

APPENDIX C. DERIVATION OF EQUATIONS OF MOTION FOR MULTIPLE DEGREE OF FREEDOM SYSTEM

Consider a linear mechanical system with n -independent degrees of freedom. Let $\{x_i(t)\}_{i=1,...,n}$ be the independent coordinates describing the motion of the system about an equilibrium position, and with $\{F_{i(t)}\}_{i=1,...,n}$ as the set of external forces applied at each degree of freedom. The kinetic and potential energy of the system can be written in the following form,

$$T = \frac{1}{2} [\dot{x}]^T [M] [\dot{x}], \quad V = \frac{1}{2} [x]^T [K] [x] \quad (1)$$

where $[x] = \{x_1 \ x_2 \ x_3 \ \dots \ x_n\}^T$, and $[\dot{x}] = \{\dot{x}_1 \ \dot{x}_2 \ \dot{x}_3 \ \dots \ \dot{x}_n\}^T$ are the vectors of displacements and velocities; $[M] = \{m_{i,j}\}_{i,j=1,n}$ and $[K] = \{k_{i,j}\}_{i,j=1,n}$ are the $(n \times n)$ matrices of generalized inertia and stiffness coefficients, respectively. The elements of these matrices are constant coefficients.

Note that energies are scalar functions, i.e. $T = T^T$. Thus, taking the transpose of the potential energy we can easily show that the stiffness matrix must be symmetric, i.e.

$$\begin{aligned} V &= \frac{1}{2} [x]^T [K] [x] = V^T = \frac{1}{2} ([K] [x])^T ([x]^T)^T = \frac{1}{2} [x]^T [K]^T [x], \\ V - V^T &= 0 = \frac{1}{2} [x]^T \{[K] - [K]^T\} [x], \quad \longrightarrow [K]^T = [K] \end{aligned} \quad (2)$$

and it also follows that $[M]^T = [M]$. We have used in equation (2) above the following fundamental matrix property $(A^T B)^T = B^T A$, where A and B are general matrices.

The **viscous power dissipation** and **viscous dissipated energy** are given by the equations

$$P_v = [\dot{x}]^T [D] [\dot{x}], \quad E_v = \int_0^t P_v dt \quad (3)$$

where $[D] = \{d_{i,j}\}_{i,j=1,n}$ is a matrix of constant damping coefficients. The work performed by external forces is given by,

$$W = \int d[x]^T [F] \quad (4)$$

The **principle of conservation of mechanical** energy establishes that for any instant of time,

$$T + V + E_v = W + T_0 + V_0 \quad (5)$$

$$\text{where } T_0 = \frac{1}{2} [\dot{x}_0]^T [M] [\dot{x}_0], \quad V_0 = \frac{1}{2} [x_0]^T [K] [x_0] \quad (6)$$

are the initial values of the system kinetic and potential energies, respectively.

Now, take the time derivative of equation (5) to obtain

$$\frac{d}{dt}(T + V + E_v - W) = 0 \quad (7)$$

Now,

$$\begin{aligned} \frac{d}{dt}(T) &= \frac{1}{2} [\ddot{x}]^T [M] [\dot{x}] + \frac{1}{2} [\dot{x}]^T [M] [\ddot{x}] = \frac{1}{2} \left\{ ([\ddot{x}]^T [M] [\dot{x}])^T + [\dot{x}]^T [M] [\ddot{x}] \right\} = \\ &= \frac{1}{2} \left\{ [\dot{x}]^T [M]^T [\ddot{x}] + [\dot{x}]^T [M] [\ddot{x}] \right\} = \frac{1}{2} \left\{ [\dot{x}]^T [M] [\ddot{x}] + [\dot{x}]^T [M] [\ddot{x}] \right\} = [\dot{x}]^T [M] [\ddot{x}] \end{aligned}$$

$$\begin{aligned} \frac{d}{dt}(V) &= \frac{1}{2} [\dot{x}]^T [K] [x] + \frac{1}{2} [x]^T [K] [\dot{x}] = \frac{1}{2} \left\{ [\dot{x}]^T [K] [x] + ([x]^T [K] [\dot{x}])^T \right\} \\ &= \frac{1}{2} \left\{ [\dot{x}]^T [K] [x] + [\dot{x}]^T [K]^T [x] \right\} = \frac{1}{2} \left\{ [\dot{x}]^T [K] [x] + [\dot{x}]^T [K] [x] \right\} = [\dot{x}]^T [K] [x] \end{aligned} \quad (8)$$

Since $[K] = [K]^T$ and $[M] = [M]^T$ and with $[\ddot{x}] = \{\ddot{x}_1, \ddot{x}_2, \ddot{x}_3, \dots, \ddot{x}_n\}^T$ as a vector of accelerations. Also,

$$\frac{d}{dt} E_v = \frac{d}{dt} \int_0^t P_v dt = P_v = [\dot{x}]^T [D] [\dot{x}] \quad (9)$$

And

$$\frac{d}{dt} W = \frac{d}{dt} \int d[x]^T [F] = \frac{d[x]^T}{dt} [F(t)] = [\dot{x}]^T [F(t)] \quad (10)$$

Substitution of equations (8), (9) and (10) into equation (7) gives

$$[\dot{x}]^T [M] [\ddot{x}] + [\dot{x}]^T [K] [x] + [\dot{x}]^T [D] [\dot{x}] - [\dot{x}]^T [F] = 0$$

$$[\dot{x}]^T \{ [M][\ddot{x}] + [K][x] + [D][\dot{x}] - [F] \} = 0,$$

and since $[\dot{x}]^T \neq [0]$, then

Thus, the n-equations of motion for the n-dof system are given by

$$[M][\ddot{x}] + [D][\dot{x}] + [K][x] = [F(t)] \quad (11).$$

The difficulty in using this approach is to devise a simple method to establish the elements of the matrices $[M]$, $[K]$, $[D]$. The use of the Lagrangian equations of motion is particularly useful in this case.

Derivation of equations of motion using Lagrange's approach¹

Consider a mechanical system with n-independent degrees of freedom, and where $\{x_i, \dot{x}_i\}_{i=1, \dots, n}$ are the generalized coordinates and velocities for each degree of freedom in the system. The Work performed on the system by external generalized forces is given by

$$W = \int (F_1 dx_1 + F_2 dx_2 + F_3 dx_3 + \dots F_n dx_n) = \int \sum_{i=1}^n F_i dx_i \quad (12)$$

Here we use the term generalized to denote that the product of a generalized displacement, say x_i , and the generalized effort, F_i , produce units of work [N.m]. For example if $x_2 = \theta$ denotes an angular coordinate, then the effort F_2 corresponds to a moment or torque.

Let the **total kinetic energy** and **potential energy** of the n-dof mechanical system be given by the generic expressions

$$\begin{aligned} T &= f \{ \dot{x}_1, \dot{x}_2, \dot{x}_3, \dots, \dot{x}_n, x_1, x_2, \dots, x_n, t \} \\ V &= g \{ x_1, x_2, \dots, x_n, t \} \end{aligned} \quad (13)$$

The kinetic energy above is a function of the generalized displacements, velocities and time, while the potential energy in a conservative system is only a function of the generalized displacements and time.

¹ Sources Meirovitch, L., Analytical Methods in Vibrations, pp. 30-50, and San Andrés, L., Vibrations Class Notes, 1996.

The **viscous dissipated power** is a general function of the velocities, i.e.

$$P_v = P_v \{ \dot{x}_1 \dot{x}_2 \dot{x}_3 \dots \dot{x}_n \} \quad (14)$$

The n-equations of motion for the system are derived using the Lagrangian approach, i.e.

$$\frac{\partial}{\partial t} \left(\frac{\partial T}{\partial \dot{x}_i} \right) - \frac{\partial T}{\partial x_i} + \frac{\partial V}{\partial x_i} + \frac{1}{2} \frac{\partial P_v}{\partial \dot{x}_i} = F_i \quad i=1,2,\dots,n \quad (15)$$

Once you have performed the derivatives above for each coordinate, $i=1, \dots, n$, the resulting equations are of the form:

$$\begin{aligned} m_{11} \ddot{x}_1 + \dots + m_{1n} \ddot{x}_n + d_{11} \dot{x}_1 + \dots + d_{1n} \dot{x}_n + k_{11} x_1 + \dots + k_{1n} x_n &= F_1 \\ m_{21} \ddot{x}_1 + \dots + m_{2n} \ddot{x}_n + d_{21} \dot{x}_1 + \dots + d_{2n} \dot{x}_n + k_{21} x_1 + \dots + k_{2n} x_n &= F_2 \\ \dots & \\ m_{n1} \ddot{x}_1 + \dots + m_{nn} \ddot{x}_n + d_{n1} \dot{x}_1 + \dots + d_{nn} \dot{x}_n + k_{n1} x_1 + \dots + k_{nn} x_n &= F_n \end{aligned} \quad (16)$$

or written in matrix form as

$$[M][\ddot{x}] + [D][\dot{x}] + [K][x] = [F] \quad (17)=(11)$$