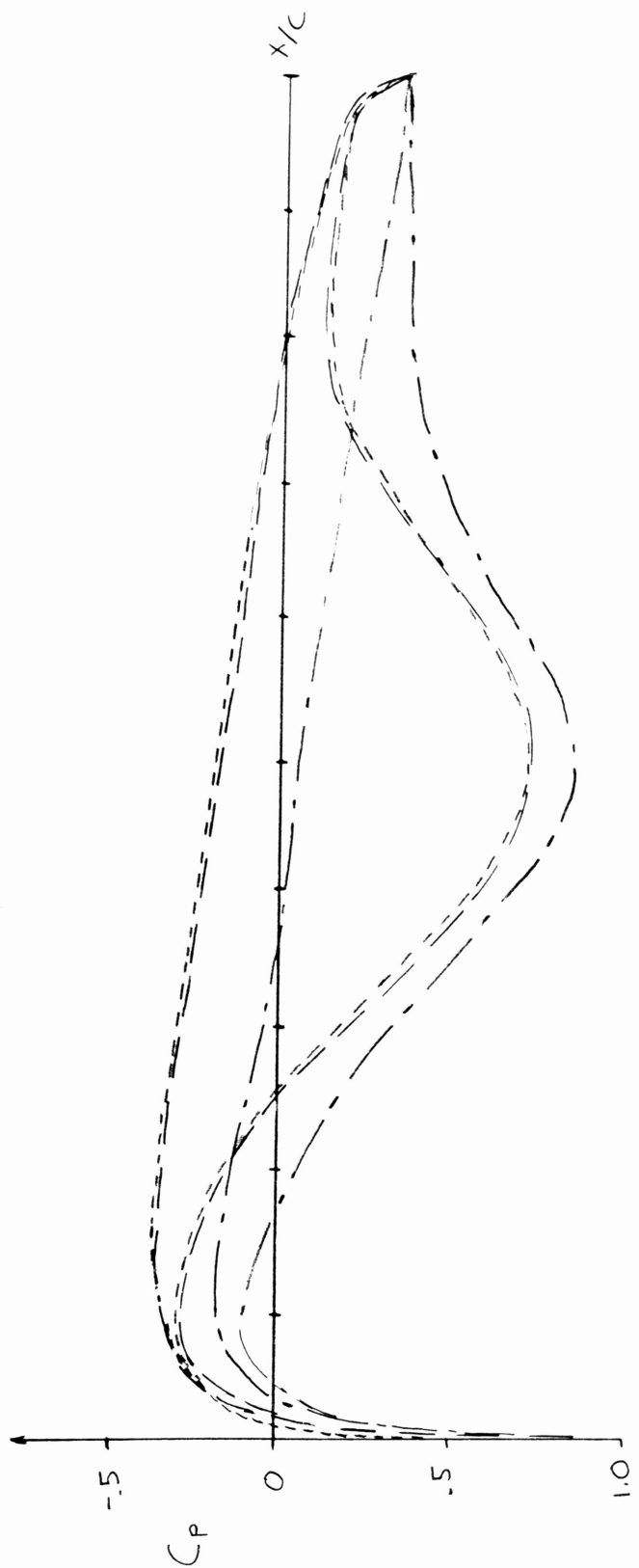


Figure 8 Case 8 Pressure Distribution

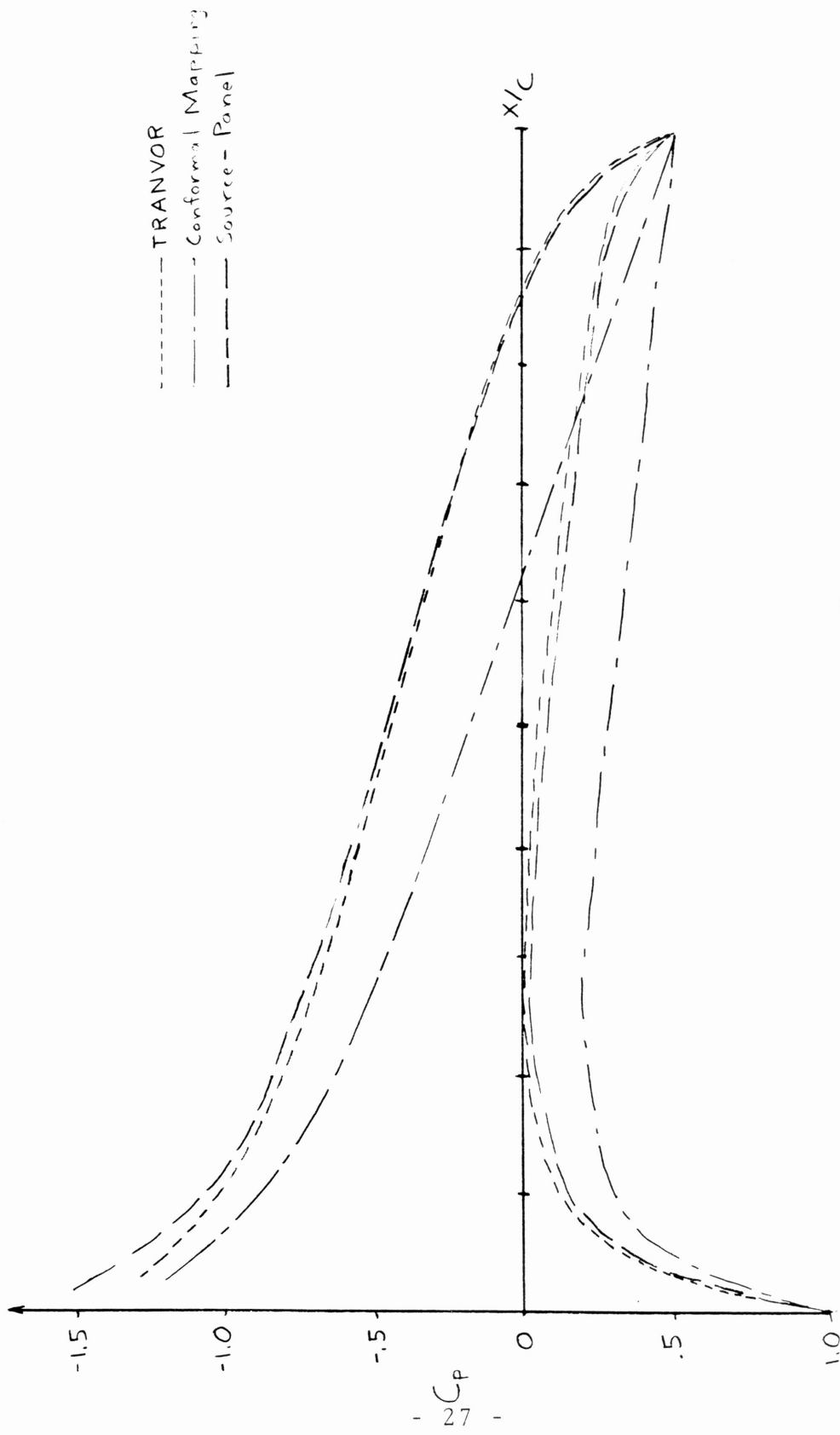


Figure 9 Case 10 Pressure Distribution

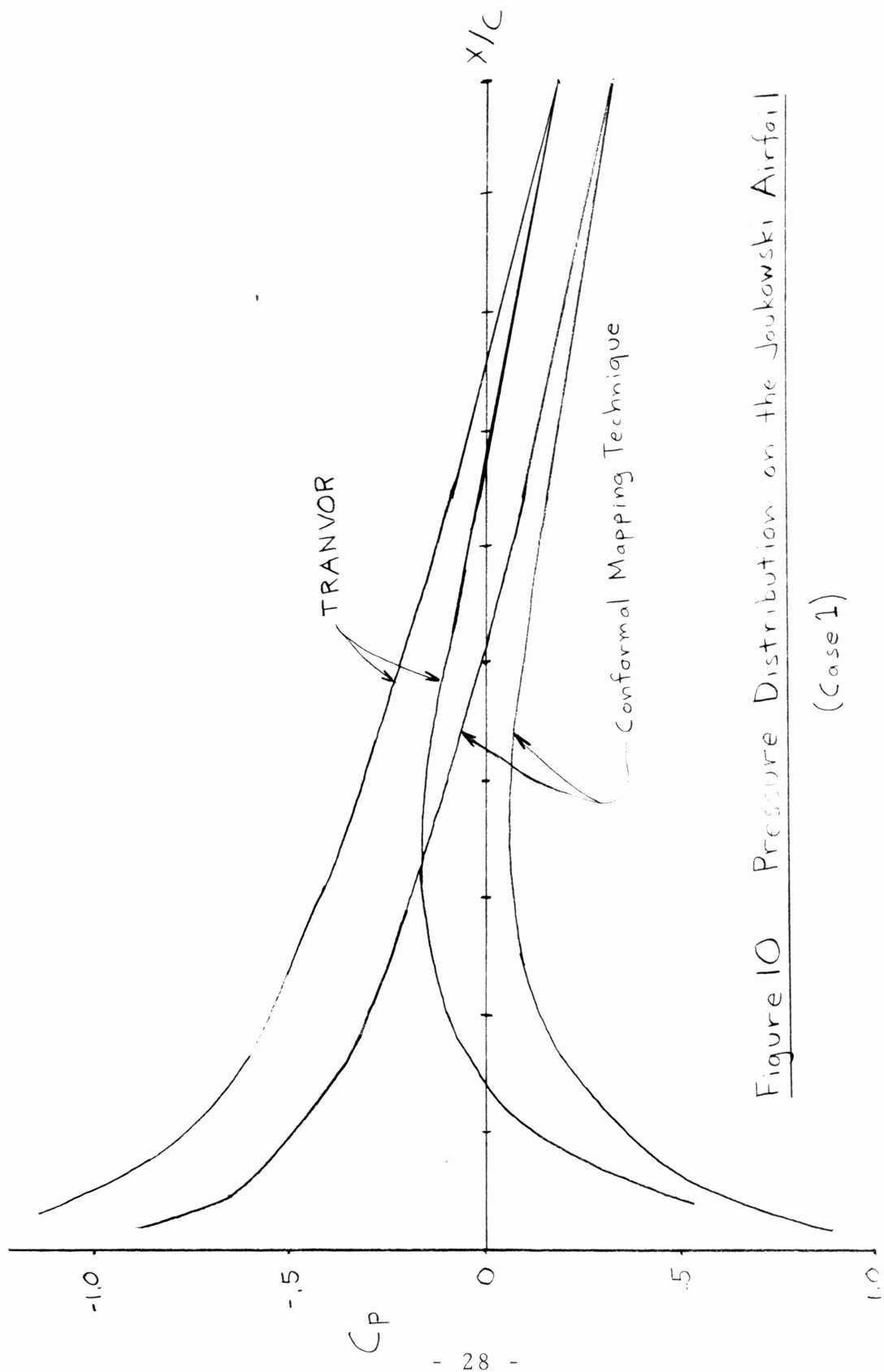


Figure 10 Pressure Distribution on the Joukowski Airfoil
(Case 1)

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APPENDIX A:

Finite Difference Scheme

$$\begin{aligned}
& \left[\frac{u^2}{q^2} \left(\frac{dn}{dy} \right)_j \left(\frac{dn}{dy} \right)_{j-\frac{1}{2}} \frac{1}{(\Delta\eta)^2} + \epsilon \frac{v}{q} \left(\frac{dx}{dx} \right)_i \left(\frac{dn}{dy} \right)_{j-\frac{1}{2}} \frac{1}{\Delta\xi \Delta\eta} \right] \Phi_{i,j-1} \\
& + \left[-\frac{v^2}{q^2} \left(\frac{dx}{dx} \right)_i \left(\frac{dx}{dx} \right)_{i-\frac{1}{2}} \frac{1}{(\Delta\xi)^2} - \frac{u^2}{q^2} \left(\frac{dn}{dy} \right)_j \left(\frac{dn}{dy} \right)_{j+\frac{1}{2}} + \left(\frac{dn}{dx} \right)_i \frac{1}{\Delta\xi} \left(\frac{dn}{dy} \right)_{j-\frac{1}{2}} \frac{1}{\Delta\eta} + \frac{v}{q} \left(\frac{dn}{dy} \right)_{j-\frac{1}{2}} \frac{1}{\Delta\eta} \right] \Phi_{i,j} \\
& + \left[\frac{u^2}{q^2} \left(\frac{dn}{dy} \right)_j \left(\frac{dn}{dy} \right)_{j+\frac{1}{2}} \frac{1}{(\Delta\eta)^2} \right] \Phi_{i,j+1} \\
& = - \left(1 - \frac{q^2}{a^2} \right) \left\{ \frac{u^2}{q^2} \left(\frac{dx}{dx} \right)_i \left(\frac{dx}{dx} \right)_{i-\frac{1}{2}} \left[\left(\frac{dn}{dx} \right)_{i-\frac{1}{2}} \left(\Phi_{i,j} - \Phi_{i-1,j}^* \right) - \left(\frac{dn}{dx} \right)_{i-\frac{1}{2}} \left(\Phi_{i-1,j}^* - \Phi_{i-2,j} \right) \right] + 2 \frac{uv}{q^2} \left(\frac{dx}{dx} \right)_i \left(\frac{dn}{dy} \right)_{j-\frac{1}{2}} \frac{1}{\Delta\xi \Delta\eta} \left(\Phi_{i,j} - \Phi_{i-1,j}^* \right) \right. \\
& - \left. \left(\Phi_{i,j-1} + \Phi_{i-1,j-1}^* \right) + \frac{v^2}{q^2} \left(\frac{dn}{dy} \right)_j \left(\frac{dn}{dy} \right)_{j-\frac{1}{2}} \left[\left(\frac{dn}{dy} \right)_{j-\frac{1}{2}} \left(\Phi_{i,j-1} - \Phi_{i,j-2} \right) \right] \right\} - \frac{v^2}{q^2} \left(\frac{dx}{dx} \right)_i \frac{1}{(\Delta\xi)^2} \left[\left(\frac{dn}{dy} \right)_{i+\frac{1}{2}} \left(\Phi_{i+1,j} \right) \right. \\
& - \left. \left(\frac{dn}{dx} \right)_{i-\frac{1}{2}} \left(\Phi_{i-1,j} \right) \right] + \frac{uv}{2q^2} \left(\frac{dx}{dx} \right)_i \left(\frac{dn}{dy} \right)_{j-\frac{1}{2}} \frac{1}{\Delta\xi \Delta\eta} \left[\left(\Phi_{i-1,j-1} - \Phi_{i-1,j} + \Phi_{i+1,j-1} \right) + \epsilon \left(\frac{dx}{dx} \right)_i \frac{1}{\Delta\xi \Delta\eta} \left[\frac{u}{q} \left(\frac{dn}{dy} \right)_{i-\frac{1}{2}} \left(\Phi_{i,j} \right) \right. \right. \\
& \left. \left. - \Phi_{i-1,j} + \Phi_{i-1,j}^* \right) + \frac{v}{q} \left(\frac{dn}{dy} \right)_{j-\frac{1}{2}} \left(\Phi_{i,j-1} - \Phi_{i,j} \right) \right]
\end{aligned}$$

Case 1a: Subsonic Flow, Positive Vertical Velocity

* denotes a potential value from the previous sweep

$$\begin{aligned}
& \left[\frac{u^2}{q^2} \left(\frac{dn}{dy} \right)_j \frac{1}{(\Delta\eta)^2} \right] \Phi_{i,j-1} \\
& + \left[\frac{v^2}{q^2} \left(\frac{ds}{dx} \right)_{i-\frac{1}{2}} \frac{1}{(\Delta\xi)^2} - \frac{u^2}{q^2} \left(\frac{dn}{dy} \right)_j \left(\left(\frac{dn}{dy} \right)_j + \left(\frac{dn}{dy} \right)_{j+\frac{1}{2}} \right) \frac{1}{(\Delta\eta)^2} - \epsilon \left(\frac{ds}{dx} \right)_{i-\frac{1}{2}} \frac{1}{\Delta\xi} \left(\frac{u}{q} \left(\frac{ds}{dx} \right)_{i-\frac{1}{2}} \frac{1}{\Delta\xi} - \frac{v}{q} \left(\frac{dn}{dy} \right)_{j+\frac{1}{2}} \frac{1}{\Delta\eta} \right) \right] \Phi_{i,j} \\
& + \left[\frac{u^2}{q^2} \left(\frac{dn}{dy} \right)_j \frac{1}{(\Delta\eta)^2} - \epsilon \frac{v}{q} \left(\frac{ds}{dx} \right)_i \left(\frac{dn}{dy} \right)_{i+\frac{1}{2}} \frac{1}{\Delta\xi \Delta\eta} \right] \Phi_{i,j+1} \\
& = - \left(1 - \frac{q^2}{\sigma^2} \right) \left\{ \frac{u^2}{q^2} \left(\frac{ds}{dx} \right)_i \frac{1}{(\Delta\xi)^2} \left[\left(\frac{ds}{dx} \right)_{i-\frac{1}{2}} (\Phi_{i,j} - \Phi_{i-1,j}^*) - \left(\frac{ds}{dx} \right)_{i-\frac{1}{2}} (\Phi_{i-1,j}^* - \Phi_{i-2,j}) \right] + \frac{2uv}{q^2} \left(\frac{ds}{dx} \right)_i \left(\frac{dn}{dy} \right)_j \frac{1}{\Delta\xi \Delta\eta} (-\Phi_{i,j} + \Phi_{i-1,j}^*) \right. \\
& \quad + \Phi_{i,j+1} - \Phi_{i-1,j+1} \left. \right) + \frac{v^2}{q^2} \left(\frac{dn}{dy} \right)_j \frac{1}{(\Delta\eta)^2} \left[\left(\frac{dn}{dy} \right)_{j+\frac{1}{2}} (\Phi_{i,j} - \Phi_{i,j+1}) - \left(\frac{dn}{dy} \right)_{j+\frac{1}{2}} (\Phi_{i,j-1} - \Phi_{i,j+2}) \right] \left. \right\} - \frac{v^2}{q^2} \left(\frac{ds}{dx} \right)_i \frac{1}{(\Delta\xi)^2} (\Phi_{i+1,j} - \Phi_{i,j}) \\
& \quad + \left(\frac{ds}{dx} \right)_i \frac{1}{\Delta\xi} \left[\frac{u}{q} \left(\frac{ds}{dx} \right)_{i-\frac{1}{2}} \frac{1}{\Delta\xi} - \frac{v}{q} \left(\frac{dn}{dy} \right)_{j+\frac{1}{2}} \frac{1}{\Delta\eta} \right] + \frac{uv}{2q^2} \left(\frac{ds}{dx} \right)_i \left(\frac{dn}{dy} \right)_j \frac{1}{\Delta\xi \Delta\eta} [\Phi_{i-1,j-1} - \Phi_{i-1,j+1} - \Phi_{i+1,j-1} + \Phi_{i+1,j+1}] \\
& \quad + \epsilon \left(\frac{ds}{dx} \right)_i \frac{1}{\Delta\xi \Delta\eta} \left[\frac{u}{q} \left(\frac{ds}{dx} \right)_{i-\frac{1}{2}} \frac{1}{(\Delta\xi)^2} (-\Phi_{i,j} - \Phi_{i-1,j} + \Phi_{i-1,j}^*) + \frac{v}{q} \left(\frac{dn}{dy} \right)_{j+\frac{1}{2}} (\Phi_{i,j} - \Phi_{i,j+1}) \right]
\end{aligned}$$

Case Ib: Subsonic Flow, Negative Vertical Velocity

* denotes a potential value from the previous sweep

$$\begin{aligned}
& \left\{ \left(1 - \frac{v^2}{a^2}\right) \left(\frac{d\eta}{dx}\right)_j \left(\frac{dx}{dy}\right)_{j-\frac{1}{2}} \frac{1}{(\Delta\eta)^2} \right\} \Phi_{i,j-1} \\
& + \left\{ -\frac{2}{w} \left(1 - \frac{v^2}{a^2}\right) \left(\frac{d\xi}{dx}\right)_{i+\frac{1}{2}} \frac{1}{(\Delta\xi)^2} \left[\left(\frac{d\xi}{dx}\right)_{i+\frac{1}{2}} \left(\frac{d\eta}{dy}\right)_j \right] \frac{1}{(\Delta\xi)^2} - \left(1 - \frac{v^2}{a^2}\right) \left(\frac{d\eta}{dy}\right)_j \left[\left(\frac{d\eta}{dy}\right)_{j+\frac{1}{2}} + \left(\frac{dx}{dy}\right)_{j-\frac{1}{2}} \right] \frac{1}{(\Delta\eta)^2} - \epsilon \frac{v}{q} \left(\frac{d\xi}{dx}\right)_{i+\frac{1}{2}} \frac{1}{(\Delta\xi)^2} \right. \\
& \quad \left. + \epsilon \frac{v}{q} \left(\frac{d\xi}{dx}\right)_i \left(\frac{d\eta}{dy}\right)_{j+\frac{1}{2}} \frac{1}{\Delta\xi \Delta\eta} \right\} \Phi_{i,j} \\
& + \left\{ \left(1 - \frac{v^2}{a^2}\right) \left(\frac{d\eta}{dy}\right)_j \left(\frac{d\eta}{dy}\right)_{j+\frac{1}{2}} \frac{1}{(\Delta\eta)^2} - \epsilon \frac{v}{q} \left(\frac{d\xi}{dx}\right)_i \left(\frac{d\eta}{dy}\right)_{j+\frac{1}{2}} \frac{1}{\Delta\xi \Delta\eta} \right\} \Phi_{i,j+1} \\
& = \left(1 - \frac{v^2}{a^2}\right) \left(\frac{d\xi}{dx}\right)_i \left\{ -\left(\frac{d\xi}{dx}\right)_{i+\frac{1}{2}} \frac{1}{(\Delta\xi)^2} \Phi_{i+1,j} + \left[\left(\frac{d\xi}{dx}\right)_{i+\frac{1}{2}} + \left(\frac{dx}{dy}\right)_{i+\frac{1}{2}} \right] \frac{1}{(\Delta\xi)^2} \left(1 - \frac{1}{w}\right) \Phi_{i,j} - \left(\frac{d\xi}{dx}\right)_{i-\frac{1}{2}} \frac{1}{(\Delta\xi)^2} \Phi_{i-1,j} \right\} \\
& + \frac{v}{a^2} \left(\frac{d\xi}{dx}\right)_i \left(\frac{d\eta}{dy}\right)_j \frac{1}{2\Delta\xi \Delta\eta} \left(\Phi_{i-1,j-1} - \Phi_{i-1,j+1} - \Phi_{i-1,j-1} + \Phi_{i+1,j+1} \right) + \epsilon \frac{v}{q} \left(\frac{d\xi}{dx}\right)_i \left(\frac{d\xi}{dx}\right)_{i+\frac{1}{2}} \frac{1}{(\Delta\xi)^2} \left(-\Phi_{i,j} \right. \\
& \quad \left. - \Phi_{i-1,j} + \Phi_{i-1,j}^* \right) + \epsilon \frac{v}{q} \left(\frac{d\xi}{dx}\right)_i \left(\frac{d\eta}{dy}\right)_{j+\frac{1}{2}} \frac{1}{\Delta\xi \Delta\eta} \left(\Phi_{i,j} - \Phi_{i,j+1} \right)
\end{aligned}$$

Case 2: Supersonic Flow

* denotes a potential value from the previous sweep

APPENDIX B:
The Flat Plate Approximation¹¹

The airfoil is modelled as a flat plate. The flat plate is represented by a finite number of panels. A bound vortex is located at the quarter chord of each panel. At the three-quarters chord of each panel is a control point as shown in Figure A1.

A unique vorticity distribution is determined by applying the tangent flow boundary condition at the control point of each panel. Each bound vortex with circulation density γ_j at x_j will induce a velocity normal to a control point at x_i .

$$V_{yn_i} = \frac{\gamma_j \Delta x}{2\pi(x_i - x_j)}$$

A component of the freestream flow may be normal to each panel, depending on the angle of attack.

$$V_{\infty n_i} = V_{\infty} \sin \alpha$$

The free vortex in the flowfield will also induce a velocity at each control point normal to the plate.

$$V_{vn_i} = \frac{\Gamma}{2\pi r_{vi}} \cos T_i$$

The sum of the normal velocities induced by each bound vortex, the normal component of the freestream, and the normal velocity induced by the free vortex must equal zero at each control point if the flow is tangent.

$$\sum_{j=1}^{np} V_{yn_{ij}} + V_{\infty n_i} + V_{vn_i} = 0$$

This equation can be rearranged and a system of np simultaneous equations solved for the circulation density of each panel, where np is the number of panels.

$$\sum_{j=1}^{np} \gamma_j \left[\frac{\Delta x}{2\pi(x_i - x_j)} \right] = -V_{\infty} \sin \alpha - \frac{\Gamma}{2\pi r_{vi}} \cos T_i \quad \text{for } i=1, np$$

The Kutta-Joukowski theorem provides a simple relationship between the lift coefficient of the airfoil and the total circulation of the bound vortex distribution.

$$C_l = 2\Gamma = 2 \sum_{i=1}^{np} \gamma_i \Delta x_i$$

A theoretical correction factor¹² for the thickness of the airfoil is applied to the results of this method.

$$C'_l = \left(1 + \frac{4}{3\sqrt{3}} (t/c) \right) C_l$$

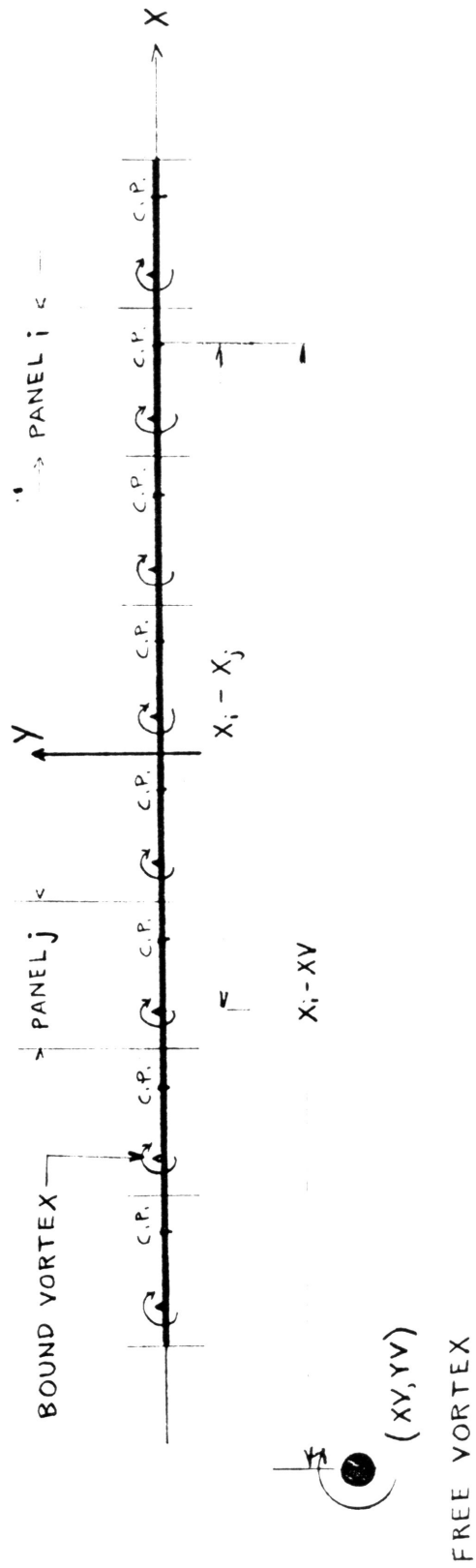


Figure B1 Flat Plate Approximation

APPENDIX C:
The Source-Panel Method¹¹

The airfoil surface is represented by a finite number of panels. The tangent flow boundary condition is satisfied at a control point on the midpoint of each panel. The tangent flow is achieved by placing a source sheet of constant strength on each panel. To generate lift, the Kutta condition must be satisfied. A vortex sheet of constant circulation density is placed on each panel to provide the circulation required to satisfy the Kutta condition of smooth flow at the trailing edge. See Figure C1.

The source strength and circulation density of each panel must be determined so that the flow is tangent to the surface at each control point and the smooth at the trailing edge. Since the partial differential equation governing incompressible potential flow is linear, this problem can be solved in parts and the final solution realized by superimposing the flow of each part.

The first flow considered is that of the freestream past the airfoil and the vortex in the flowfield without considering the Kutta condition, so there is no circulation about the airfoil. A source strength distribution that makes the flow tangent is calculated. The normal component of the flow at control point (x_i, y_i) induced by the source sheet on panel j with strength λ_j is found by integrating along panel j .

$$V_{\lambda_{n,i}} = \frac{\lambda_j}{2\pi} \int_j \frac{\partial}{\partial n_i} (\ln r_{ij}) ds_j$$

The free vortex also induces a flow normal to each panel.

$$V_{v_{n,i}} = \frac{\Gamma_v}{2\pi r_{v,i}} \sin(\tau_i - \beta_i)$$

A component of the freestream may also be normal to the panel.

$$V_{\infty_{n,i}} = \cos(\beta_i - \alpha)$$

The sum of the normal velocities induced by each source sheet and the free vortex and the normal component of the freestream velocity will equal zero if the flow is tangent.

$$\sum_{j=1}^{np} V_{\lambda_{n,i}} + V_{v_{n,i}} + V_{\infty_{n,i}} = 0$$

This equation is rearranged and a system of np simultaneous equations is solved for the source strength of each panel, where np is the number of panels.

$$\sum_{j=1}^{np} \lambda_j \left[\frac{1}{2\pi} \int_j \frac{\partial}{\partial n_i} (\ln r_{ij}) ds_j \right] = -\cos(\beta_i - \alpha) - \frac{\Gamma_v}{2\pi r_{v,i}} \sin(\tau_i - \beta_i)$$

This system of equations is solved twice with a uniform flow of unit velocity, at zero and ninety degree angles of attack. The speed of the tangential flow on the surface of the airfoil is calculated separately for each angle of attack by summing the tangential components of the flow induced by each of the source sheets and adding the tangential component of the freestream velocity.

$$V_{s_i} = \sum_{j=1}^{np} \frac{\lambda_j}{2\pi} \int_j \frac{\partial}{\partial s_i} (\ln r_{ij}) ds_j + \sin(\beta_i - \alpha) + \frac{\Gamma_v}{2\pi r_i} \cos(T_i - \beta_i)$$

Now the tangential velocity distribution for any angle of attack and magnitude of the freestream velocity is found by using the appropriate superposition of the known velocity distributions.

$$V_{o_i} = V_{\infty} \left(V_{s_i} \cos \alpha + V_{s_i} \sin \alpha \right)$$

$(\alpha=0^\circ)$ $(\alpha=90^\circ)$

The second flow considered is purely circulatory about the airfoil. Each panel is assigned a unit vortex density. A source strength distribution is found to make this circulatory flow tangent to the airfoil surface. The normal component of the flow induced at the control point of panel i by the vortex sheet on panel j with circulation density λ_j is found by integrating along panel j .

$$V_{n_{x_{ij}}} = \frac{1}{2\pi} \int_j \frac{\partial}{\partial n_i} \left(\tan^{-1} \frac{y_i - y_j}{x_i - x_j} \right) ds_j$$

The sum of the normal velocities induced by each vortex sheet and source sheet must equal zero at each control point if the flow is tangent.

$$\sum_{j=1}^{np} V_{n_{\lambda_{ij}}} + \sum_{j=1}^{np} V_{n_{x_{ij}}} = 0$$

This equation is rearranged and a system of np simultaneous equations is solved for the source strength of each panel.

$$\sum_{j=1}^{np} \lambda_j \left[\frac{1}{2\pi} \int_j \frac{\partial}{\partial n} (\ln r_{ij}) ds_j \right] = - \sum_{j=1}^{np} \frac{1}{2\pi} \int_j \frac{\partial}{\partial n} \left(\tan^{-1} \frac{y_i - y_j}{x_i - x_j} \right) ds_j \quad \text{for } i=1, np$$

From the resulting distribution of source strengths and the unit circulation density distribution, the tangential speed of this circulatory flow is calculated at each control point.

$$V_{c_i} = \sum_{j=1}^{np} \frac{\lambda_j}{2\pi} \int_j \frac{\partial}{\partial s_i} (\ln r_{ij}) ds_j + \sum_{j=1}^{np} \frac{1}{2\pi} \int_j \frac{\partial}{\partial s_i} \left(\tan^{-1} \frac{y_i - y_j}{x_i - x_j} \right) ds_j$$

The final solution is found by superimposing enough of the circulatory flow on the zero-lift flow to satisfy the Kutta condition. The flow at the trailing edge will be smooth if the tangential velocity at the last panel on the upper and lower surfaces is equal. A constant is calculated from the zero-lift and circulation velocities of these panels.

$$k = \frac{V_{oL} - V_{oU}}{V_{cU} - V_{cL}}$$

Now the velocity distribution of the circulatory flow is multiplied by this constant and superimposed on the velocity distribution of the zero-lift flow.

$$V_i = V_{o_i} + k V_{c_i}$$

The resulting flow satisfies the tangent flow boundary condition at each control point and is smooth at the trailing edge.

Pressure coefficients are calculated on each panel.

$$C_p = 1 - \left(\frac{V_i}{V_{\infty}} \right)^2$$

The lift coefficient of the airfoil is calculated by integrating the vertical component of the pressure force on the surface.

$$C_l = \sum_{i=1}^{np} C_{p_i} l_i \sin \beta_i$$

NOTE:

All of the integrals involved have a similar form after the integrands are differentiated.

$$I_{ij} = \int_0^l \frac{b - c s_j}{s_j^2 - e s_j + f} ds_j$$

Only two sets of integrals need to be calculated to use this method. The coefficients of the integrand are identical for the normal velocity induced by a source sheet and the tangential velocity induced by a vortex sheet. The coefficients of the numerator have opposite signs for the tangential velocity induced by a source sheet and the normal velocity induced by a vortex sheet. The best approach is to solve the two sets of integrals and store the results rather than solving the integrals each time they are encountered.

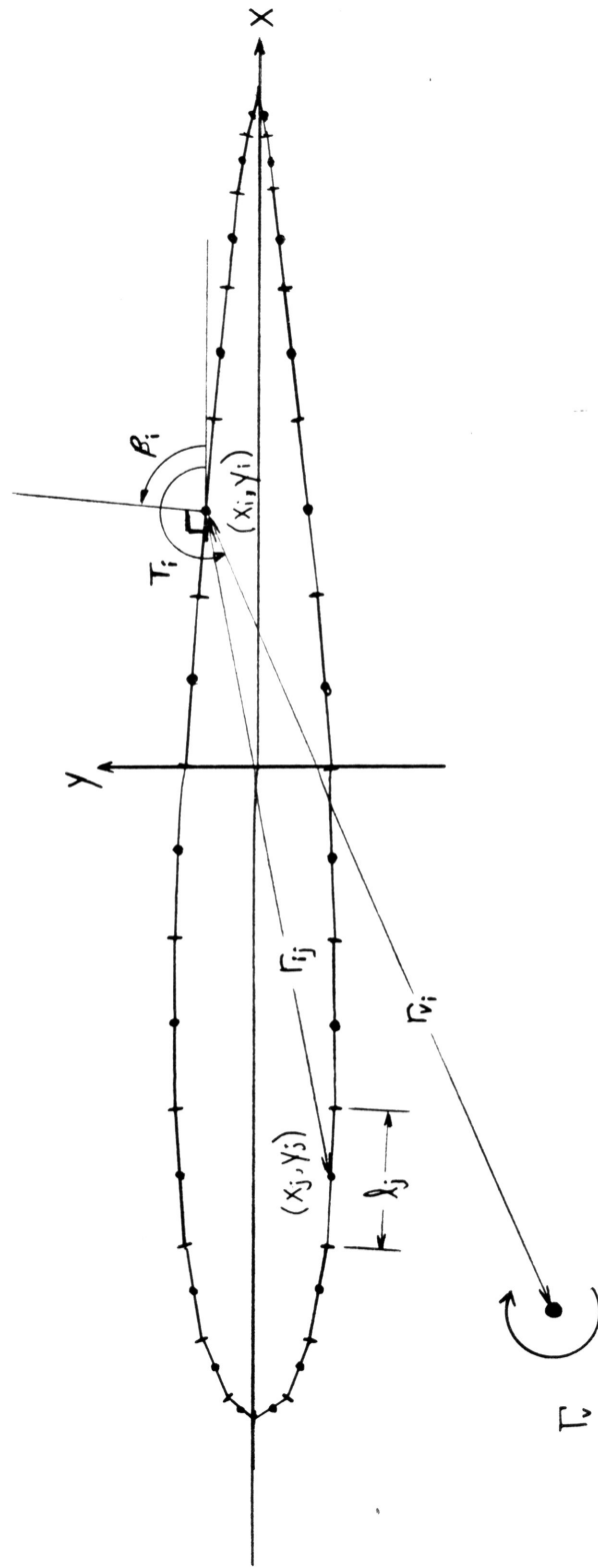


Figure C1 Source - Panel Method

APPENDIX D:
The Conformal Mapping Technique¹³

Two-dimensional incompressible, irrotational, inviscid flow can be described by a complex potential function. The velocity field is the conjugate of the gradient of the potential function. The potential functions for various flows given in Table D1 may be added to superimpose flows since the governing equation is linear.

Table D1: Potential functions

Uniform flow:	$F_1(W) = V_\infty W$
Vortex at W_v :	$F_2(W) = \frac{i\Gamma_v}{2\pi} \ln(W - W_v)$
Uniform flow past a vortex at W_v :	$F_3(W) = F_1(W) + F_2(W)$

The circle theorem¹⁴ determines the potential function for a flow is a circle of radius a is introduced into the flowfield.

$$F_4(W) = F_3(W) + \bar{F}_3\left(\frac{a^2}{W}\right) = V_\infty \left(W + \frac{a^2}{W}\right) + \frac{i\Gamma_v}{2\pi} \ln\left(\frac{W^2 - W_v W}{a^2 - \bar{W}_v W}\right)$$

The circle theorem is applicable to a flow if there are no rigid boundaries in the flow and the singularities of the potential function are all at a distance greater than a , the radius of the circle, from the origin.

A circulatory flow about the circle is superimposed by adding another term to the potential function.

$$F_5(W) = V_\infty \left(W + \frac{a^2}{W}\right) + \frac{i\Gamma_v}{2\pi} \ln\left(\frac{W^2 - W_v W}{a^2 - \bar{W}_v W}\right) + \frac{i\Gamma}{2\pi} \ln \frac{W}{a}$$

Now the potential function describes a uniform flow passing a circle with circulatory flow and a free vortex somewhere in the flowfield.

If an analytic function $R(W)$ is used to map the circle to another shape in the R -plane, the potential function $F(R)$ will describe the flow about the new shape. The objective is to map the circle into a shape resembling an airfoil.

Two consecutive transformations are used as shown in Figure D1. First the circle is shifted horizontally and the radius is increased. The second transformation results in a shape called a Joukowski airfoil.

The potential function $F_5(Z)$ describes a uniform flow past a Joukowski airfoil with a vortex present in the flowfield. Since the velocity is the conjugate of the gradient of the potential function, their magnitudes are equal.

$$|V(z)| = \left| \frac{dF_5(z)}{dz} \right|$$

Rather than stumbling through the tedious algebra required to determine the potential function $F(Z)$ and differentiate it, the chain rule is used to expand the derivative.

$$|V(Z)| = \left| \frac{dF(W)}{dW} \frac{dW}{dR} \frac{dR}{dZ} \right|$$

The pressure distribution is calculated from the velocities and integrated to determine the lift coefficient of the airfoil due to the presence of

the vortex in the flowfield.

The derivative dR/dZ approaches infinity at the trailing edge, implying an infinite velocity. The Kutta condition¹² requires smooth flow at the trailing edge. The flow will have a finite velocity at the trailing edge only if one of the first two derivatives goes to zero at the trailing edge. The derivative dW/dR is constant, so the derivative dF/dW should equal zero for the value of W corresponding to the trailing edge.

$$\left(\frac{dF}{dW}\right)_{W=a} = 0$$

The constraint of the Kutta condition provides a relationship between the circulation of the free vortex and the circulation of the airfoil.

$$\Gamma = \left[\frac{-2a(a-u_v)}{(a-u_v)^2 + v_v^2} \right] \Gamma_v$$

The Kutta-Joukowski theorem¹¹ relates the lift of an airfoil to its circulation, so the lift coefficient can be calculated as a function of the position and circulation of the vortex in the flowfield.

$$C_l = 2\Gamma$$

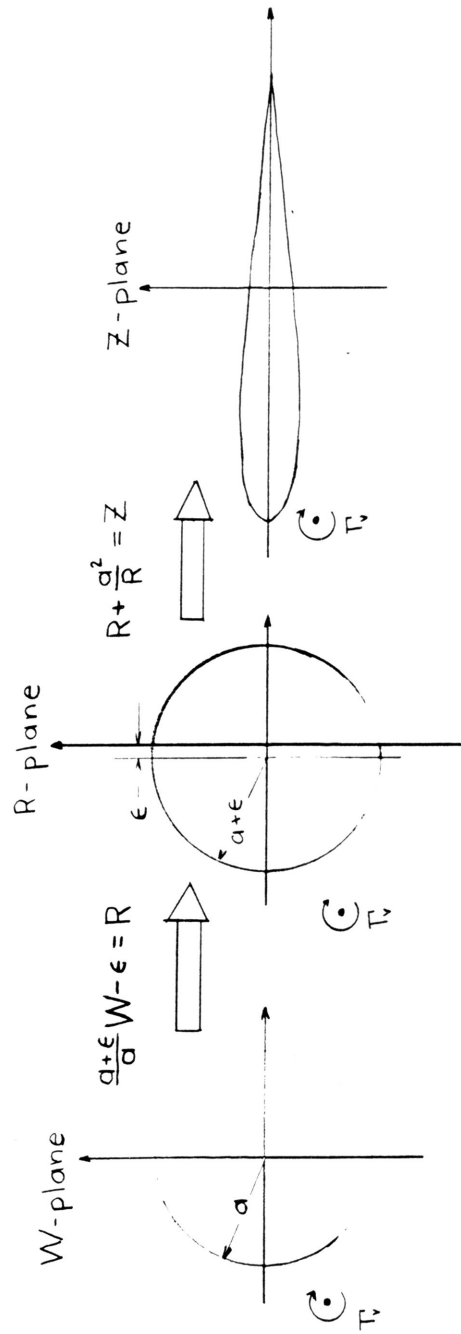


Figure D1 Transformation of a Circle to a Joukowski Airfoil

APPENDIX E:

TRANVOR Program Listing

```

1. //TRANVOR JOB (T177,O10A,O10,O10,DC),FLOW1 B'
2. //**MAIN SYSTEM=ANY,ORG=TCC
3. //**TAMU P=O
4. // EXEC FORTXCG,PARM.FORT='OPT(2),NOSOURCE',PARM.GO='SIZE=320K',
5. // REGION.GO=320K,FXLN5PC='3120,(100,10)'
6. //FORT.SYSIN DD *
7. C ***** T R A N V O R *****
8. C *****
9. C ***** A FORTAN PROGRAM FOR COMPUTING THE FLOW ABOUT AIRFOILS *****
10. C ***** AT LOW SPEEDS WITH A VORTEX IN THE FLOWFIELD. *****
11. C ***** TRANVOR IS A MODIFIED VERSION OF TRANDES *****
12. C ***** DISCUSSED IN NASA CR-2821. THUS, IT CAN ALSO BE USED *****
13. C ***** FOR TRANSONIC AIRFOIL ANALYSIS AND/OR DESIGN. *****
14. C ***** LELAND A. CARLSON, AEROSPACE ENGINEERING DEPARTMENT *****
15. C ***** TEXAS A&M UNIVERSITY, COLLEGE STATION, TEXAS, 77843 *****
16. C ***** APRIL 1984 *****
17. C *****
18. C
19. REAL M
20. DIMENSION UVEL(99),VVEL(99)
21. DIMENSION NTITLE(20),AA(500),IONIC(99)
22. COMMON CPU(99),CPL(99),E(99),DU1(99),DU2(99),DL1(99),DL2(99),D(99)
23. 1,FF(99),FFP12(99),FFM12(99),FFM1(99),FFM32(99),
24. 1P1(99),P2(99),PB(99),P(99,99),RS(99),S(99),SUP(99),SUB(99),TEMP(99)
25. 2),X(99),Y(99),YU(99),SLU(99),SLL(99),
26. 3A1,A2,AI2,ALP,CIR,EPS,EPS,DE,DS,DP,DPM,F,FP12,FM12,FM32,M,QI,QI2,
27. 4W,X1,X2,VVUB,VVUB1,AAJB,AAJB,QQJB,QQJB1,UUJB,VVUBP1,AAJB1,
28. 5,Q,QQ,UUJB1,PI,PI2,A22,A11,X4,S4
29. COMMON I,ITE,ITE1,ILE,ILE1,I1,I11,ICON,IMAX,IMAX1,INV,JB,JA1,JB1,
30. 1JMAX,JCON,UMAX1,NSSP,IW
31. COMMON/JS/GG(99),GGP12(99),GGM12(99),GGM32(99),GGP32(99),A3
32. COMMON/FIX/MHALF
33. COMMON/DELTA/ITER
34. COMMON/TAMU/DELTAY
35. COMMON/RED/ITERP
36. COMMON/FIPUT/IREAD
37. COMMON/NASH/RN,IBDLY,ITACT,YUORIG(99),YLORIG(99),SUPPER(99),SLOWER
38. 1(99),DEL(99),DUPOLD(99),DLWOLD(99),CDF
39. COMMON/IPT1/XIBDLY,RDEL,RDELFN,RCPB,SP,XSEP,CONV,CPB,XMON,XLSEP,
40. 1 MITER,LP,ITEUPC,ITELWC,XPC
41. 2,LBDLY,XLBDLY
42. COMMON/IPT2/IMASS
43. COMMON/SEICPS/CPSP0,RLAX
44. COMMON/IPT3/ISIDE,ILAM,RADUS
45. C***** ADDITION *****
46. COMMON/SEITRP/LSEP,LSEP1
47. COMMON/VORTEX/VORCIR,IVLOC,XV,YV,IVOR,JVOR
48. C*****
49. NAMELIST/FINP/M,W,X1,X2,ALP,EPS,EPSS,X4,S4,CONV,A1,A2,A3,RN,
50. 1 XIBDLY,CIR,CDCORR,RDEL,RDELFN,SP,XSEP,RCPB,CPB,XMON,XLSEP,XPC
51. 3,XLBDLY,RLAX,RADUS
52. 4,CLALP,VORCIR,XV,YV
53. NAMELIST/IINP/IMAX,JMAX,IKASE,INV,MITER,NHALF,ITACT,ISKP2,ISKP3,
54. 1 ISKP4,ITERP,IREAD,LP,ITEUPC,ITELWC
55. 2,IMASS,ILAM
56. 2,IPRT1,IPRT2
57. DELTAY=0.0
58. CPSP0=0.0
59. CDF=0.
60. CDCORR=0.0

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61. DPM=0.0
62. ITER=0
63. MHALF=1
64. IW=0
65. CIR=0.0
66. DPMSUM=0.0
67. IDPM=1
68. DPOLD=0.0
69. M=0.5
70. W=1.7
71. X1=0.5
72. X2=10000.0
73. IPRT1=0
74. IPRT2=0
75. ILAM=0
76. RADUS=0.035
77. ALP=0.0
78. EPS=0.0
79. EPSS=0.4
80. X4=0.49
81. S4=2.0
82. A1=0.246
83. A2=0.15
84. A3=3.87
85. RN=20.OE+06
86. XIBDLY=-.44
87. XLBDLY=-.44
88. CPB=0.4
89. RDEL=0.25
90. RDELFN=0.125
91. RLAX=1.0
92. SP=0.004
93. CLALP=.10966
94. XSEP=0.44
95. XLSEP=0.50
96. RCPB=0.2
97. XMON=0.47
98. CONV=1.E-05
99. IMAX=13
100. JMAX=7
101. IKASE=100
102. INV=0
103. MITER=800
104. NHALF=0
105. ITACT=0
106. IMASS=0
107. ISKP2=0
108. ISKP3=0
109. ISKP4=0
110. IITERP=0
111. IREAD=0
112. LP=1000
113. ITEUPC=0
114. ITELWC=0
115. XPC=0.10
116. VORCIR=0.0
117. IVLOC=0

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C+***** ADDITION *****
DO 50 I=1,99
50 CPU(I)=0.0
C+*****

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122. READ(5,1)(NTITLE(I),I=1,20)
123. 1 FORMAT(20A4)
124. PRINT 2
125. 2 FORMAT(1H1)
126. READ(5,FINP)
127. EPSSO=EPSS
128. EPSO=EPS
129. BETA=SQRT(1.-M*M)
130. READ(5,IINP)
131. ICASE=IKASE
132. 8001 CONTINUE
133. ALPDEG=ALP
134. CPSTAR=1.428/(M*M)*(((1.+0.2*M*M)/1.2)**3.5-1.)
135. PI=4.*ATAN(1.0)
136. PI2=0.5*PI
137. ALP=ALP*PI/180.
138. A22=2./(PI*A2)
139. A11=2./(PI*A1)
140. CALL VALUE
141. 101 PRINT 3,(NTITLE(I),I=1,20)
142. 3 FORMAT(20A4)
143. CALL COORD
144. IF (ABS(VORCIR).LT.0.001) GO TO 630
145. 605 DO 610 I=2,IMAX1
146. IF (XV.LT.X(I)) GO TO 615
147. 610 CONTINUE
148. 615 IVOR=I-1
149. DO 620 J=2,JMAX1
150. IF (YV.LT.Y(J)) GO TO 625
151. 620 CONTINUE
152. 625 JVOR=J-1
153. IVLOC=1
154. IF (YV.LT.O.O) IVLOC=-1
155. IVORP1=IVOR+1
156. JVORP1=JVOR+1
157. IF (MHALF.EQ.1) GO TO 750
158. IF (IVLOC.EQ.-1) GO TO 730
159. IF ((IVOR/2-IVOR/2.+1).GT.O.O) GO TO 722
160. DO 714 J=JVORP1,JMAX
161. P(IVORP1,J)=P(IVORP1,J)-VORCIR/2.
162. IF ((JVOR/2-JVOR/2.+1).GT.O.O) P(IVORP1,JVOR)=P(IVORP1,JVOR)
163. 1-VORCIR/4.
164. GO TO 750
165. 722 DO 724 J=JVORP1,JMAX
166. P(IVOR,J)=P(IVOR,J)+VORCIR/2.
167. IF ((JVOR/2-JVOR/2.+1).GT.O.O) P(IVOR,JVOR)=P(IVOR,JVOR)
168. 1+VORCIR/4.
169. GO TO 750
170. 730 IF ((IVOR/2-IVOR/2.+1).GT.O.O) GO TO 742
171. DO 734 J=1,JVOR
172. P(IVORP1,J)=P(IVORP1,J)+VORCIR/2.
173. IF ((JVOR/2-JVOR/2.+1).LT.O.O) P(IVORP1,JVORP1)=
174. 1P(IVORP1,JVORP1)+VORCIR/4.
175. GO TO 750
176. 742 DO 744 J=1,JVOR
177. P(IVOR,J)=P(IVOR,J)-VORCIR/2.
178. IF ((JVOR/2-JVOR/2.+1).LT.O.O) P(IVOR,JVORP1)=P(IVOR,JVORP1)
179. 1-VORCIR/4.
180. 750 PRINT 617,IVOR,JVOR,VORCIR
181. 617 FORMAT(1H,IVOR=',I2,5X,JVOR=',I2,5X,VORCIR=',F10.6)
182. 630 PRINT 6,M,ALPDEG,X1,ICASE

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183. 6 FORMAT(1H0.3X,'MACH NO. IS ',F5.3,' ANGLE OF ATTACK IS ',F9.3,' DE00000112
184. 1GREES',/,10X,' DIRECT SOLUTION TO ',F8.2,
185. 225X,'CASE NUMBER',I6)
186. IF(INV.EQ.0)PRINT 6001
187. 6001 FORMAT(1H0.3X,'INVISCID ANALYSIS CASE')
188. IF(ITACT.EQ.1)PRINT 6002
189. 6002 FORMAT(1H.3X,'WITH VISCOUS INTERACTION')
190. IF(INV.EQ.1)PRINT 6003
191. 6003 FORMAT(1H0.3X,'INVERSE DESIGN CASE')
192. IF(IMASS.EQ.1) PRINT 6005
193. 6005 FORMAT(1H.3X,'AND MASSIVE SEPARATION')
194. IF(IMASS.EQ.0)GO TO 6000
195. SPP=0.0
196. ALPNU=0.0
197. ALPT=ALPDEG
198. IF(ALPDEG.LE.15.3) GO TO 6006
199. ALPNU=ALPT-15.3
200. ALPT=15.3
201. 6006 SP=-7.14352E-05*ALPT+(0.0142857*CLALP+0.004714337)
202. IF(ALPDEG.LE.15.3) GO TO 6008
203. SPP=(-8.4074E-11*RN+2.1707E-04)*ALPNU
204. SP=SP+SPP
205. 6008 CONTINUE
206. IF(SP.GT.0.0055) SP=0.0055
207. IF(SP.LT.0.004) SP=0.004
208. PRINT 6007,SP
209. 6007 FORMAT(1H.3X,'SP PARAMETER VALUE IS CALCULATED TO BE ',F10.5)
210. 6000 CONTINUE
211. WRITE(6,F10P)
212. WRITE(6,I1NP)
213. IF(MHALF.EQ.1)GO TO 102
214. JB=JMAX/2+1
215. DO 104 I=ILE,IMAX
216. P(1,JB-1)=0.5*(P(I,JB-2)+PB(I))
217. P(IMAX,JMAX-1)=P(IMAX,JMAX-2)
218. P(IMAX-1,JMAX)=P(IMAX-2,JMAX)
219. P(2,JMAX)=P(3,JMAX)
220. P(1,JMAX-1)=P(1,JMAX-2)
221. P(1,2)=P(1,3)
222. P(2,1)=P(3,1)
223. P(IMAX-1,1)=P(IMAX-2,1)
224. P(IMAX,2)=P(IMAX,3)
225. 102 CONTINUE
226. ILE1=ILE-1
227. I11=I1-1
228. ITE=IMAX-ILE1
229. ITE1=ITE+1
230. CALL FOIL
231. IF(ITREAD.EQ.1.AND.MHALF.EQ.1)MHALF=MHALF+1
232. 7 DO 8 J=1,JMAX
233. 8 P1(J)=P(1,J)
234. CALL FLOW1
235. CALL FLOW2
236. IF(MHALF.EQ.1) GO TO 9
237. IF(IMASS.EQ.1)GO TO 5001
238. IF(INV.EQ.0) GO TO 9
239. GO TO 5002
240. 5001 IF(MHALF.GT.2.OR.ITER.GT.50)GO TO 5002
241. GO TO 9
242. 5002 IF(I1.GT.ITE) GO TO 9
243. CALL FLOW3

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244. IF(X2.GT.1000.0)GO TO 10
245. 9 CALL WAKE
246. 10 STE=S4+2./PI*ATAN((O.5-X4)/A2)
247. CIR=(STE-S(ITE+1))/DS*(P(ITE,JB)-PB(ITE))+ (STE-S(ITE))/DS+
248. 1(P(ITE+1,JB)-PB(ITE+1))
249. IF(IMASS.EQ.O)GO TO 1441
250. JB2=JB-1
251. DO 1442 J=JB2, JMAX1
252. IF(YU(ITE).GT.E(J).AND.YU(ITE).LE.E(J+1))GO TO 1443
253. 1442 CONTINUE
254. 1443 JA=J+1
255. IF(JA.LE.JB)JA=JB+1
256. PHITE=P(ITE,JA-1)+(P(ITE,JA)-P(ITE,JA-1))*(YU(ITE)-E(JA-1))/DE
257. 1441 CONTINUE
258. QUAN1=-.5*CIR/PI
259. QUAN2=ATAN(BETA*A1/A2*DS/DE)
260. QUAN3=ATAN(BETA*TAN(ALP))
261. IF(M.GT.1.)GO TO 11
262. IF(ALP.GT.O.O)GO TO 108
263. IF(ALP.LT.O.O)GO TO 1081
264. P(IMAX, JMAX)=QUAN1*QUAN2
265. DO 12 I=2, IMAX1
266. P(I, JMAX)=- CIR/4.O
267. 12 P(I, 1)=-O.75*CIR
268. P(1, JMAX)=QUAN1*(PI-QUAN2)
269. P(1, 1)=QUAN1*(PI+QUAN2)
270. P(IMAX, 1)=QUAN1*(2.*PI-QUAN2)
271. DO 13 J=2, JMAX1
272. 13 P(1, J)=-O.5*CIR
273. JBM1=JB-1
274. DO 14 J=2, JBM1
275. 14 P(IMAX, J)=-CIR
276. DO 1414 J=JB, JMAX1
277. 1414 P(IMAX, J)=O.O
278. GO TO 109
279. 1081 DO 1083 I=2, IMAX1
280. P(I, JMAX)=QUAN1*(PI+ATAN(BETA/TAN(ALP)))
281. 1083 P(I, 1)=QUAN1*PI+P(I, JMAX)
282. GO TO 1082
283. 108 DO 110 I=2, IMAX1
284. P(I, JMAX)=QUAN1*ATAN(BETA/TAN(ALP))
285. 110 P(I, 1)=QUAN1*PI+P(I, JMAX)
286. 1082 CONTINUE
287. DO 111 J=2, JMAX1
288. 111 P(1, J)=QUAN1*(PI-QUAN3)
289. JBM1=JB-1
290. DO 112 J=2, JBM1
291. 112 P(IMAX, J)=QUAN1*(2.*PI-QUAN3)
292. DO 113 J=JB, JMAX1
293. 113 P(IMAX, J)=QUAN1*(-QUAN3)
294. P(IMAX, JMAX)=QUAN1*QUAN2
295. P(1, JMAX)=QUAN1*(PI-QUAN2)
296. P(1, 1)=QUAN1*(PI+QUAN2)
297. P(IMAX, 1)=QUAN1*(2.*PI-QUAN2)
298. 109 CONTINUE
299. IF (IVLOC.NE.O) CALL VORBCI(BETA, QUAN2, QUAN3)
300. PB(IMAX)=-CIR+P(IMAX, JB)
301. 11 ITER=ITER+1
302. DPMSUM=DPMSUM+DPM
303. IDPM=IDPM+1
304. IF(IDPM.LE.10)GO TO 512
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305. DPOLD=DPMSUM
306. DPMSUM=0.0
307. IDPM=1
308.
309. 512 CONTINUE
310. IF(IMASS.EQ.1)DELTAY=YU(ITE)-YUORIG(ITE)
311. IF(IMASS.EQ.1)GO TO 5003
312. IF(ITACT.EQ.1)DELTAY=DUPOLD(ITE)
313. IF(ITER/10*10.EQ.ITER)
314. 1PRINT 15,ITER,CIR,DPM,ICON,JCON,NSSP,DELTAY
315. 15 FORMAT(1H,' ITERATION',I4,' CIR =',F8.5,' DPM =',F11.8,' AT',
316. 12I3,' NSSP =',I4,' DELTAY OR DELSTAR =',F7.4)
317. IF(M.LE.1.0)GO TO 16
318. C ADD P(IMAX,J) CARD HERE FOR M GT 1.0 CASE
319. 16 IF(INV.EQ.0.AND.ITACT.EQ.0)GO TO 24
320. IF(MHALF.EQ.1)GO TO 24
321. IF(ITER.LT.50)GO TO 24
322. IF(ITACT.EQ.1)GO TO 9005
323. IF(MHALF.EQ.2.AND.ISKP2.EQ.1)GO TO 24
324. IF(MHALF.EQ.3.AND.ISKP3.EQ.1)GO TO 24
325. IF(MHALF.EQ.4.AND.ISKP4.EQ.1)GO TO 24
326. IF(ITER/10*10.EQ.ITER)CALL SHAPE
327. GO TO 9006
328. 9005 IF(ITER/10*10.EQ.ITER)CALL VISACT
329. C*****ADDITION*****
330. IF(ITER/10*10.EQ.ITER.AND.IMASS.EQ.1) LSEP1=LSEP
331. C*****
332. IF(MHALF.EQ.2.AND.ITER.LE.50)GO TO 9006
333. IF(ITER/10*10.EQ.ITER.AND.IMASS.EQ.1)CALL SHAPE
334. IF(IMASS.EQ.0)GO TO 9006
335. DO 9112 I=1,ITE
336. IF(YU(I).GE.0.0)GO TO 9112
337. YU(I)=YU(I-1)
338. SLU(I)=0.0
339. 9112 CONTINUE
340. IF(ITER/LP*LP.EQ.ITER)PRINT22,(X(I),YU(I),YL(I),I=ILE,IMAX1)
341. IF(ITER/LP*LP.EQ.ITER)PRINT 22,(X(I),SLU(I),SLL(I),I=ILE,IMAX1)
342. 24 CONTINUE
343. IF(ITER.GE.MITER)GO TO 17
344. IF(INV.EQ.0.AND.ITACT.EQ.0)GO TO 106
345. IF(MHALF.GT.1)GO TO 106
346. IF(MHALF.EQ.1.AND.ITER.LT.50)GO TO 106
347. DPM=0.
348. 106 CONTINUE
349. IF(DPM.LT.CONV)GO TO 17
350. 21 DPM=0.0
351. GO TO 7
352. 17 CONTINUE
353. C *** THE FOLLOWING CAN BE USED TO PRINT OUT THE *****
354. C *****PERTURBATION POTENTIAL FLOWFIELD SOLUTION IF DESIRED*****
355. IF(IPRT1.EQ.0)GO TO 3776
356. DO 18 JJ=1,UMAX
357. J=JMAX+1-JJ
358. PRINT 19,J
359. 19 FORMAT(1H,'ROW',I5)
360. PRINT 20,(P(I,J),I=1,IMAX)
361. 20 FORMAT(1H,'10E11.3)
362. 18 CONTINUE
363. PRINT 19,JB
364. PRINT 20,(PB(I),I=1,IMAX)
365. 3776 CONTINUE

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366. IF (MHALF.LE.NHALF)GO TO 8007
367. C ***** THE FOLLOWING CA BE USED TO PUNCH OUTPUT IF DESIRED*****
368. C DO 8005 JJ=1,JMAX
369. C8006 FORMAT(5E15.7)
370. C J=JMAX-JJ+1
371. C8005 CONTINUE
372. C8007 CONTINUE
373. C PRINTE SHAPE HERE IF REQUIRED
374. IF (MHALF.EQ.1)GO TO 26
375. IF (INV.EQ.1)CALL SHAPE
376. IF (ITACT.EQ.0)GO TO 26
377. IF (ITER.GE.MITER)GO TO 7501
378. CALL VISACT
379. C ***** ADDITION *****
380. IF (IMASS.EQ.1)LSEP1=LSEP
381. C *****
382. IF (IMASS.EQ.1)CALL SHAPE
383. 7501 PRINT 9008,RN
384. 9008 FORMAT('O','BOUNDARY LAYER ANALYSIS FOR REYNOLDS NUMBER OF',E12.3,00000285
385. *//,'5X','X','9X','YUORIG','4X','DU','8X','SLU','7X','YLORIG','4X','DL','8X','SLL00000286
386. *')
387. PRINT 9009,(X(I),YUORIG(I),DUOLD(I),SLU(I),YLORIG(I),DLWOLD(I),
388. *SLL(I),I=ILE,ITE)
389. 9009 FORMAT(5X,7F10.5)
390. GO TO 9007
391. 26 CALL PRESS
392. 9007 DO 25 I=ILE,IMAX1
393. YU(I)=A1*TAN(PI/2.*YU(I))
394. 25 YL(I)=A1*TAN(PI/2.*YL(I))
395. PRINT 6004
396. 6004 FORMAT(1H,' CP BY CENTRAL DIFFERENCES')
397. PRINT 9010
398. 9010 FORMAT(1H,'X',10X,'CPU',10X,'CPL')
399. PRINT 9011,(X(I),CPU(I),CPL(I),I=ILE,IMAX1)
400. 9011 FORMAT(1H,'3F10.3)
401. IMAX2=IMAX-2
402. PRINT 221
403. 221 FORMAT(1H,'X',10X,'YU',10X,'YL',10X,'SLU',8X,'SLL')
404. 22 FORMAT(3,'X','F7.4','YU='F7.4','YL='F7.4)
405. PRINT 220,(X(I),YU(I),YL(I),SLU(I),SLL(I),I=ILE,ITE)
406. 220 FORMAT(1H,'5F10.5)
407. IF (MHALF.LE.NHALF)GO TO 8014
408. 8014 CONTINUE
409. DO 9002 I=ILE,ITE
410. YU(I)=ATAN(YU(I)/A1)/PI2
411. YL(I)=ATAN(YL(I)/A1)/PI2
412. NMACH=2
413. JL=2
414. JU=JMAX1
415. JDUM=JMAX-2
416. IF (JDUM.LE.43)GO TO 513
417. NMACH=1
418. JU=JB
419. 513 CONTINUE
420. PRINT 514
421. 514 FORMAT(/,'.38X','MACH CHART IN COMPUTATIONALNIONAL
422. *PLANE-FREE STREAM FROM TOP',/)
423. PRINT 515,IMAX1
424. 515 FORMAT(3X,'I=2','I2,' TOP TO BOTTOM',/)
425. PRINT 516,IL,JU
426. 516 FORMAT(3X,'J='I2,1H,.,I2,' LEFT TO RIGHT',/)

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427. DO 500 I=2,ILE1
428. DO 501 J=2,JMAX1
429. U=QI*(COS(ALP)+FF(I)*(P(I+1,J)-P(I-1,J))/(2.*DS))
430. IF (IVLOC.EQ.O) GO TO 691
431. IF (I.NE.IVOR.AND.I.NE.(IVOR+1)) GO TO 691
432. IF (IVLOC.EQ.1.AND.J.GT.JVOR.OR.IVLOC.EQ.-1.AND.J.LE.JVOR)
433. U=U+IVLOC*QI*FF(I)*VORCIR/2./DS
434. V=QI*(SIN(ALP)+GG(J)*(P(I,J+1)-P(I,J-1)))/(2.*DE))
435. UU=U*U
436. VV=V*V
437. AD=A12-O.2*(UU+VV-QI2)
438. UVEL(J)=U
439. VVEL(J)=V
440. IONIC(J)=100.O*SQRT((UU+VV)/AD)
441. PRINT 28,(IONIC(J),J=JL,JU)
442. IF(IPRT2.EQ.O) GO TO 500
443. PRINT 2878,(UVEL(J),J=2,JMAX1)
444. PRINT 2878,(VVEL(J),J=2,JMAX1)
445. FORMAT(1H,15F8.1)
446. 500 CONTINUE
447. DO 502 I=1LE,ITE
448. DO 503 J=2,JMAX1
449. UVEL(J)=O.O
450. VVEL(J)=O.O
451. IONIC(J)=O
452. JB2=JB-2
453. DO 504 J=JB2,JMAX1
454. IF(YU(I).GT.E(J).AND.YU(I).LE.E(J+1))GO TO 505
455. 504 CONTINUE
456. 505 JA=J+1
457. IF(JA.LE.JB)JA=JB+1
458. DO 506 J=JA,JMAX1
459. U=QI*(COS(ALP)+FF(I)*(P(I+1,J)-P(I-1,J))/(2.*DS))
460. IF (IVLOC.EQ.O) GO TO 692
461. IF (I.NE.IVOR.AND.I.NE.(IVOR+1)) GO TO 692
462. IF (IVLOC.EQ.1.AND.J.GT.JVOR.OR.IVLOC.EQ.-1.AND.J.LE.JVOR)
463. U=U+IVLOC*QI*FF(I)*VORCIR/2./DS
464. V=QI*(SIN(ALP)+GG(J)*(P(I,J+1)-P(I,J-1)))/(2.*DE))
465. UU=U*U
466. VV=V*V
467. AD=A12-O.2*(UU+VV-QI2)
468. UVEL(J)=U
469. VVEL(J)=V
470. IONIC(J)=100.O*SQRT((UU+VV)/AD)
471. JB2=JB+2
472. DO 507 JJ=1,JMAX1
473. J=JB2-JJ
474. IF(YL(I).GE.E(J).AND.YL(I).LT.E(J+1))GO TO 508
475. 507 CONTINUE
476. 508 JA=J
477. IF(JA.GE.JB)JA=JB-1
478. DO 509 J=2,JA
479. U=QI*(COS(ALP)+FF(I)*(P(I+1,J)-P(I-1,J))/(2.*DS))
480. IF (IVLOC.EQ.O) GO TO 693
481. IF (I.NE.IVOR.AND.I.NE.(IVOR+1)) GO TO 693
482. IF (IVLOC.EQ.1.AND.J.GT.JVOR.OR.IVLOC.EQ.-1.AND.J.LE.JVOR)
483. U=U+IVLOC*QI*FF(I)*VORCIR/2./DS
484. V=QI*(SIN(ALP)+GG(J)*(P(I,J+1)-P(I,J-1)))/(2.*DE))
485. IF(J.EQ.(JB-1))V=QI*(SIN(ALP)+GG(J)*(PB(I)-P(I,J-1)))/(2.*DE))
486. UU=U*U
487. VV=V*V
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488. AD=AI2-0.2*(UU+VV-QI2)
489. UVEL(J)=U
490. VVEL(J)=V
491.
492. 509 IONIC(J)=100.0*SQR((UU+VV)/AD)
493. PRINT 28,(IONIC(J),J=JL,JU)
494. IF(IPRT2.EQ.0) GO TO 502
495. PRINT 2878,(UVEL(J),J=2,JMAX1)
496. PRINT 2878,(VVEL(J),J=2,JMAX1)
497. 502 CONTINUE
498. DO 510 I=ITE1,IMAX1
499. DO 511 J=2,JMAX1
500. U=Q1*(COS(ALP)+FF(I)*P(I+1,J)-P(I-1,J))/(2.*DS))
501. IF (IVLOC.EQ.0) GO TO 694
502. IF (I.NE.IVOR.AND.I.NE.(IVOR+1)) GO TO 694
503. IF (IVLOC.EQ.1.AND.J.GT.JVOR.OR.IVLOC.EQ.-1.AND.J.LE.JVOR)
504. 1U=U+IVLOC*QI*FF(I)+VORCIR/2./DS
505. V=Q1*(SIN(ALP)+GG(J)*P(I,J+1)-P(I,J-1))/(2.*DE))
506. IF (J.EQ.JB)V=V-QI*(GG(J)*(CIR/(2.*DE)))
507. U=U+U
508. V=V+V
509. AD=AI2-0.2*(UU+VV-QI2)
510. UVEL(J)=U
511. VVEL(J)=V
512. 511 IONIC(J)=100.0*SQR((UU+VV)/AD)
513. PRINT 28,(IONIC(J),J=JL,JU)
514. IF(IPRT2.EQ.0) GO TO 510
515. PRINT 2878,(UVEL(J),J=2,JMAX1)
516. PRINT 2878,(VVEL(J),J=2,JMAX1)
517. 510 CONTINUE
518. 28 FORMAT(1H,4O13)
519. IF(NMACH.EQ.2)GO TO 519
520. NMACH=NMACH+1
521. JL=JB
522. JU=JMAX1
523. JDUM=JU-JL-42
524. IF(JDUM.GT.0)JU=JL+42
525. GO TO 513
526. 519 CONTINUE
527. DO 9003 I=ILE,ITE
528. YU(I)=A1*TAN(PI/2.*YU(I))
529. YL(I)=A1*TAN(PI/2.*YL(I))
530. CL=0.5*(CPL(ILE)-CPU(ILE))*X(ILE)+0.5)
531. CPSTAG=2./(1.4*M*M)*(1.+0.2*M*M)**3.5-1.)
532. CD=(CPSTAG+CPU(ILE))*(YU(ILE))*O.5-(CPSTAG+CPL(ILE))*(YL(ILE))*O.500000374
533. CML=0.5*(CPU(ILE)-CPL(ILE))*X(ILE)+0.5)**2
534. IEND=ITE-1
535. DO 9000 I=ILE,IEND
536. T1=CPL(I)-CPU(I)
537. T2=CPL(I+1)-CPU(I+1)
538. T3=(X(I+1)-X(I))*O.5
539. CL=CL+(T1+T2)*T3
540. IF(ITACT.EQ.1)GO TO 8010
541. CD=CD+(CPU(I)+CPU(I+1))*O.5*(YU(I+1)-YU(I))-(CPL(I)+CPL(I+1))*O.5
542. 1*(YL(I+1)-YL(I))
543. GO TO 8011
544. CD=CD+(CPU(I)+CPU(I+1))*5*(YUORIG(I+1)-YUORIG(I))-(CPL(I)+CPL(I+1)+CPU(I+1)
545. *)*5*(YLORIG(I+1)-YLORIG(I))
546. 8011 CONTINUE
547. T6=-T1*(X(I)+0.5)
548. T7=-T2*(X(I+1)+0.5)

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549. 9000 CMLE=CMLE+(T6+T7)*T3
550. CL=CL+O.5*(CPL(ITE)-CPU(ITE))*(O.5-X(ITE))
551. CMLE=CMLE+O.5*(CPU(ITE)-CPL(ITE))*(X(ITE)+O.5)*(O.5-X(ITE))
552. IF(ITACT.EQ.1)GO TO 8012
553. CD=CD-(CPU(ITE)+CPL(ITE))*O.5*(YU(ITE)-YL(ITE))
554. GO TO 8013
555. CD=CD-CD CORR
556. 8012 CONTINUE
557. FN=CL*COS(ALP)-CD*SIN(ALP)
558. FT=CL*SIN(ALP)+CD*COS(ALP)
559. CL=FN
560. CD=FT
561. CMC4=CMLE+CL/4.
562. CDWAV=CD
563. CD=CDWAV+CDF
564. PRINT 9012,CDWAV
565. 9012 FORMAT(1H0.20X,'WAVE CD = ',F10.6)
566. NOV=ITE-ILE+1
567. DO 114 I=ILE,ITE
568. J=I-ILE+1
569. J1=J+NOV
570. J2=J+2*NOV
571. J3=J+3*NOV
572. J4=J+4*NOV
573. AA(J)=X(I)
574. AA(J1)=CPU(I)
575. AA(J2)=CPL(I)
576. AA(J3)=-YU(I)
577. AA(J4)=-YL(I)
578. NL=50
579. IF(NOV.GT.45)NL=100
580. CALL PLOT(ICASE,AA,NOV,5,NL,O)
581. CLCIR=2.*CIR
582. PRINT 8002,CPSTAR,CLCIR
583. 8002 FORMAT(1H ,40X,'PRESSURE COEFFICIENT',///,41X,'CPSTAR = ',F10.4,
584. 1 5X,'CLCIR = ',F10.4)
585. PRINT 9001,CL,CD,CMLE,CDF,CMC4
586. 9001 FORMAT(1H0.20X,'CL = ',F10.4,' CD = ',F10.6,' CMLE = ',F10.4,
587. *' CDF = ',F10.6,' CMC4 = ',F10.4)
588. C***** ADDITION *****
589. XUSEP=X(ITE)
590. IF(MHALF.EQ.1)GO TO 9051
591. IF(INV.EQ.1)GO TO 9051
592. IF(ITACT.EQ.0)GO TO 9051
593. IF(IMASS.EQ.0)LSEP=LSEP1
594. IF(MHALF.GT.1.AND.ITACT.NE.0)XUSEP=X(LSEP)
595. PRINT 9050,XUSEP
596. 9050 FORMAT('OXUSEP = ',F10.5)
597. C*****
598. 9051 PRINT 8003
599. 8003 FORMAT(1H1)
600. IF(MHALF.GT.NHALF)GO TO 100
601. MHALF=MHALF+1
602. MITER=MITER/2
603. CALL HALVE
604.
605. IF(INV.EQ.1.AND.MHALF.EQ.3)MITER=400
606. IF(IMASS.EQ.1.AND.MHALF.EQ.3)MITER=400
607. IF(MHALF.EQ.4)MITER=400
608.
609. DPM=O.O

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610. DPOLD=0.0
611. IDPM=1
612. DPMSUM=0.0
613. EPSS=EPSSO
614. EPS=EPSO
615. ITER=0
616. DELTAY=0.0
617. GO TO 101
618.
619. 100 CONTINUE
620. IF(INV.EQ.1)CALL BDLY
621. IF(ITACT.EQ.1)GO TO 9014
622. WRITE(7,9015)(X(I),YU(I),YL(I),CPU(I),CPL(I),I=ILE,ITE)
623. 9015 FORMAT(5F10.5)
624. STOP
625. 9014 WRITE(7,9015)(X(I),YUORIG(I),YLORIG(I),CPU(I),CPL(I),I=ILE,ITE)
626. STOP
627. END
628. SUBROUTINE FOIL
629. C ***** READS IN INITIAL AIRFOIL SHAPE AND DETERMINES ORDINATES
630. C ***** AND SLOPES AT COMPUTATIONAL GRID POINTS *****
631. REAL M
632. DIMENSION XI(99),YI(99),X0(99),Y0(99),SI(99),SO(99),XP(99),YP(99),
633. 1D1Y(99),D2Y(99),D3Y(99),XIB(99),YIB(99)
634. DIMENSION XOR(99)
635. COMMON CPU(99),CPL(99),E(99),DU1(99),DU2(99),DL1(99),DL2(99),D(99)
636. 1,FF(99),FFP12(99),FFM12(99),FFM1(99),FFM32(99),
637. 1P1(99),P2(99),PB(99),P(99,99),RS(99),S(99),SUP(99),SUB(99),TEMP(99)
638. 2),X(99),Y(99),YU(99),YL(99),SLU(99),SLL(99),
639. 3A1,A2,AI2,ALP,CIR,EPS,EPSS,DE,DS,DP,DPM,F,FP12,FM12,FM32,M,QI,QI2,
640. 4W,X1,X2,VVUB,VVJB1,AAJB1,AAJB,QQJB,QQJB1,UUJB,VVJBP1,QQJBP1,AAJBP1
641. 5,Q,QQ,UUJB1,PI,PI2,A22,A11,X4,S4
642. COMMON I,ITE,ITE1,ILE,ILE1,I1,I11,ICON,IMAX,INV,JB,JA1,JB1,
643. 1JMAX,JCON,JMAX1,NSSP,IW
644. COMMON/FIX/MHALF
645. COMMON/RED/ITERP
646. COMMON/FIPUT/IREAD
647. COMMON/NASH/RN,IBDLY,ITACT,YUORIG(99),YLORIG(99),SUPPER(99),SLOWER
648. 1(99),DEL(99),DUPOLD(99),DLWOLD(99),DLWOLD(99),CDF
649. COMMON/IPT1/XIBDLY,RDEL,RDELFN,RCPB,SP,XSEP,CONV,CPB,XMON,XLSEP,
650. 1 MITER,LP,ITEUPC,ITELWC,XPC
651. 2,IBDLY,XLBDLY
652. C THIS PROGRAM DEPENDS UPON AIRFOIL BEING STUDIED
653. PRINT 2
654. 2 FORMAT(1HO,2OX,'AIRFOIL COORDINATES',/,5X,'X YL
655. 1 UPPER SLOPE LOWER SLOPE')
656. IBDLY=ILE-1
657. 215 IBDLY=IBDLY+1
658. IF(X(IBDLY).LT.XIBDLY)GO TO 218
659. LBDLY=ILE-1
660. 218 LBDLY=IBDLY+1
661. IF(X(LBDLY).LT.XIBDLY)GO TO 218
662. IF(ITACT.EQ.1)GO TO 35
663. IF(INV.EQ.0)GO TO 7
664. 35 IF(MHALF.LE.2)GO TO 7
665. I=IMAX1/2
666. II=IMAX-2
667. ISTOP=I11
668. IF(ITACT.EQ.1)I11=IBDLY-1
669. CPU(II)=CPU(I)
670. CPL(II)=CPL(I)
671. SLU(II)=SLU(I)

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671. SLL(II)=SLL(I)
672. DUPOLD(II)=DUPOLD(I)
673. DLWOLD(II)=DLWOLD(I)
674. YU(II)=YU(I)
675. YL(II)=YL(I)
676. I=I-1
677. II=II-2
678. IF(II.GE.I11)GO TO 8
679. IMAX2=IMAX-2
680. IS=II+3
681. DO 9 I=IS,IMAX2,2
682. DUPOLD(I)=.5*(DUPOLD(I+1)+DUPOLD(I-1))
683. DLWOLD(I)=.5*(DLWOLD(I+1)+DLWOLD(I-1))
684. CPU(I)=0.5*(CPU(I+1)+CPU(I-1))
685. CPL(I)=0.5*(CPL(I+1)+CPL(I-1))
686. SLU(I)=0.5*(SLU(I+1)+SLU(I-1))
687. SLL(I)=0.5*(SLL(I+1)+SLL(I-1))
688. YU(I)=0.5*(YU(I+1)+YU(I-1))
689. YL(I)=0.5*(YL(I+1)+YL(I-1))
690. YU(IMAX1)=0.0001
691. YL(IMAX1)=-0.0001
692. SLL(IMAX1)=0.0
693. SLL(IMAX1)=0.0
694. DUPOLD(IMAX1)=0.
695. DLWOLD(IMAX1)=0.
696. I11=ISTOR
697. GO TO 10
698.
699. 7 CONTINUE
700. DO 6 I=ITE1,IMAX
701. YUORIG(I)=.0001
702. YLORIG(I)=-0.0001
703. DUPOLD(I)=0.
704. DLWOLD(I)=0.
705. YU(I)=0.0001
706. YL(I)=-0.0001
707. SLU(I)=0.0
708. 6 SLL(I)=0.0
709. 10 IF(INV.EQ.1)IEND=I11
710. IF(INV.EQ.0)IEND=ITE
711. IF(MHALF.LT.3)IEND=ITE
712. C UPPER SURFACE,XI IN PERCENT CHORD
713. IF(MHALF.GT.1)GO TO 21
714. READ 14,NI
715. READ 15,(XI(I),YI(I),I=1,NI)
716. READ15,DERIX,DERIV,DERFX,DERFY
717. 14 FORMAT(I5)
718. DO 18 I=1,NI
719. XI(I)=XI(I)-0.5
720. II=I-ILE+1
721. 15 FORMAT(8F10.4)
722. 15 FORMAT(2F10.4)
723. 16 X0(II)=X(I)
724. NO=IEND-ILE+1
725. CALL ARC(XI,YI,X0,Y0,SI,SO,XP,YP,D1Y,D2Y,D3Y,DERIX,DERFX,DERIV,DERFY)
726. 1DERFY,NI,NO,1)
727. IF(ITACT.EQ.1)GO TO 23
728. DO 17 I=ILE,IEND
729. II=I-ILE+1
730. DUPOLD(I)=0.
731. YU(I)=YU(II)

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793. C      YUORIG(I)=YU(I)
794. PRINT 3, X(I), YU(I), YL(I), SLU(I), SLL(I)
795. 3 FORMAT(5F10.5)
796. 1 CONTINUE
797. C      FINDING COORDS IN ETA-PSI SYSTEM
798. DO 4 I=ILE,IMAX1
799. YU(I)=ATAN(YU(I)/A1)/PI2
800. 4 YL(I)=ATAN(YL(I)/A1)/PI2
801. IF(INV.EQ.0)RETURN
802. IF(IREAD.EQ.1.AND.MHALF.EQ.1)GO TO 103
803. IF(MHALF.EQ.1)RETURN
804. IF(MHALF.GT.3.AND.ITERP.EQ.1)GO TO 100
805. 103 CONTINUE
806. READ(5,5)(CPU(I),I=11,ITE)
807. CPU(I11)=0.0
808. READ(5,5)(CPL(I),I=11,ITE)
809. CPL(I11)=0.0
810. ITEP1=ITE+1
811. DO 339 I=ITEP1,IMAX
812. CPU(I)=0.
813. 339 CPL(I)=0.
814. 5 FORMAT(8F10.3)
815. 100 CONTINUE
816. PRINT 101
817. 101 FORMAT(1H0,20X,'UPPER CP INPUT')
818. PRINT 5,(CPU(I),I=11,ITE)
819. PRINT 102
820. 102 FORMAT(1H0,20X,'LOWER CP INPUT')
821. PRINT 5,(CPL(I),I=11,ITE)
822. RETURN
823. END
824. SUBROUTINE VISACT
825. C
826. C ***** COMPUTES BOUNDARY LAYER WHEN VISCOUS INTERACTION INCLUDED
827. C ***** IN THE ANALYSIS CASE *****
828. C
829. REAL M,NEW
830. INTEGER SEPMK
831. COMMON CPU(99),CPL(99),E(99),DU1(99),DU2(99),DL1(99),DL2(99),D(99)
832. 1,FF(99),FFP12(99),FFM12(99),FFM1(99),FFM32(99),
833. P1(99),P2(99),PB(99),P(99,99),RS(99),S(99),SUP(99),SUB(99),TEMP(99)
834. 2),X(99),Y(99),YU(99),YL(99),SLU(99),SLL(99),
835. 3A1,A2,AI2,ALP,CIR,EPS,EPSS,DE,DS,DP,DPM,F,FP12,FM12,FM32,M,QT,QI2,
836. 4W,X1,X2,VVJB,VVJB1,AAJB1,AAJB,QQJB,QQJB1,UUJB,VVJB1,AAJB1,
837. 5,Q,QQ,UUJB1,PI,PI2,A22,A11,X4,S4
838. COMMON I,ITE,ITE1,ILE,ILE1,I1,I11,ICON,IMAX,IMAX1,INV,JB,JA1,JB1,
839. 1JMAX,JCON,UMAX1,NSSP,IW
840. COMMON/NASH/RN,IBDLY,ITACT,YUORIG(99),YLORIG(99),SUPPER(99),SLOWER
841. 1(99),DEL(99),DUPOLD(99),DLWOLD(99),CDF
842. COMMON/DELTA/ITER
843. COMMON/IPT1/XIBDLY,RDEL,RDELFN,RCPB,SP,XSEP,CONV,CPB,XMON,XLSEP,
844. 1 MITER,LP,ITEUPC,ITELWC,XPC
845. 2,LEBLY,XLEBLY
846. COMMON/IPT2/IMASS
847. COMMON/FIX/MHALF
848. COMMON/SETCPS/CPSPD,RLAX
849. COMMON/IPT3/ISIDE,ILAM,RADUS
850. C *****
851. COMMON/SETRP/LSEP,LSEP1
852. C *****
853. DIMENSION UE(99),DSS(99),DUDS(99),YUN(99),YLN(99),EM(99)

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854. DIMENSION XI(99),YI(99),X0(99),Y0(99),SI(99),SO(99),XP(99),YP(99),O0000672
855. ID1Y(99),D2Y(99),D3Y(99),X1B(99),Y1B(99),X2B(99),Y2B(99),O0000673
856. DIMENSION HS(99),XOR(99)O0000674
857. DIMENSION CPUT(99),CPLT(99)O0000675
858. IF(MHALF.EQ.2.AND.ITER.LE.50)LSPOLD=ITEO0000676
859. IF(MHALF.GT.2.AND.ITER.LE.50)LSPOLD=LSPOLD*2-1O0000677
860. SEPMK=OO0000678
861. C*****ADDITION *****O0000678
862. LSEP1=ITE
863. C*****RDEL=RDLEFN *****O0000679
864. IF(IMAX.GT.55)RDEL=RDELFN
865. ISIDE=O
866. ICYCLE=1
867. ICYBOT=1
868. CALL PRESS
869. IF(DPM.LE.CONV)GO TO 5009
870. IF(ITER.GE.(MITER-1))GO TO 5009
871. GO TO 5005
872. DO 5006 J=ILE,IMAX1
873. CPUT(J)=CPUT(J)
874. CPLT(J)=CPL(J)
875. 5005 CONTINUE
876. JB2=JB-2
877. DO 3010 J=JB2,JMAX1
878. IF(YU(ITE).GT.E(J).AND.YU(ITE).LE.E(J+1))GO TO 3011
879. 3010 CONTINUE
880. 3011 JA=J+1
881. IF(JA.LE.JB)JA=JB+1
882. PHITE=P(ITE,JA-1)+(P(ITE,JA)-P(ITE,JA-1))*(YU(ITE)-E(JA-1))/DE
883. DO 500 J=ILE,ITE
884. YU(J)=A1*TAN(PI/2.*YU(J))
885. 500 YL(J)=A1*TAN(PI/2.*YL(J))
886. 5061 CONTINUE
887. TR=O.3424
888. TE1=5.E-03
889. TE2=5.E-05
890. LMON=IMAX1/2+1
891. 4001 LMON=LMON+1
892. IF(X(LMON).LT.XMON)GO TO 4001
893. LSEP=IMAX1/2+1
894. LSEP=LSEP+1
895. IF(X(LSEP).LT.XLSEP)GO TO 4002
896. IF(IMASS.EQ.1)LSEP=ITE
897. CM=1.+2.*M**2
898. 1000 ISIDE=ISIDE+1
899. SEPMK=O
900. DO 2 J=ILE,ITE
901. DEL(J)=O.
902. IF(ISIDE.EQ.2)GO TO 3
903. CP=CPU(J)
904. 4 TEST=(5.*(CM/(1.+7.*CP*M**2))*(.2857143)-1.)
905. EM(J)=O.OO1
906. IF(TEST.GT.O)EM(J)=SQRT(TEST)
907. DD=1.+2.*EM(J)**2
908. T=CM/DD
909. UE(J)=EM(J)/M*SQRT(T)
910. GO TO 2
911. 3 CP=CPL(J)
912. GO TO 4
913. 2 CONTINUE
914. IF(ISIDE.EQ.1)USTR=UE(ITE)

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915. ILEP1=ILE+1
916. DSS(ILE)=SLOWER(ILE)
917. IF(1SIDE.EQ.1)DSS(ILE)=SUPPER(ILE)
918. DO 5 J=ILEP1,ITE
919. IF(1SIDE.EQ.2)GO TO 6
920. DSS(J)=SUPPER(J)-SUPPER(J-1)
921. GO TO 5
922. 6 DSS(J)=SLOWER(J)-SLOWER(J-1)
923. 5 DUDS(J)=(UE(J)-UE(J-1))/DSS(J)
924. DT=1.
925. SEPR=0.
926. HH=0.
927. IBDS=ITE-1
928. IF(1SIDE.EQ.1)ISTART=IBDLV
929. IF(1SIDE.EQ.2)ISTART=LBDLV
930. ILAM=1
931. IF(1LAM.EQ.0)GO TO 5060
932. CALL THWAIT(THETA,HH,UE,DSS,DUDS,ISTART)
933. IF(1SIDE.EQ.1)IBDLV=ISTART
934. IF(1SIDE.EQ.2)LBDLV=ISTART
935. IF(1START.GE.ITE)THET2=THETA
936. IF(1START.GE.ITE)GO TO 202
937. 5060 CONTINUE
938. IF(ITER/LP*LP.EQ.ITER)PRINT 1,RN
939. 1 FORMAT(1H0,10X,'BOUNDARY LAYER ANALYSIS FOR REYNOLDS NO. OF ',E10.
940. 13,/,5X,'X',9X,
941. 210X,'H',9X,'PI',5X,'TAU')
942. DO 200 J=ISTART,IBDS
943. EMT=(EM(J+1)+EM(J))/2.
944. UESA=(UE(J+1)+UE(J))/2.
945. VM=1.+2*EMT**2
946. T=CM/VM
947. RFT=UESA*(T+TR)*T/(1.+TR)*RN
948. IF(J.NE.ISTART)GO TO 30
949. THET1=320./RFT
950. IF(1LAM.EQ.1)THET1=THETA
951. THET2=THET1
952. GE=6.5
953. 30 FC=1.+0.066*EMT**2-.008*EMT**3
954. FR=1.-.134*EMT**2+.027*EMT**3
955. IND=0
956. 40 IND=IND+1
957. IF(THET1.LT.1.E-06)THET1=1.E-06
958. IF(FR.LT.0.)FR=ABS(FR)
959. IF(RFT.LT.0.)RFT=ABS(RFT)
960. TAU=(FC*(2.4711*ALOG(FR*RFT*THET1)+4.75)+1.5*GE+1724.)/(GE**2+
961. 1200.)-16.87)
962. IF(TAU.LT.0.)TAU=-TAU
963. TAU=1./TAU**2
964. IF(TAU.LT.1.E-06)TAU=1.E-06
965. HB=1./((1.-GE*SQRT(TAU))
966. H=(HB+1.)*(1.+178*EMT**2)-1.
967. SEP=THET1*DUDS(J+1)/UESA
968. IF(SEP.GT.1.0)SEP=1.0
969. IF(SEP.LT.SP)GO TO 41
970. IF(1SIDE.EQ.1.AND.IMASS.EQ.1)GO TO 3005
971. IF(X(J+1).LT.XSEP)SEP=SP
972. GO TO 3006
973. 3005 IF(X(J+1).LT.XLSEP)SEP=SP
974. 3006 CONTINUE
975. 41 PII=H+SEP/TAU

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976. IF(PII.LT.-1.5)PII=-1.5
977. IF(PII.GT.1.E4)PII=1.E4
978. 50 CONTINUE
979. G=6.1*SQR(PII+1.81)-1.7
980. T2=ABS((G-GE)/GE)
981. GE=G
982. DT2=DT
983. DT=(H+2.-EMT**2)*SEP+TAU
984. IF(IND.GT.1)GO TO 100
985. THT=THEI2
986. THEI1=DT*DSS(J+1)+THT
987. THEI1=.5*(THEI1+THT)
988. GO TO 40
989. 100 DT=(DT2+DT)/2.
990. TI=ABS((DT-DT2)/DT)
991. IF(TI.LT.TE2)GO TO 120
992. 110 THEI1=DT*DSS(J+1)+THT
993. THEI1=.5*(THEI1+THT)
994. IF(IND.LE.500)GO TO 40
995. IF(PII.EQ.-1.5)GO TO 130
996. GO TO 130
997. 120 IF(T2.GE.TE1)GO TO 110
998. 130 THEI2=DT*DSS(J+1)+THT
999. THEI1=.5*(THEI2+THT)
1000. SEP=-THEI1*DUDS(J+1)/UESA
1001. SEPR=(SEPR*DSS(J+1)+SEP*DSS(J))/(DSS(J)+DSS(J+1))
1002. HH=(HH*DSS(J+1)+H*DSS(J))/(DSS(J)+DSS(J+1))
1003. DELS=HH*THT
1004. DEL(J)=DELS
1005. HS(J)=HH
1006. IF(DEL(J).GT.0.1)DEL(J)=0.1
1007. IF(IMASS.EQ.1) GO TO 3001
1008. GO TO 3004
1009. 3001 IF(1SIDE.EQ.2)GO TO 3004
1010. IF(J.NE.LSPOLD)GO TO 3015
1011. EMSTR=EM(LSPOLD)
1012. USTR=UE(LSPOLD)
1013. HSTR=HH
1014. TSTR=THT/(X(LSPOLD)+0.50)
1015. 3015 CONTINUE
1016. IF(SEPMK.EQ.1) GO TO 3004
1017. IF(SEPR.GT.SP)LSEP=J
1018. IF(LSEP.LT.ITE)SEPMK=1
1019. 3004 CONTINUE
1020. IF(ITER/LP*LP.EQ.ITER)PRINT 10,X(J),EM(J),DELS,THT,SEPR,HH,PII,TAU
1021. 10 FORMAT(9F10.5,I10,F10.5)
1022. C+***** ADDITION *****
1023. IF(IMASS.EQ.1)GOTO 205
1024. IF(1SIDE.EQ.2)GOTO 205
1025. IF(SEPMK.EQ.1)GOTO 205
1026. IF(SEPR.GT.SP)LSEP1=J
1027. IF(LSEP1.LT.ITE)SEPMK=1
1028. C+*****
1029. 205 CONTINUE
1030. 9 CONTINUE
1031. IF(J.EQ.IBDS)GO TO 200
1032. SEPR=SEP
1033. HH=H
1034. 200 CONTINUE
1035. SEPR=-SEPR+2.*SEP
1036. HH=HS(ITE-1)+(DSS(ITE)/DSS(ITE-1))*(HS(ITE-1)-HS(ITE-2))
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1037. HS(ITE)=HH
1038. DELS=HH*THET2
1039. DEL(ITE)=DELS
1040. IF(DEL(ITE).GT.O.1)DEL(ITE)=O.1
1041. IF(IMASS.EQ.1)GO TO 3002
1042. 3002 CONTINUE
1043. IF(ITER/LP*LP.EQ.ITER)PRINTO,X(ITE),EM(ITE),DELS,THET2,SEPR,
1044. *HH,PII,TAU
1045. 202 IF(1SIDE.EQ.2)GO TO 203
1046. C***** ADDITION *****
1047. IF(LSPOLD.EQ.ITE)GOTO 72
1048. IF(IMASS.EQ.1)GO TO 440
1049. 72 EMSTR=EM(ITE)
1050. USTR=UE(ITE)
1051. C*****
1052. HSTR=HH
1053. TSTR=THET2
1054. 440 CONTINUE
1055. DO 170 J=ILE,IRDS
1056. 170 IF(DEL(J+1).LT.DEL(J))DEL(J+1)=DEL(J)
1057. 203 CONTINUE
1058. IF(1SIDE.EQ.1)GO TO 2200
1059. J=ILE
1060. 2180 J=J+1
1061. IF(DEL(J+1).LT.DEL(J))GO TO 2185
1062. IF(J.LT.IBDS)GO TO 2180
1063. GO TO 2200
1064. 2185 IF(X(J).GT.XPC)GO TO 2190
1065. DEL(J+1)=DEL(J)
1066. GO TO 2180
1067. 2190 J=J+1
1068. IF(J.GT.IBDS)GO TO 2200
1069. IF(DEL(J+1).GT.DEL(J))DEL(J+1)=DEL(J)
1070. IF(J.LT.IBDS)GO TO 2190
1071. 2200 CONTINUE
1072. ISMOTH=2
1073. IF(IMAX.GT.55)ISMOTH=4
1074. DO 171 JU=1,ISMOTH
1075. OLD=DEL(ILE)
1076. ILEP2=ILE+2
1077. DO 171 J=ILEP2,ITE
1078. NEW=DEL(J-1)
1079. DEL(J-1)=-.25*(OLD+NEW+NEW+DEL(J))
1080. 171 OLD=NEW
1081. FAC=-DSS(ITE)/DSS(ITE-1)
1082. DEL(ITE)=FAC*DEL(ITE-2)+(1.-FAC)*DEL(ITE-1)
1083. DO 172 J=ILEP1,IBDS
1084. SLOPE=SLU(J)
1085. IF(1SIDE.EQ.2)SLOPE=SLL(J)
1086. CO=ABS(ATAN(SLOPE))
1087. CO=COS(CO)
1088. IF(1SIDE.EQ.2)GO TO 173
1089. DY=DUPOLD(J)+RDEL*(DEL(J)-DUPOLD(J))
1090. YU(J)=YUORIG(J)+DY/CO
1091. DUPOLD(J)=DY
1092. GO TO 172
1093. 173 DY=DLWOLD(J)+RDEL*(DEL(J)-DLWOLD(J))
1094. YL(J)=YLORIG(J)-DY/CO
1095. DLWOLD(J)=DY
1096. GO TO 172
1097. 172 CONTINUE

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1098. SLOPE=SLU(ITE)
1099. IF(ISIDE.EQ.2)SLOPE=SLL(ITE)
1100. CO=ABS(ATAN(SLOPE))
1101. CO=COS(CO)
1102. IF(ISIDE.EQ.2)GO TO 175
1103. DY=DUPOLD(ITE)+RDEL*(DEL(ITE)-DUPOLD(ITE))
1104. YU(ITE)=YUORIG(ITE)+DY/CO
1105. DUPOLD(ITE)=DY
1106. GO TO 204
1107. 175 DY=DLWOLD(ITE)+RDEL*(DEL(ITE)-DLWOLD(ITE))
1108. YL(ITE)=YLORIG(ITE)-DY/CO
1109. DLWOLD(ITE)=DY
1110. 204 CONTINUE
1111. IF(ITEUPC.EQ.0)GO TO 5003
1112. C **INSERT SEPERATED CORRECTION HERE IF DESIRED**
1113. C ** SEPERATED COORRECTION**
1114. IF(ISIDE.EQ.2)GO TO 5003
1115. IF(ICYCLE.GT.1)GO TO 300
1116. LMON=IMAX/2+1
1117. CPB=0.
1118. DO 5001 J=LMON,IBDS
1119. CPN=CPL(J)
1120. CPB=AMAX1(CPB,CPN)
1121. 5001 CONTINUE
1122. CPB=0.6
1123. PRINT 5002,CPB
1124. FORMAT(' ',BASE PRESSURE COEFFICIENT = ',F10.3)
1125. IF(LSEP.EQ.ITE)LSEP=ITE-1
1126. LSEP1=LSEP+1
1127. SLOP=(CPB-CPU(LSEP))/(.5-X(LSEP))
1128. DO 501 J=LSEP1,ITE
1129. CPU(J)=SLOP*(X(J)-X(LSEP))+CPU(LSEP)
1130. ICYCLE=ICYCLE+1
1131. ISIDE=0
1132. GO TO 1000
1133. 5003 CONTINUE
1134. IF(ITEWC.EQ.0)GO TO 300
1135. IF(ISIDE.EQ.1)GO TO 300
1136. C ** LOWER SURFACE CORRECTION, IF DESIRED**
1137. IF(ICYBOT.GT.1)GO TO 300
1138. IF(LSEP.EQ.ITE)LSEP=ITE-1
1139. SLOP=(CPB-CPL(LSEP))/(.5-X(LSEP))
1140. LSEP1=LSEP+1
1141. DO 5004 J=LSEP1,ITE
1142. CPL(J)=SLOP*(X(J)-X(LSEP))+CPL(LSEP)
1143. ICYBOT=ICYBOT+1
1144. ISIDE=1
1145. GO TO 1000
1146. C ** END SEPERATED REGION CORRECTION **
1147. 300 CONTINUE
1148. IF(ISIDE.LT.2)GO TO 1000
1149. XO(1)=-.5
1150. XI(1)=-.5
1151. YI(1)=0.
1152. NI=ITE-ILE+2
1153. DO 210 I=ILE,ITE
1154. II=I-ILE+2
1155. XI(II)=X(I)
1156. XO(II)=X(I)
1157. 210 YI(II)=YU(I)
1158. ND=NI

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1159. CALL ARC(XI, YI, XO, YO, SI, SO, XP, YP, D1Y, D2Y, D3Y, O.O.O.O., 1.O.O.O.NI,
1160. 1NO, 1)
1161. DO 211 I=ILE, ITE
1162. II=I-ILE+2
1163. YI(II)=YL(I)
1164. IF(I.LT.LBOLDY)GO TO 211
1165. SLU(I)=YP(II)/XP(II)
1166. 211 CONTINUE
1167. IF(ITEUPC.EQ.O)GO TO 5025
1168. LSEP1=LSEP+1
1169. IF(XPC.LT.O.495)GO TO 5029
1170. DO 5030 J=LSEP1, ITE
1171. IF(SLU(J).GT.O.O)GO TO 5031
1172. CONTINUE
1173. GO TO 5025
1174. DO 5032 I=J, ITE
1175. YU(I)=YU(J-1)
1176. 5032 SLU(I)=O.O
1177. GO TO 5025
1178. CONTINUE
1179. DO 5026 I=LSEP1, ITE
1180. YU(I)=YU(LSEP)+SLU(LSEP)*(X(I)-X(LSEP))
1181. SLU(I)=SLU(LSEP)
1182. CONTINUE
1183. CALL ARC(XI, YI, XO, YO, SI, SO, XP, YP, D1Y, D2Y, D3Y, O.O.O.O., -1.O.O.O.O.,
1184. 1NI, NO, 1)
1185. DO 212 I=ILE, ITE
1186. II=I-ILE+2
1187. YU(II)=ATAN(YU(I)/A1)/PI2
1188. YL(II)=ATAN(YL(I)/A1)/PI2
1189. IF(I.LT.LBOLDY)GO TO 212
1190. SLL(I)=YP(II)/XP(II)
1191. 212 CONTINUE
1192. IF(ITELWC.EQ.O)GO TO 5027
1193. LSEP1=LSEP+1
1194. IF(XPC.LT.O.495)GO TO 5036
1195. DO 5033 J=LSEP1, ITE
1196. IF(SLL(J).LT.O.O)GO TO 5034
1197. 5033 CONTINUE
1198. GO TO 5027
1199. DO 5035 I=J, ITE
1200. YL(I)=YL(J-1)
1201. 5035 SLL(I)=O.O
1202. GO TO 5027
1203. CONTINUE
1204. DO 5028 I=LSEP1, ITE
1205. YL(I)=YL(LSEP)+SLL(LSEP)*(X(I)-X(LSEP))
1206. SLL(I)=SLL(LSEP)
1207. CONTINUE
1208. HBT=(HSTR+1.)/(1.+178*EMSTR**2)-1.
1209. HBB=(HH+1.)/(1.+178*EM(ITE)**2)-1.
1210. CDF=TSTR*(USTR**(2.5+.5*HBT))+THET2*(UE(ITE)**(2.5+.5*HBB))
1211. CDF=2.*CDF
1212. IF(DPM.LE.CONV) GO TO 5010
1213. IF(ITER.GE.(MITER-1))GO TO 5010
1214. GO TO 5008
1215. 5010 DO 5007 J=ILE, IMAX1
1216. CPU(J)=CPUT(J)
1217. 5007 CPL(J)=CPLT(J)
1218. 5008 CONTINUE
1219. IF(IMASS.EQ.O)GO TO 3007

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1220. IF(MHALF.EQ.4)LSEP=LSPOLD
1221. IF(LSEP.GT.LSPOLD)LSEP=LSPOLD
1222. IF(LSEP.GE.(ITE-1))GO TO 3008
1223. I1=LSEP
1224. I11=I1-1
1225. X1=X(I1)-O.OO1
1226. X2=O.5
1227. JB2=JB-2
1228. DO 3012 J=JB2,JMAX1
1229. IF(YU(I1).GT.E(J).AND.YU(I1).LE.E(J+1))GO TO 3013
1230. 3012 CONTINUE
1231. 3013 JA=J+1
1232. IF(JA.LE.JB)JA=JB+1
1233. PHSEP=P(I1,JA-1)+(P(I1,JA)-P(I1,JA-1))*(YU(I1)-E(JA-1))/DE
1234. CPU(LSEP)=-2.*(PHITE-PHSEP)/(X(ITE)-X(LSEP))
1235. CPU(LSEP)=CPSPO+RLAX*(CPU(LSEP)-CPSPO)
1236. CPSPO=CPU(LSEP)
1237. DO 3009 J=LSEP,ITE
1238. CPU(J)=CPU(LSEP)
1239. PRINT 6152,X(LSEP),CPU(LSEP)
1240. 6152 FORMAT(' ',2X,'SEPARATION AT ',F10.5,5X,'SEPARATED CP IS ',F10.5)
1241. LSPOLD=LSEP
1242. RETURN
1243. 3008 I1=ITE+1
1244. I11=I1-1
1245. X1=O.5
1246. X2=10000.O
1247. 3007 CONTINUE
1248. C*****ADDITION *****
1249. IF(X(LSEP1).GE.X(ITE))GOTO 3091
1250. PRINT 3092,X(LSEP1)
1251. 3092 FORMAT(' UPPER SURFACE SEPARATION AT ',G15.9)
1252. RETURN
1253. 3091 PRINT 3093,X(ITE)
1254. 3093 FORMAT(' NO UPPER SURFACE SEPARATION BEFORE ',F10.5)
1255. C*****
1256. RETURN
1257. END
1258. SUBROUTINE THWAIT(THETA,HH,UE,DSS,DUDS,ISTART)
1259. C ***** THIS SUBROUTINE IS BASED UPON A NASA LANGLEY *****
1260. C ***** PROGRAM ORIGINALLY DEVELOPED BY THE GRUMMAN *****
1261. C ***** AEROSPACE CORPORATION *****
1262. REAL M
1263. COMMON CPU(99),CPL(99),E(99),DU1(99),DU2(99),DL1(99),DL2(99),D(99)
1264. 1,FF(99),FFP12(99),FFM12(99),FFM1(99),FFM32(99),
1265. 1P1(99),P2(99),PB(99),P(99,99),RS(99),S(99),SUP(99),SUB(99),TEMP(99)
1266. 2),X(99),Y(99),YU(99),YL(99),YU(99),YLL(99),
1267. 3A1,A2,AI2,ALP,CIR,EPS,EPSS,DE,DS,DP,DPM,F,FP12,FM12,FM32,M,OI,QI2,
1268. 4W,X1,X2,VVJB,VVJB1,AAJB,AAJB1,AAJB,QQJB,QQJB1,UUJB,VVJB1,QQJB1,AAJB1,
1269. 5,O,QQ,UUJB1,PI,PI2,A22,A11,X4,S4
1270. COMMON I,ITE,ITE1,ILE,ILE1,I1,I11,ICON,IMAX,IMAX1,INV,JB,JA1,JB1,
1271. 1,JMAX,JCON,JMAX1,NSSP,IW
1272. COMMON/NASH/RN,IBDLY,ITACT,YUORIG(99),YLORIG(99),SUPPER(99),SLOWER
1273. 1(99),DEL(99),DUPOLD(99),DLWOLD(99),CDF
1274. COMMON/DELTA/ITER
1275. COMMON/IPT1/XIBDLY,RDEL,RDELFN,RCPB,SP,XSEP,XCONV,CPB,XMON,XLSEP,
1276. 1 MITER,LP,ITEUPC,ITELWC,XPC
1277. 2, LBDLY,XLBDLY
1278. COMMON/IPT2/IMASS
1279. COMMON/FIX/MHALF
1280. COMMON/SETCPS/CPSPO,RLAX

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1281. COMMON/IPT3/ISIDE,ILAM,RADIUS
1282. DIMENSION UE(99),DSS(99),DUDS(99)
1283. DIMENSION TWM(29),TWL(29),TWH(29),UBAR(500)
1284. DIMENSION HP(29),HPP(29),HPPP(29),PL(29),PPL(29),PPPL(29)
1285. F1(Y1,Y1,Y2,Y3,DB)=YY+DB*(Y1+.5*DB*(Y2+DB*Y3/3.))
1286. F2(A1,A2,DS)=.5*DS*(A1+A2)
1287. DATA TWL/0.500,0.463,0.404,0.382,0.359,0.333,0.313,
1288. 1 0.291,0.268,0.244,0.220,0.208,0.195,0.182,0.168,
1289. 2 0.153,0.138,0.130,0.122,0.113,0.104,0.095,0.085,
1290. 3 0.072,0.056,0.038,0.027,0.015,0.000/
1291. DATA TWH/2.00,2.07,2.18,2.23,2.28,2.34,2.39,2.44,2.49,
1292. 1 2.55,2.61,2.64,2.67,2.71,2.75,2.81,2.87,2.90,2.94,2.99,
1293. 2 3.04,3.09,3.15,3.22,3.30,3.39,3.44,3.49,3.55/
1294. DATA TWM/-0.25,-0.20,-0.14,-0.12,-0.10,-0.080,-0.064,
1295. 1 -0.048,-0.032,-0.016,0.0,0.008,0.016,0.024,0.032,0.040,
1296. 2 0.048,0.052,0.056,0.060,0.064,0.068,0.072,
1297. 3 0.076,0.080,0.084,0.086,0.088,0.090/
1298. DATA MM /0/
1299. IBUB=0
1300. IF(MM.NE.0) GO TO 2
1301. CALL FIT2 (29,TWM,TWH,HP,HPP,HPPP,3,3,0.,0.)
1302. CALL FIT2 (29,TWM,TWL,PL,PPL,PPPL,3,3,0.,0.)
1303. MM = 1
1304. RE=RN
1305. AMACH=M
1306. R=1.0
1307. OMEG=1.0
1308. RCVF=0.89
1309. RADUS=0.035
1310. 2 CONTINUE
1311. KTRAN= 0
1312. SINT= 0.
1313. VAL = .2
1314. UBAR5B= 0.
1315. IF(ITER/LP*LP.EQ.ITER)PRINT 100
1316. TRAT = SQRT(.5*RADUS/RE)*(1+.2*AMACH**2)**(-.75)
1317. DELTA1= 0.64474*TRAT
1318. DELTA2= 0.29478*TRAT
1319. H= 2.187
1320. TM= -0.08695
1321. RD1= 0.
1322. RD2= 0.
1323. CFV=1.E+10
1324. N=ILE-1
1325. T1 = 0.
1326. R1 = 1.
1327. XSURF=-0.50
1328. DUDS(ILE)=UE(ILE)/DSS(ILE)
1329. SLG=DSS(ILE)
1330. IF(ISIDE.EQ.1)GO TO 1001
1331. DO 1002 J=ILE,ITE
1332. IF(CPL(J+1).LT:CPL(J))GO TO 1003
1333. 1002 CONTINUE
1334. 1003 IF(J.EQ.ILE)GO TO 1001
1335. N=J
1336. XSURF=X(N)
1337. SLG=DSS(N+1)
1338. 1001 CONTINUE
1339. IF(ITER/LP*LP.EQ.ITER)PRINT 101,XSURF,CFV,DELTA1,DELTA2,H,RD2,
1340. 1 RD1, TM
1341. 5 DELTP1= DELTA1
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1342. DELTP2= DELTA2
1343. U=UE(N+1)
1344. UP=DUDS(N+1)
1345. T2 = U**2*((1+.2*AMACH**2+(U**2-1))**.5
1346. UBAR(N+1)= U
1347. TMO = TM
1348. UBAR5A= UBAR5B
1349. QQQ= SQRT(1.+VAL*AMACH**2*(1.-UBAR(N+1)**2))
1350. FMACH= AMACH*UBAR(N+1)/QQQ
1351. TRAT= 1.+VAL*FMACH**2
1352. UBAR5B= UBAR(N+1)**5/TRAT**((1.5)*R**2)
1353. SINT=SINT+F2(UBAR5A,UBAR5B,DSS(N+1))
1354. TTT= 0.45*SINT/UBAR(N+1)**6*TRAT**3/R**2
1355. TM = -UP*TTT/SQRT(TRAT)
1356. IF(TM.GT.0.090) GO TO 19
1357. DO 6 J=1,28
1358. IF(TWM(J+1).GT.TM) GO TO 60
1359. 6 CONTINUE
1360. DB=TM-TWM(J)
1361. TL=F1 (TWL(J),PL(J),PPL(J),PPPL(J),DB)
1362. HINC=F1 (TWH(J),HP(J),HPP(J),HPPP(J),DB)
1363. IF(HINC.LT.1.0) HINC= 1.0
1364. IF(TL.LT.0.) TL= 0.
1365. H= TRAT*(HINC+1.)-1.
1366. DELTA2 = SQRT(TTT/RE)*(1+.2*AMACH**2)*(-.75)
1367. DELTA1= H *DELTA2
1368. RD2 = RE*UBAR(N+1)*DELTA2*QQQ**3.
1369. RD1= H *RD2
1370. CFV=2.*TL/RD2
1371. DEL(N+1)=DELTA1
1372. N= N+1
1373. SM=SLG
1374. C*****ADDITION *****
1375. IF(N.EQ.ITE) GO TO 30
1376. C*****
1377. SLG=SLG+DSS(N+1)
1378. C*****MODIFY *****
1379. 30 IF(ITER/LP*LP.EQ.ITER)PRINT 101,X(N),CFV,DELTA1,DELTA2,H,RD2,RD1,
1380. 1 TM
1381. 14 IF(KTRAN.GT.0) GO TO 15
1382. RD2TR= 217.-11787.*TM+366762*TM**2-4380632.*TM**3
1383. 1 +10453860.*TM**4
1384. IF(RD2.LT.RD2TR) GO TO 21
1385. KTRAN= 1
1386. KT=1
1387. IF(ITER/LP*LP.EQ.ITER)PRINT 33,X(N)
1388. 33 FORMAT(3X,'INSTABILITY DETECTED AT X=',F10.5)
1389. UNSTM= -TM
1390. RD2UNS= RD2
1391. SSHF= 0.
1392. SUNST= SM
1393. GO TO 21
1394. 15 SSHF=SSHFF-F2(TMO,TM,DSS(N))/(SM-SUNST)
1395. RD2TR= RD2UNS+914.+27250.*SSHFF+328333*SSHFF**2
1396. IF(RD2.GT.RD2TR) GO TO 25
1397. GO TO 21
1398. 19 IBUB=1
1399. IF(ITER/LP*LP.NE.ITER)GO TO 27
1400. WRITE(6,102)X(N)
1401. IF(RD2.GT.135.)WRITE(6,107)X(N)
1402. IF(RD2.LT.135.)WRITE(6,108)X(N)
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1403. GO TO 27
1404. 21 IF(N-ITE)5,28,28
1405. 25 IF(ITER/LP*LP.EQ.ITER)PRINT 106,X(N)
1406. 27 THETA=DELTA2
1407. HH=H
1408. ISTART=N
1409. IF(UBUB.EQ.1)ISTART=N+1
1410. RETURN
1411. 28 IF(ITER/LP*LP.EQ.ITER)PRINT 109
1412. THETA=DELTA2
1413. HH=H
1414. ISTART=N
1415. RETURN
1416. 100 FORMAT(12X,'X',13X,'CF',11X,'D-STAR',9X,'D-THETA',10X,'H',12X,
1417. 'RE-THETA',7X,'RE-STAR',10X,'TM'/)
1418. 101 FORMAT(4X,8E15.4)
1419. 102 FORMAT(/10X,'SEPARATION OCCURRED AT X= ',F10.5)
1420. C 103 FORMAT(/10X,'FINAL LAMINAR BOUNDARY LAYER PROFILES+//)
1421. C 104 FORMAT(/10X,'*Y',19X,'*VEL. RATIO*',10X,'*STRESS*//)
1422. C 105 FORMAT(3(10X,F10.5))
1423. 106 FORMAT(/10X,'TRANSITION OCCURS AT X= ',F10.5)
1424. 107 FORMAT(10X,'SHORT BUBBLE FORMED? ',
1425. 'TRANSITION TO TURBULENT FLOW IS ASSUMED. X=',F10.5//)
1426. 108 FORMAT(10X,'LONG BUBBLE? LAMINAR STALL MAY OCCUR. X=',F10.5,
1427. '/10X,'BOUNDARY LAYER CALCULATION WILL BE CONTINUED ',
1428. 'AS TURBULENT BUT ACCURACY OF RESULTS IS QUESTIONABLE'//)
1429. 109 FORMAT(/10X,'BOUNDARY LAYER CALCULATION COMPLETED'//)
1430. 1 /10X,'NEITHER SEPARATION NOR TRANSITION WAS DETECTED'//)
1431. C 110 FORMAT(/10X,'SPECIFIED SEPARATION POINT REACHED. X=',F10.5,
1432. C 1 /10X,'*NO TURBULENT CALCULATION WILL BE PERFORMED*')
1433. END
1434. SUBROUTINE FIT2(N,X,F,FP,FPP,FPPP,K1,KN,END1,ENDN)
1435. C IMPLICIT REAL*4 (A-H,O-Z)
1436. DIMENSION X(1),F(1),FP(1),FPP(1),FPPP(1)
1437. NM1=N-1
1438. IF (N.LT.3) X(N+1)=X(N)+1.0
1439. IF (N.LT.3) F(N+1)=F(N)
1440. DX2=X(2)-X(1)
1441. GO TO (1,2,3),K1
1442. 1 FP(1)=0.5
1443. FPPP(1)=3.*(F(2)-F(1))/DX2-END1)/DX2
1444. GO TO 4
1445. 2 FP(1)=0.0
1446. FPPP(1)=END1
1447. GO TO 4
1448. 3 FP(1)=-1.0
1449. FPPP(1)=-DX2*END1
1450. 4 DO 5 I=2,NM1
1451. IP = I+1
1452. IM = I-1
1453. DX1=X(I)-X(IM)
1454. DX2=X(IP)-X(I)
1455. FP(I)=.5*DX2/(DX1+DX2)-.5*DX1*FP(IM)
1456. 5 FPPP(I)=(6.*(F(IP)-F(I))/DX2-6.*(F(I)-F(IM))/DX1-DX1+FPPP(IM)
1457. 1*FP(I))/DX2
1458. DX1=X(N)-X(NM1)
1459. FP(N)=0.0
1460. GO TO (6,7,8),KN
1461. 6 FPPP(N)=(6.*(ENDN-(F(N)-F(NM1))/DX1)-FPPP(NM1))/(2.-FP(NM1))
1462. GO TO 9
1463. 7 FPPP(N)=ENDN
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1464. GO TO 9
1465. 8 FPPP(N)=(ENDN*DX1+FPPP(NM1))/(1.+FP(NM1))
1466. 9 FPP(N)=FPPP(N)
1467. DO 10 II=1,NM1
1468. I=N-II
1469. IP = I+1
1470. DX2=X(IP)-X(I)
1471. FPP(I)=FPPP(I)-FPP(IP)*FPP(IP)
1472. FPPP(I)=(FPP(IP)-FPP(I))/DX2
1473. 10 FP(I)=(F(IP)-F(I))/DX2-DX2*(FPP(IP)+2.*FPP(I))/6.
1474. FPPP(N)=FPPP(NM1)
1475. DX1=X(N)-X(NM1)
1476. FP(N)=(F(N)-F(NM1))/DX1+DX1*(FPP(NM1)+2.*FPP(N))/6.
1477. RETURN
1478. END
1479. SUBROUTINE BDLY
1480.
1481. C ***** COMPUTES BOUNDARY LAYER IN THE DESIGN CASE *****
1482. C
1483. REAL M,NEW
1484. COMMON CPU(99),CPL(99),E(99),DU1(99),DU2(99),DL1(99),DL2(99),D(99)
1485. 1,FF(99),FFP12(99),FFM12(99),FFM1(99),FFM32(99),
1486. 1P1(99),P2(99),PB(99),P(99),RS(99),S(99),SUP(99),SUB(99),TEMP(99)
1487. 2),X(99),Y(99),YU(99),YL(99),SLU(99),SLL(99),
1488. 3A1,A2,AI2,ALP,CIR,EPS,EPSS,DE,DS,DP,DPM,F,FP12,FM12,FM32,M,OI,QI2,
1489. 4W,X1,X2,VVUB,VVUB1,AAJB1,AAJB,QQJB,QQJB1,UUJB,VVJB1,AAJB1,AAJB1,
1490. 5,Q,QQ,UUJB1,PI,PI2,A22,A11,X4,S4
1491. COMMON I,ITE,ITE1,ILE,ILE1,I1,I11,ICON,IMAX,INV,JB,JA1,JB1,
1492. 1JMAX,JCON,UMAX1,NSSP,IW
1493. COMMON/NASH/RN,IBDLY,ITACT,YUORIG(99),YLORIG(99),SUPPER(99),SLOWER
1494. 1(99),DEL(99),DUOLD(99),DLWOLD(99),CDF
1495. COMMON/DELTA/ITER
1496. COMMON/IPT1/XIBDLY,RDEL,RDELFN,RCPB,SP,XSEP,CONV,CPB,XMON,XLSEP,
1497. 1,MITER,LP,ITEUPC,ITELWC,XPC
1498. 2,IBDLY,XLBDLY
1499. DIMENSION UE(99),DSS(99),DUDS(99),YUN(99),YLN(99),EM(99)
1500. DIMENSION HS(99)
1501. DIMENSION XI(99),YI(99),XO(99),YO(99),SI(99),XP(99),DIY(99),
1502. 1D2Y(99),D3Y(99),XIB(99),YIB(99),SO(99),YP(99)
1503. ISIDE=0
1504. LSEP=ITE
1505. SEPMK=0
1506. ICYCLE=1
1507. DO 500 J=ILE,ITE
1508. YUN(J)=YU(J)
1509. YLN(J)=YL(J)
1510. TR=0.3424
1511. TE1=5.E-03
1512. TE2=5.E-05
1513. CM=1.+2.*M**2
1514. 1 FORMAT(1H1,10X,'BOUNDARY LAYER ANALYSIS FOR REYNOLDS NO. OF ',E10,
1515. 13,'//,5X,'X',9X,'Y',9X,'YNEW',8X,'M',8X,'DELS',4X,'THETA',3X,'SEP',
1516. 210X,'H',9X,'PI',5X,'TAU')
1517. 1000 ISIDE=ISIDE+1
1518. PRINT 1,RN
1519. DO 2 J=ILE,ITE
1520. DEL(J)=0.
1521. IF (ISIDE.EQ.2)GO TO 3
1522. CP=CPU(J)
1523. 4 TEST=(5.*(CM/(1.+7*CP*M**2))*(.2857143)-1.)
1524. EM(J)=0.

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1525. IF(TEST.GT.O.)EM(J)=SQRT(TEST)
1526. DD=1.+2*EM(J)**2
1527. T=CM/DD
1528. UE(J)=EM(J)/M*SQRT(T)
1529. GO TO 2
1530. 3 CP=CPL(J)
1531. GO TO 4
1532. 2 CONTINUE
1533. IF(ISIDE.EQ.1)USTR=UE(ITE)
1534. ILEP1=ILE+1
1535. X0(1)=-.5
1536. XI(1)=-.5
1537. Y1(1)=O.
1538. NI=ITE-ILE+2
1539. DO 210 I=ILE,ITE
1540. II=I-ILE+2
1541. XI(II)=X(I)
1542. X0(II)=X(I)
1543. Y1(II)=YU(I)
1544. NO=NI
1545. CALL ARC(XI,YI,X0,Y0,SI,S0,XP,YP,D1Y,D2Y,D3Y,O.O.O.O,1.O.O.O,NI,
1546. INO,1)
1547. DO 211 I=ILE,ITE
1548. II=I-ILE+2
1549. Y1(II)=Y1(I)
1550. SLL(I)=YP(II)/XP(II)
1551. SUPPER(I)=S0(II)
1552. 211 CALL ARC(XI,YI,X0,Y0,SI,S0,XP,YP,D1Y,D2Y,D3Y,O.O.O.O,-1.O.O.O,
1553. INI,NO,1)
1554. DO 212 I=ILE,ITE
1555. II=I-ILE+2
1556. SLL(I)=YP(II)/XP(II)
1557. SLOWER(I)=S0(II)
1558. DO 5 J=ILEP1,ITE
1559. IF(ISIDE.EQ.2)GO TO 6
1560. DSS(J)=SUPPER(J)-SUPPER(J-1)
1561. GO TO 5
1562. 6 DSS(J)=SLOWER(J)-SLOWER(J-1)
1563. 5 DUDS(J)=(UE(J)-UE(J-1))/DSS(J)
1564. DT=1.
1565. SEPR=O.
1566. HH=O.
1567. IBDS=ITE-1
1568. DO 200 J=IBDLY,IBDS
1569. EMT=(EM(J+1)+EM(J))/2.
1570. UESA=(UE(J+1)+UE(J))/2.
1571. VM=1.+2*EMT**2
1572. T=CM/VM
1573. RFT=UESA*(T+TR)*T/(1.+TR)*RN
1574. IF(J.NE.IBDLY)GO TO 30
1575. THET1=320./RFT
1576. THET2=THET1
1577. GE=6.5
1578. 30 FC=1.+066*EMT**2-.008*EMT**3
1579. FR=1.-.134*EMT**2+.027*EMT**3
1580. IND=O
1581. 40 IND=IND+1
1582. TAU=1./((FC*(2.4711*ALOG(FR*RFT*THET1)+4.75)+1.5*GE+1724.)/(GE**2+
1583. 1200.)-16.87)**2
1584. HB=1./((1.-GE*SQRT(TAU))
1585. H=(HB+1.)*(1.+178*EMT**2)-1.
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1586. SEP=-THET1*DUDS(J+1)/UESA
1587. IF(SEP.LT.SP)GO TO 41
1588. IF(X(J+1).LT.XSEP)SEP=SP
1589. 41 PII=H*SEP/TAU
1590. IF(PII.LT.-1.5)PII=-1.5
1591. IF(PII.GT.1.E4)PII=1.E4
1592. 50 CONTINUE
1593. G=6.1*SQRT(PII+1.81)-1.7
1594. T2=ABS((G-GE)/GE)
1595. GE=G
1596. DT2=DT
1597. DT=(H+2.-EMT**2)*SEP+TAU
1598. IF(IND.GT.1)GO TO 100
1599. THT=THET2
1600. THET1=DT*DSS(J+1)+THT
1601. THET1=.5*(THET1+THT)
1602. GO TO 40
1603. 100 DT=(DT2+DT)/2.
1604. TI=ABS((DT-DT2)/DT)
1605. IF(TI.LT.TE2)GO TO 120
1606. 110 THET1=DT*DSS(J+1)+THT
1607. THET1=.5*(THET1+THT)
1608. IF(IND.LE.500)GO TO 40
1609. IF(PII.EQ.-1.5)GO TO 130
1610. PRINT 160
1611. 160 FORMAT(/ PROBLEMS/)
1612. GO TO 130
1613. 120 IF(T2.GE.TE1)GO TO 110
1614. 130 THET2=DT*DSS(J+1)+THT
1615. THET1=.5*(THET2+THT)
1616. SEP=-THET1*DUDS(J+1)/UESA
1617. SEPR=(SEPR*DSS(J+1)+SEP*DSS(J))/(DSS(J)+DSS(J+1))
1618. HH=(HH*DSS(J+1)+H*DSS(J))/(DSS(J)+DSS(J+1))
1619. DELS=HH*THT
1620. DEL(J)=DELS
1621. IF(DEL(J).GT.0.1)DEL(J)=0.1
1622. HS(J)=HH
1623. IF(1SIDE.EQ.2)GO TO 8
1624. SLOPE=SLU(J)
1625. CO=ABS(ATAN(SLOPE))
1626. CO=COS(CO)
1627. YUN(J)=YU(J)-DELS/CO
1628. PRINT 10,X(J),YU(J),YUN(J),EM(J),DELS,THT,SEPR,HH,PII,
1629. 1IND,TAU
1630. 10 FORMAT(9F10.5,I10,F10.5)
1631. IF(SEPMK.EQ.1)GO TO 205
1632. IF(SEPR.GT.SP)LSEP=J
1633. IF(LSEP.NE.ITE)SEPMK=1
1634. 205 CONTINUE
1635. GO TO 9
1636. 8 SLOPE=SLL(J)
1637. CO=ABS(ATAN(SLOPE))
1638. CO=COS(CO)
1639. YLN(J)=YL(J)+DELS/CO
1640. PRINT 10,X(J),YL(J),YLN(J),EM(J),DELS,THT,SEPR,HH,PII,
1641. 1IND,TAU
1642. 9 CONTINUE
1643. IF(J.EQ.IBDS)GO TO 200
1644. SEPR=SEP
1645. HH=H
1646. 200 CONTINUE
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1647. SEPR=-SEPR+2.*SEP
1648. HH=HS(ITE-1)+(DSS(ITE)/DSS(ITE-1))*(HS(ITE-1)-HS(ITE-2))
1649. HS(ITE)=HH
1650. DELS=HH*THET2
1651. DEL(ITE)=DELS
1652. IF(DEL(ITE).GT.O.1)DEL(ITE)=O.1
1653. IF(ISIDE.EQ.2)GO TO 201
1654. SLOPE=SLU(ITE)
1655. CO=ABS(ATAN(SLOPE))
1656. CO=COS(CO)
1657. YUN(ITE)=YU(ITE)-DELS/CO
1658. PRINT 10,X(ITE),YU(ITE),YUN(ITE),EM(ITE),DELS,THET2,SEPR,HH,PII,
1659. IIND,TAU
GO TO 202
1660.
1661. 201 SLOPE=SLL(ITE)
1662. CO=ABS(ATAN(SLOPE))
1663. CO=COS(CO)
1664. YLN(ITE)=YL(ITE)+DELS/CO
1665. PRINT 10,X(ITE),YL(ITE),YLN(ITE),EM(ITE),DELS,THET2,SEPR,HH,PII,
1666. IIND,TAU
1667. 202 IF(ISIDE.EQ.2)GO TO 203
1668. EMSTR=EM(ITE)
1669. HSTR=HH
1670. TSTR=THET2
1671. DO 170 J=ILE,IBDS
1672. 170 IF(DEL(J+1).LT.DEL(J))DEL(J+1)=DEL(J)
1673. 203 CONTINUE
1674. IF(ISIDE.EQ.1)GO TO 2200
1675. J=ILE
1676. 2180 J=J+1
1677. IF(DEL(J+1).LT.DEL(J))GO TO 2185
1678. IF(J.LT.IBDS)GO TO 2180
1679. GO TO 2200
1680. 2185 IF(X(J).GT.XPC)GO TO 2190
1681. DEL(J+1)=DEL(J)
1682. GO TO 2180
1683. 2190 J=J+1
1684. IF(DEL(J+1).GT.DEL(J))DEL(J+1)=DEL(J)
1685. IF(J.LT.IBDS)GO TO 2190
1686. CONTINUE
1687. 2200 ISMOTH=2
1688. IF(IMAX.GT.55)ISMOTH=4
1689. DO 171 JU=1,ISMOTH
1690. OLD=DEL(ILE)
1691. ILEP2=ILE+2
1692. DO 171 J=ILEP2,ITE
1693. NEW=DEL(J-1)
1694. DEL(J-1)=-.25*(OLD+NEW+NEW+DEL(J))
1695. OLD=NEW
1696. FAC=-DSS(ITE)/DSS(ITE-1)
1697. DEL(ITE)=FAC*DEL(ITE-2)+(1.-FAC)*DEL(ITE-1)
1698. PRINT 180
1699. 180 FORMAT(' X YOLD YNEW DELSTAR')
1700. DO 172 J=ILEP1,IBDS
1701. SLOPE=SLU(J)
1702. IF(ISIDE.EQ.2)SLOPE=SLL(J)
1703. CO=ABS(ATAN(SLOPE))
1704. CO=COS(CO)
1705. IF(ISIDE.EQ.2)GO TO 173
1706. YUN(J)=YU(J)-DEL(J)/CO
1707. PRINT 174,X(J),YU(J),YUN(J),DEL(J)

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1708. GO TO 172
1709. YLN(J)=YL(J)+DEL(J)/CO
1710. PRINT 174,X(J),YLN(J),YLN(J),DEL(J)
1711. 174 FORMAT(4F10.5)
1712. 172 CONTINUE
1713. SLOPE=SLU(ITE)
1714. IF( (SIDE.EQ.2) )SLOPE=SLL(ITE)
1715. CO=ABS(ATAN(SLOPE))
1716. CO=COS(CO)
1717. IF( (SIDE.EQ.2) )GO TO 175
1718. YUN(ITE)=YU(ITE)-DEL(ITE)/CO
1719. PRINT 174,X(ITE),YU(ITE),YUN(ITE),DEL(ITE)
1720. GO TO 204
1721. YLN(ITE)=YL(ITE)+DEL(ITE)/CO
1722. PRINT 174,X(ITE),YL(ITE),YLN(ITE),DEL(ITE)
1723. 204 IF( (SIDE.LT.2) )GO TO 1000
1724. HBT=(HSTR+1.)/(1.+178*EMSTR**2)-1.
1725. HBB=(HH+1.)/(1.+178*EM(ITE)**2)-1.
1726. CDF=TSTR*(USTR**(2.5+.5*HBT))+THET2*(UE(ITE)**(2.5+.5*HBB))
1727. CDF=2.*CDF
1728. PRINT 3010,CDF
1729. FORMAT(4H0,' CDF = ',F10.6)
1730. IF(X(LSEP).GE.XSEP)GO TO 3011
1731. PRINT 3012,X(LSEP)
1732. 3012 FORMAT(1H,'UPPER SURFACE SEPARATION DETECTED AT ',F10.5)
1733. RETURN
1734. 3011 PRINT 3013,XSEP
1735. 3013 FORMAT(1H,'NO UPPER SURFACE SEPARATION BEFORE',F10.5)
1736. RETURN
1737. END
1738. SUBROUTINE VALUE
1739. C
1740. C ***** THIS DETERMINES THE INITIAL SOLUTION *****
1741. C
1742. REAL M
1743. COMMON CPU(99),CPL(99),E(99),DU1(99),DU2(99),DL1(99),DL2(99),D(99)
1744. 1,FF(99),FFP12(99),FFM12(99),FFM1(99),FFM32(99),
1745. 1P1(99),P2(99),PB(99),P(99,99),RS(99),S(99),SUP(99),SUB(99),TEMP(99)
1746. 2),X(99),Y(99),YU(99),YL(99),SLU(99),SLL(99),
1747. 3A1,A2,A12,ALP,CTR,EPS,EPS,DE,DS,DP,DPM,F,FP12,FM12,FM32,M,OI,QI2,
1748. 4W,X1,X2,VVJB,VVJB1,AAJB,AAJB1,AAJB,QQJB,QQJB1,UUJB,VVJB1,QQJB1,AAJB1
1749. 5,Q,QQ,UUJB1,PI,P12,A22,A11,X4,S4
1750. COMMON I,ITE,ITE1,ILE,ILE1,I1,I11,ICON,IMAX,IMAX1,INV,JB,JA1,JB1,
1751. 1JMAX,JCON,JMAX1,NSSP,IW
1752. COMMON/FIPIUT/IREAD
1753. C INITIALIZES VALUES
1754. IF( (IREAD.EQ.0) )GO TO 3
1755. DO 4 J=1,JMAX
1756. J=JMAX-JJ+1
1757. READ 5,(P(I,J),I=1,IMAX)
1758. 5 FORMAT(5E15.7)
1759. 4 CONTINUE
1760. READ5,(PB(I),I=1,IMAX)
1761. RETURN
1762. 3 CONTINUE
1763. DO 1 I=1,IMAX
1764. PB(I)=0.0
1765. DO 1 J=1,JMAX
1766. 1 P(I,J)=0.0
1767. RETURN
1768. END
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1830. GO TO 7
1831. VVJB1=VV
1832. VJB1=V
1833. AAJB1=AA
1834. QQJB1=QQ
1835. UUBJ1=UU
1836. GO TO 7
1837. VVJBP1=VV
1838. VJBP1=V
1839. QQJBP1=QQ
1840. AAJBP1=AA
1841. GO TO 7
1842. IF(J.EQ.QJB+1)GO TO 10
1843. 7 CONTINUE
1844. ML=(UU+VV)/AA
1845. IF(ML.GT.1.0)GO TO 4
1846. SUBSONIC POINT
1847. FAV=1.0*(FP12+FM12)
1848. FPF=0.5*F*FAV
1849. SUB(J-1)=(1.-VV/AA)*GDE*GM12/DE
1850. D(J)=-2.*(1.-UU/AA)*FPF/DSDS/W-(1.-VV/AA)*G*(GP12+GM12)/DEDE
1851. 1-EPS*FDS*U/Q*FM12/DS
1852. IF(D(J).EQ.0.0)GO TO 21
1853. SUP(J)=(1.-VV/AA)*GDE*GP12/DE
1854. RS(J)=(1.-UU/AA)*F*(-FP12/DSDS*P(I+1,J)+FAV/DSDS*(1.-1./W)
1855. 1*P(I,J)-FM12/DSDS*P(I-1,J)+U*V/AA*FDS*GDE*0.5*(P(I-1,J-1)
1856. 2-P(I-1,J+1)-P(I+1,J-1)+P(I+1,J+1))
1857. RS(J)=RS(J)+EPS*FDS*(U/Q*FM12*(-P(I,J)-P(I-1,J)+P1(J))/DS)
1858. IF(V.LE.0.0)GO TO 200
1859. SUB(J-1)=SUB(J-1)+EPS*FDS*V/Q*GM12/DE
1860. D(J)=D(J)-EPS*FDS*V/Q*GM12/DE
1861. RS(J)=RS(J)+EPS*FDS*V/Q*GM12/DE*(P(I,J-1)-P(I,J))
1862. GO TO 3
200 SUP(J)=SUP(J)-EPS*FDS*V/Q*GP12/DE
1863. D(J)=D(J)+EPS*FDS*V/Q*GP12/DE
1864. RS(J)=RS(J)+EPS*FDS*V/Q*GP12/DE
1865. RS(J)=RS(J)+EPS*FDS*V/Q*GP12/DE*(P(I,J)-P(I,J+1))
1866. GO TO 3
1867. C DAMPING COEFF IS EPSS AT SUPERSONIC POINTS
1868. C SUPERSONIC CASE. V GT 0
1869. 4 GM32=GGM32(J)
1870. Nssp=Nssp+1
1871. GP32=GGP32(J)
1872. IF(V.LT.0.0)GO TO 5
1873. SUB(J-1)=UU/QQ*GDE*GM12/DE+EPSS*FDS*V/Q*GM12/DE
1874. D(J)=-VV/QQ*FDS*FM12/DS-UU/QQ*GDE*(GP12+GM12)/DE-EPSS*FDS*
1875. 1(U/Q*FM12/DS+V/Q*GM12/DE)
1876. SUP(J)=UU/QQ*GDE*GP12/DE
1877. RS(J)=-((1.-QQ/AA)*(UU/QQ)*F DS*(FM12*(P(I,J)-P1(J))-FM32*(P1(J)-
1878. 1P2(J)))/DS+2.*U*V/QQ*F*G*(P(I,J)-P1(J)-P(I,J-1)+P1(J-1))/DSDE
1879. 2+VV/QQ*G*(GM12*(P(I,J)-P(I,J-1))-GM32*(P(I,J-1)-P(I,J-2)))/
1880. 3DEDE)
1881. RS(J)=RS(J)-VV/QQ*F*(FP12*(P(I+1,J)-P(I,J))+FM12*(P(I-1,J))/DSDS
1882. 1+U*V/QQ*F*G*(P(I-1,J-1)-P(I-1,J+1)-P(I+1,J-1)+P(I+1,J+1))/DSDE
1883. 2*0.5
1884. 3+EPSS*F*(U/Q*FM12*(-P(I,J)-P(I-1,J)+P1(J))/DSDS+V/Q*GM12*(P(I,J-1)
1885. 4-P(I,J))/DSDE)
1886. GO TO 3
1887. C SUPERSONIC CASE V LT 0
1888. 5 SUB(J-1)=UU/QQ*G DE*GM12/DE
1889. D(J)=-VV/QQ*F DS*FM12/DS-UU/QQ*G DE*(GM12+GP12)/DE-EPSS*F DS*
1890. 1(U/Q*FM12/DS-V/Q*GP12/DE)

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1891. SUP(J)=UU/QQ*GDE*GP12/DE-EPSS*FDS*V/Q*GP12/DE
1892. RS(J)=-((1.-QQ/AA)*(UU/QQ)*F DS*(FM12*(P(I,J)-P1(J))-FM32*(P1(J)-
1893. 1P2(J)))/DS+2.*U*V/QQ*F*G*(-P(I,J)+P1(J)+P(I,J+1)-P1(J+1))/DSDE
1894. 2*VV/QQ*G*(GP12*(P(I,J)-P(I,J+1))-GP32*(P(I,J+1)-P(I,J+2)))/
1895. 3DEDE)
1896. RS(J)=RS(J)-VV/QQ*F*(FP12*(P(I+1,J)-P(I,J))+FM12*(P(I-1,J)))/DSDS
1897. 1+U*V/QQ*F*G*(P(I-1,J-1)-P(I-1,J+1)-P(I+1,J-1)+P(I+1,J+1))/DSDE
1898. 1*O.5
1899. 2*EPSS*F*(U/Q*FM12*(-P(I,J)-P(I-1,J)+P(I,J)))/DSDS+V/Q*GP12*(P(I,J)-
1900. 3P(I,J+1))/DSDE)
1901. IF(I.NE.ILE1)GO TO 3
1902. IF(J.NE.JB-1)GO TO 3
1903. P(ILE,JB)=HLD
1904. 3 CONTINUE
1905. IF (IVLOC.EQ.O) GO TO 30
1906. IF (I.NE.IVOR) GO TO 31
1907. IF (IVLOC.EQ.1.AND.J.LE.JVOR.OR.IVLOC.EQ.-1.AND.J.GT.JVOR)
1908. 1 GO TO 33
1909. 1 IF (ML.LE.1.) RS(J)=RS(J)-IVLOC*(1.-UU/AA)*F*FP12
1910. *VORCIR/DSDS
1911. IF (ML.GT.1.) RS(J)=RS(J)-IVLOC*VV/QQ*F*FP12*VORCIR/DSDS
1912. IF (J.NE.JVOR.AND.J.NE.JVOR+1) GO TO 31
1913. IF (ML.LE.1.) RS(J)=RS(J)+U*V/AA*F*G*VORCIR/2./DS/DE
1914. IF (ML.GT.1.) RS(J)=RS(J)+U*V/AA*F*G*VORCIR/2./DS/DE
1915. 31 IF (I.NE.IVOR+1) GO TO 32
1916. IF (IVLOC.EQ.1.AND.J.LE.JVOR.OR.IVLOC.EQ.-1.AND.J.GT.JVOR)
1917. 1 GO TO 34
1918. IF (ML.LE.1.) RS(J)=RS(J)+IVLOC*(1.-UU/AA)*F*FM12
1919. *VORCIR/DSDS
1920. IF (ML.GT.1.) RS(J)=RS(J)+IVLOC*VV/QQ*F*FM12*VORCIR/DSDS-
1921. IVLOC*(1.-QQ/AA)*UU/QQ*F*FM12*VORCIR/DSDS
1922. IF (J.NE.JVOR.AND.J.NE.JVOR+1) GO TO 32
1923. IF (ML.LE.1.) RS(J)=RS(J)+U*V/AA*F*G*VORCIR/DS/DE/2.
1924. IF (ML.LE.1.) GO TO 32
1925. RS(J)=RS(J)+U*V/AA*F*G*VORCIR/2./DS/DE
1926. IF (J.EQ.JVOR+1.AND.V.GE.O.OR.J.EQ.JVOR.AND.V.LT.O.O)
1927. 1 RS(J)=RS(J)-(1.-QQ/AA)*2.*U*V/QQ*F*G*VORCIR/DS/DE
1928. IF ((I.EQ.IVOR+2.AND.ML.GT.1.)AND.(IVLOC.EQ.1.AND.
1929. J.GT.JVOR.OR.IVLOC.EQ.-1.AND.J.LE.JVOR))
1930. 2 RS(J)=RS(J)+IVLOC*(1.-QQ/AA)*UU/QQ*F*FM32*VORCIR/DSDS
1931. 30 CONTINUE
1932. RETURN
1933. 21 DO 18 JU=1,JMAX
1934. J=JMAX+1-JJ
1935. PRINT 19,J
1936. FORMAT(1H,'ROW ',I5)
1937. PRINT 20,(P(I,J),I=1,IMAX)
1938. FORMAT(1H,'10E11.3)
1939. 18 CONTINUE
1940. PRINT 19,JB
1941. PRINT 20,(PB(I),I=1,IMAX)
1942. STOP
1943. END
1944. SUBROUTINE PRESS
1945. C ***** THIS COMPUTES THE CP DISTRIBUTION ON THE AIRFOIL *****
1946. C
1947. C
1948. REAL M
1949. COMMON CPU(99),CPL(99),E(99),DU1(99),DU2(99),DL1(99),DL2(99),D(99)
1950. 1,FF(99),FFP12(99),FFM12(99),FFM1(99),FFM32(99),
1951. 1P1(99),P2(99),PB(99),P(99,99),RS(99),S(99),SUP(99),SUB(99),TEMP(99)

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1952. 2).X(99),Y(99),YU(99),YL(99),SLU(99),SLL(99), 00001700
1953. 3A1,A2,AI2,ALP,CIR,EPSS,DE,DS,DP,DBM,F,FP12,FM12,FM32,M,QI,QI2,00001701
1954. 4W,X1,X2,VVUB,VVUB1,AAJB1,AAJB,QQJB,QQJB1,UUJB,VVJB1,QQJB1,AAJB1 00001702
1955. 5,Q,QQ,UUJB1,PI,PI2,A22,A11,X4,S4 00001703
1956. COMMON I,ITE,ITE1,ILE,ILE1,I1,I11,ICON,IMAX,IMAX1,INV,JB,JA1,JB1, 00001704
1957. 1JMAX,JCON,JMAX1,NSSP,IW 00001705
1958. COMMON/FIX/MHALF 00001706
1959. COMMON/NASH/RN,IBDLY,ITACT,YUORIG(99),YLORIG(99),SUPPER(99),SLOWER 00001707
1960. 1(99),DEL(99),DUPOLD(99),DLWOLD(99),CDF 00001708
1961. COMPUTES CP ON AIRFOIL 00001709
1962. IPRM=O 00001710
1963. IF(ITACT.EQ.1)IPRM=1 00001711
1964. IPRM=IPRM+1 00001712
1965. IEND=IMAX1 00001713
1966. JB2=JB-2 00001714
1967. DO 1 I=ILE,IEND 00001715
1968. TEMP2=YU(I) 00001716
1969. IF(I.GT.ITE)YU(I)=O.0001 00001717
1970. DO 2 J=JB2,JMAX1 00001718
1971. IF(YU(I).GT.E(J).AND.YU(I).LE.E(J+1))GO TO 3 00001719
1972. 2 CONTINUE 00001720
1973. 3 JA=J+1 00001721
1974. IF(JA.LE.JB)JA=JB+1 00001722
1975. F=FF(I) 00001723
1976. IF(IPRM.EQ.2)GO TO 20 00001724
1977. IF(I.GT.(ILE+1))GO TO 15 00001725
1978. 20 U=O.O 00001726
1979. U=Q1*(COS(ALP)+F*((P(I+1,JA-1)-P(I-1,JA-1))/(2.*DS)+(YU(I)-E(JA-1)) 00001727
1980. 1)*(P(I+1,JA)-P(I-1,JA-1)-P(I-1,JA)+P(I-1,JA-1))/(2.*DS*DE))) 00001728
1981. GO TO 16 00001729
1982. 15 CONTINUE 00001730
1983. U USING BACKWARD DIFFERENCE ON PHIX 00001731
1984. U=Q1*(COS(ALP)+F*(3.*P(I,JA-1)-4.*P(I-1,JA-1)+P(I-2,JA-1))/(2.*DS 00001732
1985. 1)+(YU(I)-E(JA-1)) 00001733
1986. 1)*(P(I+1,JA)-P(I-1,JA-1)-P(I-1,JA)+P(I-1,JA-1))/(2.*DS*DE))) 00001734
1987. 16 CONTINUE 00001735
1988. UU=U*U 00001736
1989. GB=A11/(1.+TAN(PI2*YU(I)))**2) 00001737
1990. V=Q1*(SIN(ALP)+GB*((-3.*P(I,JA-1)+4.*P(I,JA)-P(I,JA+1))/(2.*DE) 00001738
1991. 1+(YU(I)-E(JA-1))*(P(I,JA-1)-2.*P(I,JA)+P(I,JA+1))/(DE**2))) 00001739
1992. 101 VV=V*V 00001740
1993. YU(I)=TEMP2 00001741
1994. 1 CPU(I)=(1./(O.7*M*M))*((1.+O.2*M*M*(1.-(UU+VV)/QI2))**3.5-1.) 00001742
1995. ITE1=ITE+1 00001743
1996. DO 4 I=ILE1,IMAX 00001744
1997. TEMP1=PB(I) 00001745
1998. PB(I)=P(I,JB) 00001746
1999. 4 P(I,JB)=TEMP1 00001747
2000. JB2=JB+2 00001748
2001. DO 5 I=ILE,IEND 00001749
2002. TEMP2=YL(I) 00001750
2003. IF(I.GT.ITE)YL(I)=-O.0001 00001751
2004. DO 6 JJ=1,JB 00001752
2005. J=JB2-JJ 00001753
2006. IF(YL(I).GE.E(J).AND.YL(I).LT.E(J+1))GO TO 7 00001754
2007. 6 CONTINUE 00001755
2008. 7 JA=J 00001756
2009. IF(JA.GE.JB)JA=JB-1 00001757
2010. F=FF(I) 00001758
2011. IF(IPRM.EQ.2)GO TO 21 00001759
2012. IF(I.GT.(ILE+1))GO TO 17 00001760

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2013. 21 U=O.O                                00001761
2014. U=QI*(COS(ALP)+F*(P(I+1,JA+1)-P(I-1,JA+1)))/(2.*DS)+(YL(I)-E(JA+1))00001762
2015. 1*(P(I+1,JA+1)-P(I+1,JA)-P(I-1,JA+1)+P(I-1,JA))/(2.*DS+DE))) 00001763
2016. GO TO 18                                00001764
2017. 17 CONTINUE                             00001765
2018. C U USING BACKWARDS DIFFERENCE SCHEME ON PHIX 00001766
2019. U=QI*(COS(ALP)+F*(3.*P(I,JA+1)-4.*P(I-1,JA+1)+P(I-2,JA+1)))/(2.*DS00001767
2020. 1)+(YL(I)-E(JA+1)) 00001768
2021. 1*(P(I+1,JA+1)-P(I+1,JA)-P(I-1,JA+1)+P(I-1,JA))/(2.*DS*DE))) 00001769
2022. 18 CONTINUE                             00001770
2023. UU=U*U 00001771
2024. GB=A11/(1.+TAN(YL(I)*PI2)**2) 00001772
2025. V=QI*(SIN(ALP)+GB*((3.*P(I,JA+1)-4.*P(I,JA)+P(I,JA-1)))/(2.*DE)+ 00001773
2026. 1*(YL(I)-E(JA+1))*(P(I,JA+1)-2.*P(I,JA)+P(I,JA-1))/(DE**2))) 00001774
2027. VV=V*V 00001775
2028. YL(I)=TEMP2 00001776
2029. 5 CPL(I)=(1./(O.7*M*M))*(((O.2*M*M*(1.-((UU+VV)/QI2)))*3.5-1.) 00001777
2030. DO 8 I=ILE1,IMAX 00001778
2031. TEMP1=PB(I) 00001779
2032. PB(I)=P(I,JB) 00001780
2033. P(I,JB)=TEMP1 00001781
2034. IF(ITACT.EQ.1)RETURN 00001782
2035. 11 IF(IPRM.EQ.1)PRINT 200 00001783
2036. 200 FORMAT(1H,'CP BY BACKWARD DIFFERENCES') 00001784
2037. IF(IPRM.EQ.2)PRINT 201 00001785
2038. 201 FORMAT(1H,'CP BY CENTRAL DIFFERENCES') 00001786
2039. PRINT 12 00001787
2040. 12 FORMAT(1H,'X',10X,'CPU',10X,'CPL') 00001788
2041. PRINT 13,(X(I),CPU(I),CPL(I),I=ILE,IMAX1) 00001789
2042. 13 FORMAT(1H,'3F10.3) 00001790
2043. IF(IPRM.LT.2)GO TO 19 00001791
2044. RETURN 00001792
2045. END 00001793
2046. SUBROUTINE FLOW1 00001794
2047. C ***** SOLVES FLOW IN FRONT OF THE AIRFOIL ***** 00001795
2048. C 00001796
2049. C 00001797
2050. REAL M 00001798
2051. COMMON CPU(99),CPL(99),F(99),DU1(99),DU2(99),DL1(99),DL2(99),D(99)00001799
2052. 1,FF(99),FFP12(99),FFM12(99),FFM1(99),FFM32(99), 00001800
2053. 1P1(99),P2(99),PB(99),P(99,99),RS(99),S(99),SUP(99),SUB(99),TEMP(99)00001801
2054. 2),X(99),Y(99),YU(99),YL(99),SLU(99),SLL(99), 00001802
2055. 3A1,A2,AI2,ALP,CIR,EPS,EPS,DE,DS,DP,DPM,F,FP12,FM12,FM32,M,QI,QI2,00001803
2056. 4W,X1,X2,VVJB,VVJB1,AAJB,AAJB1,AAJB,QQJB,QQJB1,QQJB,VVJBP1,AAJBP1,00001804
2057. 5,Q,QQ,UUJB1,PI,PI2,A22,A11,X4,S4 00001805
2058. COMMON I,ITE,ITE1,ILE,ILE1,I1,I11,ICON,IMAX,IMAX1,INV,JB,JA1,JB1, 00001806
2059. 1,UMAX,JCON,UMAX1,NSSP,IW 00001807
2060. RELAXES FLOW IN FRONT OF AIRFOIL 00001808
2061. C***** ADDITION ***** 00001809
2062. JB=JMAX/2+1 00001810
2063. NSSP=O 00001811
2064. C***** ADDITION ***** 00001812
2065. C***** ADDITION ***** 00001813
2066. FFM32(2)=O.O 00001814
2067. C***** ADDITION ***** 00001815
2068. ISTAR=2
2069. IF(M.LT.1.O)GO TO 1
2070. ISTAR=3
2071. DO 2 J=1,UMAX
2072. P1(J)=P(2,J)
2073. 2 P2(J)=P(1,J)

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2074. 1 CONTINUE
2075. AI=1117.0
2076. AI2=AI**2
2077. QI=M*AI
2078. QI2=QI**2
2079. DO 1000 I=ISTAR,ILE1
2080. F=FF(I)
2081. FP12=FFP12(I)
2082. FM12=FFM12(I)
2083. FM32=FFM32(I)
2084. CALL SOLVE(2,JMAX1)
2085. RS(2)=RS(2)-SUB(1)*P(I,1)
2086. RS(JMAX1)=RS(JMAX1)-SUP(JMAX1)*P(I,JMAX)
2087. CALL TRID(2,JMAX1)
2088. DO 6 J=2,JMAX1
2089. DP=ABS(P(I,J)-RS(J))
2090. IF(DP.GT.DPM)ICON=I
2091. IF(DP.GT.DPM)JCON=J
2092. IF(DP.GT.DPM)DPM=DP
2093. P2(J)=P1(J)
2094. P1(J)=P(I,J)
2095. 6 P(I,J)=RS(J)
2096. P2(1)=P1(1)
2097. P2(JMAX)=P1(JMAX)
2098. P1(1)=P(I,1)
2099. P1(JMAX)=P(I,JMAX)
2100. 1000 CONTINUE
2101. RETURN
2102. END
2103. SUBROUTINE COORD
2104.
2105. C ***** SETS UP COORDINATES IN COMPUTATIONAL AND PHYSICAL GRIDS *
2106. C
2107. REAL M
2108. COMMON CPU(99),CPL(99),E(99),DU1(99),DU2(99),DL1(99),DL2(99),D(99),D(99),D(99)
2109. 1,FF(99),FFP12(99),FFM12(99),FFM1(99),FFM32(99),
2110. 1P1(99),P2(99),PB(99),P(99,99),RS(99),S(99),SUP(99),SUB(99),TEMP(99)
2111. 2,X(99),Y(99),YU(99),YL(99),SLU(99),SLL(99),
2112. 3A1,A2,AI2,ALP,CIR,EPS,EPSS,DE,DS,DP,DPM,F,FP12,FM12,FM32,M,QI,QI2,
2113. 4W,X1,X2,VVJB,VVJB1,AAJB1,AAJB,QQJB,QQJB1,UUJB,VVJB1,AAJB1,AAJB1,
2114. 5,Q,QQ,UUB1,PI,PI2,A22,A11,X4,S4
2115. COMMON I,ITE,ITE1,ILE,ILE1,I1,I11,ICON,IMAX,IMAX1,INV,JB,JA1,JB1,
2116. 1JMAX,JCON,JMAX1,NSSP,IW
2117. COMMON/FIX/MHALF
2118. COMMON/JS/GG(99),GGP12(99),GGM12(99),GGM32(99),GGP32(99),A3
2119. DE=2.0/(JMAX-1)
2120. IF(INV.EQ.0)GO TO 999
2121. READ 997,X1,X2
2122. 997 FORMAT(2F10.5)
2123. 999 CONTINUE
2124. DS=2.*(1.+S4)/(IMAX-1)
2125. C THIS PROGRAM DEPENDS UPON TRANSFORMATION USED
2126. S(1)=-1.0-S4
2127. E(1)=-1.0
2128. S(IMAX)=1.0+S4
2129. E(JMAX)=1.0
2130. IMAX1=IMAX-1
2131. JMAX1=JMAX-1
2132. DO 2 I=2,IMAX1
2133. 2 S(I)=S(I-1)+DS.
2134. S3=-S4+0.5+DS-0.01

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2135. DO 11 I=1,IMAX1
2136. IF(S3.GE.S(I).AND.S3.LT.S(I+1))GO TO 12
2137. 11 CONTINUE
2138. 12 I3=I+1
2139. I31=I3-1
2140. IM=IMAX/2+1
2141. I4=IMAX-I31
2142. I41=I4+1
2143. DO 13 I=2,I31
2144. X(I)=-X4+A2*TAN(PI2*(S(I)+S4))+A3*TAN(PI2*(S(I)+S4)**3)
2145. TERM1=1.5*X4/S4-.25*PI*A2
2146. TERM2=(.5*PI*A2*S4-X4)/(2.*S4**3)
2147. DO 14 I=I3,I4
2148. X(I)=S(I)*(TERM1+TERM2*S(I)**2)
2149. DO 16 I=I41,IMAX1
2150. X(I)=X4+A2*TAN(PI2*(S(I)-S4))+A3*TAN(PI2*(S(I)-S4)**3)
2151. DO 3 J=2,JMAX1
2152. E(J)=E(J-1)+DE
2153. 3 Y(J)=A1*TAN(PI2*E(J))
2154. PRINT 4
2155. 4 FORMAT(//,25X,'X-Y GRID SYSTEM',//)
2156. PRINT 5,(I,X(I),I=2,IMAX1)
2157. 5 FORMAT( 6(I5,E12.4))
2158. PRINT 5,(J,Y(J),J=2,JMAX1)
2159. DO 7 I=2,IMAX1
2160. IF(X1.GE.X(I).AND.X1.LT.X(I+1))GO TO 8
2161. 7 CONTINUE
2162. 8 I1=I+1
2163. SLE=-0.5
2164. DO 9 I=2,IMAX1
2165. IF(SLE.GE.X(I).AND.SLE.LE.X(I+1))GO TO 10
2166. 9 CONTINUE
2167. 10 ILE=I+1
2168. QUAN1=S(2)+S4
2169. FF(2)=PI2*A2*(1.+TAN(PI2*QUAN1)**2)+1.5*A3*(1.+TAN(PI2*QUAN1**300001911
2170. 1)**2)*(QUAN1**2)*PI
2171. FF(2)=1./FF(2)
2172. QUAN1=S(2)+0.5*DS+S4
2173. FFP12(2)=PI2*A2*(1.+TAN(PI2*QUAN1)**2)+1.5*A3*(1.+TAN(PI2*QUAN1**300001915
2174. 1)**2)*(QUAN1**2)*PI
2175. FFP12(2)=1./FFP12(2)
2176. QUAN1=S(2)-0.5*DS+S4
2177. FFM12(2)=PI2*A2*(1.+TAN(PI2*QUAN1)**2)+1.5*A3*(1.+TAN(PI2*QUAN1**300001919
2178. 1)**2)*(QUAN1**2)*PI
2179. FFM12(2)=1./FFM12(2)
2180. FFM1(2)=0.0
2181. DO 18 I=3,I31
2182. QUAN1=S(I)+S4
2183. FF(I)=PI2*A2*(1.+TAN(PI2*QUAN1)**2)+1.5*A3*(1.+TAN(PI2*QUAN1**300001924
2184. 1)**2)*(QUAN1**2)*PI
2185. FF(I)=1./FF(I)
2186. QUAN1=S(I)+0.5*DS+S4
2187. FFP12(I)=PI2*A2*(1.+TAN(PI2*QUAN1)**2)+1.5*A3*(1.+TAN(PI2*QUAN1**300001928
2188. 1)**2)*(QUAN1**2)*PI
2189. FFP12(I)=1./FFP12(I)
2190. FFM12(I)=FFP12(I-1)
2191. FFM1(I)=FF(I-1)
2192. FFM32(I)=FFM12(I-1)
2193. FFP12(I31)=1./((TERM1+3.*TERM2*(S(I31)+0.5*DS)**2)
2194. IM1=IM-1
2195. DO 19 I=I3,IM

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2196. FF(I)=1./((TERM1+3.*TERM2*S(I))**2)
2197. FFP12(I)=1./((TERM1+3.*TERM2*(S(I)+O.5*DS) **2)
2198. FFM12(I)=FFP12(I-1)
2199. FFM1(I)=FF(I-1)
2200. FFM32(I)=FFM12(I-1)
2201. FFP12(IM)=FFM12(IM)
2202. DO 800 II=2,IM1
2203. I=IMAX-II+1
2204. FF(I)=FF(II)
2205. FFP12(I)=FFM12(II)
2206. FFM12(I)=FFP12(II)
2207. FFM1(I)=FF(II+1)
2208. FFM32(I)=FFP12(II+1)
2209. GGP32(2)=A11*COS(PI2*(E(3)+O.5*DE))**2
2210. GG(2)=A11*COS(PI2*(E(2))**2)
2211. GGP12(2)=A11*COS(PI2*(E(2)+O.5*DE))**2
2212. GGM12(2)=A11*COS(PI2*(E(2)-O.5*DE))**2
2213. GGM32(2)=O.O
2214. DO 801 J=3,JMAX1
2215. IF(J.EQ.JMAX1)GO TO 804
2216. GGP32(J)=A11*COS(PI2*(E(J)+1.5*DE))**2
2217. GG(J)=A11*COS(PI2*(E(J))**2)
2218. GGP12(J)=A11*COS(PI2*(E(J)+O.5*DE))**2
2219. GGM12(J)=GGP12(J-1)
2220. GGM32(J)=GGM12(J-1)
2221. GGP32(JMAX1)=O.O
2222. RETURN
2223. END
2224. SUBROUTINE FLOW3
2225.
2226. C
2227. C ***** SOLVES FOW IN THE INVERSE REGION *****
2228. C
2229. REAL M
2230. COMMON CPU(99),CPL(99),E(99),DU1(99),DU2(99),DL1(99),DL2(99),D(99)
2231. 1,FF(99),FFP12(99),FFM12(99),FFM1(99),FFM32(99),
2232. 1P1(99),P2(99),PB(99),P(99),RS(99),S(99),SUP(99),SUB(99),TEMP(99)
2233. 2),X(99),Y(99),YU(99),YU(99),SLL(99),
2234. 3A1,A2,AI2,ALP,CIR,EPS,EPSS,DE,DS,DP,DPM,F,FP12,FM12,FM32,M,QI,QI2,
2235. 4W,X1,X2,VVUB,VVUB1,AAJB,AAJB1,AAJB,QQJB,QQJB1,UUUB,VVUBP1,AAJBP1,
2236. 5,O,QQ,UUUB1,PI,PI2,A22,A11,X4,S4
2237. COMMON I,ITE,ITE1,ILE,ILE1,I1,I11,ICON,IMAX,IMAX1,INV,JB,JA1,JB1,
2238. 1JMAX,JCON,JMAX1,NSSP,IW
2239. COMMON/BAKER/TEMP3,TEMP4
2240. COMMON/DELTA/ITER
2241. COMMON/FIX/MHALF
2242. COMMON/TPT2/IMASS
2243. RELAXES FLOW IN INVERSE REGION
2244. JA=JA1
2245. IS=I1-2
2246. DO 14 I=IS,IMAX
2247. 14 TEMP(I)=P(I,JB-1)
2248. DO 3000 I=I1,IMAX1
2249. IF(X(I).GE.X2)GO TO 3100
2250. FLOW ABOVE AIRFOIL
2251. JB=JB-2
2252. DO 3 J=JB2,JMAX1
2253. IF(YU(I).GT.E(J).AND.YU(I).LE.E(J+1))GO TO 4
2254. 3 CONTINUE
2255. 4 JA=J+1
2256. IF(JA.LE.JB)JA=JB+1
2257. F=FF(I)
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2257. FP12=FFP12(I)
2258. FM12=FFM12(I)
2259. FM1=FFM1(I)
2260. FM32=FFM32(I)
2261. GB=A11/(1.+TAN(YU(I) )+PI2)**2)
2262. VV=SLU(I)**2
2263. UU=1.0
2264. 4000 DU1(I)=-COS(ALP)+(1./(1.+VV/UU))*(1.-((1.+O.7*M*M*CPU(I) )**O.28
16-1.)*5./(M*M)))*O.5-F*((-4.*P1(JA-1)+P2(JA-1))/(2.*DS))
2265. 2-F*(YU(I)-E(JA-1))*(P(I+1,JA)-P(I+1,JA-1)-P1(JA)+P1(JA-1))/(2.
2266. 3*DS*DE)
2267. DU1(I)=DU1(I)/(F*(1.5/DS))
2268. 4001 CONTINUE
2269. DU2(I)=-P(I,JA)+2.0*DU1(I)
2270. P(I,JA-1)=DU1(I)
2271. P(I,JA-2)=DU2(I)
2272. CALL SOLVE(JA,JMAX1)
2273. RS(JA)=RS(JA)-SUB(JA-1)*P(I,JA-1)
2274. RS(JMAX1)=RS(JMAX1)-SUP(JMAX1)*P(I,JMAX)
2275. CALL TRID(JA,JMAX1)
2276. DO 1 J=JA,JMAX1
2277. DP=ABS(P(I,J)-RS(J))
2278. IF(DP.GT.DPM)ICON=I
2279. IF(DP.GT.DPM)JCON=J
2280. IF(DP.GT.DPM)DPM=DP
2281. P2(J)=P1(J)
2282. P1(J)=P(I,J)
2283. 1 P(I,J)=RS(J)
2284. JAM1=JA-1
2285. DO 2 J=JB,JAM1
2286. P2(J)=P1(J)
2287. P1(J)=P(I,J)
2288. 2 P1(J)=P(I,J)
2289. VV=SLU(I)**2
2290. UU=1.0
2291. 4002 DU1(I)=-COS(ALP)+(1./(1.+VV/UU))*(1.-((1.+O.7*M*M*CPU(I) )**O.28
2292. 16-1.)*5./(M*M)))*O.5-F*((-4.*P(I-1,JA-1)+P(I-2,JA-1))/(2.*DS))
2293. 2-F*(YU(I)-E(JA-1))*(P(I+1,JA)-P(I+1,JA-1)-P(I-1,JA)+P(I-1,JA-1))/
2294. 3(2.*DS*DE)
2295. DU1(I)=DU1(I)/(F*(1.5/DS))
2296. 4003 CONTINUE
2297. DU2(I)=-P(I,JA)+2.0*DU1(I)
2298. P(I,JA-1)=DU1(I)
2299. P(I,JA-2)=DU2(I)
2300. P2(JMAX)=P1(JMAX)
2301. P1(JMAX)=P(I,JMAX)
2302. JA1=JA
2303. 3000 CONTINUE
2304. 3100 JA=JB1
2305. DO 5 I=IS,IMAX
2306. P(I,JB-1)=TEMP(I)
2307. TEMP(I)=P(I,JB+1)
2308. TEMP1=PB(I)
2309. PB(I)=P(I,JB)
2310. 5 P(I,JB)=TEMP1
2311. 6 TEMP1=TEMP4
2312. TEMP4=P1(JB)
2313. P1(JB)=TEMP1
2314. TEMP1=TEMP3
2315. TEMP3=P2(JB)
2316. P2(JB)=TEMP1
2317. IF(IMASS.EQ.1)GO TO 3600

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2318. DO 3500 I=I1,IMAX1
2319. FLOW BELOW AIRFOIL
2320. IF(X(I).GE.X2)GO TO 3600
2321. JB2=JB+2
2322. DO 10 JU=1,JB
2323. J=JB2-JU
2324. IF(YL(I).GE.E(J).AND.YL(I).LT.E(J+1))GO TO 11
2325. 10 CONTINUE
2326. 11 JA=J
2327. IF(JA.GE.JB)JA=JB-1
2328. F=FF(I)
2329. FP12=FFP12(I)
2330. FM12=FFM12(I)
2331. FM1=FFM1(I)
2332. FM32=FFM32(I)
2333. GB=A11/(1.+TAN(YL(I) )*PI2)**2)
2334. VV=SLL(I)**2
2335. UU=1.0
2336. 4004 DL1(I)=-COS(ALP)+((1./(1.+VV/UU))*(1.-((1.+0.7*M*M*CPL(I) )**0.2800002078
16-1. )*5./(M*M))**0.5-F*((-4.*P1(JA+1)+P2(JA+1))/(2.*DS) )
2337. 2-F*(YL(I)-E(JA+1))*(P(I+1,JA+1)-P(I+1,JA)-P1(JA+1)+P1(JA))/(2.
2338. 3*DS*DE)
2339. DL1(I)=DL1(I)/(F*(1.5/DS) )
2340. 4005 CONTINUE
2341. DL2(I)=2.*DL1(I)-P(I,JA)
2342. P(I,JA+1)=DL1(I)
2343. P(I,JA+2)=DL2(I)
2344. CALL SOLVE(2,JA)
2345. RS(2)=RS(2)-SUB(1)*P(I,1)
2346. RS(JA)=RS(JA)-SUP(JA)*P(I,JA+1)
2347. CALL TRID(2,JA)
2348. DO 7 J=2,JA
2349. DP=ABS(P(I,J)-RS(J) )
2350. IF(DP.LE.DPM)GO TO 8
2351. ICON=I
2352. JCON=J
2353. DPM=DP
2354. 8 P2(J)=P1(J)
2355. P1(J)=P(I,J)
2356. 7 P(I,J)=RS(J)
2357. JAM1=JA+1
2358. DO 9 J=JAM1,JB
2359. P2(J)=P1(J)
2360. P1(J)=P(I,J)
2361. 9 P1(J)=P(I,J)
2362. VV=SLL(I)**2
2363. UU=1.0
2364. 4006 DL1(I)=-COS(ALP)+((1./(1.+VV/UU))*(1.-((1.+0.7*M*M*CPL(I) )**0.2800002106
16-1. )*5./(M*M))**0.5-F*((-4.*P(I-1,JA+1)+P(I-2,JA+1))/(2.*DS) )
2365. 2-F*(YL(I)-E(JA+1))*(P(I+1,JA+1)-P(I+1,JA)-P(I-1,JA)+P(I-1,JA) )/
2366. 3(2.*DS*DE)
2367. DL1(I)=DL1(I)/(F*(1.5/DS) )
2368. 4007 CONTINUE
2369. DL2(I)=2.*DL1(I)-P(I,JA)
2370. P(I,JA+1)=DL1(I)
2371. P(I,JA+2)=DL2(I)
2372. P2(1)=P1(1)
2373. P1(1)=P(I,1)
2374. JB1=JA
2375. 3500 CONTINUE
2376. 3600 DO 12 I=IS,IMAX
2377. P(I,JB+1)=TEMP(I)
2378.

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2379. TEMP1=PB(I)
2380. PB(I)=P(I,JB)
2381. P(I,JB)=TEMP1
2382. P1(JB)=TEMP4
2383. P2(JB)=TEMP3
2384. RETURN
2385. END
2386. SUBROUTINE FLOW2
2387.
2388. C
2389. C ***** SOLVES FLOW IN THE DRICT REGION *****
2390. C
2391. REAL M
2392. COMMON CPU(99),CPL(99),E(99),DU1(99),DU2(99),DL1(99),DL2(99),D(99)
2393. 1,FF(99),FFP12(99),FFM12(99),FFM1(99),FFM32(99)
2394. 1P1(99),P2(99),PB(99),P(99,99),RS(99),S(99),SUP(99),SUB(99),TEMP(99)
2395. 2),X(99),Y(99),YU(99),YL(99),SLU(99),SLL(99)
2396. 3A1,A2,A12,ALP,CIR,EPS,EPSS,DE,DS,DP,DPM,F,FP12,FM12,FM32,M,QI,QI2,
2397. 4W,X1,X2,VVJB,VVJB1,AAJB1,AAJB,QQJB,QQJB1,UUJB,VVJB1,QQJB1,AAJB1,
2398. 5,Q,QQ,UUJB1,PI,PI2,A22,A11,X4,S4
2399. COMMON I,ITE,ITE1,ILE,ILE1,I1,I11,ICON,IMAX,IMAX1,INV,JB,JA1,JB1,
2400. 1JMAX,JCON,JMAX1,NSSP,IW
2401. COMMON/BAKER/TEMP3,TEMP4
2402. COMMON/IPT2/IMASS
2403. RELAXES FLOW ABOVE AND BELOW AIRFOIL
2404. JB=JMAX/2+1
2405. JB1=JB-1
2406. JA1=JB+1
2407. JB2=JB-2
2408. TEMP5=P1(JB)
2409. TEMP6=P2(JB)
2410. DO 12 I=ILE,ITE1
2411. TEMP(I)=P(I,JB-1)
2412. IF(ILE.GT.I11)GO TO 2001
2413. DO 2000 I=ILE,I11
2414. FLOW ABOVE AIRFOIL
2415. F=FF(I)
2416. FP12=FFP12(I)
2417. FM12=FFM12(I)
2418. FM32=FFM32(I)
2419. GB=A11/(1.+TAN(PI2*YU(I)))**2)
2420. DO 1 J=JB2,JMAX1
2421. IF(YU(I).GT.E(J).AND.YU(I).LE.E(J+1))GO TO 2
2422. 1 CONTINUE
2423. 2 JA=J+1
2424. IF(JA.LE.JB)JA=JB+1
2425. DU1(I)=SLU(I)*(COS(ALP)+F*(P(I+1,JA-1)-P1(JA-1)))/(2.*DS)
2426. 1+(YU(I)-E(JA-1))*(P(I+1,JA)-P(I+1,JA-1)-P1(JA)+P1(JA-1))/(2.*DS*DE
2427. 2)))-SIN(ALP)-GB*(4.*P(I,JA)-P(I,JA+1))/(2.*DE)+(YU(I)-E(JA-1))*
2428. 3(-2.*P(I,JA)+P(I,JA+1))/(DE**2))
2429. DU1(I)=DU1(I)/(-1.5*GB/DE + (YU(I)-E(JA-1))/(DE**2)*GB)
2430. DU2(I)=P(I,JA)+DU1(I)**2.O
2431. P(I,JA-1)=DU1(I)
2432. P(I,JA-2)=DU2(I)
2433. CALL SOLVE(JA,JMAX1)
2434. RS(JA)=RS(JA)-SUB(JA-1)*P(I,JA-1)
2435. RS(JMAX1)=RS(JMAX1)-SUP(JMAX1)*P(I,JMAX1)
2436. CALL TRID(JA,JMAX1)
2437. DO 4 J=JA,JMAX1
2438. DP=ABS(P(I,J)-RS(J))
2439. IF(DP.GT.DPM)ICON=I
2440. IF(DP.GT.DPM)JCON=J
2441.
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2440. IF(DP.GT.DPM)DPM=DP
2441. P2(J)=P1(J)
2442. P1(J)=P(I,J)
2443. 4 P(I,J)=RS(J)
2444. JAM1=JA-1
2445. DO 5 J=JB,JAM1
2446. P2(J)=P1(J)
2447. P1(J)=P(I,J)
2448. 5 P2(JMAX)=P1(JMAX)
2449. P1(JMAX)=P(I,JMAX)
2450. JA1=JA
2451. DU1(I)=SLU(I)*(COS(ALP)+F*(P(I+1,JA-1)-P(I-1,JA-1)))/(2.*DS)
2452. 1+(YU(I)-E(JA-1))*P(I+1,JA)-P(I+1,JA-1)-P(I-1,JA)+P(I-1,JA-1))/
2453. 2(2.*DS*DE)))-SIN(ALP)-GB*(4.*P(I,JA)-P(I,JA+1))/(2.*DE)+
2454. 3(YU(I)-E(JA-1))*(-2.*P(I,JA)+P(I,JA+1))/(DE**2))
2455. DU1(I)=DU1(I)/(-1.5*GB/DE+(YU(I)-E(JA-1))/(DE**2))*GB)
2456. DU2(I)=-P(I,JA)+DU1(I)*2.0
2457. P(I,JA-1)=DU1(I)
2458. P(I,JA-2)=DU2(I)
2459. 2000 CONTINUE
2460. 2001 CONTINUE
2461. TEMP3=P2(JB)
2462. TEMP4=P1(JB)
2463. FLOW BELOW AIRFOIL
2464. DO 8 I=ILE,ITE1
2465. P(I,JB-1)=TEMP(I)
2466. TEMP(I)=P(I,JB+1)
2467. TEMP1=PB(I)
2468. PB(I)=P(I,JB)
2469. P(I,JB)=TEMP1
2470. 8 CONTINUE
2471. P1(JB)=TEMP5
2472. P2(JB)=TEMP6
2473. ITEMP1=I1
2474. ITEMP11=I11
2475. IF(IMASS.EQ.1)I1=ITE+1
2476. IF(IMASS.EQ.1)I11=ITE
2477. IF(ILE.GT.I11)GO TO 2501
2478. DO 2500 I=ILE,I11
2479. GB=A11/(1.+TAN(PI2*YL(I))*2)
2480. F=FF(I)
2481. FP12=FFP12(I)
2482. FM12=FFM12(I)
2483. FM32=FFM32(I)
2484. DO 6 JJ=1,JMAX1
2485. J=JB-JJ+2
2486. IF(YL(I).GE.E(J).AND.YL(I).LT.E(J+1))GO TO 7
2487. 6 CONTINUE
2488. 7 JA=J
2489. IF(JA.GE.JB)JA=JB-1
2490. DL1(I)=SLU(I)*(COS(ALP)+F*(P(I+1,JA+1)-P(I+1,JA-1)))/(2.*DS)+
2491. 1(YL(I)-E(JA+1))*P(I+1,JA+1)-P(I+1,JA)-P(I,JA+1)+P1(JA))/(2.*DS*DE)
2492. 2)-SIN(ALP)-GB*((-4.*P(I,JA)+P(I,JA-1)))/(2.*DE)+(YL(I)-E(JA+1))*
2493. 3(-2.*P(I,JA)+P(I,JA-1))/(DE**2))
2494. DL1(I)=DL1(I)/(1.5*GB/DE+(YL(I)-E(JA+1))/(DE**2))*GB)
2495. DL2(I)=2.*DL1(I)-P(I,JA)
2496. P(I,JA+1)=DL1(I)
2497. P(I,JA+2)=DL2(I)
2498. CALL SOLVE(2,JA)
2499. RS(2)=RS(2)-SUB(4)*P(I,1)
2500. RS(JA)=RS(JA)-SUP(JA)*P(I,JA+1)
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2501. CALL TRID(2,JA)
2502. DO 9 J=2,JA
2503. DP=ABS(P(I,J)-RS(J))
2504. IF(DP.GT.DPM)ICON=I
2505. IF(DP.GT.DPM)JCON=J
2506. IF(DP.GT.DPM)DPM=DP
2507. P2(J)=P1(J)
2508. P1(J)=P(I,J)
2509. 9 P(I,J)=RS(J)
2510. JAM1=JA+1
2511. DO 10 J=JAM1,JB
2512. P2(J)=P1(J)
2513. 10 P1(J)=P(I,J)
2514. P2(1)=P1(1)
2515. P1(1)=P(I,1)
2516. JBT=JA
2517. DL1(I)=SLL(I)*(COS(ALP)+F*((P(I+1,JA+1)-P(I-1,JA+1))/(2.*DS))+
2518. 1*(YL(I)-E(JA+1))*(P(I+1,JA+1)-P(I+1,JA)-P(I-1,JA+1)+P(I-1,JA))/(2.
2519. 2*DS*DE)))-SIN(ALP)-GB*(-4.*P(I,JA)+P(I,JA-1))/(2.*DE)+(YL(I)-E(
2520. 3JA+1))*(-2.*P(I,JA)+P(I,JA-1))/(DE**2))
2521. DL1(I)=DL1(I)/(1.5*GB/DE+(YL(I)-E(JA+1))/(DE**2)*GB)
2522. DL2(I)=2.*DL1(I)-P(I,JA)
2523. P(I,JA+1)=DL1(I)
2524. P(I,JA+2)=DL2(I)
2525.
2526. 2500 CONTINUE
2527. 2501 CONTINUE
2528. DO 11 I=ILE,ITE1
2529. P(I,JB+1)=TEMP(I)
2530. TEMP1=PB(I)
2531. PB(I)=P(I,JB)
2532. 11 P(I,JB)=TEMP1
2533. TEMP1=TEMP4
2534. P1(JB)=TEMP1
2535. TEMP1=TEMP3
2536. TEMP3=P2(JB)
2537. P2(JB)=TEMP1
2538. PB(ILE1)=P(ILE1,JB)
2539. PB(ILE-2)=P(ILE-2,JB)
2540. I1=ITMP1
2541. I1=ITMP11
2542. RETURN
2543. END
2544. SUBROUTINE WAKE
2545.
2546. C ***** SOLVES FLOW BEHIND THE AIRFOIL *****
2547. C
2548. C
2549. REAL M
2550. COMMON CPU(99),CPL(99),E(99),DU1(99),DU2(99),DL1(99),DL2(99),D(99)
2551. 1,FF(99),FFP12(99),FFM12(99),FFM1(99),FFM32(99),
2552. 1P1(99),P2(99),PB(99),P(99,99),RS(99),S(99),SUP(99),SUB(99),TEMP(99)
2553. 2),X(99),Y(99),YU(99),YL(99),SLU(99),SLL(99),
2554. 3A1,A2,A12,ALP,CIR,EPS,EPSS,DE,DS,DP,DPM,F,FP12,FM12,FM32,M,QI,QI2,
2555. 4W,X1,X2,VVJR,VVJB1,AAJB1,AAJB,QQJB,QQJB1,UUJB,VVJB1,QQJB1,AAJB1,
2556. 5,Q,QQ,UUJB1,PI,PI2,A22,A11,X4,S4
2557. COMMON I,ITE,ITE1,ILE,ILE1,I1,I11,ICON,IMAX,IMAX1,INV,JB,JA1,JB1,
2558. 1JMAX,JCON,JMAX1,NSSP,IW
2559. COMMON/ADAM/VJB,VJB1,VJBP1
2560. COMMON/IPT2/IMASS
2561. RELAXES FLOW IN WAKE DIRECTLY
2562. DIMENSION PTEMP(99)

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2562. I MARK=O
2563. IF (IMASS.EQ.O)GO TO 100
2564. JB2=JB-1
2565. DO 101 J=JB2, JMAX1
2566. IF (YU(ITE).GT.E(J).AND.YU(ITE).LE.E(J+1))GO TO 102
2567. 101 CONTINUE
2568. JA=J+1
2569. 102
2570. IF (JA.LE.JB)JA=JB+1
2571. STE=S4+2./PI*ATAN((O.5-X4)/A2)
2572. QUAN1=STE-S4
2573. F=PI*A2*O.5*(1.+TAN(PI2*QUAN1)**2)
2574. F=1./F
2575. JAM1=JA-1
2576. DO 103 J=JB, JAM1
2577. I MARK=1
2578. PTEMP(J)=P(ITE, J)
2579. P(ITE, J)=O.5/F* CPU(I1)+(4.*P(ITE+1, J)-P(ITE+2, J))/(2.*DS)
2580. 1+(STE-S(ITE))*(-2.*P(ITE+1, J)+P(ITE+2, J))/(DS*DS)
2581. P(ITE, J)=P(ITE, J)/(1.5/DS-(STE-S(ITE)))/(DS*DS))
2582. P2(J)=-P(ITE+1, J)+2.*P1(J)
2583. 103 CONTINUE
2584. 100 CONTINUE
2585. I W=1
2586. DO 4000 I=ITE1, I MAX1
2587. F=FF(I)
2588. FP12=FFP12(I)
2589. FM12=FFM12(I)
2590. FM32=FFM32(I)
2591. CALL SOLVE(2, JMAX1)
2592. RS(2)=RS(2)-SUB(1)*P(I, 1)
2593. RS(JMAX1)=RS(JMAX1)-SUP(JMAX1)*P(I, JMAX)
2594. IF (QQJBP1.LE.AAJBP1)GO TO 1
2595. IF (VJBP1.LT.O.)GO TO 1
2596. G=A11/(1.+TAN(PI2*E(JB+1))**2)
2597. GM32=A11/(1.+TAN(PI2*(E(JB+1)-1.5*DE))**2)
2598. RS(JB+1)=RS(JB+1)-(1.-QQJBP1/AAJBP1)*(VVJBP1/QQJBP1+G*GM32*CIR/
2599. 1(DE**2))
2600. 1 IF (QQJB.LE.AAJB)GO TO 2
2601. IF (VJB.LT.O.)GO TO 3
2602. G=A11/(1.+TAN(PI2*E(JB))**2)
2603. GM12=A11/(1.+TAN(PI2*(E(JB)-O.5*DE))**2)
2604. RS(JB)=RS(JB)+(1.-QQJB/AAJB)*(VVJB/QQJB*G*GM12*CIR/(DE**2))
2605. 1-UUJB/QQJB*G*GM12*CIR/(DE**2)
2606. GO TO 4
2607. 3 G=A11/(1.+TAN(PI2*E(JB))**2)
2608. GM12=A11/(1.+TAN(PI2*(E(JB)-O.5*DE))**2)
2609. RS(JB)=RS(JB)-UUJB/QQJB*G*GM12*CIR/(DE**2)
2610. GO TO 4
2611. 2 G=A11/(1.+TAN(PI2*E(JB))**2)
2612. C=(1.-VVJB/AAJB)*G
2613. GM12=A11/(1.+TAN(PI2*(E(JB)-O.5*DE))**2)
2614. RS(JB)=RS(JB)-C*GM12*CIR/(DE**2)
2615. 4 IF (QQJB1.GT.AAJB1)GO TO 5
2616. G=A11/(1.+TAN(PI2*E(JB-1))**2)
2617. C=(1.-VVJB1/AAJB1)*G
2618. GP12=A11/(1.+TAN(PI2*(E(JB-1)+O.5*DE))**2)
2619. RS(JB-1)=RS(JB-1)+C*GP12*CIR/(DE**2)
2620. GO TO 6
2621. 5 IF (VJB1.LT.O.)GO TO 7
2622. G=A11/(1.+TAN(PI2*E(JB-1))**2)

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2623. GP12=A11/(1.+TAN(PI2*(E(JB-1)+O.5*DE)))**2)
2624. RS(JB-1)=RS(JB-1)+UUJB1/QQJB1*G*GP12*CIR/(DE**2)
2625. GO TO 6
2626. 7 G=A11/(1.+TAN(PI2*(E(JB-1)))**2)
2627. GP12=A11/(1.+TAN(PI2*(E(JB-1)+O.5*DE)))**2)
2628. RS(JB-1)=RS(JB-1)-(1.-QQJB1/AAJB1)*VVJB1*G*GP12*CIR/(DE**2)
2629. 1+UUJB1/QQJB1*G*GP12*CIR/(DE**2)
2630. 6 CALL TRID(2,JMAX1)
2631. DO 8 J=2,JMAX1
2632. DP=ABS(P(I,J)-RS(J))
2633. IF(DP.LT.DPM)GO TO 9
2634. ICON=1
2635. JCON=J
2636. DPM=DP
2637. 9 P2(J)=P1(J)
2638. P1(J)=P(I,J)
2639. 8 P(I,J)=RS(J)
2640. P2(1)=P1(1)
2641. P2(JMAX)=P1(JMAX)
2642. P1(1)=P(I,1)
2643. P1(JMAX)=P(I,JMAX)
2644. 4000 CONTINUE
2645. C IF(IMARK.EQ.O)GO TO 105
2646. C DO 104 J=JB,JAM1
2647. C 104 P(ITE,J)=PTEMP(J)
2648. C 105 CONTINUE
2649. DO 10 I=ITE1,IMAX1
2650. PB(I)=P(I,JB)-CIR
2651. 10 CONTINUE
2652. PB(ILE1)=P(ILE1,JB)
2653. IW=O
2654. RETURN
2655. END
2656. SUBROUTINE SHAPE
2657. C
2658. C ***** COMPUTES SHAPE OF AIRFOIL IN INVERSE DESIGN CASE*****
2659. C
2660. REAL M
2661. COMMON CPU(99),CPL(99),E(99),DU1(99),DU2(99),DL1(99),DL2(99),D(99)
2662. 1,FF(99),FFP12(99),FFM12(99),FFM1(99),FFM32(99),
2663. 1P1(99),P2(99),PB(99),P(99,99),RS(99),S(99),SUP(99),SUB(99),TEMP(99)
2664. 2),X(99),Y(99),YL(99),YU(99),SLU(99),SLL(99),
2665. 3A1,A2,AI2,ALP,CIR,EPS,EPSS,DE,DS,DP,DPM,F,FP12,FM12,FM32,M,QI,QI2,
2666. 4W,X1,X2,VVJB,VVJB1,AAJB,AAJB1,AAJB,QQJB,QQJB1,UUJB,VVJB1,AAJB1,
2667. 5,Q,QQ,UUJB1,PI,PI2,A22,A11,X4,S4
2668. COMMON I,ITE,ITE1,ILE,ILE1,I1,I11,ICON,IMAX,IMAX1,INV,JB,JA1,JB1,
2669. 1JMAX,JCON,JMAX1,NSSP,IW
2670. COMMON/TAMU/DELTAY
2671. COMMON/PT2/IMASS
2672. IF(I1.GE.ITE)RETURN
2673. DELTAY=O
2674. IF(IMASS.EQ.1)GO TO 100
2675. 1F(INV.EQ.O)I1=ILE+2
2676. 100 CONTINUE
2677. IP1=I1
2678. DO 1 I=IP1,ITE1
2679. YOLD=YU(I)
2680. JB2=JB-2
2681. DO 3 J=JB2,JMAX1
2682. 3 IF(YU(I-1).GT.E(J).AND.YU(I-1).LE.E(J+1))GO TO 4
2683. CONTINUE

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2684. 4 JA=J+1
2685. L=I-1
2686. IF(JA.LE.JB)JA=JB+1
2687. F=FF(L)
2688. U=Q1*(COS(ALP)+F*(P(I,JA-1)-P(I-2,JA-1)))/(2.*DS)+(YU(L)-E(JA-1)
2689. 1)*P(I,JA)-P(I,JA-1)-P(I-2,JA)+P(I-2,JA-1))/(2.*DS*DE))
2690. GB=A11/(1.+TAN(PI2*YU(I-1)**2))
2691. V=Q1*(SIN(ALP)+GB*((-3.*P(L,JA-1)+4.*P(L,JA)-P(L,JA+1))/(2.*
2692. 1DE)+(YU(L)-E(JA-1))*P(L,JA-1)-2.*P(L,JA)+P(L,JA+1))/(DE**2)))
2693. FY=(GB/F)*V/U
2694. IF(1.EQ.1)GO TO 14
2695. SLU(I-1)=V/U
2696. 14 CONTINUE
2697. FK1=DS*FY
2698. YN=YU(L)+O.5*FK1
2699. F=FFM12(I)
2700. DO 20 J=JB2,JMAX1
2701. IF(YN.GT.E(J).AND.YN.LE.E(J+1))GO TO 50
2702. 20 CONTINUE
2703. 50 JA=J+1
2704. IF(JA.LE.JB)JA=JB+1
2705. U=Q1*(COS(ALP)+F*(P(I,JA-1)-P(I-1,JA-1))/DS+(YN-E(JA-1))*
2706. 1P(I,JA)-P(I,JA-1)-P(L,JA)+P(L,JA-1))/(DS*DE))
2707. GB=A11/(1.+TAN(PI2*YN)**2)
2708. V=Q1*(SIN(ALP)+GB*((-3.*P(I,JA-1)+P(L,JA-1))+4.*P(I,JA)+P(L,
2709. 1JA)-P(I,JA+1)-P(L,JA+1))/(4.*DE)+(YN-E(JA-1))*O.5*P(I,JA-1)
2710. 2+P(I-1,JA-1)-2.*P(I,JA)+P(L,JA)+P(I,JA+1)+P(L,JA+1))/(DE**2)))
2711. FK2=GB/F*DS*V/U
2712. YN=YU(L)+O.5*FK2
2713. DO 21 J=JB2,JMAX1
2714. IF(YN.GT.E(J).AND.YN.LE.E(J+1))GO TO 22
2715. 21 CONTINUE
2716. 22 JA=J+1
2717. IF(JA.LE.JB)JA=JB+1
2718. U=Q1*(COS(ALP)+F*(P(I,JA-1)-P(I-1,JA-1))/DS+(YN-E(JA-1))*
2719. 1P(I,JA)-P(I,JA-1)-P(L,JA)+P(L,JA-1))/(DS*DE))
2720. GB=A11/(1.+TAN(PI2*YN)**2)
2721. V=Q1*(SIN(ALP)+GB*((-3.*P(I,JA-1)+P(L,JA-1))+4.*P(I,JA)+P(L,
2722. 1JA)-P(I,JA+1)-P(L,JA+1))/(4.*DE)+(YN-E(JA-1))*O.5*P(I,JA-1)
2723. 2+P(I-1,JA-1)-2.*P(I,JA)+P(L,JA)+P(I,JA+1)+P(L,JA+1))/(DE**2)))
2724. FK3=GB/F*DS*V/U
2725. YN=YU(L)+FK3
2726. F=FF(I)
2727. DO 2 J=JB2,JMAX1
2728. IF(YN.GT.E(J).AND.YN.LE.E(J+1))GO TO 5
2729. 2 CONTINUE
2730. 5 JA=J+1
2731. IF(JA.LE.JB)JA=JB+1
2732. U=Q1*(COS(ALP)+F*(P(I+1,JA-1)-P(I-1,JA-1))/(2.*DS)+(YN-E(JA-1))*
2733. 1P(I+1,JA)-P(I+1,JA-1)-P(I-1,JA)+P(I-1,JA-1))/(2.*DS*DE))
2734. GB=A11/(1.+TAN(PI2*YN)**2)
2735. V=Q1*(SIN(ALP)+GB*((-3.*P(I,JA-1)+4.*P(I,JA)-P(I,JA+1))/(2.*DE)
2736. 1+(YN-E(JA-1))*P(I,JA-1)-2.*P(I,JA)+P(I,JA+1))/(DE**2)))
2737. FK4=GB/F*DS*V/U
2738. YU(I)=YU(L)+(FK1+2.*FK2+2.*FK3+FK4)/6.
2739. IF(I.GT.ITE)GO TO 1
2740. CHANGE=ABS(YU(I)-YOLD)
2741. IF(CHANGE.GT.DELTAY)DELTA=CHANGE
2742. 1 CONTINUE
2743. IF(IMASS.EQ.O)GO TO 1000
2744. RETURN

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2803. 00002545
2804. 00002546
2805. 00002547

1000 CONTINUE
DO 6 I=ILE1,IMAX
TEMP1=P(I,JB)
P(I,JB)=PB(I)
6 PB(I)=TEMP1
DO 7 I=IP1,ITE1
YOLD=YL(I)
JB2=JB+2
DO 8 JJ=1,JB
J=JB2-JJ
IF(YL(I-1).GE.E(J).AND.YL(I-1).LT.E(J+1))GO TO 9
8 CONTINUE
9 JA=J
IF(JA.GE.JB)JA=JB-1
L=I-1
F=FF(L)
U=QI*(COS(ALP)+F*(P(I,JA+1)-P(I-2,JA+1))/(2.*DS)+(YL(L)-E(JA+1))*0.0002503
1(P(I,JA+1)-P(I,JA)-P(I-2,JA+1)+P(I-2,JA))/(2.*DS*DE))
GB=A11/(1.+TAN(PI2*YL(L))*2)
V=QI*(SIN(ALP)+GB*((3.*P(L,JA+1)-4.*P(L,JA)+P(L,JA-1))/(2.*DE)+
1(YL(L)-E(JA+1))*P(L,JA+1)-2.*P(L,JA)+P(L,JA-1))/(DE**2)))
FY=GB/F*V/U
IF(I.EQ.I1)GO TO 15
SLL(I-1)=V/U
15 CONTINUE
FK1=DS*FY
YN=YL(L)+0.5*FK1
F=FFM12(I)
DO 25 JJ=1,JB
J=JB2-JJ
IF(YN.GE.E(J).AND.YN.LT.E(J+1))GO TO 26
26 JA=J
IF(JA.GE.JB)JA=JB-1
U=QI*(COS(ALP)+F*(P(I,JA+1)-P(L,JA+1))/DS+(YN-E(JA+1))*P(I,JA+1)
1-P(I,JA)-P(L,JA+1)+P(L,JA))/(DS*DE))
GB=A11/(1.+TAN(PI2*YN))*2)
V=QI*(SIN(ALP)+GB*((3.*P(I,JA+1)+P(L,JA+1))-4.*P(I,JA)+P(L,JA)
1+P(I,JA-1)+P(L,JA-1))/(4.*DE)+(YN-E(JA+1))*P(I,JA+1)+P(L,JA+1)
2-2.*P(I,JA)+P(L,JA)+P(I,JA-1)+P(L,JA-1))*0.5/(DE**2)))
FK2=GB/F*DS*V/U
YN=YL(L)+0.5*FK2
DO 27 JJ=1,JB
J=JB2-JJ
IF(YN.GE.E(J).AND.YN.LT.E(J+1))GO TO 28
27 CONTINUE
28 JA=J
IF(JA.GE.JB)JA=JB-1
U=QI*(COS(ALP)+F*(P(I,JA+1)-P(I,JA+1)-P(L,JA+1))/DS+(YN-E(JA+1))*P(I,JA+1)
1-P(I,JA)-P(L,JA+1)+P(L,JA))/(DS*DE))
GB=A11/(1.+TAN(PI2*YN))*2)
V=QI*(SIN(ALP)+GB*((3.*P(I,JA+1)+P(L,JA+1))-4.*P(I,JA)+P(L,JA)
1+P(I,JA-1)+P(L,JA-1))/(4.*DE)+(YN-E(JA+1))*P(I,JA+1)+P(L,JA+1)
2-2.*P(I,JA)+P(L,JA)+P(I,JA-1)+P(L,JA-1))*0.5/(DE**2)))
FK3=GB/F*DS*V/U
YN=YL(L)+FK3
F=FF(I)
DO 10 JJ=1,JB
J=JB2-JJ
IF(YN.GE.E(J).AND.YN.LT.E(J+1))GO TO 11
10 CONTINUE

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2806. 11 JA=J
2807.   IF(JA.GE.JB)JA=JB-1
2808.   U=QI*(COS(ALP)+F*(P(I+1,JA+1)-P(I-1,JA+1)))/(2.*DS)+(YN-E(JA+1))*
2809.   1(P(I+1,JA+1)-P(I+1,JA)-P(I-1,JA+1)+P(I-1,JA))/(2.*DS*DE))
2810.   GB=A11/(1.+TAN(PI2*YN)**2)
2811.   V=QI*(SIN(ALP)+GB*(3.*P(I,JA+1)-4.*P(I,JA)+P(I,JA-1)))/(2.*DE)+
2812.   1(YN-E(JA+1))*(P(I,JA+1)-2.*P(I,JA)+P(I,JA-1))/(DE**2))
2813.   FK4=GB/F*DS*V/U
2814.   YL(I)=YL(L)+(FK1+2.*FK2+2.*FK3+FK4)/6.
2815.   IF(I.GT.ITE)GO TO 7
2816.   CHANGE=ABS(YL(I)-YOLD)
2817.   IF(CHANGE.GT.DELTAY)DELTAY=CHANGE
2818.   7 CONTINUE
2819.   DO 12 I=ILE1,IMAX
2820.     TEMP1=P(I,JB)
2821.     P(I,JB)=PB(I)
2822.     12 PB(I)=TEMP1
2823.   RETURN
2824.   END
2825.   SUBROUTINE TRID(IL,IH)
2826.
2827. C ***** TRIAGONAL EQUATION SOLVER *****
2828. C
2829.   REAL M
2830.   COMMON CPU(99),CPL(99),E(99),DU1(99),DU2(99),DL1(99),DL2(99),D(99)
2831.   1,FF(99),FFP12(99),FFM12(99),FFM1(99),FFM32(99),
2832.   1P1(99),P2(99),PB(99),P(99,99),RS(99),S(99),SUP(99),SUB(99),TEMP(99)
2833.   2),X(99),Y(99),YU(99),YL(99),SLU(99),SLL(99),
2834.   3A1,A2,A12,ALP,CIR,EPS,EPSS,DE,DS,DP,DPM,F,FP12,FM12,FM32,M,QI,QI2,
2835.   4W,X1,X2,VVJB,VVJB1,AAJB1,AAJB,QQJB,QQJB1,UUJB,VVJB1,QQJB1,AAJB1,
2836.   5,Q,QQ,UUJB1,PI,PI2,A22,A11,X4,S4
2837.   COMMON I,ITE,ITE1,ILE,ILE1,I1,I11,ICON,IMAX,IMAX1,INV,JB,JA1,JB1,
2838.   1JMAX,UCON,JMAX1,NSSP,IW
2839.   N=IH
2840.   NN=N-1
2841.   SUP(IL)=SUP(IL)/D(IL)
2842.   RS(IL)=RS(IL)/D(IL)
2843.   IDUM=IL+1
2844.   DO 10 L=IDUM,N
2845.     II=L-1
2846.     D(L)=D(L)-SUP(II)*SUB(II)
2847.     IF(L.EQ.N)GO TO 10
2848.     IF(D(L).EQ.O)PRINT 1000,IL,IH,L
2849.     1000 FORMAT(3I5)
2850.     SUP(L)=SUP(L)/D(L)
2851.     10 RS(L)=(RS(L)-SUB(II)*RS(II))/D(L)
2852.     DO 20 K=IL,NN
2853.       L=N-K+IL-1
2854.       20 RS(L)=RS(L)-SUP(L)*RS(L+1)
2855.     RETURN
2856.     END
2857.     SUBROUTINE HALVE
2858.
2859. C ***** THIS SUBROUTINE HALVES THE GRID SPACING ETC. *****
2860. C
2861.   REAL M
2862.   COMMON CPU(99),CPL(99),E(99),DU1(99),DU2(99),DL1(99),DL2(99),D(99)
2863.   1,FF(99),FFP12(99),FFM12(99),FFM1(99),FFM32(99),
2864.   1P1(99),P2(99),PB(99),P(99,99),RS(99),S(99),SUP(99),SUB(99),TEMP(99)
2865.   2),X(99),Y(99),YU(99),YL(99),SLU(99),SLL(99),
2866.   3A1,A2,A12,ALP,CIR,EPS,EPSS,DE,DS,DP,DPM,F,FP12,FM12,FM32,M,QI,QI2,

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2928. 15 CONTINUE
2929. 16 IF (NLL) 20, 18, 20
2930. 18 NLL=50
2931. 20 WRITE(6,1)NO
2932. XSCAL=(A(N)-A(1))/(FLOAT(NLL-1))
2933. M1=N+1
2934. YMIN=A(M1)
2935. YMAX=YMIN
2936. M2=M*N
2937. DO 40 J=M1,M2
2938. IF(A(J)-YMIN) 28,26,26
2939. 26 IF(A(J)-YMAX) 40,40,30
2940. 28 YMIN=A(J)
2941. GO TO 40
2942. 30 YMAX=A(J)
2943. 40 CONTINUE
2944. YSCAL=(YMAX-YMIN)/100.0
2945. XB=A(1)
2946. L=1
2947. MY=M-1
2948. I=1
2949. 45 F=I-1
2950. XPR=XB+F*XSCAL
2951. IF(A(L)-XPR) 50,50,70
2952. 50 DO 55 IX=1,101
2953. 55 OUT(IX)=BLANK
2954. 2954. DO 60 J=1,MY
2955. LL=L+J*N
2956. JP=((A(LL)-YMIN)/YSCAL)+1.0
2957. OUT(JP)=ANG(J)
2958. 60 CONTINUE
2959. WRITE(6,2)XPR,(OUT(IZ),IZ=1,101)
2960. L=L+1
2961. GOT080
2962. 70 WRITE(6,3)
2963. 80 I=I+1
2964. IF(I-NLL) 45,84,86
2965. 84 XPR=A(N)
2966. GO TO 50
2967. 86 WRITE(6,7)
2968. YPR(1)=YMIN
2969. DO 90 KN=1,9
2970. 90 YPR(KN+1)=YPR(KN)+YSCAL*10.0
2971. YPR(11)=YMAX
2972. WRITE(6,8)(YPR(IP),IP=1,11)
2973. RETURN
2974. END
2975. SUBROUTINE ARC(XI,YI,X0,Y0,SI,S0,XP,YP,D1Y,D2Y,D3Y,DERIX,DERFX,
2976. 1DERIY,DERFY,NI,NO,INT)
C ***** DETERMINES THE ARC LENGTH OF THE AIRFOIL POINTS *****
C
C DIMENSION XI(1),YI(1),X0(1),Y0(1),SI(1),S0(1),XP(1),YP(1),D1Y(1),D2Y(1),D3Y(1),
C 1D2Y(1),D3Y(1)
C SI - INPUT CHORD LENGTH SO - OUTPUT CHORD LENGTH
C COMPUTE ARC LENGTH SI USING CIRCULAR ARC SEGMENTS
C INT=1 SPLINE XI AND YI VS SI
C EPSI=1 E-10
C NI=NI-1
C SI(1)=0.
C H1=0.
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2989. DX1=XI(2)-XI(1)
2990. DY1=YI(2)-YI(1)
2991. C1=SQRT(DX1**2+DY1**2)
2992. SI(2)=C1
2993. IF(NI.EQ.2)RETURN
2994. D0 1 I=2,N1
2995. DX1=XI(I)-XI(I-1)
2996. DY1=YI(I)-YI(I-1)
2997. DX2=XI(I+1)-XI(I)
2998. DY2=YI(I+1)-YI(I)
2999. DX=XI(I+1)-XI(I-1)
3000. DY=YI(I+1)-YI(I-1)
3001. C2=SQRT(DX2**2+DY2**2)
3002. C=SQRT(DX**2+DY**2)
3003. A=(DY1*DX-DY*DX1)/2.
3004. H=4.*A/(C+C1*C2)
3005. HAV=(H1+H)/2.
3006. DS=C1*(1.+(C1/2.*HAV)**2/6.)
3007. SI(I)=SI(I-1)+DS
3008. C1=C2
3009. H1=H
3010. 1 CONTINUE
3011. DS=C1*(1.+(C1/2.*H)**2/6.)
3012. SI(NI)=SI(NI-1)+DS
3013. IF(INT.NE.1)RETURN
3014. 2 CONTINUE
3015. C SPLINE XI AS A FUNCTION OF SI
3016. CALL SPLINE(SI,XI,SO,XO,XP,D1Y,D2Y,D3Y,1,3,DERIX,DERFX,NI,NO,O)
3017. 3 CONTINUE
3018. C SPLINE YI AS A FUNCTION OF SI
3019. CALL SPLINE(SI,YI,SO,YO,YP,D1Y,D2Y,D3Y,1,3,DERIY,DERFY,NI,NO,1)
3020. RETURN
3021. END
3022. SUBROUTINE SPLINE(XIN,YIN,XOUT,YOUT,DYDX,D1Y,D2Y,D3Y,NDERI,NDERF,
3023. DERIVI,DERIVF,NIN,NOUT,INTERP)
3024. E B KLUNKER JANUARY 1973
3025. C COMPUTE A CUBIC SPLINE THROUGH THE SET OF POINTS XIN(I),YIN(I)
3026. C XIN MUST BE MONOTONIC
3027. C XIN,YIN INPUT INDEPENDENT AND DEPENDENT VARIABLES
3028. C XOUT,YOUT OUTPUT INDEPENDENT AND DEPENDENT VARIABLES
3029. C D1Y,D2Y,D3Y 1ST, 2ND, AND 3RD DERIVATIVE AT SPLINE POINTS XIN
3030. C DYDX DERIVATIVE AT XOUT
3031. C NIN,NOUT NUMBER OF INPUT AND OUTPUT VALUES
3032. C NDERI ORDER OF DERIVATIVE AT INITIAL SPLINE POINT (1,2,OR 3)
3033. C NDERF ORDER OF DERIVATIVE AT FINAL SPLINE POINT (1,2,OR 3)
3034. C DERIVI VALUE OF DERIVATIVE AT INITIAL SPLINE POINT
3035. C INTERP NE 1 INTERPOLATE FOR GIVEN VALUES YOUT
3036. C NTIMES NE 1 SPLINE COEFFICIENTS ARE NOT RECOMPUTED
3037. DIMENSION XIN(1),YIN(1),XOUT(1),YOUT(1),DYDX(1),D1Y(1),D2Y(1),
3038. D3Y(1)
3039. EPSI1=-1.E-10
3040. EPSI2=-EPSI1
3041. NIM1=NIN-1
3042. DX=XIN(2)-XIN(1)
3043. I=2
3044. IF(DX.EQ.0.)GO TO 35
3045. DF=(YIN(2)-YIN(1))/DX
3046. IF(NDERI-2)1,2,3
3047. 1 C=.5
3048. F=3.*(DF-DERIVI)/DX
3049. GO TO 4

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2 C=0.
   F=DERIVI
   GO TO 4
3 C=-1.
   F=-DX*DERIVI
   FORWARD LOOP OF TRIANGULAR MATRIX COMPUTATION
4 D1Y(1)=-C
   D2Y(1)=F
   DO 5 I=2,NIM1
   DX1=XIN(I+1)-XIN(I)
   IF(DX1.EQ.0.)GO TO 36
   DF1=(YIN(I+1)-YIN(I))/DX1
   B=2.*(DX+DX1)
   F=6.*(DF1-DF)
   DENOM=B+DX*D1Y(I-1)
   D2Y(I)=(F-DX*D2Y(I-1))/DENOM
   D1Y(I)=-DX1/DENOM
   DX=DX1
   DF=DF1
5 CONTINUE
   I=NIN
   IF(NDERF-2)6,7,8
6 A=.5
   F=-3.*(DF1-DERIVF)/DX1
   GO TO 9
7 A=0.
   F=DERIVF
   GO TO 9
8 A=-1.
   F=DX1*DERIVF
   DENOM=1.+A*D1Y(I-1)
   D2Y(I)=(F-A*D2Y(I-1))/DENOM
   D1Y(I)=0.
9
C
   BACK SUBSTITUTION OF TRIANGULAR MATRIX COMPUTATION
   K=NIN
   DO 11 I=1,NIM1
   K=K-1
   D2Y(K)=D2Y(K)+D1Y(K)*D2Y(K+1)
10 DX1=XIN(K+1)-XIN(K)
   DF1=(YIN(K+1)-YIN(K))/DX1
   D1Y(K+1)=DF1+DX1/6.*(D2Y(K)+2.*D2Y(K+1))
   D3Y(K+1)=(D2Y(K+1)-D2Y(K))/DX1
11 CONTINUE
   D1Y(1)=DF1-DX1/6.*(2.*D2Y(1)+D2Y(2))
   D3Y(1)=D3Y(2)
   IF(INTERP.NE.1)GO TO 16
   INTERPOLATE FOR GIVEN VALUES OF XOUT
   DO 15 J=1,NOUT
   DO 12 I=1,NIN
   DX=XIN(I)-XOUT(J)
   IF(DX.GE.EPSI1.AND.DX.LE.EPSI2)GO TO 13
   IF(DX.GE.EPSI2)GO TO 14
12 CONTINUE
   GO TO 37
13 YOUT(J)=YIN(I)
   DYDX(J)=D1Y(I)
   GO TO 15
14 DX=XOUT(J)-XIN(I)
   YOUT(J)=YIN(I)+DX*(D1Y(I)+DX/2.*(D2Y(I)+DX/3.*D3Y(I)))
   DYDX(J)=D1Y(I)+DX*(D2Y(I)+DX/2.*D3Y(I))
15 CONTINUE

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3111. GO TO 23
3112. INTERPOLATION FOR GIVEN VALUES OF YOUT
3113. 16 DO 22 J=1,NOUT
3114. DO 17 I=1,NIN
3115. DY=YIN(I)-YOUT(J)
3116. IF(DY.GE.EPSI1,AND.DY.LE.EPSI2)GO TO 18
3117. IF(DY.GE.EPSI2)GO TO 19
3118. 17 CONTINUE
3119. GO TO 38
3120. 18 YOUT(J)=YIN(I)
3121. XOUT(J)=XIN(I)
3122. DYDX(J)=D1Y(I)
3123. GO TO 22
3124. 19 DX=-DY/D1Y(I)
3125. 20 YO=YIN(I)+DX*(D1Y(I)+DX/2.*(D2Y(I)+DX/3.*D3Y(I)))
3126. DY=YO-YOUT(J)
3127. IF(DY.GE.EPSI1,AND.DY.LE.EPSI2)GO TO 21
3128. YP=D1Y(I)+DX*(D2Y(I)+DX/2.*D3Y(I))
3129. DELX=-DY/YP
3130. DX=DX+DELX
3131. GO TO 20
3132. 21 XOUT(J)=XIN(I)+DX
3133. DYDX(J)=D1Y(I)+DX*(D2Y(I)+DX/2.*D3Y(I))
3134. 22 CONTINUE
3135. 23 RETURN
3136. 35 PRINT 100
3137. PRINT 101,XIN(1),XIN(2)
3138. STOP
3139. 36 PRINT 100
3140. PRINT 102,I,XIN(I),XIN(I+1)
3141. STOP
3142. 37 PRINT 100
3143. PRINT 103,J,XOUT(J),XIN(NIN)
3144. STOP
3145. 38 PRINT 100
3146. PRINT 104,J,YOUT(J),YIN(NIN)
3147. STOP
3148.
3149.
3150. 100 FORMAT(/5X,'SUBROUTINE SPLINE'//)
3151. 101 FORMAT(/5X,'ERROR IN INPUT XIN(1)='E12.4,5X,'XIN(2)='E12.4/)
3152. 102 FORMAT(/5X,'ERROR IN INPUT I='I5.5X,'XIN(I)='E12.4,5X,'XIN(I+1)='E12.4/)
3153. 103 FORMAT(/5X,'XOUT(J) IS OUT OF RANGE J='I5.5X,'XOUT(J)='E12.4,5X,00002893
3154. 1'XIN(NIN)='E12.4/)
3155. 104 FORMAT(/5X,'YOUT(J) IS OUT OF RANGE J='I5.5X,'YOUT(J)='E12.4,5X,00002895
3156. 1'YIN(NIN)='E12.4/)
3157.
3158. END
3159. C +*** SUPERPOSES THE VORTEX BC POTENTIALS AT INFINITY ****
3160. SUBROUTINE VORBCI(BETA,QUAN2,QUAN3)
3161. COMMON CPU(99),CPL(99),E(99),DU1(99),DU2(99),DL1(99),DL2(99),D(99)00000007
3162. 1,FF(99),FFP12(99),FFM12(99),FFM1(99),FFM32(99),
3163. 1P1(99),P2(99),PB(99),P(99,99),RS(99),S(99),SUP(99),SUB(99),TEMP(99)00000009
3164. 2),X(99),Y(99),YU(99),YL(99),SLU(99),SLL(99),
3165. 3A1,A2,A12,ALP,CTR,EPS,EPSS,DE,DS,DP,DPM,F,FP12,FM12,FM32,M,QI,QI2,00000011
3166. 4W,X1,X2,VVJB,VVJB1,AAJB,AAJB1,AAJB,QQJB,QQJB1,UUJB,VVJB1,QQJB1,AAJB10000012
3167. 5,Q,QQ,UUJB1,PI,P12,A22,A11,X4,S4
3168. COMMON I,ITE,ITE1,ILE,ILE1,I1,I11,ICON,IMAX,IMAX1,INV,JB,JA1,JB1,
3169. 1JMAX,JCON,JMAX1,NSSP,IW
3170. COMMON/VORTEX/VORCIR,IVLOC,XV,YV,IVOR,JVOR
3171. QUAN1=-.5*VORCIR/PI

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3172. IVORP1=IVOR+1
3173. IF (IVLOC.EQ.1) GO TO 910
3174. P(IMAX,1)=P(IMAX,1)+QUAN1*QUAN2
3175. P(IMAX,JMAX)=P(IMAX,JMAX)+QUAN1*(PI-QUAN2)
3176. P(1,JMAX)=P(1,JMAX)+QUAN1*(PI+QUAN2)
3177. P(1,1)=P(1,1)+QUAN1*(2.*PI-QUAN2)
3178. GO TO 920
3179.
3180. P(1,JMAX)=P(1,JMAX)+QUAN1*QUAN2
3181. P(1,1)=P(1,1)+QUAN1*(PI-QUAN2)
3182. P(IMAX,1)=P(IMAX,1)+QUAN1*(PI+QUAN2)
3183. P(IMAX,JMAX)=P(IMAX,JMAX)+QUAN1*(2.*PI-QUAN2)
3184. QUAN4=ATAN(BETA/TAN(ALP))
3185. IF (IVLOC.EQ.1) GO TO 950
3186. IF (ALP.GT.O.O) GO TO 930
3187. DO 922 J=2,JMAX1
3188. P(IMAX,J)=P(IMAX,J)+QUAN1*(PI+QUAN4)
3189. P(1,J)=P(1,J)+QUAN1*(2.*PI+QUAN4)
3190. GO TO 940
3191.
3192. DO 932 J=2,JMAX1
3193. P(IMAX,J)=P(IMAX,J)+QUAN1*QUAN4
3194. P(1,J)=P(1,J)+QUAN1*(PI+QUAN4)
3195. DO 943 I=2,IMAX1
3196. P(I,JMAX)=P(I,JMAX)+QUAN1*(PI-QUAN3)
3197. DO 946 I=2,IVOR
3198. P(I,1)=P(I,1)+QUAN1*(2.*PI-QUAN3)
3199. DO 949 I=IVORP1,IMAX1
3200. P(I,1)=P(I,1)+QUAN1*(-QUAN3)
3201. RETURN
3202.
3203. IF (ALP.GT.O.O) GO TO 960
3204. DO 952 J=2,JMAX1
3205. P(1,J)=P(1,J)+QUAN1*(PI+QUAN4)
3206. P(IMAX,J)=P(IMAX,J)+QUAN1*(2.*PI+QUAN4)
3207. GO TO 970
3208.
3209. DO 962 J=2,JMAX1
3210. P(1,J)=P(1,J)+QUAN1*QUAN4
3211. P(IMAX,J)=P(IMAX,J)+QUAN1*(PI+QUAN4)
3212. DO 973 I=2,IMAX1
3213. P(I,1)=P(I,1)+QUAN1*(PI-QUAN3)
3214. DO 976 I=2,IVOR
3215. P(I,JMAX)=P(I,JMAX)+QUAN1*(-QUAN3)
3216. DO 979 I=IVORP1,IMAX1
3217. P(I,JMAX)=P(I,JMAX)+QUAN1*(2.*PI-QUAN3)
3218. RETURN
3219.
3220. IF (IVLOC.EQ.1) GO TO 990
3221. DO 983 J=2,JMAX1
3222. P(1,J)=P(1,J)-.75*VORCIR
3223. P(IMAX,J)=P(IMAX,J)-.25*VORCIR
3224. DO 986 I=2,IMAX1
3225. P(I,JMAX)=P(I,JMAX)-.5*VORCIR
3226. DO 989 I=2,IVOR
3227. P(I,1)=P(I,1)-VORCIR
3228. RETURN
3229.
3230. DO 993 J=2,JMAX1
3231. P(1,J)=P(1,J)-.25*VORCIR
3232. P(IMAX,J)=P(IMAX,J)-.75*VORCIR
3233. DO 996 I=2,IMAX1
3234. P(I,1)=P(I,1)-.5*VORCIR
3235. DO 999 I=IVORP1,IMAX1
3236. P(I,JMAX)=P(I,JMAX)-VORCIR
3237. RETURN
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