

# Furrow Diking Technology for Agricultural Water Conservation and Its Impact on Crop Yields in Texas

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## RESEARCH PROJECT COMPLETION REPORT

# FURROW DIKING TECHNOLOGY FOR AGRICULTURAL WATER CONSERVATION AND ITS IMPACT ON CROP YIELDS IN TEXAS

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#### ABSTRACT

Furrow Diking Technology for Agricultural Water Conservation and Its

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Furrow diking is a practical, efficient and low-cost technique to conserve water and increase crop yields. Improvements in diker design and the increased use of herbicides have resulted in the rapid spread of furrow diking in the Texas High Plains and other regions.

To quantify the long-term effects of diking on crop yields, a computer simulation approach was used. Three crop models for sorghum, corn and cotton were combined with surface runoff hydrology algorithms, based on the USDA-SCS curve number methodology. The combination models called SORDIKE, CORDIKE and COTDIKE were run to determine the effects of conserving the runoff (by diking) on crop yields. Three scenarios of not diking, diking in the growing season, and diking all year were simulated. Daily weather data for 25 years from five Texas regions were used for the analyses. Depending on the location, furrow diking in the growing season increased average annual sorghum yields by 320 to 570 kg/ha, corn yields by 180 to 570 kg/ha, and cotton lint yields by 10 to 20 kg/ha. Diking the land throughout the year increased mean annual yields by 440 to 1080 kg/ha of sorghum, 210 to 800 kg/ha of corn and 10 to 30 kg/ha of cotton lint. The study indicated that furrow diking can be a valuable management practice for about 3.4 million ha of cropped area in the semi-arid and sub-humid regions of Texas. The practice may be useful in other areas also, to mitigate the effects of short duration moisture stress on crop yields.

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#### INTRODUCTION

Texas agriculture uses 72% of the state's total water consumption. There are 10.5 million hectares of cropped area in Texas, and approximately one-fourth of it is irrigated. Because of declining ground water levels, increased energy costs for pumping, and competition for water resources from municipal and industrial users, it is projected that approximately one-third less water would be available for agricultural use by the year 2000. To maintain crop production at current levels, it is critical that new and improved agricultural water conservation technologies be applied in dryland and irrigated agriculture. Furrow diking is a practical, efficient and low-cost technique to conserve water in row-crop agriculture. It is also known as row-damming, tied-ridging or basin listing, and is a practice of building small dikes or dams at regular intervals in the furrows to hold runoff or irrigation water for infiltration (Figure 1).

Furrow diking is not a new technology. Practices similar to diking were first attempted in the United States more than fifty years ago (Wood, 1933; Hughes, 1933; Shedd et al., 1935; and Cole and Morgan, 1938). However, the basin lister was used during the 1940's primarily in the fallow period after wheat each year, and very little improvement in yields was noted between basin listing and other conventional treatments (Daniel, 1950; Luebs, 1962). The practice of basin listing was given up in most areas by 1950. Kuska and Mathews (1956) reported that basin listing of wheat did not significantly increase yields. Slow operating speed, poor weed control and difficulty with seedbed preparation were among the reasons given for abandoning the practice. Dagg and Macartney (1967) and Hudson (1971), however, reported successful results with basin tillage in Africa.

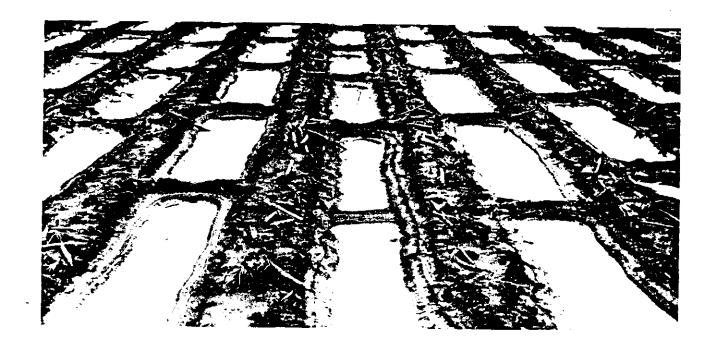


Fig. 1. Furrow dikes to hold runoff (Courtesy: O. R. Jones, USDA-ARS, Bushland, Texas).

The first attempts to systematically study furrow diking in Texas appear to have begun in 1975 with a replicated grain sorghum experiment at the USDA Conservation and Production Research Laboratory at Bushland (Clark and Jones, 1980) and a dryland cotton study at Lubbock (Bilbro and Hudspeth, 1977). Improvement in diker design (Lyle and Dixon, 1977), as well as the development and use of herbicides have resulted in the practice of furrow diking to spread rapidly in the High Plains and other Texas regions. Colburn and Alexander (1986) estimate that approximately 1.6 million ha are currently diked in Texas.

A research review of past furrow diking studies in Texas is included as Section I of this report. Crop yield increases reported earlier have varied considerably between locations and between years at any particular location. Field experiments were limited to a few sites and for relatively short periods of time. Although positive results were obtained, they did not adequately quantify the long-term benefits from furrow-diking. Besides, those results may not be directly transferable to other sites in Texas.

To evaluate the long-term impact of furrow diking, a computer simulation approach combining hydrologic and crop growth models was used. A runoff prediction method based on the USDA-SCS methodology was included with three crop models, validated with field data, and run for a 25 year period. The modeling results are discussed in Section II of this report.

The Soil Conservation Service (SCS) of the U. S. Department of Agriculture in Texas developed technical standards and specifications for furrow diking (USDA/SCS/TX, 1983; Lindemann, 1984). These standards do not consider evaporation or infiltration, but do provide broad specifications for furrow dike spacing and use. The following is the technical standard as developed for Texas:

## A. Crops Applicable:

- 1. Summer growing crops such as: cotton, sunflowers, grain sorghum, corn, soybeans, etc.
- 2. Applicable to fallow period prior to planting following warmor cool-season crop.

#### B. Date and Duration of Installation:

- 1. As a minimum dikes will be installed between April 1 and no later than July 10 each year.
- Dikes shall be utilized for at least 90 consecutive days starting anytime between April 1 and July 10.
- 3. Dikes may be installed prior to April 1 when being used to increase soil water content at planting time.

## C. Applicable Slopes:

- 1. Dikes may be used with up-and-down hill planting where slopes are 1.0% gradient or less.
- Dikes may be used on all slope ranges where the field is actually worked on the contour.

# D. <u>Dike Spacing</u>, Height, and Size:

- On slopes with less than 1% gradient the spacing between dikes in the furrow can vary from 2.5 feet to 20 feet (0.75 m to 6 m). On slopes with 1% gradient, the optimum spacing is about 10 feet (3 m).
- 2. On slopes with 1.1% gradient or greater (which requires contour farming), the spacing between dikes in the furrow shall not exceed 12 feet (3.65 m). The normal spacing ideally should not be less than about 8 feet (2.45 m).

#### OBJECTIVES

The objectives of this research were to determine the feasibility, potential geographic extent and impact of furrow diking in Texas, by

- consolidating and synthesizing results of previous furrow diking studies conducted in Texas,
- 2. analyzing rainfall and runoff at representative locations, and
- assessing the impact of furrow diking on crop yields, using hydrologic and crop modeling techniques.

The following five Texas regions were targeted to determine the effect of conserving runoff (by diking) on crop yields:

High Plains

Rolling Plains

Blackland Prairie

Edwards Plateau

Coastal Bend.

### SECTION I

#### FURROW DIKING IN TEXAS - A RESEARCH REVIEW

## High Plains

Bushland: Dryland crop yields in semi-arid climates are generally dependent on available soil water. Even a modest timely increase in soil water can result in a significant yield increase under semi-arid conditions. Furrow diking can retain surface runoff and increase soil moisture availability for crop production. The effectiveness of furrow diking would depend on the timing at which dikes are installed. Runoff data from dryland wheat-fallow-sorghum-fallow plots (Jones et al., 1984) can be used to show that the greatest benefit from diking at Bushland would result if dikes were built in April each year (Figure 2), so that the runoff during the period of May through September could be captured.

Clark and Jones (1980) reported a five-year furrow dike study conducted at the USDA Conservation and Production Research Laboratory at Bushland, Texas. Their replicated study began in 1975 with non-diked furrows, diked furrows, and flat planting to evaluate the diking technique. All plots were on Pullman clay loam which has a low infiltration rate (0.15 cm/hr) and a slope of 0.2%. Furrows were made with a conventional 75-cm lister or a tri-level lister allowing for two 75-cm rows of grain sorghum the first 3 years (1975-1977). In 1975 and 1976, furrow dikes were first made every 15 m with a laboratory designed blade-like scoop. In 1977, a hydraulic tripping diker designed by Lyle and Dixon (1977) was built and used. A commercial dammer was used in 1979 which spaced dams 3.5 m apart. Grain sorghum was planted between June 5 and 15 and harvested in October. Initially dikes were constructed in a separate operation immediately after herbicide application. Later,

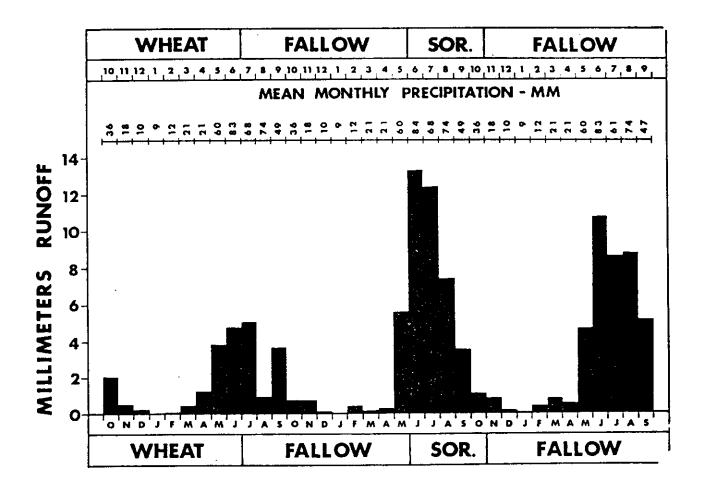


Fig. 2. Twenty-six year (1958-83) mean monthly precipitation and runoff, wheat-sorghum-fallow sequence, Bushland, Texas (Jones et al., 1984).

herbicide was applied as an integral part of the diking operation. Grain yields were obtained by combine harvesting 0.67 ha plots. Storm runoff from the non-diked treatment was measured with 30-cm "H" flumes equipped with water stage recorders. Soil water content was monitored with the neutron method.

Furrow diking benefits in any particular year were shown to depend on the seasonal precipitation and storm runoff. Seasonal (June 1 to October 31) precipitation and runoff are shown in Table 1. Yield increases due to furrow dikes were observed only in years with above average runoff. Only one significant runoff event occurred in 1975 to produce a seasonal runoff of 2.1 cm and no runoff occurred in 1976. In 1977, all four runoff events occurred in August, while in 1978, one event of 3.8 cm occurred in September. Only 0.2 cm of runoff was measured in 1979.

Table 1. Seasonal (June 1 - October 31) rainfall and runoff from non-diked furrows, Bushland, Texas (Clark and Jones, 1980).

Year	Seasonal rainfall (cm)	Seasonal runoff (cm)		
1975	21.8	2.1		
1976	21.9	0.0		
1977	27.5	8.5		
1978	35.8	3.8		
1979	29.2	0.2		
20 yr. Avg.	29.4	3.8		

Grain yields were variable, ranging from 0 to 2,900 kg/ha during the 5 year test (Table 2). High yields were produced in 1975 and 1979

because of high levels of soil water stored at planting followed by timely precipitation. Although seasonal precipitation was much below average in 1975, rainfall was adequate during July to maintain a high soil water content in early August. August rainfall was limited, but plants reached maturity using stored soil water. Furrow diked treatment grain yields were increased 340 kg/ha by conserving 2.1 cm of runoff in 1975.

Plot areas for the 1975 and 1979 crops had been fallowed the previous year, resulting in high soil water contents at planting and high grain yields. Plot areas for the 1976, 1977 and 1978 crops had been planted in sorghum the previous year and therefore less soil moisture available at planting time may have lowered yields. In 1976 all sorghum treatments were destroyed by hail. Although seasonal precipitation was near average in 1977, low soil water content and precipitation during June and July resulted in small, severely stressed plants unable to efficiently use the ample August rainfall. Even though 1977 sorghum yields were low, furrow diking increased yields 650 and 870 kg/ha, respectively, compared to the flat and non-diked treatments.

Table 2. Yields of grain sorghum planted in 75-cm rows at Bushland, Texas (Clark and Jones, 1980).

	Treatments						
Year	Diked	Non-Diked	Flat				
		kg/ha					
1975	2,920	2,580	2,470				
1976 1977	1 200	0	0				
1978	1,380 1,050	510	730				
1979	2,890	1,120 2,870					
Avg.	1,650	1,420					

Seasonal precipitation in 1978 was above average, however, below average July and August precipitation caused low yields. Runoff in September 1978 occurred too late in the season to benefit the crop and the excess soil water resulting from conserved runoff on the furrow-diked treatment possibly reduced sorghum yields compared to the non-diked treatment (Table 2).

Little difference in sorghum yields should be expected between diked and non-diked treatments in years when adequate moisture is available. However, in dry years, diking can prevent a crop failure, as in 1977. In each of the years when runoff was caught in the diked furrows before August 15, yields were increased. Unger (1972) indicated that each additional 1 cm of stored soil water at planting could increase yields about 275 kg/ha.

Treatment effects on soil water content are shown in Figs. 3-6.

All treatments had similar soil water contents at planting in 1975

(Fig. 3) and only small differences were observed until July 10. Runoff caught from rainfall on July 10 and 11 increased the soil water content in the diked treatment by 1.3 cm. This difference continued until all treatments reached a similar dry condition at harvest. A similar condition existed in 1977 (Fig. 4), except all treatments were much drier at planting and remained dry until the large rain on August 11. The diked treatment increased in soil water content after the rainfall on August 11 and August 22, reaching a maximum difference of 5.6 cm by August 24. In 1978, the diked treatment had approximately 1 cm more soil water during most of the season until the large rain in September when the soil water content reached field capacity in both treatments (Fig. 5). In 1979 soil water contents were similar throughout the season because little runoff occurred (Fig. 6).

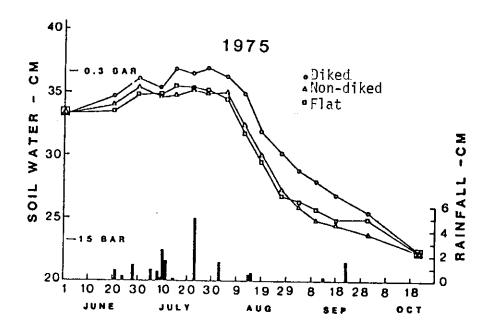


Fig. 3. Soil water content (0-120 cm) and seasonal precipitation for grain sorghum on diked, non-diked and flat tillage treatments, 1975, Bushland, Texas (Clark and Jones, 1980).

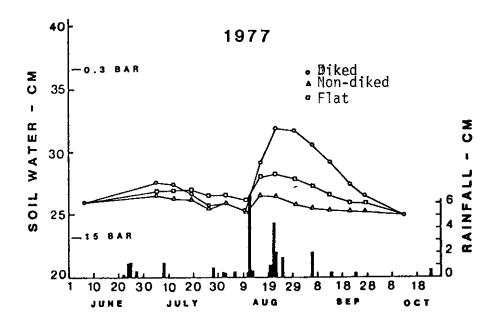


Fig. 4. Soil water content (0-120 cm) and seasonal precipitation for grain sorghum on diked, non-diked and flat tillage treatments, 1977, Bushland, Texas (Clark and Jones, 1980).

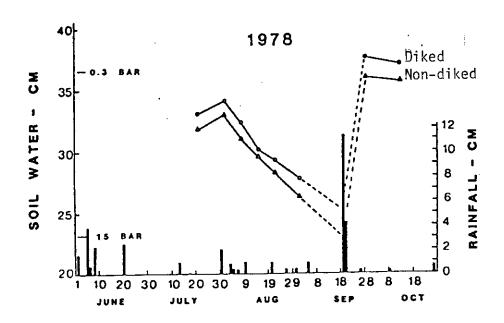


Fig. 5. Soil water content (0-120 cm) and seasonal precipitation for grain sorghum on diked and non-diked treatments, 1978, Bushland, Texas (Clark and Jones, 1980).

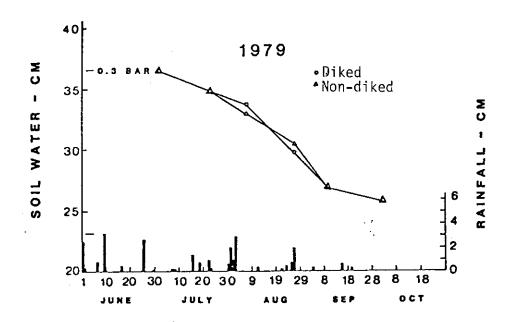


Fig. 6. Soil water content (0-120 cm) and seasonal precipitation for grain sorghum on diked and non-diked treatments, 1979, Bushland, Texas (Clark and Jones, 1980).

Limited Irrigation - Dryland (LID) System:

Stewart et al. (1983) developed a limited irrigation-dryland (LID) farming system using furrow diked land and limited supplies of irrigation water for efficient grain sorghum production. The objective of the LID concept is to maximize the conjunctive use of growing season rainfall with a limited supply of irrigation water. The unique feature of the LID system is the flexible adjustment during the crop growing season of the amount of land irrigated, allowing more land to be irrigated during above average rainfall years than during dry years. Risk is low in the LID system, and response is good in favorable rainfall years.

The LID system concept is illustrated in Fig. 7. A graded furrow field, 600 m long on 0.3 to 0.4% slope, was divided into three water management sections. The upper half of the field was managed as "fully irrigated." The next one-fourth was managed as a "tailwater runoff" section that utilized furrow runoff from the fully irrigated section. Finally, the lower one-fourth was managed as a "dryland" section capable of receiving and utilizing any runoff resulting from either irrigation or rainfall on the wetter, fully irrigated and tailwater runoff sections. Plant densities and fertility were reduced down the field to decrease stress because irrigation water was decreased down the field. Furrow dikes were placed about every 4 m throughout the length of the field. Alternate 76-cm furrows were irrigated, and the dikes in the irrigated furrows were notched to insure that irrigation water moved over the dikes and down the furrow, rather than across the beds. The remaining furrow dikes on the lower part of the field and the dikes in the non-irrigated furrows for the entire length of the field prevented rainfall runoff. A predetermined amount of irrigation water was applied

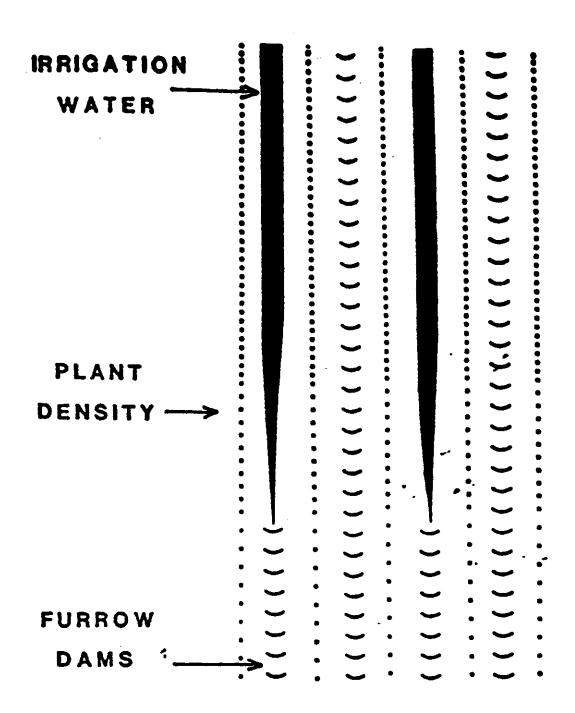


Fig. 7. Schematic drawing of the Limited Irrigation-Dryland (LID) System (Stewart, 1985).

at regular time intervals. The extent to which the entire field was irrigated depended on the rainfall received — the wetter the year, the greater the advance of a fixed application down the field. The objective was to prevent or minimize any water from rainfall or irrigation from leaving the field. More recent studies with the LID system have utilized a medium seeding rate throughout the field and furrow dikes in only alternate furrows that are not used for irrigation (Stewart, 1985). These changes make the system somewhat easier to manage, and the benefits are similar. The treatments that were compared in the 3 year study (Stewart et al., 1983) and the irrigation water use efficiency achieved in each of the treatments is shown in Table 3.

Table 3. Irrigation water use efficiencies for various treatments, Bushland, Texas.

Treatment	Irrigation water use efficiency kg grain/m <sup>3</sup>
Dryland	
Dryland, diked (4 m intervals)	0.02
Fully irrigated	0.92
LID - 250 mm	1.36
LID - 185 mm	1.50
LID - 125 mm	1.70
LSD (0.05)	0.64

Even though the fully irrigated treatment may result in the highest yield, the irrigation water use efficiency is the important element to consider when only limited amounts of irrigation water are available.

As indicated in Table 3, the highest water use efficiency with limited irrigation application was obtained with the LID-125 mm treatment.

Lubbock: Bilbro and Hudspeth (1977) reported the results of a furrow diking study with cotton at Lubbock in 1975. The dikes were made in three dryland tests in which half of each plot was left non-diked and the other half kept diked from March until October or later. Dikes were spaced about 3 m apart. Rainfall from May through September exceeded the 50-percent probability level each month, but October rainfall was only 2 percent of normal. The total for these 7 months was 30 cm, and the 59-year average was 29.7 cm. Air temperatures were below normal, and the cotton plants were 1-2 weeks behind normal growth by September. Cold, cloudy, windy, wet weather from September 13-15 was followed by several days of hot, dry, windy conditions. Consequently, most cotton leaves were desiccated and later dropped from the plants resulting in lower lint yields. The following three tests were conducted:

Test A: There were four replicated plots (8 m x 94 m) with slopes of 0.9%, row spacing 1 m, and access tubes for periodic soil moisture measurement. The diked and non-diked plots produced 336 kg/ha and 304 kg/ha respectively. The 10.6% lint increase for the diked plots was statistically significant. Moisture measurements about 36 hrs after a 39 mm rain on July 21 showed that the top 30 cm of the soil had 19.2% more total water (6.35 mm) than the non-diked plots. This indicated that considerable runoff occurred from the non-diked rows.

Test B: The plots were 8 m x 18 m replicated on land having 0.2% slope. Row spacing was 1 m. The average lint yields in the diked plots was 383 kg/ha, 14.7% greater than non-diked, which was statistically significant.

Test C: Plots were 8 m x 213 m, replicated four times on a land slope of 0.2%; both 1 m row spacing and 25 cm double row spacing on beds were used. Diked and non-diked plots on 1 m spacing yielded 279 kg/ha and 224 kg/ha while the double row plot yields were 264 kg/ha and 252 kg/ha, respectively. Even though the diked yields were higher, they were not statistically significant in this test.

All fields were observed following each rain, and evidence of runoff from the diked plots was not visible. After some of the heavy
rains, considerable soil erosion was noticed in the non-diked rows of
the 0.9% slope field (Test A). Erosion was less extensive in non-diked
rows of Tests B and C (0.2% slope). These tests revealed that furrow
diking could effectively prevent runoff and erosion and increase
yields.

Irrigated-dryland basin tillage evaluations were conducted with cotton in 1977 (Lyle and Dixon, 1977), and with sorghum in 1978 at Lubbock (Lyle et al., 1978). The replicated experiments had  $8.2m \times 335m$  plots on Olton loam soil with 0.9m row spacing. The five treatments were:

- Basin tillage Alternate Furrow-Irrigated (BT-AF-I)
- 2. Conventional Irrigated (C-I)
- Basin tillage Every Furrow Dryland (BT-EF-D)
- 4. Basin tillage Alternate Furrow Dryland (BT-AF-D)
- 5. Conventional Dryland (C-D)

Relevant fertilizer application, dike installation, irrigation and rainfall information during the two seasons are given below:

#### 1977

Crop Fertilizer : Cotton : None

Dikes

: Installed - June 17; Removed - September 7 : Pre-irrigated March 21-24 with 13.2 cm:

Irrigation : Pre-irrigated March 21-24 with 13.2 cm; alternate furrow irrigation of 3.3 cm on July

4-5

Rainfall

: 9.4 cm received while dikes were in place

1978

Crop

: Sorghum

Fertilizer

180 kg/ha N applied as NH3 and 45 kg/ha P

applied as P<sub>2</sub>0<sub>5</sub>

Dikes Irrigation : Installed May 12; remained through harvest : Preplant April 14 with 5.7 cm and four later

alternate furrow irrigations of approximately

3.0 cm each

Rainfall

: 14.4 cm received during the growing season

In 1977, the limited rainfall after diking prevented large yield increases in the diked plots. The date of the runoff producing rain (June 21) was also early and closely followed a spring with adequate soil moisture. However, the retained rainfall supplemented alternate furrow irrigation to the extent that a significant yield increase did result. The results are shown in Table 4.

Table 4. Basin tillage cotton lint yields (kg/ha), 1977, Lubbock, Texas (Lyle and Dixon, 1977).

Treatments	BT-AF-I	C-I	BT-EF-D	C-D	BT-AF-D
Yields	448 a	404 b	319 c	298 c	294 с

 $L.S.D_{0.05} = 37.6 \text{ kg/ha}$ 

<sup>\*</sup> Yields followed by the same letter are not significantly different at the 5% level.

Results of the basin tillage evaluation with 1978 grain sorghum were similar to those obtained in the 1977 with cotton. Minimal runoff producing rains and little growing season rainfall in both years resulted in failure to produce significant responses from basin tillage on dryland plots. However, furrow dikes placed in alternate furrows both years and irrigated in the open furrow produced significant yield increases at the 5% level compared to conventional tilled plots irrigated every other furrow with an equal water application.

The results of the 1978 basin tillage grain sorghum evaluation are shown in Table 5.

Table 5. Basin tillage grain sorghum yields (kg/ha), 1978, Lubbock, Texas (Lyle et al., 1978).

Treatments	BT-AF-I	C-I	BT-AF-D	BT-EF-D	C-D
Yields*	1540 a	1251 b	303 с	289 c	276 c

 $L.S.D_{0.05} = 258.3 \text{ kg/ha}$ 

Dryland crop yields in the Southern Great Plains are normally dependent upon the available soil water. Grain sorghum is highly responsive to water and in some instances even 1 cm of additional stored water can produce significant yield increases. Most rainfall there occurs from May through September. Rainfall during that time is from thunderstorms which have high intensities and short durations. These storms frequently have intensities greater than the intake rate, thereby causing water to pond and leave the field as storm runoff. Furrow diking, under these circumstances, provides additional opportunity time for ponded runoff to infiltrate and recharge the soil profile.

<sup>\*</sup> Yields followed by the same letter are not significantly different at the 5% level.

Low Energy Precision Application (LEPA):

The LEPA (Low Energy Precision Application) irrigation concept and the application system have been described by Lyle and Bordovsky (1981). The system distributes water directly to the furrow at very low pressure through drop tubes and emitters which are located at a height of 5 to 10 cm above the furrow. The system was designed to minimize the effect of soil and climatic variables that adversely influence furrow and sprinkler irrigation efficiencies. It would also maximize rainfall utilization by conjunctive use with microbasin tillage.

Lyle and Bordovsky (1983) describe the results of the LEPA irrigation system evaluation on soybeans. Factors analyzed in comparing the LEPA system with sprinkler and furrow methods included distribution uniformity, application efficiency, water use efficiency and energy savings. Three irrigation systems (LEPA, furrow and sprinkler) and the presence or absence of furrow dikes were compared. Approximately equal amounts of water per unit land area were delivered to each system. Four furrow treatments consisted of eight rows per treatment, each with 305 m length of run. The furrow treatments were (a) furrow irrigated - conventional; (b) furrow dryland - conventional; (c) furrow irrigated - micro-basin; and (d) furrow dryland - micro-basin. Soil surface modification to form micro-basins is considered an integral part of the LEPA system and was found to effectively eliminate runoff.

The irrigation application efficiency was defined by Lyle and Bordovsky, 1983 as:

$$E_{a} = \frac{W_{d} - e_{a} - e_{ws} - e_{ss} - D_{p} - R}{W_{d}}$$
 (100)

where  $E_a$  is application efficiency,  $W_d$  is water delivered to the field,  $e_a$  is spray evaporation in the air,  $e_{ws}$  is evaporation from a free water surface,  $e_{ss}$  is evaporation from the soil surface during irrigation,  $D_p$  is deep percolation and R is runoff.

The application efficiency data are summarized in Table 6. For all three systems, LEPA, sprinkler and furrow, the application efficiencies were higher with basin tillage than with conventional tillage.

Below average rainfall in 1980 and above average rainfall in 1981 resulted in a total of 49.3 cm and 23.6 cm of irrigation water applied in 1980 and 1981, respectively. Total water delivered to the crop (rainfall plus gross irrigation) averaged 66.5 cm in 1980, and 62.0 cm in 1981. The 1980 results should more accurately represent the normal yield responses from the irrigation methods tested. Frequent rainfall late in the 1981 growing season practically masked the response to irrigation and favored furrow treatments where no ponding occurred. The Application Efficiency (Ea) summary, Lubbock, Texas (Lyle and Table 6. Application for the first of the perfection of the foundation of the follows of the formation of the follows of the f

ρq Квиде IZ Average E<sub>a</sub> ₽8 **L6 L6** Капge IJ L L Average E<sub>d</sub> 9/ LLτ6 Sprinkler Sprinkler Monnul LEPA Furrow LEPA Conventional tillage Sasin tillage Bordovsky, 1983).

Average E<sub>a</sub>

Two-year

Lyle and Bordovsky (1983) showed that the LEPA system with basin tillage resulted in the lowest irrigation energy expense (2¢/kg). The two-year average grain yields and net returns (after expenses) for the various treatments are shown in Table 7. The LEPA system in conjunction with basin listing (furrow diking) was superior to all the other treatments.

Table 7. Two-year soybean yields and net returns for various treatments, Lubbock, Texas.

		Basin tilla	ge	Conventional tillage				
	LEPA	Sprinkler	Furrow	LEPA	Sprinkler	Furrow		
Two-year average yield (kg/ha)	2633	2212	2386	2294	2004	2455		
Two-year average net return (\$/ha)	546	439	463	445	379	486		

## Rolling Plains

Gerard et al. (1983) conducted studies in 1980 and 1981 on Miles fine sandy loam soil near Vernon to determine the effect of subsoiling and furrow diking on cotton yields. These cultural practices did not show any effect on cotton yields in 1980 because of low rainfall and extremely high temperatures. However, in 1981, diking prevented runoff and increased yields from 365 Kg/ha to 481 Kg/ha. Yield increases above the non-diked treatment were 15% for the half-diked (alternate row diked), 32% for the fully diked and 38% for the diked-subsoiled treatment. The average non-diked treatment runoff during the 1981 crop season was estimated to be 35% of the rainfall. Gerard et al. (1984) reported 1981 and 1982 studies of sorghum and cotton on an Abilene loam soil and on a Miles fine sandy loam soil respectively. The tillage

treatments during 1981 and 1982 are shown in Table 8, and the rainfall received during those two years is shown in Table 9. The slopes in the furrows ranged from 0.1% on the lower half to 0.4% on the upper half of

Table 8. Sorghum and cotton tillage treatments, 1981 and 1982, near Chillicothe, Texas (Gerard et al., 1984).

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very other furrow.  and 5 (sorghum) and 3 and 4 (cotton) was	a Half diked refers to diking e b Every furrow for Ireatments 4 diked.
Diked b and subsoiled 0.35 m	Þ
Diked b	3
Half diked <sup>a</sup>	2
Conventional beds (check)	I
nottoo	Treatment No.
slavnatni m č.0	
Diked b and subsoiled 0.4 m deep at	g
Diked b	ħ
Subsoiled 0.4 m deep at 0.5 m intervals	3
Half diked <sup>a</sup>	2
Conventional beds (check)	· T
Sorghum	Treatment No.
*/LOCT 10 P P P P P P	n) cnval (augustitus)

Table 9. Monthly rainfall for sorghum and cotton, 1981 and 1982, near Chillicothe, Texas (Gerard et al., 1984).

Total	2119	716.2	<u>621.2</u>	6*089
Decemper	Ι* Δ	₽*82	I * Z	7°97
<b>∏o∧ember</b>	8*91	9° / b	11.2	L*89
0ctober	6°	8.2	81.5	<b>9</b> *E
September	18*8	9*09	9°98	9 <b>*</b> 61
tsuguA	ZJ°1	0.67	0.77	8.78
չևոն	9"/[	9 <b>°</b>	6*87	9*79
əunբ	£*86	<b>∠*</b> 901	120.1	120.1
May	132.1	9*861	126.2	1.722
ſinqA	0.18	<b>6*8£</b>	62,2	43.2
Магсһ	₽*68	[*99	34.0	42,2
February	20*3	<b>9*</b> 8	21.1	<b>†*</b> 9
าฐมหาฐา	1.0	9°I8 W	I*3	8.88
	1861	7861	1861	Z86 I
	θ <b>γ</b>		Э <u>Д</u>	9L
	Sorg	աույն	<b>.</b> 10ე	uoı

The sorghum grain and cotton lint yields recorded in 1981 and 1982 are shown in Tables 10 and 11, respectively. Diking and subsoiling reduced runoff and significantly increased yields of sorghum and cotton. Yields of diked sorghum and cotton were 108% and 32% higher than the check, respectively. Yields of sorghum on the diked treatment in 1985 and 1986 however, were only 14% and 8.5% higher than non-diked (Gerard, 1987). These data confirm the high variability that exists from year to year in the yield increases due to furrow diking. The data further establish the need to analyze furrow diking yields on a long term basis, to adequately account for the year to year variability.

Table 10. Grain sorghum yields, treatments and locations along the slope, 1981-82, Chillicothe, Texas (Gerard et al., 1984).

		1981		
Treatments	Upper	Middle	Lower	Average
		kg/	'ha	
Check Subsoiled Half diked Diked Diked and subsoiled	536 a* 350 a 1615 b 2027 b 2175 b	1065 a 591 a 1995 b 2579 bc 2872 c	1887 a 2805 a 2644 a 2872 a 2507 a	1163 a 1249 a 2084 b 2493 b 2518 b
Average	1341	1821	2544	

<sup>\*</sup>Values for each location on slope or averages followed by same letter are not significantly different at the 5% level.

		1001/1000			
Treatments	Upper	Middle	Lower	Average	1981/1982 Average
		kg/	ha		
Check	735 a	1694 a	3162 a	1864 a	1513 a
Subsoiled	1439 b	2558 a	3799 a	2598 б	1924 b
Half diked	2285 c	2410 a	3273 a	2656 b	2370 с
Diked	3083 d	4036 b	4324 a	3815 c	3154 d
Diked and subsoiled	3827 e	4169 b	3633 a	3876 c	3197 d
Average	2274	2973	3638		

<sup>\*</sup> Values for each location on slope or averages followed by same letter are not significantly different at the 5% level.

Table 11. Lint cotton yields for different treatments and locations along the slope, 1981-82, Chillicothe, Texas (Gerard et al., 1984).

		1981		
Treatments	Upper	Middle	Lower	Average
		kg/	ha	
Check Half diked Diked Diked and subsoiled	303 a* 374 b 447 c 445 c	370 a 404 b 514 c 538 c	422 a 480 a 482 a 533 a	365 a 420 b 481 b 506 b
Average	393	457	479	

	1982				1001/1002
Treatments	Upper	Middle	Lower	Average	1981/1982 Average
		kg/	ha		
Check Half diked Diked Diked and subsoiled	292 a 436 b 490 c 478 c	381 a 452 ab 515 b 483 b	433 a 488 a 468 a 438 a	369 a 459 b 491 b 466 b	367 a 439 b 486 c 486 c
Average	424	458	457		

<sup>\*</sup> Values within each location on slope or averages followed by same letter are not significantly different at the 5% level.

Clark (1983) reported the results of a tillage test on an Abilene clay loam soil which compared diked, alternate row diked and non-diked treatments for conventional and reduced tillage systems. Satisfactory rainfall was received during the year (85% of the normal). The yield response of cotton is shown in Table 12. Furrow diking prior to the spring planting resulted in significant yield increases. Diking alternate and every furrow resulted in average yield increases of 16 and 36 percent, respectively.

Table 12. Yield response of cotton to tillage treatments, 1981, Chillicothe, Texas (Clark, 1983).

		Lint	yield (kg/ha	)	
Tillage System	Subsoiled	F None	urrows diked Alternate	All	Average
Conventional Reduced Reduced	100 cm 50 cm	214 255	294 261 259	314 314 330	274 a 277 a 294 a
Average		234 c*	271 b	319 a	

<sup>\*</sup> Means within a row or column followed by the same letter are not significantly different at the 5% probability level.

The gross monetary values from the cotton tillage test (Clark, 1983) are shown in Table 13.

Table 13. Gross value in dollars per hectare of cotton from tillage test, 1981, Chillicothe, Texas (Clark, 1983).

		Value per	hectare in d	ollars	
Tillage System	Subsoiled	Fo None	urrows diked Alternate	A11	Average
Conventional		195	269	287	250 a
Reduced	100 cm	237	242	288	256 a
Reduced	50 cm		250	306	278 a
Average		216 c*	253 b	294 a	

<sup>\*</sup> Means within a row or column followed by the same letter are not significantly different at the 5% probability level.

Bordovsky (1983) reported that cotton grown on furrow diked plots at Munday yielded an average of 10.5% higher than non-diked check plots; however, this increase was not statistically significant at the 5% level of probability. Only 5 cm of rainfall were received from mid-June to mid-September.

### Central Texas

Krishna and Arkin (1985) conducted a furrow diking feasibility evaluation for Central Texas by analyzing hydrologic data from two research watersheds monitored by USDA-ARS near Riesel, Texas. Both watersheds are located on Blackland soils and their physical characteristics are shown in Table 14.

Table 14. Physical characteristics and cropping systems of two USDA-ARS watersheds, Riesel, Texas (Krishna and Arkin, 1985).

Watershed	Area (ha)	Average slope (%)	Cropping system
Y-6	6.6	3.2	oats, corn, sorghum (rotation) oats, corn, sorghum (not in rotation)
Y-7	16.2	1.9	

Runoff data for 26 years from watershed Y-6 and 20 years from Y-7 were analyzed and it was determined that there is an 80-90% probability of receiving runoff during the late spring months in Central Texas and, that on average, more than 50 mm of runoff can be expected to occur between March and June in the Waco-Temple area, most of which occurs in April and May. Krishna and Arkin (1985) found that at least 70% of the late spring and/or early summer runoff occurs between April 16 and June 15 and, therefore, an appropriate period to build furrow dikes would be no later than mid-April in the Temple area.

The analysis showed further that while runoff events of 3.80 cm or less contributed the major portion of total runoff, most events were less than 2.54 cm and approximately 75% of these were 1.25 cm or less (Table 15). This indicates that the chances of water ponding in diked furrows for more than a day are low in the Blacklands. The dikes should, however, be at least 7.6 cm high after settling to hold the large and infrequent runoff volumes. Furrow diking appears to be

feasible in the Central Texas Blacklands, and field studies have been initiated to ascertain the benefit/cost ratio of adopting this practice in Central Texas.

Table 15. Runoff distribution by amount and month\*, Central Texas (Krishna and Arkin, 1985).

Amount (cm)	March	April	May	June	March-June	Total (cm)
		Y-6	runoff	events	·	
0.25-1.25	15	18	19	10	62	37.8
1.26-2.53	2	5	5	4	16	31.7
2.54-3.80	2	3	7	3	15	43.2
3.81-5.06	1	2	1	0	4	16.8
>5.07	1	2	2	1	6	38.1**
		Y-7	runoff	events		
0.25-1.25	5	18	9	6	30	18.3
1.26-2.53	0	3	9	4	16	24.9
2.54-3.80	2	1	2	1	6	23.9
3.81-5.06	0	1	2	0	3	17.0
>5.07	0	3	2	0	5	55.9**

<sup>\* 26</sup> years of data for watershed Y-6 and 20 years of data for Y-7.

Krishna et al. (1987) evaluated the likely long-term impact of furrow diking on sorghum yields by combining SORGF, a grain sorghum simulation model with the surface runoff hydrology from the USDA-ARS model EPIC (Erosion-Productivity Impact Calculator). A twenty-year simulation was conducted using climatic data from Temple, Uvalde, and Lubbock. It was shown that diking during the growing season is likely to increase long-term mean sorghum yields by approximately 350 kg/ha at Temple, 590 kg/ha at Uvalde and 450 kg/ha at Lubbock. The increase in net benefits due to furrow diking in the growing season can therefore range from approximately \$20 per ha at Temple to \$35 per ha at Uvalde.

<sup>\*\* 1957</sup> was an extremely high rainfall year. Runoff events > 5.0 cm contributed 19.0 cm in Y-6 and 27.4 cm in Y-7 in 1957.

### Edwards Plateau

Mulkey (1986) reported the results of a furrow diking study at Uvalde during 1985. Sorghum was grown on Uvalde silt loam, with a row spacing of 96 cm and plant population of 124,000 per ha. There were three treatments: non-diked, diked during the fallow season and diked during the growing season. The yields reported were 3,500 kg/ha for non-diked, 4,874 kg/ha for diked during the fallow season, and 4,069 kg/ha for diked during the growing season. The treatment that was diked during the fallow season had the highest yield because at planting time it stored 17.6 cm of water in the root zone (180 cm) compared to only about 12 cm in the other treatments. The treatment that was diked during the growing season, however, had the greatest amount of soil water remaining in the profile (1.4 cm) at harvest. In 1986, diking in the growing season resulted in only 100 kg/ha yield increase over the non-diked treatment. Diking in the fallow season resulted in less yield than non-diked, but this was probably due to a lower plant population in that treatment (66500 plants/ha) as compared to the non-diked treatment (75,100 plants/ha). The Uvalde data for both 1985 and 1986 were used for model validation.

### FURROW DIKING COSTS

Furrow diking equipment requires an initial investment of \$150 to \$300 per row of cultivation, depending upon the design selected. Wistrand (1984) estimated that even with a high financing rate of 14%, the annual cost of owning and operating furrow dike equipment was only about \$2.50/hectare (Table 16).

Table 16. Estimated costs of purchasing and operating nine row furrow dike equipment (Wistrand, 1984).

Costs	Dollars
Investment Costs: Financed 3 years at 14%	9.77
Operating Costs/ha: Fuel1 Labor2 Maintenance3	0.22 0.13 0.71
Subtotal	1.06
Total Annual Cost/ha (\$1.40 +1.06)	2.46

<sup>1</sup> Three passes x 7.0 gallons/hour x 0.198 hr/ha x  $$1.05/gallon \times 0.05$  additional fuel.

3 Price x 0.65 repair ratio/260 ha x 7 year life.

Fuel costs and interest rates have decreased substantially since 1984, while other costs remain approximately the same. The total annual cost now should therefore be lower than \$2.50/ha.

<sup>2</sup> Three times over x 0.198 hr/ha x 4.50 wage/hr x 0.05 added labor.

### SECTION II

#### MODEL DEVELOPMENT AND VALIDATION

Three crop growth models, SORGF (Arkin et al., 1976; Maas and Arkin, 1978), CORNF (Stapper and Arkin, 1980), and COTTAM (Jackson et al., 1984) were combined with the surface runoff hydrology algorithms from the Erosion-Productivity Impact Calculator (EPIC) model (Williams et al., 1984). Additional subroutines have been added to the crop models to compute surface runoff, and changes were made in the soil water balance subroutine to include the runoff component. The sorghum, corn and cotton models, modified to evaluate the impact of diking are called SORDIKE, CORDIKE, and COTDIKE, respectively. The input data that are required include soil bulk density and water holding capacity, initial water content, latitude, land slope, curve number (AMC-II), plant population, maturity type, and row spacing. Meteorological data requirements include daily maximum and minimum temperatures, rainfall and solar radiation.

Surface runoff is predicted for daily rainfall using the curve number equation developed by the USDA-Soil Conservation Service (1972):

$$Q = \frac{(P - 0.2s)^2}{(P + 0.8s)}; P \ge (0.2)s \dots [1]$$

where Q is the daily runoff, P is daily rainfall and s is a retention parameter related to available soil water content SW, as shown below (Williams et al., 1984):

$$s = s_1 \left[ 1 - \frac{SW}{SW + exp(w_1 - w_2(SW))} \right]$$
 [2]

where  $w_1$  and  $w_2$  are shape parameters. The value of  $s_1$  is computed from  $CN_1$  (dry) soil moisture condition curve number as follows:

$$s_1 = 254(100/CN_1-1)$$
 .....[3]

Values of  $CN_1$  and  $CN_3$  corresponding to  $CN_2$  (AMC-II) are tabulated in the SCS Hydrology Handbook (USDA-SCS, 1972) and for computing purposes,  $CN_1$  and  $CN_3$  are related to  $CN_2$  by the following equations:

$$CN_1 = CN_2 - \frac{20(100-CN_2)}{100-CN_2+exp(2.533-0.063(100-CN_2))}$$
 ....[4]

The shape parameters  $w_1$  and  $w_2$  are computed as follows:

$$w_{2} = \frac{\ln \left(\frac{FC}{1-(s_{3}/s_{1})} - FC\right) - \ln \left(\frac{ULM}{1-(2.54/s_{1})} - ULM\right)}{ULM - FC}$$

where FC is the root zone water content at field capacity minus wilting point water content in mm, ULM is the upper limit of water storage in the root zone (porosity minus wilting point) in mm, and  $s_3$  corresponds to the field capacity (wet) moisture condition curve number  $CN_3$ .

An adjustment is made to express the slope effect (SL) on runoff by assuming that the handbook  ${\rm CN}_2$  is appropriate for .05 slope. The

equation for slope adjustment is

 $CN_{2a} = (CN_3 - CN_2) ((1 - 2 exp(-13.86 SL))/3) + CN_2 \dots [8]$  where  $CN_{2a}$  is  $CN_2$  adjusted for slope.

When land is not diked, runoff occurs as predicted by the above equations and is considered lost from the daily water budget. When dikes are in place, no runoff is subtracted from the water budget. The soil water subroutine allows the rainfall to recharge the profile consisting of up to ten soil layers. Any soil water in excess of field capacity is lost as deep percolation below the root zone. It is assumed in the model that dikes are large enough to hold any runoff that is generated and no provision is made for overtopping.

The SORDIKE model was tested for the non-diked treatment by comparing simulated sorghum yields and runoff with measured yields and runoff data from two small USDA-ARS research watersheds Y-6 and Y-8, located at Riesel, Texas (Krishna et al., 1987). Both watersheds are located on a Houston black clay vertisol. Watershed Y-6 is 6.6 ha in area with an average slope of 3.2% and Y-8 is 8.4 ha with a slope of 2.2%. Sorghum was grown on watershed Y-6 in 1974, 77, and 80 and on Y-8 in 1972, 75, and 78. The measured and simulated runoff and crop yields are shown in Table 17. The SORDIKE model was also tested with data sets from Uvalde and Vernon, Texas. Replicated field experiments were conducted in 1985 and 1986 on Uvalde silt loam and Abilene Loam at the Texas A&M University Agricultural Research and Extension Centers at Uvalde and Vernon, respectively (Mulkey, 1987; Gerard, 1987). simulated runoff during the growing season compared well with measured runoff at Vernon in 1985 and 1986. At Uvalde, runoff could not be measured accurately due to overtopping of the dikes. Measured and

simulated yields for three treatments at Uvalde, and two at Vernon are shown in Table 18.

Table 17. Measured and simulated runoff during the growing season, and crop yields, Riesel, Texas.

Year	Surface Runoff (mm)		Sorghum Yield (kg/ha)		
<del></del>	Measured	Simulated	Measured	Simulated	
1972	0	0	3870	3690	
1974	21	34	2940	2650	
1975	54	53	4520	5440	
1977	34	46	3030	3810	
1978	87	99	4870	6190	
1980	76	83	2370	2660	
₹:	45	52	3600	4070	
۸۰ S:	33	35	980	1450	

Table 18. Measured and simulated sorghum yields at Uvalde, and Vernon, Texas.

Location	Year	Treatment	Measured Yield (kg/ha)	Simulated Yield (kg/ha)
Uvalde	1985	Non-diked	3500	3610
Ovarac	1500	Diked in growing sease	on 4070	3990
		Diked in fallow season		4960
Uvalde	1986	Non-diked	2540	2810
ovarue	1300	Diked in growing seas		2980
		Diked in fallow seaso		2590
Vernon	1985	Non-diked	3440	3280
vernon	1903	Diked	4000	3780
Vernon	1986	Non-diked	3810	3200
ver non	1300	Diked	4130	3310

At Uvalde, the predicted crop yields as well as the yield response to diking were in excellent agreement with measured results, both in

1985 and in 1986. At Vernon too, the simulated yields compared well with measured yields in both the years. The simulated yield response to diking was closer to the observed response in 1985 than in 1986. In all cases, the yields predicted by SORDIKE deviated less than 20% from measured yields.

The corn and cotton models, CORNF and COTTAM respectively, have been tested previously against several sets of non-diked data (Maas and Arkin, 1980; Jackson et al., 1984). Data for 1985 on furrow diked corn at the Stiles Farm Foundation was obtained to validate CORDIKE. The simulated non-diked and diked yields were 7650 kg/ha and 7950 kg/ha against measured yields of 7340 and 7520 kg/ha. Attempts were made to obtain additional furrow diking field data on corn at Temple in 1987. but due to a good rainfall season, no differences were found between diked and non-diked treatments. Inadequate runoff and yield data for cotton were available for conducting a robust validation of COTDIKE. However, the data reported by Gerard et al. (1984) for cotton on a Sandy loam soil at Vernon were used to test the model. The non-diked simulated lint yields in 1981 and 1982 were 372 kg/ha and 319 kg/ha respectively, against measured yields of 365 kg/ha and 369 kg/ha. The simulated diked yields were 429 kg/ha and 346 kg/ha in 1981 and 1982 against reported yields of 481 kg/ha and 491 kg/ha. Under non-diked conditions, the predicted yields agreed well with measured yields, but the simulated lint yield response to diking was less than that reported by Gerard et al. (1984).

#### METHODOLOGY

Mean annual rainfall in Texas ranges from 200 mm in West Texas to more than 1300 mm in the East (Fig. 8). Five major agricultural areas in the semi-arid and sub-humid (300-800 mm annual rainfall) regions of Texas, viz., The High Plains, Rolling Plains, Blackland Prairie, Edwards Plateau and the Coastal Bend (Fig. 9) were targeted for conducting furrow dike simulation studies. Daily weather data (rainfall, maximum and minimum temperatures and solar radiation) for a 25 year period (1960-84) were obtained for Lubbock, Vernon, Temple, Uvalde and Corpus Christi (Fig. 10) to represent the five targeted regions. For each location, SORDIKE, CORDIKE and COTDIKE were run to predict the surface runoff each year, and the likely effect of conserving it (by diking) on sorghum, corn and cotton yields. Even though dryland corn is not an accepted cultural practice in the High Plains and Rolling Plains, CORDIKE was run for those locations because the weather data and the model were already available, and little additional effort was needed to obtain the simulation results. Besides, there is always a possibility that crops and cropping systems can change in the future.

A diking option enables the user to allow the excess rainfall to either run off, or to dike it and allow it to infiltrate into the soil. Diking can be simulated for any part of the year, or for the entire year. In the analyses conducted, three scenarios were simulated: non-diked (ND), diked in the growing season (DIGS), and diked all year (DAY). For any given location and crop, the same planting date was used each year. A continuous soil water simulation was maintained from 1960 to 1984 at each location for SORDIKE and CORDIKE. For COTDIKE however, the soil water status was reinitialized

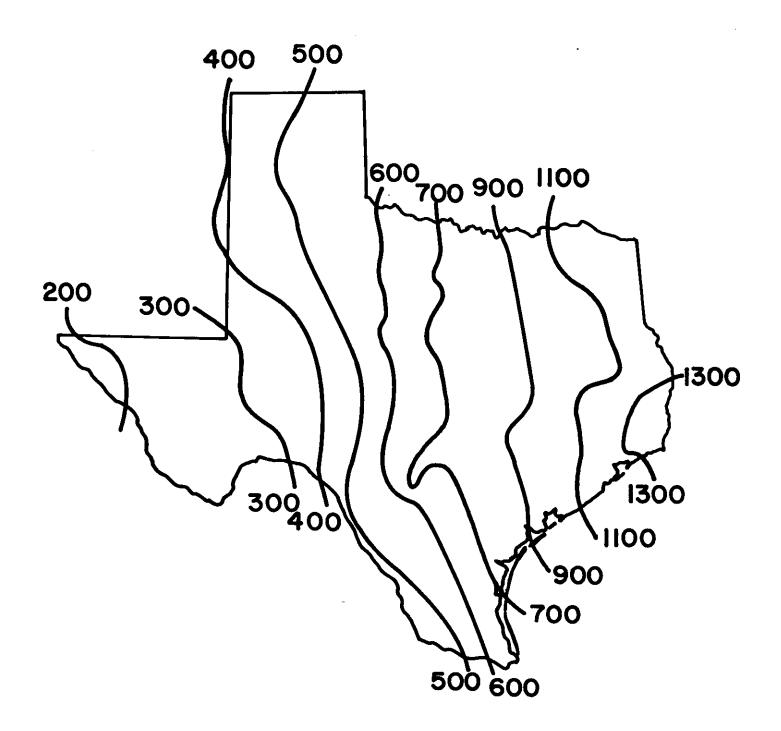


Figure 8. Mean annual rainfall (mm) in Texas.

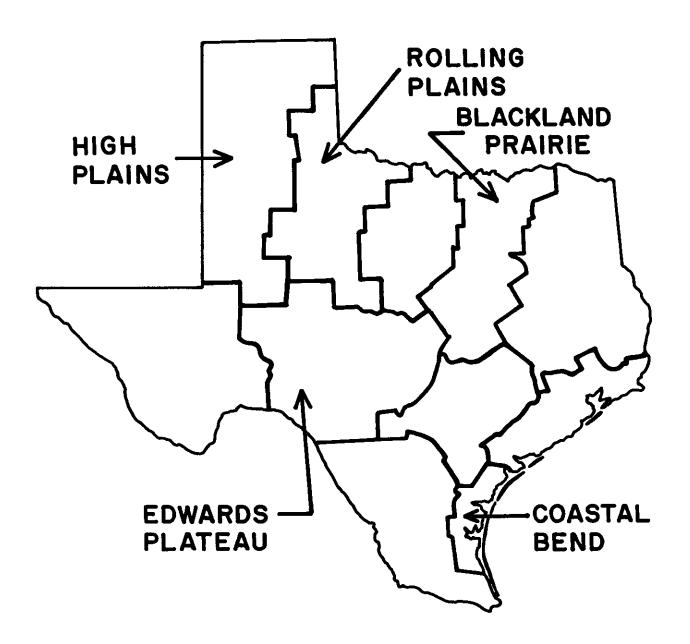


Figure 9. Map of Texas showing crop reporting districts (TDA/USDA, 1986).

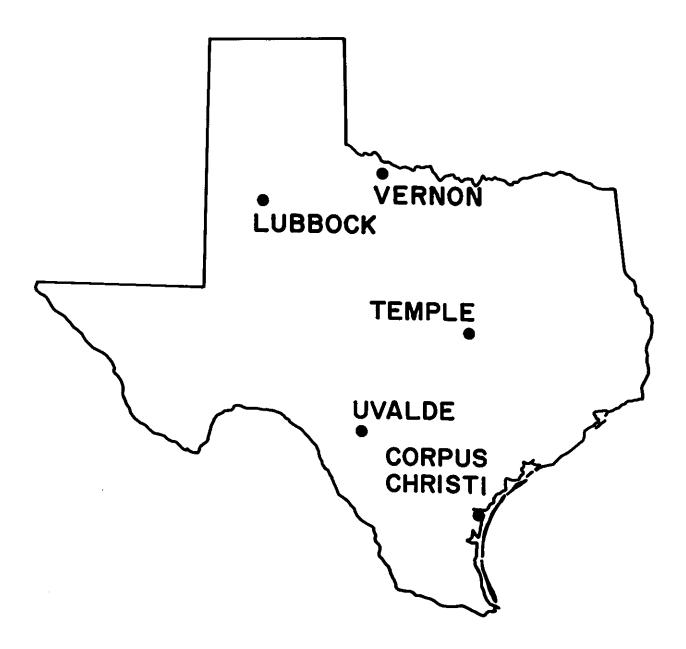


Figure 10. Five Texas locations selected for furrow dike modeling studies.

at the beginning of each year to a preset figure. SORDIKE and CORDIKE were run on a DEC minicomputer while COTDIKE was run on an IBM-AT microcomputer.

The simulated runoff amounts and crop yields were used to determine the Runoff Conservation Efficiency (RCE), defined here as the increase in yield per mm of runoff conserved by diking. The RCE values for the growing season are denoted as RGS and those for the entire year (all year) as RAY. The higher the value of RCE (RGS and RAY), the higher is the value of the runoff water at a given location. The site characteristics and the results of the simulation analyses for each location are described on the following pages.

### SIMULATION RESULTS

# Lubbock (Southern High Plains):

The mean annual rainfall at Lubbock is 470 mm and the mean monthly rainfall distribution is shown in Figure 11. The soil selected for the simulation analyses was Acuff fine sandy loam. Measured rainfall and simulated non-diked runoff during the sorghum growing season, and for the entire year, are shown in Table 19. Mean runoff of 21 mm were predicted for the growing season, and 29 mm annually at Lubbock. The simulated sorghum yields for non-diked (ND), diked in the growing season (DIGS), and diked all year (DAY) treatments are shown in Table 20. Mean yields of 1260 kg/ha, 1690 kg/ha and 2050 kg/ha were simulated for ND, DIGS and DAY treatments. Diking in the growing season is likely to result in an average annual yield increase of 430 kg/ha of sorghum while year round diking could increase yield by 790 kg/ha.

The runoff and crop yields that are likely under corn, are shown in Tables 21 and 22, respectively. Mean annual corn yields of 1530 kg/ha, 1800 kg/ha and 1950 kg/ha were simulated for ND, DIGS and DAY treatments. Corn yields increased by 270 kg/ha and 420 kg/ha due to diking in the growing season and diking all year, respectively. Both with sorghum and corn, as the mean yields increased due to diking, the standard deviation (s) values also increased, thereby indicating somewhat greater variability associated with the distribution of diked yields over the 25-year period. The runoff conserved and the simulated yields with cotton are shown in Table 23. Mean yields of lint cotton increased from 267 to about 275 kg/ha due to diking. Although crops are planted in May and early June in the Lubbock area, runoff can occur

from early May. Diking the land a month ahead of planting may be desirable at Lubbock. At Lubbock, RGS for sorghum, corn and cotton lint are 20.5, 15 and 0.5 kg/ha/mm, respectively. RAY values for the three crops are 27.2, 12.7 and 0.5 kg/ha/mm.

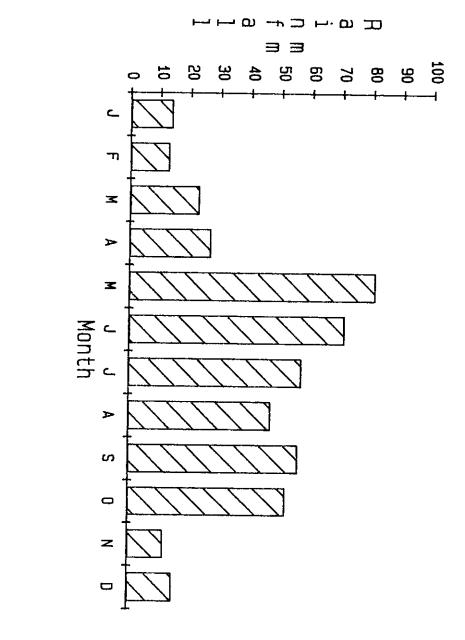


Figure 11. Mean monthly rainfall distribution at Lubbock, Texas.

Table 19. Rainfall (P) and simulated runoff (Q) under non-diked sorghum at Lubbock, Texas.

		g Season	Ann	ual
Year	P (mm)	Q /mm\	P ()	Q
	(mm)	(mm)	(mm)	(mm)
1960	301	21	562	44
1961	263	26	468	37
1962	335	0	456	0
1963	219	11	382	16
1964	264	8	361	8
1965	299	15	358	15
1966	369	46	468	53
1967	363	120	514	120
1968	227	0	479	1
1969	303	15	741	58
1970	135	2	307	50
1971	375	12	514	13
1972	396	47	632	50
1973	97	1	301	1
1974	499	45	604	45
1975	211	13	443	18
1976	284	12	499	16
1977	243	5	410	5 1 23
1978	201	0	315	1
1979	260	19	529	23
1980	193	3	403	9
1981	302	12	584	21
1982	258	6	532	22
1983	370	82	514	82
1984	220	8	369	8
x:	279	21	470	29
s:	88	28	109	29

Table 20. Simulated sorghum yields at Lubbock, Texas.

Year	ND (kg/ha)	DIGS (kg/ha)	DAY (kg/ha)
1960	840	1810	1810
1961	1030	2600	4740
1962	2110	2110	2110
1963	10	80	80
1964	530	600	600
1965	0	0	0
1966	2570	2730	3080
1967	2300	5000	5000
1968	370	390	390
1969	950	950	950
1970	850	850	870
1971	1490	1490	1490
1972	3900	5250	5250
1973	100	1290	2980
1974	1560	1560	1570
1975	4240	4840	5030
1976	1660	2050	2270
1977	2190	2180	2200
1978	<b>15</b> 0	150	150
1979	700	700	1340
1980	0	0	0
1981	2920	3460	3480
1982	560	1280	2660
1983	0	0	0
1984	500	780	3080
<del>x</del> :	1260	1690	2050
s:	1210	1570	1700

DIGS: Diked in growing season DAY: Diked all year

Table 22. Simulated corn yields at Lubbock, Texas.

YEAR	ND (kg/ha)	DIGS (kg/ha)	DAY (kg/ha)
1960	1930	2410	2410
1961	3280	3760	4280
1962	290	290	290
1963	250	280	290
1964	590	620	620
1965	1140	1140	1140
1966	1670	1760	2390
1967	2490	3890	3890
1968	730	740	740
1969	1140	1400	1400
1970	860	870	1180
1971	940	980	980
1972	5580	7760	7800
1973	30	40	40
1974	410	410	410
1975	4910	5440	5520
1976	4470	4990	4990
1977	460	460	470
1978	20	20	20
1979	1540	1570	1720
1980	110	120	130
1981	820	820	820
1982	2500	2810	3470
1983	180	180	220
1984	1960	2220	3550
<del>x</del> :	1530	1800	1950
S:	1570	1980	2060

Non-diked ND:

DIGS: Diked in growing season DAY: Diked all year

Table 21. Rainfall (P) and simulated runoff (Q) under non-diked corn at Lubbock, Texas.

		g Season	Ann	ual
Year	P	Q	, P	Q .
	(mm)	(mm)	(mm)	(mm)
1960	307	65	562	94
1961	263	28	468	45
1962	213	0	456	0
1963	129	10	382	13
1964	159	5	361	5
1965	126	0	358	15
1966	314	49	468	64
1967	363	129	514	132
1968	227	0	479	1
1969	114	9	741	50
1970	46	9 2 2	307	51
1971	243	2	514	12
1972	465	60	632	64
1973	138	2	301	2
1974	215	4	604	44
1975	211	10	443	16
1976	349	22	499	22
1977	121	2	410	4
1978	67	0	315	1
1979	173	2 0 3 2	529	1 22
1980	51	2	403	8
1981	249	12	584	30
1982	258	16	532	32
1983	69	1	514	79
1984	220	11	369	11
<del>x</del> :	204	18	470	33
s:	106	30	109	34

Table 23. Simulated runoff and the impact of diking on cotton lint yields at Lubbock, Texas.

YEAR	ND	D	IGS	D	АҮ
	YIELD (KG/HA)	RC (MM)	YIELD (KG/HA)	RC (MM)	YIELD (KG/HA)
1960	230	40	230	40	230
1961	245	20	245	20	245
1962	168	0	168	0	168
1963	234	10	234	10	234
1964	212	0	214	0	214
1965	180	10	180	10	180
1966	536	20	547	20	550
1967	255	100	259	100	259
1968	120	0	117	0	119
1969	497	20	556	20	556
1970	179	0	200	10	216
1971	205	0	205	0	213
1972	797	20	801	20	801
1973	129	0	129	0	129
1974	482	10	483	10	483
1975	222	0	222	0	222
1976	412	10	427	10	427
1977	304	0	306	0	309
1978	0	0	0	0	0
1979	248	10	248	30	248
1980	166	0	167	10	169
1981	152	10	169	10	169
1982	257	0	283	10	285
1983	129	50	129	50	129
1984	325	0	326	0	326
₹:	267	13	274	15	275
S:	168	23	173	22	172

Non-Diked ND:

DIGS: Diked in growing season DAY: Diked all year RC: Runoff conserved

## Vernon (Rolling Plains):

The mean annual rainfall at Vernon is 650 mm and the mean monthly rainfall distribution is shown in Figure 12. The simulation analyses for the Rolling Plains were conducted using the Abilene Loam soil.

Daily weather data for 25 years from Vernon were used. There is a bimodal rainfall pattern at Vernon. The long-term rainfall and runoff and the simulated sorghum yields are shown in Tables 24 and 25. Even though crops are planted in June, there may be an advantage in diking ahead of planting, to conserve pre-plant moisture. It can be seen from Table 24 that year round diking, if feasible, will allow an average of 38 mm of runoff to be stored in the soil, against only 11 mm by diking in the growing season. Mean annual sorghum yields increased from 1410 kg/ha to 1900 kg/ha (490 kg/ha increase) by diking in the growing season. Sorghum yields increased by 810 kg/ha from 1410 kg/ha to 2220 kg/ha, by maintaining dikes all year long (Table 25).

The simulation results for corn are shown in Tables 26 and 27. The average runoff that can be conserved during the growing season is 15 mm and that during the entire year is 49 mm. Mean annual corn yields are likely to increase by 570 kg/ha from 3080 kg/ha to 3650 kg/ha by diking in the growing season. Year-round diking could increase average yields by 800 kg/ha to 3880 kg/ha (Table 27).

The runoff conserved and the effect of diking on cotton lint yields are shown in Table 28. Mean annual cotton yields increase from 268 kg/ha to 279 kg/ha by diking in the growing season and to 301 kg/ha by diking all year. RGS at Vernon for sorghum is 44.5 and RAY is 21. The RGS for corn is 38 and RAY is 16. RGS and RAY for cotton are 0.58 and 1.14, respectively.

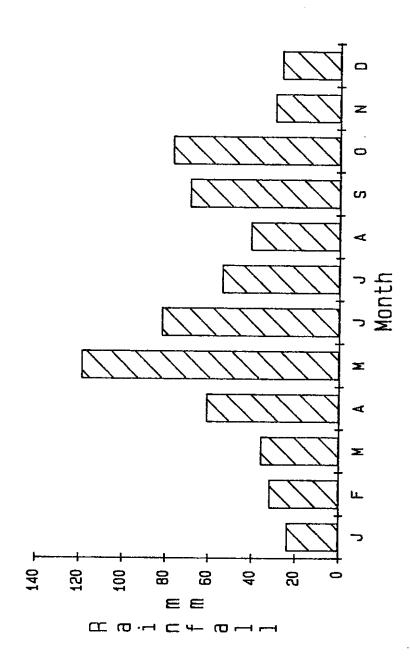


Figure 12. Mean monthly rainfall distribution at Vernon, Texas.

Table 24. Rainfall (P) and simulated runoff (Q) under non-diked sorghum at Vernon, Texas.

	Growing	Season	Annua	1
Year	Р	Q	Р	Q
	( mm )	(mm)	(mm)	(mm)
		_		
1960	109	1	680	62
1961	239	13	687	55
1962	210	16	741	34
1963	168	30	476	89
1964	333	7	600	14
1965	270	16	496	18
1966	356	20	550	20
1967	190	22	486	62
1968	206	16	726	19
1969	299	1	718	56
1970	166	0	425	3
1971	380	0 2 12	614	56 3 2 18
1972	209	12	640	18
1973	202	0	789	45
1974	309	1	636	30
1975	325	30	717	110
1976	294	0	614	6
1977	123	6	668	99
1978	252	5	509	7
1979	219	3	705	29
1980	59	0	411	7
1981	254	3	599	16
1982	111	5 3 0 3 3 74	731	43
1983	411	74	832	92
1984	110	2	466	15
<del>x</del> :	232	11	621	38
s:	92	16	117	32

Table 25. Simulated sorghum yields at Vernon, Texas.

YEAR	ND (kg/ha)	DIGS (kg/ha)	DAY (kg/ha)
1000	700	050	1.400
1960	720	950	1490
1961	2260	4490	4490
1962	190	1060	1310
1963	0	0	0
1964	70	100	100
1965	760	770	820
1966	2100	2640	2640
1967	300	580	1370
1968	1090	2310	2520
1969	2930	3190	5500
1970	260	260	260
1971	3240	3240	3240
1972	200	200	330
1973	3190	3900	3900
1974	4150	4920	5260
1975	3750	5580	5580
1976	800	810	930
1977	1790	2170	2160
1978	0	0	0
1979	4240	4440	6470
1980	0	0	0
1981	1000	1050	1050
1982	1680	1860	3090
1983	250	800	830
1984	160	2100	2250
<u>X</u> :	1410	1900	2220
s:	1430	1730	2040

ND; Non-diked
DIGS: Diked in growing season
DAY: Diked all year
RC: Runoff conserved

Table 26. Rainfall (P) and simulated runoff (Q) under non-diked corn at Vernon, Texas.

	Growing	Season	Ann	ual
Year	Р	Q	P	, Q
	(mm)	(mm)	( mm )	( mm )
1960	109	3	680	73
1961	246	25	687	67
1962	269	31	741	51
1963	139	59	476	119
1964	127	7	600	17
1965	96	0	496	19
1966	67	0	550	23
1967	106	3	486	43
1968	227	18	726	21
1969	271	14	718	71
1970	34	0	425	4
1971	195	1	614	2
1972	208	6	640	40
1973	321	33	789	80
1974	309	35	636	67
1975	373	86	717	166
1976	91	2	614	9
1977	167	12	668	104
1978	63	1	509	7
1979	219	6	705	39
1980	0		411	11
1981	149	3	599	15
1982	154	0 3 5	731	48
1983	116	27	832	109
1984	207	3	466	22
<u>x:</u>	171	15	621	49
s:	94	21	117	42

Table 27. Simulated corn yields at Vernon, Texas.

YEAR	ND (kg/ha)	DIGS (kg/ha)	DAY (kg/ha)
1000	0020	0070	2222
1960	2830	2870	2900
1961	6330	6890	6890
1962	3210	3240	3240
1963	2260	2270	2270
1964	600	660	710
1965	1450	1650	1690
1966	250	1800	1800
1967	460	2420	2930
1968	4220	5060	5480
1969	5690	6660	6690
1970	630	1460	1850
1971	1410	1410	1410
1972	4990	5360	5620
1973	6040	6540	6540
1974	2590	3740	3740
1975	6600	8200	8200
1976	1330	<b>42</b> 00	4450
1977	4220	4330	4350
1978	90	90	100
1979	7210	7230	8820
1980	550	550	1060
1981	4350	4450	5530
1982	4870	5030	5130
1983	2640	2760	2760
1984	2150	2350	2760
₹:	3080	3650	3880
s:	2230	2280	2380

Non-diked ND:

DIGS: Diked in growing season DAY: Diked all year RC: Runoff conserved

Table 28: Simulated runoff and the impact of diking on cotton lint yields at Vernon, Texas.

YEAR	ND	DIGS		DAY	
	YIELD (KG/HA)	RC (MM)	YIELD (KG/HA)	RC (MM)	YIELD (KG/HA)
1960	130	30	130	30	130
1961	204	10	207	10	210
1962	136	30	136	40	136
1963	121	70	121	70	120
1964	268	10	282	10	307
1965	0	10	0	10	0
1966	0	20	0	20	0
1967	157	10	163	50	163
1968	388	20	429	20	429
1969	539	30	550	60	575
1970	0	0	0	0	0
1971	166	0	166	0	166
1972	264	0	264	10	266
1973	381	10	405	10	405
1974	527	10	535	10	537
1975	528	90	595	90	595
1976	181	0	181	0	181
1977	219	10	219	80	219
1978	809	0	809	10	1,021
1979	447	10	453	40	453
1980	299 436	0	301	10	582
1981 1982	436 346	10	506 240	10	506
1982 1983	346 165	20 60	348 177	60 70	348 187
1983	0	10	0	10	0
<del>X</del> :	268	19	279	29	301
S:	203	23	212	28	245

Non-diked ND:

DIGS: Diked in growing season DAY: Diked all year RC: Runoff conserved

## Temple (Blackland Prairie):

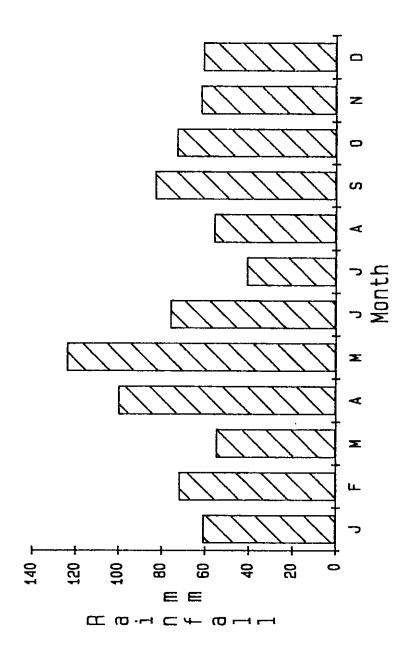
The mean annual rainfall at Temple is 860 mm and the monthly distribution is shown in Figure 13. Although the rainfall can vary from year to year, there is a 65% probability of receiving at least 750 mm annually at Temple (Tucker and Griffiths, 1965). Houston black clay was chosen as the representative soil for the simulation analyses.

The rainfall and simulated runoff under sorghum are shown in Table 29. Diking in the growing season on average could conserve 70 mm of runoff while year round diking could conserve 129 mm. The predicted sorghum yields are shown in Table 30. They range from less than 1000 to more than 8000 kg/ha. Non-diked mean yield is 5280 kg/ha, that is likely to increase by 320 kg/ha to 5600 kg/ha by diking in the growing season. DAY increases the yield only slightly to 5720 kg/ha at Temple.

The rainfall and runoff under corn (Table 31) follow a similar pattern to that of sorghum, but with somewhat higher annual runoff. The predicted corn yields (Table 32) are also in the same general range of those of sorghum. Diking in the growing season results in 180 kg/ha additional yield on the long-term, while year round diking increases yields by only 210 kg/ha. It appears from this study that corn would not be a suitable crop to grow under diked conditions in the Blacklands. A furrow-dike field experiment at Temple in 1987 with corn further corroborated the modeling results.

Runoff under cotton and predicted lint yields are shown in Table 33. DIGS increased average lint yields from 386 to 406 kg/ha, due to an additional 68 mm of runoff that could be conserved by diking. DAY made little additional difference to the simulated yields.

The RGS values for sorghum, corn and cotton at Temple are 5, 3 and 0.3 kg/ha/mm, respectively. The RAY values for the three crops are 3,



Mean monthly rainfall distribution at Temple, Texas. Figure 13.

Table 29. Rainfall (P) and simulated runoff (Q) under non-diked sorghum at Temple, Texas.

	Growin	g Season	Anr	nual
Year	Р	Q	Р	Q
<u>, , , , , , , , , , , , , , , , , , , </u>	(mm)	(mm)	(mm)	( mm )
1960	232	31	1064	218
1961	219	19	727	87
1962	302	16	769	35
1963	162	2	490	9
1964	259	30	785	44
1965	344	111	1007	220
1966	411	75	807	111
1967	285	41	820	84
1968	370	80	1057	211
1969	203	50	698	76
1970	239	51	690	80
1971	161	2	934	145
1972	211	23	649	27
1973	374	65	1056	139
1974	162	27	756	100
1975	586	192	1048	337
1976	509	176	1048	237
1977	363	142	673	196
1978	225	11	754	35
1979	624	291	1249	331
1980	310	85	660	102
1981	532	54	1169	189
1982	355	18	723	29
1983	329	132	865	142
1984	241	15	859	48
<u>x</u> :	320	70	854	129
s:	130	70	188	92

Table 30: Simulated sorghum yields at Temple, Texas.

Year	ND (kg/ha)	DIGS (kg/ha)	DAY (kg/ha)
1960	5700	5720	5720
1961	6120	6200	6200
1962	7510	8130	8230
1963	2190	2240	3700
1964	2680	4760	5010
1965	7380	7450	7450
1966	7 <b>6</b> 80	7680	7690
1967	7450	8100	8100
1968	8280	8280	8 <b>2</b> 80
1969	1270	1460	1460
1970	4560	4990	4990
1971	250	280	570
1972	5920	6900	6900
1973	6510	7060	7060
1974	2790	3170	3170
1975	7180	7180	7180
1976	6440	6490	6490
1977	6550	6720	6720
1978	5730	6300	7090
1979	7390	7390	7390
1980	1740	1760	1760
1981	8040	8040	8040
1982	8700	8730	8730
1983	3080	3340	3340
1984	760	1640	1830
<del>x</del> :	5280	5600	5720
s:	2620	2540	2450

DIGS: Diked in growing season DAY: Diked all year

Table 31. Rainfall (P) and simulated runoff (Q) under non-diked corn at Temple, Texas.

Year	P (mm)	Q (mm)	P (mm)	Q (mm)
1960	232	2	1064	210
1960	293	3 20	1064 727	219 98
1961	302	20 37	769	98
1962	229	22	769 490	32
1964	259	44	785	110
1965	344	106	1007	270
1966	411	74	807	112
1967	285	55	820	154
1968	440	81	1057	240
1969	231	57	698	84
1970	243	48	690	113
1971	161	4	934	187
1972	245	19	649	47
1973	376	66	1056	193
1974	163	22	756	139
1975	592	192	1048	334
1976	518	173	1048	270
1977	364	137	673	191
1978	225	33	75 <b>4</b>	87
1979	660	298	1249	407
1980	310	79	660	96
1981	539	103	1169	239
1982	358	18	723	31
1983	329	92	865	150
1984	241	28	859	106
<del>x</del> :	334	72	854	160
s:	130	68	188	94

Table 32. Simulated corn yields at Temple, Texas.

YEAR	ND (kg/ha)	DIGS (kg/ha)	DAY (kg/ha)
1960	3810	3880	3880
1961	6710	6800	6800
1962	7460	7630	7630
1963	4610	4650	4650
1964	5210	5610	5630
1965	6710	6760	6760
1966	7750	7830	7830
1967	7020	7370	7370
1968	7590	7620	7620
1969	2980	3090	3090
1970	5040	5350	5350
1971	1660	1730	1940
1972	4940	5440	5 <b>4</b> 40
1973	6990	7540	7540
1974	3870	4210	4210
1975	6760	6790	6790
1976	5840	5870	5870
1977 1978	4660	4680	4940
1978	4700 6750	5310	5310
1979	6750	6750	6750
1981	3180	3190	3260
1982	8700 7550	8700	8740
1983	7550 4240	8020	8170
1984	4240	4380	4380
1904	2980	3160	3160
x:	5510	5690	5720
S:	1840	1850	1830

DIGS: Diked in growing season DAY: Diked all year

Table 33. Simulated runoff and the impact of diking on cotton lint yields at Temple, Texas.

YEAR	ND	DIGS		DAY	
	YIELD (KG/HA)	RC (MM)	YIELD (KG/HA)	RC (MM)	YIELD (KG/HA)
1960	665	130	687	150	687
1961	446	50	446	90	446
1962	204	30	204	60	204
1963	216	10	224	10	227
1964	472	50	473	70	474
1965	291	90	295	170	295
1966	422	30	463	70	463
1967	281	60	314	60	314
1968	468	80	513	180	513
1969	189	0	189	40	194
1970	165	40	165	80	174
1971	713	60	759	60	759
1972	350	10	407	20	407
1973	333	90	333	120	333
1974	292	50	292	50	292
1975	813	200	817	220	818
1976	330	40	339	170	339
1977	201	20	202	150	202
1978	285	40	285	110	285
1979	675	200	725	300	725
1980	206	40	208	60	208
1981	662	190	714	210	721
1982	287	20	287	20	287
1983	422	90	507	130	507
1984	268	80	303	80	303
₹:	386	68	406	107	407
S:	187	58	199	73	199

DIGS: Diked in growing season DAY: Diked all year Runoff conserved RC:

1 and 0.2 kg/ha/mm. The low runoff conservation efficiency values indicate that the yield response to diking (kg/ha/mm of runoff) is lower at Temple than at most other locations selected for this analysis.

## Uvalde (Edwards Plateau):

The mean annual rainfall at Uvalde is 590 mm and the monthly distribution of rainfall is shown in Figure 14. Uvalde has a bimodal rainfall pattern with peaks in May and September. The soil used for the simulation study was Uvalde silt loam.

The simulated runoff amounts under sorghum are shown in Table 34. Diking all year is likely to conserve more than twice as much water as diking in the growing season alone. The predicted sorghum yields (Table 35), range from 0 to more than 8000 kg/ha. Mean annual yields increase from 2630 kg/ha for ND, to 3200 kg/ha for DIGS, and to 3710 kg/ha for the DAY treatment. Runoff under corn (Table 36) exhibits a pattern similar to that under sorghum. More than twice the amount of runoff could be conserved by diking all year as compared to diking only in the growing season. Predicted corn yields (Table 37) range from about 300 kg/ha to more than 8000 kg/ha. Mean annual corn yields increased by 430 kg/ha from 3750 kg/ha under non-diked conditions to 4180 kg/ha under diking in the growing season. Yields increased 560 kg/ha by diking all year round. The response of cotton to diking is shown in Table 38. The mean lint yield increased from 331 kg/ha to 352 kg/ha by diking in the growing season, and increased to 359 kg/ha by diking all year.

The RGS and RAY for sorghum are 29 kg/ha/mm and 25 kg/ha/mm, and for corn, 14 and 8 kg/ha/mm, respectively. RGS and RAY for cotton at Uvalde are 0.8 and 1.0, respectively.

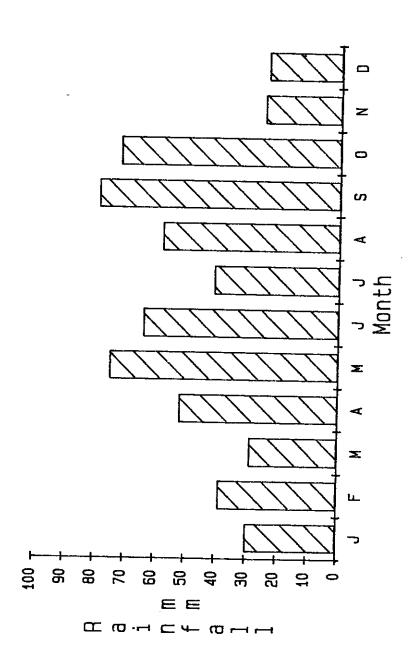


Figure 14. Mean monthly rainfall distribution at Uvalde, Texas.

Table 34. Rainfall (P) and simulated runoff (Q) under non-diked sorghum at Uvalde, Texas.

		Season	Ann	ual			
Year	P	,Q 、	P	Q			
	(mm)	(mm)	( mm )	(mm)			
1960	114	5	547	21			
1961	284	24	661	96			
1962	130	5	359	8			
1963	206	28	365	30			
1964	126	0	566	20			
1965	250	50	666	58			
1966	232	43	530	51			
1967	116	1	510	5			
1968	214	36	640	59			
1969	236	7	848	141			
1970	92	3	345	17			
1971	281	16	788	115			
1972	173	2 2	391	4			
1973	226	2	784	63			
1974	145	18	784	175			
1975	423	113	658	130			
1976	627	56	1158	199			
1977	210	51	503	57			
1978	201	24	434	27			
1979	623	167	822	169			
1980	239	18	586	70			
1981	377	57 6	662	58			
1982	202	591	27				
1983	256	6	738	52			
1984 	82	0	377	25			
x:	243	30	613	67			
s:	141	39	192	57			

Table 35. Simulated sorghum yields at Uvalde, Texas.

YEAR	ND (kg/ha)	DIGS (kg/ha)	DAY (kg/ha)
1960	120	870	3580
1961	3290	3370	3530
1962	0	0	580
1963	250	820	820
1964	670	670	670
1965	4680	6290	6990
1966	1170	27 <b>2</b> 0	3970
1967	0	0	0
1968	4130	6090	6430
1969	270	280	320
1970	970	1050	3560
1971	5740	5740	5740
1972	1250	1500	3800
1973	2610	2630	2640
1974	1100	2350	3010
1975	8170	8170	8170
1976	6040	8310	8310
1977	6620	7260	7260
1978	420	420	440
1979	5860	6650	6710
1980	3670	4230	4230
1981	6110	6700	7100
1982	1140	1710	2010
1983	1320	2070	2780
1984	90	90	130
<del>x</del> :	2630	3200	3710
s:	2570	2840	2730

ND: Non-diked DIGS: Diked in growing season DAY: Diked all year

Table 36. Rainfall (P) and simulated runoff (Q) under non-diked corn at Uvalde, Texas.

	Growing	g Season	Annua	1
Year	Р	Q	Р	Q
	( mm )	(mm)	( mm )	( mm )
1060	114	E	E 47	01
1960	114	5	547 661	21
1961	284	24 5	359	96
1962	130			8
1963	206	28	365 566	30 20
1964	126	0 50	666	58
1965	250 232		530	
1966		43 1	530 510	51 5
1967	116 214		640	59
1968		36	848	141
1969	236	7 3 16 2 2	345	17
1970	92	ر 16	788	115
1971 1972	281 173	10	391	4
1972	226	2	784	63
		18	784 784	175
1974	145		658	130
1975	423 627	113	1158	199
1976		56	503	57
1977	210 201	51	434	27
1978		24 167	822	169
1979	623	167		
1980	239	18	586	70 50
1981	377	57	662	58
1982	202	6 6	591	27 5.2
1983	256	Ö	738	52
1984	82	0	377 	25 
$\overline{x}$ :	243	30	613	67
s:	141	39	192	57

Table 37. Simulated corn yields at Uvalde, Texas.

YEAR	ND (kg/ha)	DDGS (kg/ha)	DAY (kg/ha)
1000	1070	2010	2010
1960	1970	2010	2010 5940
1961 1962	5440 2870	5660 3010	3640 3640
1962	2020	2480	3010
1963	310	350	380
1965	5660	6480	6480
1966	3920	5050	5050
1967	1620	2100	2170
1968	5450	5790	5790
1969	4760	5310	5460
1970	3770	3900	3960
1971	2770	3230	3260
1972	1380	1430	1440
1973	4030	4050	4090
1974	3530	4520	4850
1975	6490	6940	6940
1976	5670	6380	6380
1977	3530	3580	3580
1978	2630	3330	3390
1979	8480	8650	8650
1980	890	1320	1330
1981	6580	7320	7320
1982	3850	4690	4860
1983	5670	6330	7050
1984	510	550	770
<del>x</del> :	3750	4180	4310
s:	2100	2220	2220

Non-diked ND:

DIGS: Diked in growing season DAY: Diked all year

Table 38. Simulated runoff and the impact of diking on cotton lint yields at Uvalde, Texas.

YEAR	ND	D	IGS	D	AY
	YIELD (KG/HA)	RC (MM)	YIELD (KG/HA)	RC (MM)	YIELD (KG/HA)
1960	308	0	318	0	318
1961	471	30	515	30	515
1962	0	0	0	0	0
1963	229	10	238	10	238
1964	0	10	0	10	0
1965	424	0	424	10	463
1966	400	10	412	10	412
1967	0	0	0	0	0
1968	312	10	325	10	325
1969	245	90	246	90	246
1970	0	0	0	0	0
1971	864	40	941	40	941
1972	0	0	0	0	0
1973	403	20	477	20	477
1974	643	50	655	50	655
1975	649	10	664	20	664
1976	923	60	923	60	923
1977	160	10	166	10	166
1978	365	20	430	20	430
1979	424	210	424	220	424
1980	337	40	432	40	432
1981	342	0	342	20	475
1982	353	10	389	10	389
1983	417	10	482	10	483
1984	0	10	0	10	0
₹:	331	26	352	28	359
S:	258	45	271	46	273

Non-diked ND:

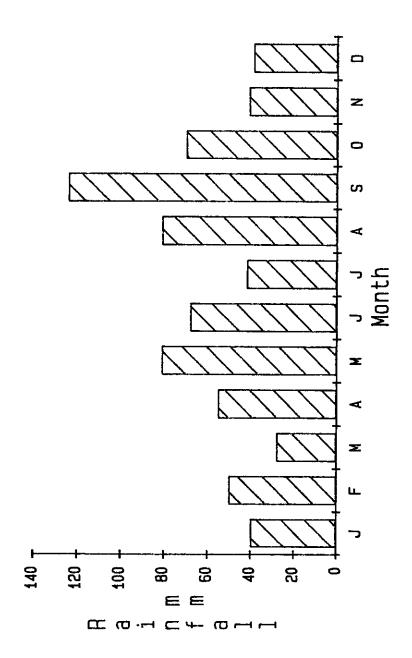
DIGS: Diked in growing season DAY: Diked all year RC: Runoff conserved

# Corpus Christi (Coastal Bend):

The mean annual rainfall at Corpus Christi is 720 mm and the mean monthly distribution of rainfall is shown in Figure 15. The Orelia sandy clay loam was used as a representative soil for the Coastal Bend region.

The simulated runoff amounts and crop yields under sorghum are shown in Tables 39 and 40, respectively. Crop yields ranged from 0 to more than 6000 kg/ha. The mean annual sorghum yield of 2610 kg/ha increased by 440 kg/ha to 3050 kg/ha by diking in the growing season. Diking all year increased the yield further to 3240 kg/ha. The simulation results with corn are shown in Tables 41 and 42. Corn yields increased by 460 kg/ha due to DIGS and by 530 kg/ha due to DAY.

Results of the simulation with cotton (Table 43) indicated that diking in the growing season could increase average annual lint yields by 14 kg/ha from 360 to 374 kg/ha. Year round diking appears to be of little further benefit for cotton at Corpus Christi. RGS for sorghum, corn and cotton lint are 10, 7 and 0.14 kg/ha/mm, respectively. The RAY values for the three crops are 4, 3 and 0.13 kg/ha/mm.



Mean monthly rainfall distribution at Corpus Christi, Texas. Figure 15.

Table 39. Rainfall (P) and simulated runoff (Q) under non-diked sorghum at Corpus Christi, Texas.

	Growin	g Season	Anr	nual
Year	Р	Q	Р	Q
	( mm )	(mm)	(mm)	(mm)
1960	283	36	1238	350
1961	125	19	585	119
1962	271	2	462	17
1963	91	1	367	3
1964	206	9	581	24
1965	184	13	696	47
1966	488	135	732	138
1967	135	1	925	300
1968	558	266	1191	413
1969	139	18	683	92
1970	234	19	686	59
1971	177	20	1111	508
1972	301	39	796	157
1973	395	44	1008	212
1974	286	71	629	82
1975	205	25	769	119
1976	298	28	1058	231
1977	209	70	562	90
1978	175	18	608	92
1979	324	62	992	246
1980	88	5	830	292
1981	367	100	1118	354
1982	367	92	1118	348
1983	155	8	561	144
1984	94	10	553	42
<u>x:</u>	246	44	794	179
s:	122	58	249	139

Table 40. Simulated sorghum yields at Corpus Christi, Texas.

YEAR	ND (kg/ha)	DIGS (kg/ha)	DAY (kg/ha)
1960	1470	1470	1470
1961	810	1430	1430
1962	0	0	0
1963	330	350	410
1964	690	1030	1090
1965	3000	3590	4870
1966	5940	6380	6380
1967	0	0	20
1968	5940	6660	6660
1969	2090	2870	2870
1970	5760	6250	6250
1971	430	1440	2550
1972	4930	6100	6240
1973	5620	6070	6300
1974	310	310	310
1975	430	1450	2460
1976	4910	6060	6060
1977	2710	3440	3440
1978	1000	1030	1080
1979	4590	5090	5090
1980	1280	1350	1530
1981	4880	5010	5010
1982	5070	5190	5190
1983	3120	3750	3750
1984	0	0	490
<del>x</del> :	2610	3050	3240
s:	2240	2410	2370

ND: Non-diked

DIGS: Diked in growing season DAY: Diked all year

Table 41. Rainfall (P) and simulated runoff (Q) under non-diked corn at Corpus Christi, Texas.

	Growin	g Season	Anr	nual					
Year	P	Q	Р	Q					
	(mm)	(mm)	(mm)						
1960	272	39	1238	391					
1961	189	31	585	133					
1962	111	0	462	30					
1963	105	16	367	40					
1964	262	55	581	85					
1965	191	44	696	100					
1966	522	183	732	191					
1967	110	4	925	313					
1968	717	335	1191	420					
1969	139	22	683	102					
1970	234	21	686	93					
1971	173	34	1111	551					
1972	325	54	796	191					
1973	395	99	1008	278					
1974	267	75	629	95					
1975	273	51	769	148					
1976	533	96	1058	261					
1977	213	82	562	105					
1978	130	24	608	119					
1979	324	78	992	283					
1980	125	12	830	343					
1981	381	128	1118	366					
1982	380	127	1118	364					
1983	162	26	561	166					
1984	90	11	553	86					
x:	265	66	794	210					
S:	156	72	249	138					

Table 42. Simulated corn yields at Corpus Christi, Texas.

YEAR	ND (kg/ha)	DIGS (kg/ha)	DAY (kg/ha)
1960	3980	4610	4670
1961	3470	3720	3720
1962	2620	2620	3710
1963	100	120	120
1964	1350	1350	1370
1965	1810	2110	2110
1966	4900	5690	5690
1967	360	380	440
1968	5030	5300	5440
1969	1440	1810	1900
1970	7470	7860	7860
1971	5170	6230	6260
1972	7220	8440	8440
1973	7350	7740	7990
1974	4650	4670	4670
1975	2050	2490	2570
1976	5660	7200	7200
1977	2070	2180	2180
1978	1550	2030	2090
1979	6270	7520	7520
1980	390	400	420
1981	7420	8200	8200
1982	7350	8190	8190
1983	1690	1910	1910
1984	220	240	320
<del>x</del> :	3660	4120	4190
S:	2590	2910	2880

ND: Non-diked
DIGS: Diked in growing season
DAY: Diked all year

Table 43. Simulated runoff and the impact of diking on cotton lint yields at Corpus Christi, Texas.

YEAR	ND	DIGS		D/	ΑY
	YIELD (KG/HA)	RC (MM)	YIELD (KG/HA)	RC (MM)	YIELD (KG/HA)
1960	475	160	509	160	514
1961	<b>24</b> 8	50	295	60	295
1962	434	0	434	0	434
1963	160	0	164	0	164
1964	176	50	177	50	177
1965	250	50	262	70	262
1966	249	80	249	130	249
1967	549	230	549	260	549
1968	410	320	428	330	<b>42</b> 8
1969	151	30	151	40	151
1970	203	40	203	40	203
1971	1,031	340	1,031	340	1,031
1972	352	60	353	100	353
1973	580	170	580	170	580
1974	189	10	210	60	210
1975	836	50	950	50	950
1976	459	120	471	130	471
1977	115	0	115	50	115
1978	158	70	158	70	<b>15</b> 8
1979	230	180	233	200	237
1980	524	150	524	150	524
1981	481	150	522	180	522
1982	404	160	449	180	449
1983	128	20	139	110	139
1984	205	20	205	50	205
₹:	360	100	374	119	375
S:	228	96	239	93	239

ND: Non-diked

DIGS: Diked in growing season DAY: Diked all year RC: Runoff conserved

## SUMMARY AND CONCLUSIONS

Results of past furrow diking research in the High Plains and Rolling Plains of Texas, have generally indicated a favorable response from diking. The increases in crop yields however varied considerably between locations, and between years at any particular location. Although positive results were obtained, they did not adequately quantify the long-term benefits from furrow diking. Besides, those results may not be transferable to other sites in Texas.

To evaluate likely long-term benefits, a runoff prediction method based on the USDA-ARS curve number methodology, was combined with three crop models for sorghum, corn and cotton. The combined models, SORDIKE, CORDIKE and COTDIKE were validated with data from several Texas sites, and modified to simulate three possible scenarios: no diking, diking in the growing season, and diking all year. The models were run with daily weather data for 25 years (1960-84), from the following five representative Texas locations: Lubbock (Southern High Plains); Vernon (Rolling Plains); Temple (Blackland Prairie); Uvalde (Edwards Plateau); and Corpus Christi (Coastal Bend). Seasonal and annual runoff amounts and crop yields were simulated for sorghum, corn and cotton under diked and non-diked conditions at each of the above locations. Even though corn is normally not grown in the High Plains and Rolling Plains of Texas, the two locations were included in CORDIKE simulations to maintain consistency. Besides, existing cropping systems can change in the future.

At Lubbock, the mean annual non-diked yields of sorghum, corn and cotton lint were 1260 kg/ha, 1530 kg/ha and 267 kg/ha. Diking in the growing season increased mean annual yields of sorghum, corn and cotton lint by 430 kg/ha, 270 kg/ha and 7 kg/ha, respectively. Diking all

year resulted in average annual yield increases of 790 kg/ha, 420 kg/ha and 8 kg/ha for the three crops.

At Vernon, average non-diked yields were 1410 kg/ha of sorghum, 3080 kg/ha of corn and 268 kg/ha of lint cotton. These yields increased by 490 kg/ha, 570 kg/ha and 11 kg/ha, respectively, for the three crops, when they were diked in the growing season. Diking all year increased sorghum, corn and cotton lint yields by an average of 810 kg/ha, 800 kg/ha and 33 kg/ha, respectively.

The average non-diked yields at Temple were 5280 kg/ha of sorghum, 5510 kg/ha of corn, and 386 kg/ha of cotton lint. Diking in the growing season increased the yields of those three crops by 320 kg/ha, 180 kg/ha and 20 kg/ha, respectively. Diking all year increases the yields 440 kg/ha, 210 kg/ha and 21 kg/ha over non-diked yields.

At Uvalde, non-diked yields of sorghum, corn and cotton lint were 2630 kg/ha, 3750 kg/ha and 331 kg/ha. Diking in the growing season increased the yields of those crops by 570 kg/ha, 430 kg/ha and 21 kg/ha. Diking all year increased sorghum yields by 1080 kg/ha, corn yields by 560 kg/ha and cotton lint yields by 28 kg/ha.

Simulation results for Corpus Christi indicated average non-diked yields of 2610 kg/ha of sorghum, 3660 kg/ha of corn and 360 kg/ha of cotton lint. Diking in the growing season increased yields of the three crops by 440 kg/ha, 460 kg/ha and 14 kg/ha, respectively. Diking all year resulted in 630 kg/ha of sorghum, 530 kg/ha of corn and 15 kg/ha of lint, over non-diked yields.

The simulated runoff amounts and crop yields were used to determine the Runoff Conservation Efficiency (RCE) for each location. Defined as the increase in crop yield per unit of runoff conserved by diking, RCE is a good measure of the relative value of furrow diking at any given location. For sorghum and corn, the highest RCE values were computed at Vernon, followed by Uvalde, Lubbock, Corpus Christi and Temple. For cotton, Uvalde had the highest RCE, followed by Vernon, Lubbock, Temple and Corpus Christi. Based on the runoff conservation efficiencies computed for the five locations, it appears that the sub-humid region between 500-800 mm annual rainfall would be the most suitable region for furrow diking (Figure 16). Moderate values of RCE were computed in the region that receives less than 500 mm mean annual rainfall, because of lower amounts of runoff generated. The impact of diking is also likely to be moderate (medium) in the region receiving more than 800 mm precipitation, because of generally higher probabilities of receiving that rainfall, resulting in presumably, fewer periods of crop water stress.

Approximately 1.3 million ha of sorghum and 0.3 million ha of corn are grown in the five regions selected for this modeling study. If those 1.6 million ha can be diked just in the growing season, an additional 450,000 tonnes of sorghum and 60,000 tonnes of corn could be produced annually. For cotton, the highest RCE and lint yield increases were computed by diking all year at Vernon and Uvalde. Even if diking is practised only in the growing season in the High Plains, Blacklands and Coastal Bend, it would be desirable to dike the land for cotton in the Rolling Plains and Edwards Plateau early in the year (January/February), to utilize the precipitation that is received ahead of planting. If this can be accomplished, an additional 24,000 tonnes of cotton lint could be produced annually. The combined value of 450,000 tonnes of sorghum, 60,000 tonnes of corn and 24,000 tonnes of lint cotton is approximately \$60 million. Furrow diking, being a low cost input (less than \$3 per ha), the technology could result in about \$50 million as net profit to farmers in the five Texas regions.

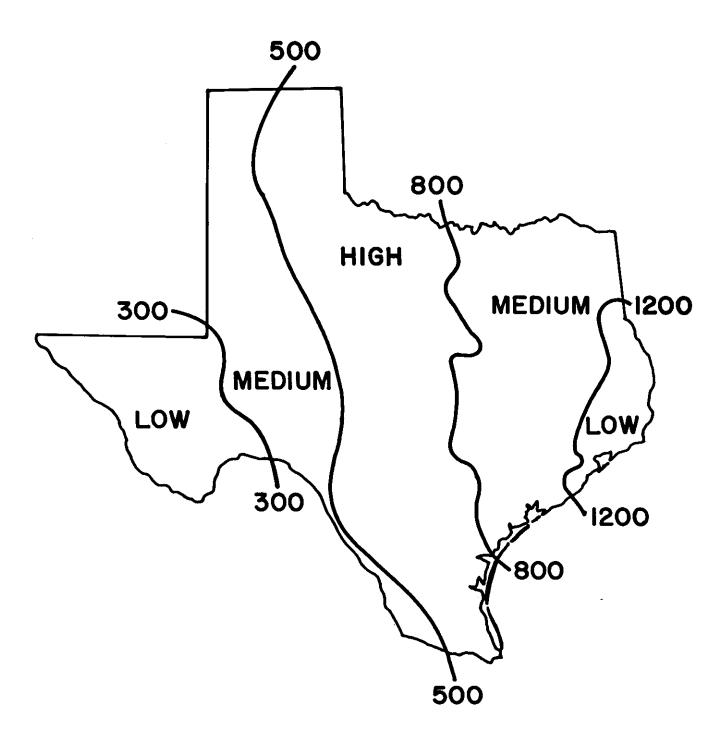


Figure 16. Relative impact of furrow diking on crop yields in Texas.

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# APPENDICES

Α.	SORDIKE	program	listing	•	•		•	•	•	•	• (	• •	•	•	•	•	•	•	•	•	•	86
В.	CORDIKE	program	listing	•	•		•	•	•	•	•		•	•	•	•	•	•	•	•	•	101
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#### PROGRAM SORDIKE

### S.O R D I K E

A FORTRAN PROGRAM COMBINING SORGE AND EPIC RUNOFF ALGORITHMS TO EVALUATE THE IMPACT OF FURROW DIKING ON SORGHUM YIELDS J. H. KRISHNA, BLACKLAND RESEARCH CENTER, TAES, 1987

```
INTEGER SUMOPT, STMO, STDAY, STYR, ENMO, ENDAY, ENYR INTEGER CHKIRR, IRR, IRRDAY, IRRIG, IRROPT, DAY INTEGER TMPMO, TMPDAY
       CHARACTER#14 SUMMRY
       CHARACTER*8 INDAT, INMET, OTDAT
CHARACTER*4 STA4
       COMMON /BLK1/ GRO(2,20), XMAX(20), PDAYS(20), SPROUT, FMRGDA,
                          DLAI (366), RCOUNT (20), ACDAYS (20), DLA, 10PT
       COMMON /BLK2/ ROSPZ, PAREA, N. IDAY3, IDAY6, IDAY9, ISTAGE, SXDIN(20),
                          SINIT, ACHU, DIFF, DIFF6
       COMMON /BLK3/ DAYPFO, LAT, TEMPMX(366), TEMPMN(366), TEMP(366), SOLRAD(366), RAIN(366), HUNITS(366), INTPAR, LITRAN COMMON /BLK4/ TEMPCO, SW, WATSCO, ED, UL, SDEPTH, WATSCO, Q, CN2, SL
       COMMON /BLK5/ WR, WL, WC, WH, WG, DRIWT, DWG, DWH, DWC, DWL, DWR, TOTWT,
                           WTLF (20)
       COMMON /BLK6/ RLE(30), RLA(30), DLE(30), DILA(30), FSHU(30), AHU(30),
                           XHU (30), DLHU (30), SHU (30), RXHU (30), RHU (30), EXHU (30),
                           TLA (30), IPL, IPL4, IPL2, IFLAG (30)
       COMMON /BSDIL/NLAYR, RTDEPM, DLAYR(20), ULAYR(20), SWLAYR(20), SMI, RTDEP1, W1, W2, S1, SSW, PWC
        COMMON /BLK7/ SUMOPT
        DIMENSION TITLE (20), ICOR(12), IRRDAY(450), IRRIG(450)
DATA ICOR/1,-1,0,0,1,1,2,3,3,4,4,5/
C
     1 FORMAT(/,1X, TYPE 1 FOR DRYLAND, 2 FOR IRRIGATED: 1, $)
     2 FORMAT(II)
     3 FORMAT (///, 1X, 'ENTER DATES IRRIGATED. ', /, 1X, 'ENTER 00/00'
       # WHEN FINISHED. 1. /)
      4 FORMAT(12, 1X, 12)
      7 FORMAT(/, 1X, DATE (mm/dd):', *)
8 FORMAT(1X, AMOUNT OF IRRIGATION (cm):', *)
     11 FORMAT (/, 31X, 'S O R D I K E', /)
     12 FORMAT (16X, A)
     13 FORMAT (/, 20%, 'J. H. KRISHNA, BLACKLAND RESEARCH CENTER')
16 FORMAT (1%, 'TYPE 1 FOR DAILY SUMMARY, 2 FOR ANNUAL SUMMARY:', $)
     18 FORMAT(I1)
     43 FORMAT (22X, A)
C
         WRITE(*, 11)
         WRITE (*, 12) 'A FORTRAN PROGRAM COMBINING SORGE AND EPIC RUNOFF'
         WRITE(*, 12) 'TO EVALUATE THE IMPACT OF DIKING ON SORGHUM YIELD'
         WRITE(#, 13)
         WRITE(*, 43) 'TEXAS AGRICULTURAL EXPERIMENT STATION'
WRITE(*, 43) '808 E. BLACKLAND ROAD, TEMPLE, TEXAS 76503'
         WRITE(*, *) " "
         WRITE(*,*) 1
         WRITE (*, 101)
    101 FORMAT(1X, TYPE LOCATION AND YEAR ( T64): 1, $)
          READ(*, 104) STA4
    104 FORMAT (1A4)
```

```
. DAT
      INDAT = 1
      OTDAT - '
                     . OUT
      INMET .
                    . MET'
      INDAT (1:3) = STA4
       INMET(1:3) = STA4
С
      OPEN(UNIT = 1, FILE = INDAT, STATUS = 'OLD')
OPEN(UNIT = 3, FILE = INMET, STATUS = 'OLD')
C
       00.77 I = 1,20
       HTLF(I) = 0.
       ACDAYS(I) = 0.
       SXDIN(1) = 0.
       RCOUNT(I) = 0.
  77 CONTINUE
       SPROUT = 0.0
       IDAYFB = 0
       SINIT = 0.
       ₩R = 8.
       WL = 8.
       WC = 0.
       WH = 8.
       WG = 0.
       TOTWT = 0.
        IDAY3 = 8
        IDAY6 = 9
        IDAY9 = 8
        READ(1,1301) TITLE
  1301 FORMAT (2004)
        WRITE (+, 16)
        READ(+, 18) SUMOPT
        IF (SUMOPT .EQ. 1) THEN
        SUMMRY = 'DAILY SUMMARY'
        ELSE
        SUMMRY = 'ANNUAL SUMMARY'
        ENDIF
  1571 FORMAT (1X, 2004, 7X, A14, //)
        READ(1, *) KI, N, ROSPZ, P, LAT, PWC, UL, SW, SDEPTH, CN2, SL, IOPT
  1302 FORMAT (214, F5. 1, F10. 0, 4F5. 2)
        WRITE(#,#)
        WRITE (+, 102)
    102 FORMAT (1X, TYPE 1 IF NON-DIKED, 2 IF DIKED ALL YEAR, "
       # 3 IF DIKED PART YEAR: 1, $)
    READ(*, 103) L
103 FORMAT(I1)
        IF (L .EQ. 1) OTDAT(1:1) = 11
        IF (L .EQ. 2) OTDAT(1:1) = '2'
        IF (L .EQ. 3) OTDAT(1:1) = '3'
        OTDAT(2:4) = STA4
        OPEN (UNIT = 2, FILE = OTDAT, STATUS = 'NEW')
        WRITE (2, 300)
    300 FORMAT(1X)
     19 FORMAT(1X, 'SORDIKE', /, 1X, 'SORGHUM FURROW-DIKING PROGRAM', //)
         WRITE (2, 19)
         WRITE(2, 1571) TITLE, SUMMRY
         IF (L .EQ. 3) THEN
         WRITE (#, 701)
    701 FORMAT(1X, TYPE DATE DIKES INSTALLED (mm/dd/yyyy): 1, 5) READ(+, 777) MD, ND, IYR
    777 FORMAT (12, 1X, 12, 1X, 14)
         STMD = MD
         STDAY = ND
         STYR = IYR
         IF (MD .EQ. 1) THEN
         IDB = ND
```

```
ヒレンと
     IDB = 30 * (MO - 1) + ICOR(MO - 1) + ND
IF (MOD(IYR,4) .EQ. 0) THEN
IF (MD .GT. 2) THEN
IDB = IDB + 1
     ENDIF
     ENDIF
     ENDIF
     WRITE (+, 702)
702 FORMAT(1X, TYPE DATE DIKES REMOVED (mm/dd/yyyy)1",$)
READ(*,777) MO, ND, IYR
ENMO = MO_
      ENDAY = ND
      ENYR = IYR
      IF (MD .EQ. 1) THEN
      IDE = ND
      ELSE
      IDE = 30 * (MO - 1) + ICOR(MO - 1) + ND
IF (MOD(IYR,4) .EQ. 0) THEN
IF (MO .GT. 2) THEN
      IDE = IDE + 1
      ENDIF
      ENDIF
      ENDIF
      ENDIF
       READ(1,1003) MO, ND. IYR
       OM = OMQMT
       TMPDAY = ND
      WRITE(*,1)
READ(*,2) IRROPT
       IF (IRROPT .EQ. 2) THEN
       IRR = 1
       WRITE(+,3)
  29 WRITE (*,7)
       READ(*,4) MG, ND
IF (MD .NE. 8) THEN
IF (MO .EQ. 1) THEN
IRRDAY(IRR) = ND
       ELSE
       IRRDAY(IRR) = 30 * (MO - 1) + ICOR(MO - 1) + ND
       IF (MDD(IYR, 4) .ED. 0) THEN
IF (MD .GT. 2) THEN
IRRDAY(IRR) = IRRDAY(IRR) + 1
       ENDIF
       ENDIF
       ENDIF
       WRITE(+,8)
READ(+,+) IRRIG(IRR)
IRR = IRR + 1
        60 TO 29
        ENDIF
        ENDIF
        MD = TMPMO
ND = TMPDAY
        WRITE(*,*) 1 3
        WRITE(*,*) 1 1
        WRITE(*,*) 'PROGRAM RUNNING, PLEASE WAIT...'
        10PT = L
PAREA = 1.E08/P
        R2 = PAREA/ROSPZ
        IPL = N-10
        IPL4 = IPL+4
IPL1 = IPL-1
        IPL2 = IPL+2
        DB 14 J = 1, N
        AHU(J) = 0.0
```

```
PLHU(J) = 6.6
    8.0 - (L)UHX
     AHU(J) = 0.0
     FSHU(J) = 0.0
     DILA(J) = 0.0
     SHU(J) = 0.0
     RHU(J) = 0.0
     RXHU(J) = 0.0
     EXHU(J) = 0.0
     TLA(J) = 0.0
     RLA(1) = 10.
     RLA(2) = 55.
     IF (J.LE.16.AND.J.GT.2) RLA(J) = 55.
     IF (J.87.16) RLA(J) = 7.96+J-70.4
     IF (J.LE.4) RLE(J) = 0.10
     IF (J.GT.4.AND.J.LE.14 ) RLE(J) = 0.28#J-1.16
     IF (J.ST.14) RLE(J) = -0.57*J+10.94
     IF (RLE(J), LT.0.10) RLE(J) = 0.10
     IF (J.LE.7) DLE(J) = 13.45 + J + 16.91
      IF (J.GT.7.AND.J.LE.IPL4) DLE(J) = 120.
         (J.GT. IPL4) DLE(J) = 11.*J+(120.-11.*IPL4)
      DLE(N) = DLE(N-1)-20.
      IF (J.LE.IPL) DILA(J) = 55.25*J+179.09
IF (J.GT.IPL) DILA(J) = 104.63*J-188.98
 14 CONTINUE
      I = 1
1570 IF (I .EQ. 2) READ(1,1003) MO, ND, IYR
      IF (MO .EQ. 1) THEN
      IDY = ND
      FLSE
      IDY = 30 + (MO - 1) + ICOR(MO - 1) + ND

IF (MOD(IYR, 4) .EQ. 0) THEN

IF (MO .GT. 2) THEN
       IDY = IDY + 1
      ENDIF
      ENDIF
      ENDIF
       60 TO (65,66), I
   65 ICDAY = IDY
       WRITE(2,1572) ICDAY, MO, ND, IYR
       I = I + 1
       60 TO 1570
   66 ISOW = IDY
       WRITE(2,1573) ISOW, MO, ND, IYR
 1003 FORMAT (314)
 1572 FORMAT (1X, 5X, 14HSTARTING DATE=, 14, 6X, 13HCALENDAR DAY=, 316)
1573 FORMAT (1X, 5X, 14HPLANTING DATE=, 14, 6X, 13HCALENDAR DAY=, 316)
       IMAX = ICDAY + KI - 1
       READ (1, 1231) NLAYR, RTDEPM
 1231 FORMAT (12,1X,F5.0)
       READ (1,1234) (DLAYR(L), ULAYR(L), SWLAYR(L), L = 1, NLAYR)
 1234 FORMAT (10F8.3)
       IF (SUMOPT .EQ. 1) WRITE(2,22) P, ROSPZ, R2, PAREA
   22 FORMAT (1X, 20HPLANTS PER HECTARE= ,F10.0/13H ROW SPACING=,F6.2/
* 15H PLANT SPACING=,F6.1/16H AREA PER PLANT=,F8.2)
       WRITE (2, *)
       IF (SUMOPT .EQ. 1) WRITE(2,2000) UL, SW
 2000 FORMAT(1X, 'SWX=', F5.2, 3H CM, 5X, 'SWA=', F5.2, 3H CM)
IF (IDPT .EQ. 1) WRITE(2, 1801)
        IF (10PT .EQ. 2) WRITE(2,1802)
        IF (IDPT .EQ. 3) WRITE(2,1805) STMD. STDAY. STYR. ENMO, ENDAY, ENYR
 1801 FORMAT(1X, 'NON-DIKED')
1802 FORMAT(1X, 'DIKED')
1805 FORMAT(1X, 'DIKED')
1805 FORMAT(1X, 'DIKED FROM: ', 12, '/', 12, '/', 14, ' TO: ', 12, '/',
       +12, 1/1, 14)
           (IRROPT .EQ. 2) THEN
```

```
WRITE (2. /800) 'IRRIGATED'
     ELSE
     WRITE (2,7000) 'DRYLAND '
     ENDIF
7000 FORMAT (1X, A9, /)
     IF (SUMOPT .EQ. 1) WRITE(2, 1001)
1001 FORMAT (6X, 'DAY', 10X, 'SW(CM)', 10X, 'PRECIP (CM)', 7X, 'RUNDFF (CM)')
     READ (3, *) (RAIN(I), TEMPMX(I), TEMPMN(I), SDLRAD(I), I = ICDAY, IMAX)
     DO 6 I = ICDAY, IMAX

AVTEMP = (TEMPMX(I) + TEMPMN(I)) / 2.0

TEMP(I) = (AVTEMP - 32.0) + 5.0 / 9.0
     RAIN(I) = RAIN(I) + 2.54
   6 CONTINUE
      IF (IRROPT .EQ. 2) THEN
      IRR = IRR - 1
5000 DD 5001 DAY = 1,366
4000 DD 4001 CHKIRR = 1, IRR
      IF (IRRDAY(CHKIRR) .EQ. DAY) THEN
RAIN(DAY) = RAIN(DAY) + IRRIG(CHKIRR)
      ENDIF
4001 CONTINUE
5001 CONTINUE
      ENDIF
      DO 5 J = 1,N
      GRO(1, J) = 0.0
      GRO(2,J) = 0.0
    5 CONTINUE
      READ(1,1250) IDAYFB
 1250 FORMAT (14)
      IF (IDAYFB.EQ.@) GO TO 1249
      CALL FDBAK (IDAYFB)
      ICDAY = IDAYFB + 1
BASET = 7.0
      GO TD 1300
 1249 CONTINUE
      FMRGDA = 8.
      SPROUT - 0.
       CALL RNF
 *5X, 'RUNOFF TO DATE: 1, F6.2, /)
       CALL RUNDEF(I)
 1305 J = I
       IF (SUMOPT .EQ. 1) WRITE(2,3000) J, SSW, RAIN(I), Q
 3000 FORMAT (6X, I3, 11X, F5. 2, 12X, F5. 2, 12X, F5. 2)
       RT = RT + RAIN(I)
       RFT = RFT + Q
       IF (SPROUT .GT. 0.) GO TO 190
       DLAI(I) = 0.
IF (I .LT. ISOW) GO TO 191
CALL EMRGNC (I)
       IF (SPROUT .EQ. 0.) GO TO 191
       RCOUNT(1) = SPROUT
       BASET = 7.0
   190 CALL HFUNC (I, BASET)
        CALL LEAF(I)
        CALL STAGE (I)
   191 CALL EVAP(I)
        CALL SOLWAT (I)
        IF (SPROUT .EQ. 0.) GD TO 200
        IF (DLA .LE. 0.) GD TO 198
        CALL PHOTO (I)
   CALL GROW (I)
198 IF (TEMPMN(I) .GT. 28.0) GO TO 199
  IF (SUMOPT .EQ. 1) WRITE (2, 1222) I
```

```
1222 FURMAL (1X,
                   "FREEZE UN DAY ", 14, " KILLED CROP")
     ISTAGE = 5
 199 CONTINUE
      IPRINT = I - IFIX(RCOUNT(1) + 0.5)
      IF(ISTAGE .EQ. 5) GO TO 1006
IF(I .NE. IDAYE) GO TO 1007
      IF (SUMOPT .EQ. 1) WRITE(2,1005) I
1005 FORMAT (1X, 30HANTHESIS OCCURS ON JULIAN DAY
                                                           , [4)
1007 IF (MOD (IPRINT, 1)) 200, 1006, 200
1006 CONTINUE
      IF (ISTAGE .EQ. 5) GO TO 201
      FMRGDA = 1.0
 200 CONTINUE
      IF (ISTAGE .EQ. 5) 60 TO 201
IF (SUMOPT .EQ. 1) WRITE(2, 1884) IDAY9
1884 FORMAT(1X, 35HPHYSIOLOGICAL MATURITY NOT REACHED. /1X,
     * 23HPREDICTED ON JULIAN DAY ,2X,14////
      GO TO 99
 201 WRITE(2,1002) I
1002 FORMAT(1X, PHYSIOLOGICAL MATURITY OCCURRED ON DAY' , 14)
YLD = WG + P / 1000.
      WRITE (2, 1008) YLD
K = I + 1
      WRITE (2, 4)
       T = 0
       FT = 0
       Q = 0
       DO 250 I = K, IMAX
       CALL RUNOFF (I)
       IF (SUMOPT .EQ. 1) WRITE(2,3000) M, SSN, RAIN(I), Q
       CALL_SOLWAT(I)
       T = T + RAIN(I)
       FT = FT + Q
  250 CONTINUE
    98 WRITE(2,+)
 IF (SUMOPT .EQ. 1) WRITE(2,3600) T, FT 3600 FORMAT(7X,'RAINFALL=',F6.2,' CM',5X,'RUNOFF=',F5.2,' CM')
       TOTR = RT + T
       TORF = RFT + FT
       WRITE(2, +)
        IF (SUMOPT .EQ. 1) WRITE(2,3700) TOTR, TORF
 3700 FORMAT (7X, 'TOTAL RAINFALL=', F6.2, 3X, 'TOTAL RUNOFF=', F5.2)
99 CLOSE (UNIT = 1)
        CLOSE (UNIT = 2)
        CLOSE (UNIT = 3)
        END
SUBROUTINE LEAF(I)
        COMMON /BLK1/ GRO (2, 20), XMAX (20), PDAYS (20), SPROUT, FMRGDA,
                        DLAI (366), RCDUNT (20), ACDAYS (20), DLA, IOPT
      2
        COMMON /BLK2/ ROSPZ, PAREA, N, IDAY3, IDAY6, IDAY9, ISTAGE, SXDIN(20),
                        SINIT, ACHU, DIFF, DIFF6
       2
        COMMON /BLK3/ DAYPFO, LAT, TEMPMX(366), TEMPMN(366), TEMP(366), SOLRAD(366), RAIN(366), HUNITS(366), INTPAR, LITRAN
        COMMON /BLK4/ TEMPCO, SW, WATSCO, EOS, EO, UL, SDEPTH, WATSC2, Q, CN2, SL COMMON /BLK6/ RLE(30), RLA(30), DLE(30), DILA(30), FSHU(30), AHU(30),
                 XHU(30), DLHU(30), SHU(30), RXHU(30), RHU(30), EXHU(30),
       3TLA (30), IPL, IPL4, IPL2, IFLAG (30)
        DHU * TEMP(1)-7.
        WSC = 1.0
        SLA = 0.0
        IF (I.LT. ISOW) GO TO 1999
```

```
IF (SPRUUI.EU.W.) BU TU 1999
    DO 2000 J = 1,N
IF (J.EQ.1) GO TO 150
    IF (IFLAG(J-1).LT.2) GO TO 1000
150 GO TO (1,2,3,4), IFLAG(J)
1 WCO = WATSCO
    IF (ISTAGE.EQ. 1) WCD = WATSC2
    AHU(J) = AHU(J) + DHU + HCO
    IF (AHU(J), LT. RLA(J)) GO TO 1900
    RHU(J) = AHU(J) - RLA(J)
    \mathsf{AHU}(\mathsf{J}+\mathsf{I}) = \mathsf{RHU}(\mathsf{J})
    IFLAG(J) = 2
    IF (J.EQ.1) 60 TO 2
IF (RHU(J).GT.DHU) RHU(J) = DHU
     RCOUNT(J) = I-RHU(J)/DHU
 2 IF (RHU(J).EQ. 0.0) 60 TO 23
     EXHU(J) = RHU(J)
     RHU(J) = 0.0
     GO TO 1000
23 \text{ EXHU}(J) = \text{EXHU}(J) + \text{DHU}
     GRD(1,J) = EXHU(J)*RLE(J)*WATSC2
     TLA(J) = GRO(1,J)
     IF(EXHU(J).LT.DLE(J)) 60 TO 1000
     IFLAG(J) = 3
     RXHU(J) = EXHU(J)-DLE(J)
     GRO(1,J) = DLE(J)*RLE(J)*WATSC2
     TLA(J) = GRO(1, J)
     ACDAYS(J) = I-RXHU(J)/DHU
    IF (RXHU(J).EQ. 0.0) GO TO 33
IF (WATSCO.LT.1.) WSC = -0.1+(SW/UL)+4.0
     RADE = -0.869+0.00284+SDLRAD(I)
     IF (RADE.LE. 0. 01) RADE = 0.01
     SHU(J) = RXHU(J)+SHU(J) *HSC/RADE
      RXHU(J) = 0.0
     60 TO 1000
 33 SHU(J) = SHU(J)+DHU+WSC
      IF (SHU(J).LT.DILA(J)) GD TO 1000
      IFLAG(J) = 4
      GRD(1, J) = 0.0
      TLA(J) = 0.0
    CONTINUE
1000 CONTINUE
      SLA * TLA(J)+SLA
      DLA = SLA
      DLAI(I) = DLA/PAREA
2000 CONTINUE
1999 CONTINUE
      RETURN
      END
SUBROUTINE HFUNC(I, BASET)
      COMMON /BLK3/ DAYPFO, LAT, TEMPMX (366), TEMPMN (366), TEMP (366),
                      SOLRAD (366), RAIN (366), HUNITS (366), INTPAR, LITRAN
      PI = 3.14159
       CMIN = (TEMPMN(I)-32.)/1.8
       CMAX = (TEMPMX(I)-32.)/1.8
       AMP = CMAX - TEMP(I)
       IF (CMIN .GE. BASET) GO TO 150
IF (CMAX .LE. BASET) GO TO 103
       ZETA = ASIN((BASET-TEMP(I)) /AMP)
       HUNITS(I) = 1./PI*(AMP*COS(ZETA) + (TEMP(I)-BASET)*(PI/2.-ZETA))
       GO TO 190
  150 HUNITS(I) = TEMP(I) - BASET
       IF (TEMP(I) .GT. 30.) HUNITS(I) = 30.-BASET
       GO TO 190
   103 HUNITS(I) = 0.
```

```
TAM FOULTHOR
      RETURN
      END
SUBROUTINE EMRGNC (I)
      INTEGER SUMOPT
      COMMON /BLK1/ GRO(2,20), XMAX(20), PDAYS(20), SPROUT, FMRGDA,
                     DLAI (366), RCOUNT (28), ACDAYS (28), DLA, 10PT
      COMMON /BLK3/ DAYPFO, LAT, TEMPMX (366), TEMPMN (366), TEMP (366),
                     SOLRAD (366), RAIN (366), HUNITS (366), INTPAR, LITRAN
      COMMON /BLK4/ TEMPCO, SW, WATSCO, EOS, EO, UL, SDEPTH, WATSC2, Q, CN2, SL
      COMMON /BLK6/ RLE(30), RLA(30), DLE(30), DILA(30), FSHU(30), AHU(30),
                     XHU(30), DLHU(30), SHU(30), RXHU(30), RHU(30), EXHU(30),
                     TLA(30), IPL, IPL4, IPL2, IFLAG(30)
      COMMON /BLK7/ SUMOPT
      DATA IGERM/0/
      DCOEF = 2.8
      SUMHU1 = 18.
       SUMHU2 = 51.
       SWLIM = 0.05
       IF (IGERM .NE. 0) GO TO 200
IF (SW/UL - SWLIM) 999, 10, 10
    10 BASET = 6.3
       DEP = 0.
       CALL HFUNC (I. BASET)
       FMRGDA = FMRGDA+HUNITS(I)
       IF (FMRGDA-SUMHU1) 999, 20, 20
    20 IGERM = 1
       BASET = 11.4
       CALL HFUNC(I, BASET)
       FMRGDA = HUNITS(I)
       RETURN
   200 CALL HFUNC (1, BASET)
       FMRGDA = FMRGDA +HUNITS(I)
       IF (FMRGDA-SUMHUS) 999,999,300 -
   300 DEP = DEP +HUNITS(I)/DCDEF
        IF (DEP-SDEPTH) 999, 400, 400
   400 FMRGDA = (DEP-SDEPTH)/(HUNITS(I)/DCOEF)
        SPROUT = I - FMRGDA
        IF (SUMOPT .EQ. 1) WRITE(2, 1001) SPROUT
   1001 FORMAT (5X, DAY LEAF 1 APPEARS = ', F7.2)
        IFLAG(1) = 2.
        RHU(1) = FMRGDA
        AHU(2) = FMRGDA
    999 RETURN
        END
  SUBROUTINE PHOTO (I)
        COMMON /BLK1/ GRD (2, 20), XMAX (20), PDAYS (20), SPROUT, FMRGDA,
                       DLAI (366), RCOUNT (20), ACDAYS (20), DLA, IOPT
       2
        COMMON /BLK2/ ROSPZ, PAREA, N. IDAY3, IDAY6, IDAY9, ISTAGE, SXDIN(20),
                       SINIT, ACHU, DIFF, DIFF6
        COMMON /BLK3/ DAYPFO, LAT, TEMPMX (366), TEMPMN (366), TEMP (366)
                       SOLRAD (366), RAIN (366), HUNITS (366), INTPAR, LITRAN
        COMMON /BLK4/ TEMPCO, SW, WATSCO, EOS, EO, UL, SDEPTH, WATSC2, O, CN2, SL
        COMMON /BLK5/ WR, WL, WC, WH, WG, DRIWT, DWG, DWH, DWC, DWL, DWR, TOTWT,
                       WTLF (20)
        REAL LITRAN, INTPAR
         IF (ISTAGE.LT. 3. AND. ISTAGE. EQ. 4) MAXS = @
         R = ROSPZ/2.54
         X1 = 0.5946*R+67.9915
         xe = 0.0026*R-.322
     200 LITRAN = X1 * EXP(X2 * DLAI(I))
         TRANLI = 70.1 + EXP(-0.612 + DLAI(I))
         IF (ISTAGE.LT. 3) GO TO 201
```

```
IF (ISTRUELEW.3) MAXS = MAXS+1
     IF (MAXS. BT. 7) MAXS = 7
IF (ISTAGE. GE. 4) LITRAN = TRANLI
     IF (ISTAGE.EQ.3) LITRAN = LITRAN-(LITRAN-TRANLI) + (MAXS/7.)
 201 IF (LITRAN.LT.5.)LITRAN # 5.
      IF (TEMP(I).LT.5.0.OR.TEMP(I).GE.45.0) TEMPCO = 0.
      IF (TEMP(I).GE.25.8.AND.TEMP(I).LE.48.8) TEMPCO = 1.
     IF (TEMP(I).GE. 5. 0. AND. TEMP(I).LE.25.) TEMPCD = .05*TEMP(I)-.25
     IF (TEMP(I).GT.40.0. AND. TEMP(I).LT.45.) TEMPCO = -.2+TEMP(I)+9.
      TOFOTO - TEMPCO+WATSCO+DAYPFO
      INTPAR = 0.50 * SOLRAD(I) * (0.95-(LITRAN/100.))
      ALPHA = 3.2
      DRIWT = 4.2E-6*(ALPHA)*(WATSCO)*(TEMPCO)*(INTPAR)*(PAREA)
      RETURN
      END
SUBROUTINE EVAP (I)
      COMMON /BLK1/ GRO(2, 20), XMAX(20), PDAYS(20), SPROUT, FMRGDA,
                     DLAI (366), RCOUNT (20), ACDAYS (20), DLA, 10PT
      COMMON /BLK3/ DAYPFO, LAT, TEMPMX (366), TEMPMN (366), TEMP (366),
                     SOLRAD (366), RAIN (366), HUNITS (366), INTPAR, LITRAN
      COMMON /BLK4/ TEMPCO, SW, WATSCO, EOS, EO, UL, SDEPTH, WATSC2, Q, CN2, SL
      DATA GAMMA/.68/
      TK = TEMP(1)+273.
      DELTA = (EXP(21.255- 5304./TK))+(5304./(TK++2))
      D = DELTA/GAMMA
      ALREDO = .24
       RO = 520+193*SIN(.0172*(I-80))
       IF(SOLRAD(I).GT.RO) SOLRAD(I) = RO
       R4 = 1.-.261#EXP(-7.77E-04#TEMP(I)##2)
       R6 = (R4-.96)*1.17E-07*TK**4*(.2+.8*(SOLRAD(I)/RO))
       H = (1.-ALBEDO) *SOLRAD(I) *R6
       HO = H/583.
       ED = 1.35*DELTA/(DELTA+GAMMA)*HO
       IF (DLAI(1) .LT. 0.5) EOS = EO
IF (DLAI(1) .LT. 0.5) GO TO 41
       HOS = HO
       EDS = (D*HOS)/(D+1.)
    41 RETURN
       END
 SUBROUTINE SOLWAT (1)
       COMMON /BLK1/ GRO(2,20),XMAX(20),PDAYS(20),SPROUT,FMRGDA,
                      DLAI (366), RCOUNT (20), ACDAYS (20), DLA, 10PT
       COMMON /BLK3/ DAYPFD, LAT, TEMPMX (366), TEMPMN (366), TEMP (366),
                      SOLRAD (366), RAIN (366), HUNITS (366), INTPAR, LITRAN
       COMMON /BLK4/ TEMPCO, SW, WATSCO, EOS, EO, UL, SDEPTH, WATSC2, Q, CN2, SL
       COMMON /BSDIL/NLAYR, RTDEPM, DLAYR (20), ULAYR (20), SWLAYR (20), SMI,
       1 RTDEP1, W1, W2, S1, SSW, PWC
        DIMENSION STOR (20), SWTR (3)
        DATA U, SUMES1, SUMES2, CONA/. 6, 2+0., 0. 35/DELT/15./
        DATA SWTR/0.30, 0.10, 0.00/
 C
        IF (I.GT.1) 60 TO 40
        T = 0.
        SMI = SWLAYR(1)/ULAYR(1)
        SML = SMI
        IF (SMI.GE. 0.9) GO TO 20
        SUMES1 = UL1
        SUMES2 = 2.5-2.78*SMI
        GO TO 40
    20 SUMES1 = 10.-5MI+10.
        SUMESE = 0.
       PRECIP = RAIN(I)
        PRECIP = PRECIP-0
        RAINSI = PRECIP
```

```
IF (SUMES). GE. U) GU (U 189
IF (RAINS). GE. SUMES)) GO TO 120
     SUMES1 - SUMES1-RAINSI
     60 TO 140
120 SUMES1 = 0.
140 SUMES1 - SUMES1+EOS
     IF (SUMES1.GT.U) GO TO 160
     ES = EOS
     GO TO 260
160 ES = EOS-0.4* (SUMES1-U)
     SUMES2 = 0.6*(SUMES1-U)
     T = (SUMES2/.35) **2
     60 TO 260
180 IF (RAINSI.LT. SUMES2) 60 TO 200
      RAINSI = RAINSI-SUMES2
      SUMES1 - U-RAINSI
      T = 8.
      IF (RAINSI. GT. U) GO TD 120
      GO TO 148
200
     T = T+1.
      ES = CONA+T++0.5-SUMES2
      IF (RAINSI. GT. 0.) GO TO 220
      IF (ES.GT.EOS) ES = EOS
      60 TO 240
220 ESX = 0.8*RAINSI
      IF (ESX.LE.ES) ESX = ES+RAINSI
      IF (ESX.GT.EOS) ESX = EOS
      ES = ESX
 240 SUMES2 * SUMES2+ES-RAINSI
      T = (SUMES2/CONA) **2.
 260 IF (ES.LT.0.) ES = 0.
IF (DLAI(1).GT.3.0) GO TO 280
      EP = 0.53*EO*DLAI(I) **0.5
      60 TO-300
 280 EP = ED-ES
 300 IF(EP.LT.0.) EP = 0.
      ET = ES+EP
      IF(EO.GE.ET) GO TO 320
      ET = EO
EP = ET-ES
      CONTINUE
 320
C
     SOIL WATER BALANCE INCLUDING RAIN AND SOIL EVAPORATION,
С
     BEGINNING WITH THE TOP SOIL LAYER.
C
       DELTSW = PRECIP-ET
       IF (DELTSH. LE. 8. 0) 60 TO 340
C
       DO 330 L = 1, NLAYR
       SWLAYR(L) = SWLAYR(L) +DELTSW/DLAYR(L)
       IF(SWLAYR(L), GT. ULAYR(L)) GO TO 325
       DELTSW = 0.0
       60 10 333
C
   325 CONTINUE
       DELTSW # (SWLAYR(L)-ULAYR(L))*DLAYR(L)
       SWLAYR(L) = ULAYR(L)
   330 CONTINUE
   333 CONTINUE
       IF (DELTSW. GE. 0. 0) GO TO 365
   340 CONTINUE
       00.360 \text{ K} = 1.3
       DO 350 L = 1.NLAYR
        DMY = ULAYR(L) +SWTR(K)
        IF(SWLAYR(L).LE.DMY) GO TO 350
```

```
DMY1 = -DELTSW/DLAYR(L)
      DMY - SWLAYR(L)-DMY
      IF (DMY.LT.DMY1) GO TO 343
      SHLAYR(L) - SHLAYR(L)-DMY1
      DELTSH - 8.0
      GG TO 365
C
  343 CONTINUE
      SWLAYR(L) = SWLAYR(L)-DMY
      DELTSW = DELTSW+DMY+DLAYR(L)
  350 CONTINUE
  360 CONTINUE
  365 CONTINUE
    CALCULATE SOIL WATER STRESS FACTOR 'SMI'
C
       RTDEP = 12.0+0.403+DLA
       IF (RTDEP.LT. RTDEP1) RTDEP = RTDEP1
       RTDEP1 - RTDEP
       IF (RTDEP.GT. RTDEPM) RTDEP = RTDEPM
       DEPTH = 0.0
       SW = 0.
       UL = 0.0001
       SMI = 0.0
       IF (I.LT. ISOW) 60 TO 500
       DO 440 L = 1, NLAYR
       DEPTH = DEPTH+DLAYR(L)
       IF (RTDEP.LE.DEPTH) GO TO 460
       UL = UL+ULAYR(L) +DLAYR(L)
       SW = SW+SWLAYR(L) +DLAYR(L)
   440 CONTINUE
       GO TO 480
   460 SW = SW+SWLAYR(L) + (RTDEP+DLAYR(L) -DEPTH)
       UL = UL+ULAYR(L) + (RTDEP+DLAYR(L) -DEPTH)
       SWUL = SW/UL
       SWI = SWLAYR(1)/ULAYR(1)
   480 IF (SWUL. GT. SWI) SMI = SW/UL
IF (SWI. GT. SWUL) SMI = SWI
       IF((SMI-SML).6T.0.10) SMI = SML+0.10
       SML = SMI
       WATSC2 = 1.0
        IF (SMI.LE. 0.5) WATSC2 = SMI/0.5
        IF (SMI.ST.0.3) WATSCO = 1.0
        IF (SMI.LE.0.3) WATSCO = SMI/0.3
        EP = EP+WATSCO
        ET = ES+EP
   500 CONTINUE
        RETURN
        END
 SUBROUTINE STAGE (I)
        COMMON /BLK1/ GRO (2, 20), XMAX (20), PDAYS (20), SPROUT, FMRGDA,
                       DLAI (366), RCOUNT (20), ACDAYS (20), DLA, 10PT
        COMMON /BLK2/ ROSPI, PAREA, N. IDAY3, IDAY6, IDAY9, ISTAGE, SXDIN(20),
                       SINIT, ACHU, DIFF, DIFF6
       2
        COMMON /BLK3/ DAYPFO, LAT, TEMPMX (366), TEMPMN (366), TEMP (366), SOLRAD (366), RAIN (366), HUNITS (366), INTPAR, LITRAN
       2
        COMMON /BLK4/ TEMPCO, SW, WATSCO, EOS, EO, UL, SDEPTH, WATSC2, Q, CN2, SL
        IF (ISTAGE.GE.4) GD TO 25
        ISTAGE = 1
        DIFF = 27.6*N+12.90
        DIFF6 = 45.84*N+289.72
        HUNT = HUNITS(I) *WATSCD
        SINIT = SINIT+HUNT*FMRGDA
```

```
1+ (51N11-01++) 199, 18, 18
 10 IF (IDAY3. GT. 0) GO TO 15
     IDAY3 = I
 15 ISTAGE = 2
     IF (ACDAYS (N). EQ. 0.) GO TO 199
     ISTAGE = 3
     IF (SINIT-DIFF6) 199, 20, 20
 20 IF (IDAY6.GT.0) GO TO 25
     IDAY6 = I
     ISTAGE = 4
 25 BASET = 1.
     CALL HEUNC (I, BASET)
     ACHU = HUNITS(I)+ACHU
     BASET = 7.
      IF (ISTAGE, EQ. 5) GO TO 199
      IF(ACHU.LT.741.)GO TO 199
      IDAY9 = I
      ISTAGE = 5
199 CONTINUE
      RETURN
      END
SUBROUTINE GROW (I)
      COMMON /BLK1/ GRO(2,20), XMAX(20), PDAYS(20), SPROUT, FMRGDA,
                    DLAI (366), RCOUNT (20), ACDAYS (20), DLA, IDPT
      COMMON /BLK2/ ROSPZ, PAREA, N, IDAY3, IDAY6, IDAY9, ISTAGE, SXDIN(20),
                    SINIT, ACHU, DIFF, DIFF6
      COMMON /ELK5/ WR, WL, WC, WH, WG, DRIWT, DWG, DWH, DWC, DWL, DWR, TOTWT,
     2
                    WTLF (28)
      DATA PL, SLW/1., 200./
      IF(DLA.LE. 0.) 60 TO 5
      IF (DRIWT.LE.0.0) 60 TO 5
      IF(I-RCOUNT(1),LT.1.)PL = 1.
      YDLA = 0.
      IF (I-RCOUNT(1) .GE. 1.) YDLA = DLAI(I-1)*PAREA
      DDLA = DLA-YDLA
      SLW = 200.
      IF (WL .GE. 0.1) SLW = YDLA/WL
      GO TO (1,2,2,4,4), ISTAGE
    1 IF (SLW. GT. 200.) SLW = 200.
      IF(SLW, LT, 160.) SLW = 160.
      PDWL = DDLA/SLW
      IF (DDLA.EG. 0.) GO TO 100
      PDWA = (-0.13*(SINIT/DIFF)+0.60)*DRIWT
      IF (PDWA.LT. PDWL. GR. PDWA. GT. PDWL) PDWA = PDWL
  100 DHL = PDWA
      DWC = DRIWT-DWL
      DWR = (-0.25*(SINIT/DIFF6)+0.50)+DRIWT
      60 TO 602
    2 IF(SLW.GT.160.) SLW = 160.
       IF(SLW.LT.140.) SLW = 140.
       POWL = DDLA/SLW
       IF (DDLA. EQ. 0.) GO TO 202
       PDWA = (-0.47*(SINIT-DIFF)/(DIFF6-DIFF)+0.50)*DRIWT
       IF (PDWA.LT.@.) PDWA = 0.
       IF (PDWA.LT. PDWL. DR. PDWA. GT. PDWL) PDWA = PDWL
       PDWL = PDWA
   202 DWL = PDWL
       DWH = 0.375*(SINIT-DIFF)/(DIFF6-DIFF)*DRIWT
       DWC = DRIWT-DWL-DWH
       DWR = (-0.25*(SINIT/DIFF6)+0.50)*DRIWT
       IF (ISTAGE.LT. 3) GO TO 602
    3 DWL = 0.
       60 TO 602
       IF (ACHU. GT. 100.) GO TO 580
       DWR = (-0.25*(ACHU/100.)+0.25)*DRIWT
```

```
DMG = (M. 9# (HCHU/1MM. )) #DKINT
      DHH = (0.375+(ACHU/100.)+0.375)+DRIWT
      DWC = DRIWT-DWH-DWG
      GO TO 599
 580 DWC = 0.1+DRIWT
      DWG = 0.9+DRIWT
      DWH = 0.
 599 DWL = 0.0
      WG = WG+DWG
 602 \text{ WH} = \text{WH} + \text{DWH}
 601 WC = WC+DWC
      IF (WC.LT.0) WC = 0
 600 WR = WR+DWR
      IF(DLA.LE. 0.) GO TO 5
      WL = B.
      DO 800 J = 1, N
      IF(GRD(1,J), LE.0.) WTLF(J) = 0.
      WTLF(J) = WTLF(J) + DWL + GRO(1, J) / DLA
  800 WL = WL+WTLF(J)
    5 TOTHT = HL+HC+HH+HG
      RETURN
      END
SUBROUTINE FDBAK (IDAYFB)
      COMMON /BLK1/ GRO(2,20), XMAX(20), PDAYS(20), SPROUT, FMRGDA,
                      DLAI (366), RCOUNT (20), ACDAYS (20), DLA, 10PT
      COMMON /BLK2/ ROSPZ, PAREA, N, IDAY3, IDAY6, IDAY9, ISTAGE, SXDIN(20),
                      SINIT, ACHU, DIFF, DIFF6
      COMMON /BLK3/ DAYPFO, LAT, TEMPMX (366), TEMPMN (366), TEMP (366), SOLRAD (366), RAIN (366), HUNITS (366), INTPAR, LITRAN
       COMMON /BLK4/ TEMPCO, SW. WATSCO, EDS, ED, UL, SDEPTH, WATSC2, Q, CN2, SL
       COMMON /BLKS/ WR, HL, WC, WH, WG, DRIWT, DWG, DWH, DWC, DWL, DWR, TOTWT.
                      WTLF (29)
       DLA = 0.
       HTGTAL = 50.
       READ (1, 2001) NLF, NEULL, IDAY3, IDAY6, IDAY9, SPROUT
 2001 FORMAT (514, F7.2)
       READ (1, 2002) (RCDUNT(J), J = 1, NLF)
 2002 FORMAT ( 8F10.2)
       IF (NFULL .EQ. 0) 60 TO 105
       READ(1,2002) (ACDAYS(J), J = 1, NFULL)
  105 CONTINUE
       READ(1,2002) (GRO(1,J), J = 1,NLF)
       DO 110 J = 1, NLF
       DLA = DLA + GRO(1, J)
       PDRYS(J) = 1.

IF (J .GT. 1) SXDIN(J) = HTOTAL
   110 SINIT = SINIT + SXDIN(J)
       DLAI(IDAYFB) = DLA /PAREA
       HUNITS (IDAYFB) = 0.
       IF (NFULL .EQ. N) GO TO 120
       IF (NLF .LT. 2) GO TO 120
       T1 = RCOUNT(NLF) - RCOUNT(NLF-1)
       T2 = IDAYF8-RCOUNT(NLF)
       HUNITS(IDAYFB) = HTDTAL = T2/T1
        IF (HUNITS(IDAYFB) .GT. HTOTAL) HUNITS(IDAYFB) = HTOTAL
        IF (NLF-NFULL) 112,112,115
   112 SXDIN(NLF+1) = HUNITS(IDAYFB)
       GO TO 120
   115 SXDIN(NFULL+1) = HUNITS(IDAYFB)
   120 CONTINUE
        FMRGDA = 1.0
        CALL STAGE (IDAYFB)
        READ(1,2002) WR, WL, WC, WH, WG
        TOTHT = WL+WC+WH+WG
        IF (WL .LE. 0.) GO TO 150
```

```
DU 130 J = 1, NL⊢
WTLF(J) = WL+GRO(1,J)/DLA
  130 CONTINUE
  150 RETURN
      END
SUBROUTINE RNF
       COMMON /BLK3/ DAYPFO, LAT, TEMPMX (366), TEMPMN (366), TEMP (366),
      SOLRAD (366), RAIN (366), HUNITS (366), INTPAR, LITRAN COMMON /BLK4/ TEMPCO, SW, WATSCO, EDS, ED, UL, SDEPTH, WATSCO, Q, CN2, SL
       COMMON /BSOIL/NLAYR, RTDEPM, DLAYR(20), ÚLAYR(20), SWLAYR(20), SMÍ,
      1RTDEP1, W1, W2, S1, SSW, PWC
       SUL = 0
       DO 100 N = 1, NLAYR
       SUL = SUL+ULAYR(N) +DLAYR(N)
 100 CONTINUE
       C = 100-CN2
       D = C+0.063
       E = 2.533-D
       F = EXP(E)
       G = C+F
       H = (20 * C) / G
       CN1 = CN2-H
       CN3 = CN2*EXP(.00673*(100-CN2))
       IF(SL.EQ. 0.05) GO TO 150
       CN2A = (CN3-CN2)*((1-2*EXP(-13.86*SL))/3)+CN2
       CNS = CNSA
       C = 100-CN2
       D = C*0.063
       E = 2.533-D
       F = EXP(E)
       6 = C+F
       H = (20 + C)/G
       GN1 = CN2-H
       CN3 = CN2*EXP(.00673*(100-CN2))
       S1 = 254*((100/CN1)-1)
       S3 = 254 # ((100/CN3) - 1)
       FC = SUL+10
       ULM = PWC+10
       P = 2.54/S1
       P1 = 1-P
       P2 = ULM/P1
       P3 = P2-ULM
       Q1 = $3/$1
       Q2 = 1-Q1
       Q3 = FC/Q2
        Q4 = Q3-FC
        Q5 = ALOG(Q4) - ALOG(P3)
        W2 = Q5/(ULM-FC)
        W1 = ALDG(Q4) + (W2*FC)
        RETURN
        END
 2222222222222222222222222222222222
        SUBROUTINE RUNOFF (I)
        COMMON /BLK1/ GRO (2, 20), XMAX (20), PDAYS (20), SPROUT, FMRBDA,
                        DLAI (366), RCOUNT (20), ACDAYS (20), DLA, IOPT
        COMMON /BLK3/ DAYPFO, LAT, TEMPMX (366), TEMPMN (366), TEMP (366),
                        SOLRAD (366), RAIN (366), HUNITS (366), INTPAR, LITRAN
        COMMON /BLK4/ TEMPCO, SW, WATSCO, EOS, EO, UL, SDEPTH, WATSCE, Q, CN2, SL
COMMON /BSOIL/NLAYR, RTDEPM, DLAYR (20), ULAYR (20), SWLAYR (20), SMI,
          RTDEP1, W1, W2, S1, SSW, PWC
        SSW = 0
        DD 100 N = 1, NLAYR
        SSW = SSW+SWLAYR(N)*DLAYR(N)
    100 CONTINUE
        SSW ≠ SSW*100
```

```
5 = 514(1-(55M/(55M+EXP(M1-(W245SM)))))

CN = 25400/(5+254)

R = RAIN(I)
        R = R*10
        X = R+10

I = 0.2+5

IF(R.LT.Z) GO TO 200

Q = (R-0.2+5) + 2/(R+0.6+5)

Q = Q/10

IF(IOPT.NE.3) GO TO 230
        IOP = IOPT
IF(I.LT.90) IOP = 1
IF(I.GE.90 .AND. I.LE.213) IOP = 2
IF(I.GT.213) IOP = 1
         IF(IOP.EO.2) O = 0
        60 TO 240
230 CONTINUE
      IF(IOPT.EQ.2) Q = 0
SSW = SSW/10
240
         CONTINUE
         60 TO 250
200 0 = 0
         CONTINUE
         SSW = SSW/10
250 RETURN
         END
```

```
PROGRAM CORDIKE
C
                              CORDIKE
C
       A FORTRAN PROGRAM COMBINING CORNE AND EPIC RUNOFF ALGORITHMS
       TO EVALUATE THE IMPACT OF FURROW DIKING ON CORN YIELDS
С
       J. H. KRISHNA, BLACKLAND RESEARCH CENTER, TAES, 1987
000
       REAL IPAR
       INTEGER SUMOPT, STMO, STDAY, STYR, ENMO, ENDAY, ENYR INTEGER CHKIRR, IRR, IRRDAY, IRRIG, IRROPT, DAY
       INTEGER TMPMO, TMPDAY
       CHARACTER#4 FMT
       CHARACTER#9 OTFIL
       CHARACTER*10 INFIL
       CHARACTER#14 SUMMRY
С
       COMMON/BLK1/ALAT, TEMPMX (500), TEMPMN (500), SOLRAD (500), RAIN (500), CMAX, CAVG, DAYLN, HUNITS (500), SUMHU, IBEGIN, IEND COMMON/BLK2/MCLASS, XMAX (30), XN, NEARIN, FTASIN, FANTH, FSILK, FBLIST,
                        IDAY1, IDAY2, IDAY3, IDAY4, IDAY5, IDAY6, IDAY7, IDAY8,
                        IDAY9, ISTAGE, FDENT, HUANTH, TASINI
       COMMON /BLK3/HTOTAL (30), FEMRGN, SPROUT, RCOUNT (30), FLEAF (30),
                        PDAY, PDAYS (30), DLA (500), DLAI (500), PAREA, SDEPTH, IDAYO
        COMMON /BLK4/EOS, EO, SWLAYR (20), SW, ULLAYR (20), UL, UL1, SUMET, SMI,
                        LAYRS, DLAYR (20), RTDEP, RTDEPM, ASOILT
        COMMON /BLK5/DRIWT, TOTWT, RSRVS, GRNWT, TOTGRN, GRNMST, KRNLS, IPAR COMMON /BSOIL/ CN2, SL, PWC, W1, W2, SSW, Q, IOPT, IDB, IDE, S1
        COMMON /BLK7/ SUMOPT
        DIMENSION ICOR(12), STOR(20), TITLE(20), FMT(20)
        DIMENSION IRRDAY(450), IRRIG(450)
        DATA ICOR/1,-1,0,0,1,1,2,3,3,4,4,5/
    Format Section
     1 FORMAT(/,1X,'TYPE 1 FOR DRYLAND, 2 FOR IRRIGATED:', $)
     2 FORMAT(I1)
     3 FORMAT(///,1X,'ENTER DATES IRRISATED.',/,1X,'ENTER 00/00'
      * WHEN FINISHED. 1, /)
     4 FORMAT(I2, 1X, 12)
7 FORMAT(I1, 1X, DATE (mm/dd) 1, $)
8 FORMAT(IX, AMOUNT OF IRRIGATION (mm) 1, $)
    11 FORMAT(/,31X,'C D R D I K E',/)
    12 FORMAT (16X, A)
    13 FORMAT(/,20X,'J. H. KRISHNA, BLACKLAND RESEARCH CENTER')
16 FORMAT(/,1X,'TYPE 1 FOR DAILY SUMMARY, 2 FOR ANNUAL SUMMARY:',$)
    18 FORMAT(I1)
    19 FORMAT(1X, 'CORDIKE', /, 1X, 'CORN FURROW-DIKING PROGRAM', //)
    43 FORMAT (22X, A)
   101 FORMAT(1H . Type in station code (1A20): 1,$)
   102 FORMAT (/, 1X, TYPE 1 IF NON-DIKED, 2 IF DIKED ALL YEAR,
      *' 3 IF DIKED PART YEAR: ', $)
   104 FORMAT (1A10)
   200 FORMAT(1X, 20A4, 7X, A14, //)
   201 FORMAT (20A4)
   300 FORMAT (/1X, 20A4//)
   505 FORMAT(//, 11H LATITUDE =, F6.2, 8H DEGREE)
570 FORMAT(314)
```

```
SEE FURMATI(//IX, 'SIAKTING DATE =", 14,6X, 'CALENDAR DAY =",316)
598 FORMAT(/IX, 'PLANTING DATE =",14,6X, 'CALENDAR DAY =",316)
 699 FDRMAT (3F6.2)
 701 FORMAT(/, 1X, 'TYPE DATE DIKES INSTALLED (mm/dd/yyyy):', $)
 702 FORMAT (/, 1X, TYPE DATE DIKES REMOVED (mm/dd/yyyy):", $)
 731 FORMAT (///, 16H SOIL DEPTH (CM), 5X, 24H INITIAL SOIL WATER (CM), 5X,
     +28H EXTRACTABLE SOIL WATER (CM)/)
 732 FORMAT(2X,F4.0,' - ',F4.0,16X,F6.1,28X,F6.1)
733 FORMAT(//,' POTENTIAL DEPTH OF ROOTZONE =',F6.0,/,' EXTRACTABLE '
+'SOIL WATER WHEN ROOTZONE IS FILLED =',F6.1,/,' INITIAL SOIL'
     *' WATER CONTENT IN ROOTZONE =', F6.1)
  777 FORMAT(I2, 1X, I2, 1X, I4)
  790 FORMAT (14H ROW SPACING = F6.1/
     *16H PLANT SPACING =, F6. 1/21H PLANTS PER HECTARE =, F7. 0/
      *17H AREA PER PLANT =, F8.2/18H PLANTING DEPTH =, F5.1/
      +, /, 1 DIKING OPTION =1, 12)
  800 FORMAT(///,1X,' DAY',20X,' SW',17X,' PRECIP',17X,' RUNOFF')
  950 FORMAT (14, 20x, F6. 2, 16x, F6. 2, 19x, F6. 2)
  975 FORMAT (47H PHYSIOLOGICAL MATURITY OCCURRED ON JULIAN DAY , 14,
      */, 1H , 'GRAIN YIELD =', F6. 0, 'KG/HA',
                                            RUNOFF TO DATE: 1
      41
          RAINFALL TO DATE: ',F6.2,'
      *.F6.2)
 1010 FORMAT (/, 36H PHYSIOLOGICAL MATURITY NOT REACHED. /1X,
 */25HPREDICTED ON JULIAN DAY , [4)
1111 FORMAT(/,1H ,28X,'TOTAL RAINFALL:',F6.2,'
                                                                 TOTAL RUNOFF: 1
      *. F6.2)
 1571 FORMAT (1X, 20A4, 7X, A14, //)
 5800 FORMAT(/, 1X, A9)
 5900 FORMAT (/, 1X, 'DIKED FROM: ', 12, '/', 12, '/', 14, ' TO: ', 12, '/',
      *12,1/1,14)
7777 FORMAT(IH, 'SOWING DATE: ', I3,' RAI
*,F6.2,' RUNDFF TO DATE: ',F6.2)
8000 FORMAT(IH, 23X,'(CM)',18X,'(CM)',20X,'(CM)')
                                                           RAINFALL TO DATE:
       WRITE(*, 11)
       WRITE(*,12) 'A FORTRAN PROGRAM COMBINING CORNE & EPIC RUNOFF'
       WRITE (*, 12) 'TO EVALUATE THE IMPACT OF DIKING ON CORN YIELD'
       WRITE (*, 13)
       WRITE (+, 43) 'TEXAS AGRICULTURAL EXPERIMENT STATION'
       WRITE(*,43) '808 E.BLACKLAND ROAD, TEMPLE, TEXAS 76503'
       WRITE(*,*)
       WRITE(*,*) * *
       WRITE(*, 101)
       READ(+, 104) INFIL
C
       DO 641 I=1,365
        SOLRAD(I)=0.
        RAIN(I)=0.0
       CONTINUE
C
    INPUT NORMAL TEMPS AND POPN.
ć
        WRITE (*, 16)
        READ(*,18) SUMOPT
IF (SUMOPT .EQ. 1) THEN
SUMMRY = 'DAILY SUMMARY'
        ELSE
        SUMMRY = 'ANNUAL SUMMARY'
        ENDIF
        WRITE(*, *) ' '
        WRITE (*, 102)
        READ (+, 18) L
        IF (L .EQ. 1) OTFIL(1:1) = '1'
```

```
if (L .EU. 2) OIFIL(1:1) = '2'
IF (L .EQ. 3) OTFIL(1:1) = '3'
OTFIL(2:2) = 'C'
  OTFIL(3:3) = INFIL(1:1)
  DTFIL(4:5) = INFIL(5:6)
OTFIL(6:9) = '.OUT'
   INFIL (7:10) = '.DAT'
  OPEN(UNIT = 1,FILE = INFIL, STATUS = 'OLD')
OPEN(UNIT = 3,FILE = OTFIL, STATUS = 'NEW')
READ(1,201) TITLE
  WRITE(3,19)
WRITE(3,1571) TITLE, SUMMRY
IF (L .EQ. 3) THEN
  WRITE(*,701)
READ(*,777) MO, ND, IYR
   STMO = MO
   STDAY = ND
STYR = IYR
   IF (MO .EQ. 1) THEN
   IDB = ND
   ELSE
   IDB = 30 * (MO - 1) + ICOR(MO - 1) + ND
IF (MOD(IYR,4) .EQ. 0) THEN
IF (MO .GT. 2) THEN
IDB = IDB + 1
   ENDIF
   ENDIF
   ENDIF
   WRITE(*, 702)
   READ(*,777) MG, ND, IYR
ENMO = MO
   ENDAY = ND
   ENYR = IYR
   IF (MO .EQ. 1) THEN IDE = ND
   ELSE
   IDE = 30 * (MD - 1) + ICOR(MO - 1) + ND
IF (MOD(IYR,4) .EQ. 0) THEN
IF (MO .GT. 2) THEN
   IDE = IDE + 1
   ENDIF
   ENDIF
   ENDIF
   ENDIF
   READ(1,*) KDAY, ROSPZ, PP, SDEPTH, ALAT, LAYRS, UL1, ASOILT
  * , XMAX(1), MCLASS
    READ(1, *) CN2, SL, PWC, IOPT
    IF (SUMOPT .EQ. 1) WRITE(3,505) ALAT
    PAREA=1.E08/PP
    R2=PAREA/ROSPZ
    READ(1,570) MD, ND, IYR
    TMPMO = MO

TMPDAY = ND
    WRITE (#, 1)
    READ(*,2) IRROPT
    IF (IRROPT .EQ. 2) THEN
    IRR = 1
    WRITE(*,3)
29 WRITE (*, 7)
    READ(*,4) MO, ND
IF (MO NE. 0) THEN
    IF (MO .EQ. 1) THEN
    IRRDAY(IRR) = ND
    ELSE
```

```
INNUMY(INN) = 30 * (MU - 1) + ICUR(MU - 1) + ND
IF (MOD(IYR, 4) .EQ. 0) THEN
IF (MO .6T. 2) THEN
     IRRDAY(IRR) = IRRDAY(IRR) + 1
     ENDIF
     ENDIF
     ENDIF
     WRITE(+, 8)
     READ(*,*) IRRIG(IRR)
     IRR = IRR + 1
     60 TO 29
     ENDIF
     ENDIF
     MO = TMPMO
     ND = TMPDAY
     WRITE(*,*) ' '
     WRITE(*,*) ' '
     WRITE(*, *) 'PROGRAM RUNNING, PLEASE WAIT...'
     IOPT = L
     1 = 1
510 IF (I .EQ. 2) READ(1,570) MO, ND, IYR IF (MO .EQ. 1) THEN
     IDY = ND
     ELSE
     IDY = 30 * (MO - 1) + ICOR(MO + 1) + ND
     IF (MOD(IYR, 4) .EQ. @) THEN IF (MO .GT. 2) THEN
     IDY = IDY + 1
     ENDIF
     ENDIF
     ENDIF
     GO TO (511,512), I
511 IBEGIN = IDY
     WRITE(3,580) IBEGIN, MO, ND, IYR
     I = I +
     60 TO 516
512 IDAY0 = IDY
WRITE(3,590) IDAY0, MD, ND, IYR
     IF (IDPT .EQ. 1) WRITE(3,5800) 'NON-DIKED' IF (IDPT .EQ. 2) WRITE(3,5800) 'DIKED'
     IF (IOPT .EQ. 3) WRITE (3,5900) STMO, STDAY, STYR, ENMO, ENDAY, ENYR
     IF (IRROPT .EQ. 2) THEN WRITE(3,5800) 'IRRIGATED'
      ELSE
     WRITE (3, 5800) 'DRYLAND '
     ENDIF
      READ(1,570) MO, ND, IYR
READ(1,570) MO, ND, IYR
      DO 700 L=1, LAYRS
      READ(1,699) DLAYR(L), SWLAYR(L), ULLAYR(L)
700 CONTINUE
      DL1=0.
      RTDEPM=0.
      SW=0.
      UL=0.
      IF (SUMOPT .EQ. 1) WRITE(3,731)
      DO 730 L=1, LAYRS
      DL2=DL1+DLAYR(L)
      SWLR=SWLAYR (L) +DLAYR (L)
      ULLR=ULLAYR (L) *DLAYR (L)
      IF (SUMOPT .EQ. 1) WRITE(3,732) DL1, DL2, SWLR, ULLR
      DL1=DL2
      RTDEPM=RTDEPM+DLAYR(L)
      SW=SW+SWLR
  UL=UL+ULLR
```

```
730 CUNTINUE
      IF (SUMOPT .EQ. 1) WRITE(3,733)RTDEPM,UL,SW
DO 750 L=1,LAYRS
      STOR(L) =ULLAYR(L) -SWLAYR(L)
 750 CONTINUE
      IEND = IBEGIN + KDAY - 1
2000 DD 2001 I = IBEGIN, IEND READ(1,*) RAIN(I), TEMPMX(I), TEMPMX(I), SOLRAD(I) RAIN(I) = RAIN(I) * 25.4
      TEMPMX(I) = (TEMPMX(I) - 32) * 5 / 9

TEMPMN(I) = (TEMPMN(I) - 32) * 5 / 9
2001 CONTINUE
      IF (IRROPT .EQ. 2) THEN
      IRR = IRR - 1
5000 DO 5001 DAY = 1,366
4000 DO 4001 CHKIRR = 1,1RR
      IF (IRRDAY (CHKIRR) . EQ. DAY) THEN
      RAIN(DAY) = RAIN(DAY) + IRRIG(CHKIRR)
      ENDIF
4001 CONTINUE
5001 CONTINUE
      ENDIF
      DO 753 L=1,LAYRS
      SWLAYR(L) =ULLAYR(L) -STOR(L)
753
      CONTINUE
      DO 780 J=1,30
IF(J.EQ.1) GO TO 754
      XMAX(J)=0.
754 FLEAF (J) =0.
      PDAYS(J) =0.
      RCOUNT(J)=0.
780
      CONTINUE
       TRAIN=0.
       TRUN=0.
      SUMHU-0.
       RTDEP=0.
      SPROUT-0.
       FEMRGN=0.
       FTASIN=0.
       FANTH=0.
       FSILK=0.
       FBLIST=0.
       FDENT=0.
       IPAR=0.
       TOTWT=0.
       DRIWT-0.
       RSRVS=0.
       GRNWT=8.
       GRNMST=Ø.
       TOTGRN=0.
       ISTAGE=-1
       IDAY1=0
       IDAY2=0
       IDAY3=0
       IDAY4=0
       IDAY5≖0
       IDAY6=8
       IDAY7=0
       IDAY8=0
       IDAY9=0
       WRITE (3, 790) ROSPZ, R2, PP, PAREA, SDEPTH, IDPT
       IF (SUMOPT .EQ. 1) THEN
       WRITE (3, 800)
       WRITE (3, 8000)
```

```
FULLE
      WRITE(3, +)
C
      CALL RNF
С
      DO 1000 I = IBEGIN, 365 IF (I .EQ. IDAY0) THEN
      WRITE (3,7777) I, TRAIN, TRUN
      END 1F
       I1 = I
       CALL RUNOFF(I)
       IF(I1 .6T. 365) I1 = I1 - 365
       DECDAY = I1 + 100
       DECLIN = SIN((DECDAY*360./365.)/180.*3.141593)*(-23.47)
       SUNRIS = 12. -ACOS(-TAN(ALAT/180. *3.141593) *TAN(DECLIN/180. *
      $3.141593))/0.2618
       DAYLN=2. + (12. -SUNRIS)
       CALL HFUNC(I)
       IF (SPROUT.GT.@.) GO TO 910
       DLA(I)=0.
       DLAI (I)=0.
       IF(I .LT. IDAY@) 60 TD 930
       CALL EMRGNC(I)
       IF(SPROUT .EQ. 0.0) GD TD 920
  910 CALL LEAF(I)
  920 CALL STAGE(I)
  930 CALL EVAP(I)
       CALL SOLWAT(I)
       IF (SPROUT .EQ. 0.0) GO TO 940
       CALL PHOTO(I)
       IF(IDAY3 .EQ. 0) GD TO 940
       CALL EAR(I)
   940 IPRINT = 11 - IDAY0 + 1
       RAINT = RAIN(I) / 10
       TRAIN = TRAIN + RAINT
       TRUN = TRUN + Q
       IF (SUMOPT ,EQ. 1) WRITE(3,950) II, SSW, RAINT, Q
       IF (SPROUT .EQ. 0.0) GO TO 999
   IF(I .NE. IDAY5) GO TO 971
971 IF(I .NE. IDAY9) GO TO 980
        YLD=TOTGRN+1.18*PP/1000.
       WRITE (3, 975) I, YLD, TRAIN, TRUN
   980 PDAY=1.0
   999 CONTINUE
  1000 CONTINUE
        IF (I.GT. IDAY9) GO TO 1050
        IF (SUMOPT .EQ. 1) WRITE(3,1010) IDRY9
  1050 CONTINUE
        WRITE(3,1111) TRAIN, TRUN
        TYLD = TOTHT * PP / 1000.0
        WTKRNL = TOTGRN / KRNLS
        CLOSE (UNIT = 1)
CLOSE (UNIT = 3)
        STOP
        END
 SUBROUTINE HFUNC(I)
        COMMON/BLK1/ALAT, TEMPMX (500), TEMPMN (500), SOLRAD (500), RAIN (500),
        CMAX, CAVG, DAYLN, HUNITS (500), SUMHU, IBEGIN, IEND COMMON/BLK2/MCLASS, XMAX (30), XN, NEARIN, FTASIN, FANTH, FSILK, FBLIST,
                       IDAY1, IDAY2, IDAY3, IDAY4, IDAY5, IDAY6, IDAY7, IDAY8,
        IDAY9, ISTAGE, FDENT, HUANTH, TASINI
COMMON /BLK3/HTOTAL (30), FEMRGN, SPROUT, RCOUNT (30), FLEAF (30),
                       PDAY, PDAYS (30), DLA (500), DLAI (500), PAREA, SDEPTH, IDAY0
       2
        COMMON /BLK4/EOS, EO, SWLAYR (20), SW, ULLAYR (20), UL, UL1, SUMET, SMI,
                       LAYRS, DLAYR (20), RTDEP, RTDEPM, ASDILT
```

```
P1=3. 14159
      IF (I.GT. IBEGIN) GO TO 5
     SMI=SWLAYR(1)/ULLAYR(1)
     CUTOFT=30.
5
      IF (SPROUT. NE. 0.) GO TO 10
      BASET=8.7
      60 TO 20
      BASET-10.
10
      CMIN=TEMPMN(I)
20
      CMAX=TEMPMX(I)
      CAVG=(CMIN+CMAX)/2.
      AMP=CMAX-CAVG
      IF (AMP .LE. .01) AMP = .01
      CMOXI=CMOX
      IF(CMAXI.GE.CUTOFT) CMAXI=CUTOFT
      IF (CMIN.GE. BASET) GO TO 100
      IF (CMAXI.LE. BASET) GO TO 200
      ZETA=ASIN((BASET-CAVG)/AMP)
      HUNITS(I)=1./PI*(AMP*COS(ZETA)+(CAVG-BASET)*(PI/2.-ZETA))
      GO TO 300
      HUNITS(I) = (CMAX+CMIN) /2. -BASET
120
      GO TO 300
200
      HUNITS(I)=0.
      HUDAYL=1.-(13.-DAYLN)*0.10
300
      HURED=1.0
      IF(SOLRAD(I).LT.200..AND.SMI.GT.0.8) HURED=SOLRAD(I)/200.
      IF (ISTAGE.GT.2) HURED=1.0
      HUNITS(I)=HUNITS(I)*HUDAYL*HURED
      IF(I.LT.IDAY0) SO TO 400
      SUMHU=SUMHU+HUNITS(I)
 400
      RETURN
      END
SUBROUTINE EMRGNC(I)
      COMMON/BLK1/ALAT, TEMPMX (500), TEMPMN (500), SOLRAD (500), RAIN (500),
                     CMAX, CAVG, DAYLN, HUNITS (500), SUMHU, IBEGIN, IEND
      COMMON /BLK3/HTOTAL (30), FEMRGN, SPROUT, RCOUNT (30), FLEAF (30),
      PDAY, PDAYS (30), DLA (500), DLAI (500), PAREA, SDEPTH, IDAYO COMMON /BLK4/EOS, EO, SWLAYR (20), SW, ULLAYR (20), UL, UL1, SUMET, SMI, LAYRS, DLAYR (20), RTDEP, RTDEPM, ASOILT
       COMMON /BLK7/ SUMOPT
C
       RTDEP=RTDEP+HUNITS(I)/7.0
       IF (I.EQ. IDAYØ) RTDEP#SDEPTH
       SW=SWLAYR(1) *RTDEP
       UL=ULLAYR(1) *RTDEP
       IF(SW/UL.LT.0.2) RTDEP=SDEPTH
       IF (SW/UL.LT. 0.2) 60 TO 900
       SOILHU=75.
       TEMRGN=ASCILT#SOILHU
       FEMRGN=FEMRGN+HUNITS(I)
       IF (FEMRGN-TEMRGN) 900, 200, 200
       PDAY= (FEMRGN-TEMRGN) /HUNITS (I)
 200
       SPROUT=I-PDAY
 900
       RETURN
       END
SUBROUTINE LEAF(I)
       COMMON/BLK1/ALAT, TEMPMX (500), TEMPMN (500), SOLRAD (500), RAIN (500),
      2
                     CMAX, CAVG, DAYLN, HUNITS (500), SUMHU, IBEGIN, IEND
       COMMON/BLK2/MCLASS, XMAX (30), XN, NEARIN, FTASIN, FANTH, FSILK, FBLIST,
                      IDAY1, IDAY2, IDAY3, IDAY4, IDAY5, IDAY6, IDAY7, IDAY8, IDAY9, ISTAGE, FDENT, HUANTH, TASINI
       COMMON /BLK3/HTOTAL (30), FEMRGN, SPROUT, RCOUNT (30), FLEAF (30),
                      PDAY, PDAYS (30), DLA (500), DLAI (500), PAREA, SDEPTH, IDAYO
       COMMON /BLK4/EOS, EO, SWLAYR(20), SW, ULLAYR(20), UL, UL1, SUMET, SMI,
```

```
LAYKS, DLAYK (20), KIDEP, KIDEPM, ASUIL (
     IF (ISTAGE. GE. 5) 60 TO 500
     IF (I.LE.SPROUT+1.) CALL STAGE (I)
     N=XN+0.5
     NMAX=0.46+XN+4.03
     NTHREE=NEARIN+2
     DO 100 J=1,N
     I1=I
     IF(I1-1.EQ.IFIX(RCOUNT(J))) GO TO 45
     IF(FLOAT(I1-1).LT.RCOUNT(J)) GO TO 200
     IF(RCOUNT(J).NE.0.) GO TO 100
IF(J.GT.NEARIN) GO TO 20
     IF(J.GE.3) 60 TO 10
     HTOTAL (J) =22. *J-7.
     60 TO 30
     HTOTAL(J)=58.
10
     60 TO 30
     HTOTAL (J) =HTOTAL (J-1) -38. /(N-NEARIN)
20
     FLEAF (J) =FLEAF (J) +PDAY*HUNITS(I)
30
     IF (FLEAF (J) -HTOTAL (J)) 35, 40, 40
35
     I = I + 1
     IF(I-1.GT.SPROUT) PDAY=1.0
     CALL HFUNC(I)
     SUMHU=SUMHU-HUNITS(I)
     GO TO 30
      PDAYS(J) = (FLEAF(J) - HTOTAL(J)) / HUNITS(I)
      RCOUNT(J)=I-PDAYS(J)
     FLEAF (J+1) =FLEAF (J) -HTDTAL (J)
      IF (FLOAT (I1), LT. RCOUNT (J)) GO TO 200
      CONTINUE
46
      IF (J. EQ. NEARIN) IDAY3=I
      IF(J+1.NE.N) GD TD 200
      PDAY=0.
100 CONTINUE
200
      I=I1
      IF(DLAI(I-2).LT. 0.8. AND. DLAI(I-1).GE. 0.8) GO TO 202
      IF(DLAI(I-1).GE.0.8) GO TO 204
      DLARED=1.
      GO TO 204
202 DLARED= 2.5063-0.1613*ALDG(1.E08/PAREA)
IF(DLARED.GT.1.) DLARED=1.0
      XMAX(J) = XMAX(J) + DLARED
      XMAX (J+1) =0.
      XMAX (J+2) =0.
      XMAX (J+3) =0.
 204 DO 300 J=2,N
      IF (XMAX(J).NE.0.) GD TD 300
      IF(J.LE.3) GO TO 205
      IF (RCDUNT (J-3).EQ. 0.) GD TO 301
       IF(J.EQ.N) 60 TO 220
       IF(J.GT.NMAX) GO TO 215
       IF (J. GT. NTHREE) GO TO 210
       IF (J. GT. 4) GO TO 206
 205 XMAX(J)=1.63+XMAX(J-1)+XMAX(1)
       GO TO 300
     XMAX(J)=1.13+XMAX(J-1)+66.5+DLARED
 206
       GO TO 300
 210 IF(N.GE.23) GO TO 213
IF(N.GE.17) GO TO 212
IF(N.GE.14) GO TO 211
       XMAX(J) = 0.60 + XMAX(J-1) + 320. + DLARED
       60 TO 300
 211 XMAX(J)=0.65*XMAX(J-1)+330.*DLARED
       GD TO 300
 212 XMAX (J) =0.70 + XMAX (J-1) +340. +DLARED
       GO TO 300
```

```
213 XMAX(J)=6./5*XMAX(J-1)+356.*DLARED
GO TO 300
215 IF(XMAX(J-1).LE.870.*DLARED.AND.XMAX(NMAX).GE.870.*DLARED)GOTO 217
     XMAX(J) = XMAX(J-1) - 80. *DLARED
     60 TO 300
     XMAX(J)=1.21*XMAX(J-1)-263.*DLARED
217
     60 TO 300
220
     XMAX(J) = 0.44 * XMAX(J-1) - 26. * DLARED
300 CONTINUE
301 DO 400 J=1, N
IF(J.GT.NEARIN) GO TO 330
     IF(I.LE.SPROUT+PDAY+0.1) SUMLA=0.
      IF (J.ST. 1) GO TO 320
     DELTLA=XMAX (J)+0.7*XMAX (J+1)+0.3*XMAX (J+2)
     GO TO 350
320
     DELTLA=0.3*XMAX(J)+0.4*XMAX(J+1)+0.3*XMAX(J+2)
     60 TO 350
     IF(J.GT.NEARIN+1) GO TO 340
330
      DELTLA=0.3*XMAX(J)+0.45*XMAX(J+1)+0.5*XMAX(J+2)+0.25*XMAX(J+3)
      60 TO 350
     DELTLA=0.25*XMAX(J)+0.25*XMAX(J+1)+0.25*XMAX(J+2)+0.25*XMAX(J+3)
340
350
     IF (RCDUNT (J+1).EQ. 0.) GO TO 405
400
     CONTINUE
405
      IF(J.EQ.1) I2=SPROUT
      IF (J.GT.1) I2=RCDUNT (J-1)+PDAYS(J-1)+0.1
      I3=RCOUNT(J)+PDAYS(J)+0.1
      IF(13.EQ.12) 13=12+1
      RATELA=DELTLA/(I3-I2)
      SUMLA=SUMLA+RATELA
      IF (IDAY2. NE. 0) 60 TO 500
      K=1
      M1=0
      M2=0
      SF=0.
      CORR=0.
      60 TO 545
500
      IF (K.EQ.N) 60 TO 600
      K=K+1
      SUMWAT = SUMWAT + WATCO (SMI, . 40, 0.)
      TIME=TIME+1.
      AVWAT=SUMWAT/TIME
      IF(IDAY7.EQ.0) GO TO 520
      IF (AVWAT.LT. 0.95) M1=M1+1
      IF(IDAY8.EQ.0) GO TO 520
      IF(ISTAGE.EQ.8) SF=70.
      IF (ISTAGE. EQ. 9) SF=120.
      M2=M2+1
      SENES=TASINI+K*120.-M1*20.-M2*SF-155.+CORR
520
530
      IF (SUMHU-SENES) 550,540,540
      SUMLA=SUMLA-XMAX(K)
      IF (ISTAGE.EQ. 7) K1=K
      IF(IDAY8.EQ.0) GO TO 545
IF(K.GT.K1+1) GO TO 545
      SENES1 = SENES
       IF(SUMHU-HUNITS(I).GT.SENES1) CORR=SUMHU-HUNITS(I)-SENES1
      TIME=0.
 545
      SUMWAT=0.
      GD TO 600
      K=K-1
 550
       IF (AVWAT. LT. 0. 95. AND. IDAY7. NE. 0) M1=M1-1
       IF (IDAY8.NE. 0) M2=M2-1
 600
      IF (K.EQ.N) SUMLA=0.
       DLA(I)=SUMLA
       IF(DLA(I),LT,\emptyset,) DLA(I)=\emptyset.
       DLAI(I)=DLA(I)/PAREA
       RETURN
```

```
END
SUBROUTINE STAGE (I)
      COMMON/BLK1/ALAT, TEMPMX (500), TEMPMN (500), SOLRAD (500), RAIN (500),
     2
                    CMAX, CAVG, DAYLN, HUNITS (500), SUMHU, IBEGIN, IEND
      COMMON/BLK2/MCLASS, XMAX (30), XN, NEARIN, FTASIN, FANTH, FSILK, FBLIST,
     2
                    IDAY1, IDAY2, IDAY3, IDAY4, IDAY5, IDAY6, IDAY7, IDAY8,
                    IDAY9, ISTAGE, FDENT, HUANTH, TASINI
     3
      COMMON /BLK3/HTOTAL (30), FEMRGN, SPROUT, RCOUNT (30), FLEAF (30),
     2
                    PDAY, PDAYS (30), DLA (500), DLAI (500), PAREA, SDEPTH, IDAY0
      REAL NTASIN
      IF(I-1.EQ.SPROUT) GO TO 2
      IF (SPROUT. NE. 0.) GO TO 1
       ISTAGE=0
      GO TO 903
      GO TO (2, 100, 150, 200, 300, 400, 500, 600, 801), ISTAGE
       ISTAGE=1
       IF(I-1.GT.SPROUT) GO TO 3
       SDAYLN=0.
      FTASIN=0.
       SDAYLN=SDAYLN+DAYLN
       ADAYLN=SDAYLN/(I-IFIX(SPROUT))
       IF (ADAYLN.GT. 12.5) GO TO 6
       IF (MCLASS.GE. 7) GO TO 4
       XN=MCLASS+9.
       GO TO 40
       XN=2. *MCLASS+3.
       GO TO 40
      GO TO (10, 10, 10, 10, 10, 10, 20, 25, 30), MCLASS
 6
       A1=0.24*MCLASS+0.47
       A0=-2.0*MCLASS+3.12
       XN=A1+ADAYLN+A0
       60 TO 40
       XN=2.14*ADAYLN-9.75
 20
       60 TO 40
 25
       XN=2.5*ADAYLN-12.25
       GO TO 40
       XN=2.98*ADAYLN-16.25
 30
  40
       NTASIN=0.584*XN-4.4
       IF (NTASIN.GE. 2.) GO TO 42
       IF (NTASIN. GE. 1.) GO TO 41
       NTASIN=1.
       TASINI=15. *NTASIN
  41
       GO TO 50
       TASINI=45. + (NTASIN-2.) +58.
       FTASIN=FTASIN+PDAY*HUNITS(I)
  50
       IF (FTASIN-TASINI) 101, 60, 60
  603
       CONTINUE
       IDAY2=I
  100
       ISTAGE=2
       N=XN+0.5
  101
       NEARIN=0.45*XN+0.5
       NFIVE=0.8*XN+0.5
       IF (I.GE. IDAY3. AND. IDAY3. NE. 0) ISTAGE=3
       IF(RCOUNT(NFIVE).EQ. 0.) GO TO 903
       IDAY4=IFIX(RCOUNT(NFIVE))+1
       IF (1.LT. IDAY4) GD TO 903
       ISTAGE=4
       IF (I.LE. RCOUNT (N). DR. RCOUNT (N). EQ. 0.) GO TO 903
       IDAY5 =IFIX(RCOUNT(N))+1
       HUANTH=SUMHU
  300
       ISTAGE=5
       FSILK=FSILK+PDAY*HUNITS(I)
       TSILK=5. *10000. /PAREA
       IF (FSILK-TSILK) 900, 310, 310
  310 PDAY=(FSILK-TSILK)/HUNITS(I)
```

```
TOHAPET
400
     ISTAGE=6
     TBL IST=0. 22* (HUANTH-85.)
     FBLIST=FBLIST+PDAY*HUNITS(I)
     IF (FBLIST-TBLIST) 900, 410, 410
     PDAY=(FBLIST-TBLIST)/HUNITS(1)
410
      IDAY7=I
500
     ISTAGE=7
      TDENT=0.53*(HUANTH-85.)-TSILK
     FDENT=FDENT+PDAY*HUNITS(I)
      IF (FDENT-TDENT) 505, 510, 510
505
      IF (I-IDAY5.LT.60) GO TO 900
      IDAY8=I
510
      ISTAGE=8
600
      HUPM=2. *HUANTH-85.
      IF (SUMHU-HUPM) 700, 800, 800
      IF (I.LT. IEND) 60 TO 900
700
      IDAY9=I+(HUPM-SUMHU)/HUNITS(I)
      IF(IDAY9-IDAY5.GT.65) IDAY9=IDAY5+65
      GO TO 900
      IDAY9=I
800
      ISTAGE=9
801
900
      PDAY=1.
      RETURN
903
      END
SUBROUTINE EVAP(1)
      COMMON/BLK1/ALAT, TEMPMX (500), TEMPMN (500), SDLRAD (500), RAIN (500),
      CMAX, CAVG, DAYLN, HUNITS (500), SUMHU, IBEGIN, IEND
COMMON /BLK3/HTOTAL (30), FEMRGN, SPROUT, RCOUNT (30), FLEAF (30),
                     PDAY, PDAYS (30), DLA (500), DLAI (500), PAREA, SDEPTH, IDAY&
     2
      COMMON /BLK4/EDS, ED, SWLAYR(20), SW, ULLAYR(20), UL, UL1, SUMET, SMI, LAYRS, DLAYR(20), RTDEP, RTDEPM, ASOILT
     2
      DATA GAMMA/.68/
      TK=CAVG + 273.
      DELTA=(EXP(21.255-5304./TK))+(5304./(TK++2))
      D=DELTA/GAMMA
      ALBEDO=, 3367-, 1867*EXP(-,6*DLAI(I))
       RO=520+193*SIN(.0172*(I-80))
       IF(SOLRAD(I).6T.RO) SOLRAD(I)=RO
       R4=1.-.261#EXP(-7.77E-04#CAVG*#2)
       R6=(R4-.96)*1.17E-07*TK**4*(.2+.8*(SDLRAD(I)/RO))
       H=(1.-ALBEDO)*SOLRAD(I)*R6
       HO=H/583.
       EO=1.35*D/(D+1.)*HO
       IF(DLAI(I).LT.0.5) EOS=EO
       IF(DLAI(1).LT.0.5) GO TO 41
       HOS=HO*EXP(-0.398*DLAI(I))
       EOS=D/(D+1.)*HOS
       RETURN
  41
       END
SUBROUTINE SOLWAT(I)
       COMMON/BLK1/ALAT, TEMPMX (500), TEMPMN (500), SDLRAD (500), RAIN (500),
                      CMAX, CAVG, DAYLN, HUNITS (500), SUMHU, IBEGIN, IEND
       COMMON/BLK2/MCLASS, XMAX (30), XN, NEARIN, FTASIN, FANTH, FSILK, FBLIST,
                      IDAY1, IDAY2, IDAY3, IDAY4, IDAY5, IDAY6, IDAY7, IDAY8,
      2
                      IDAY9, ISTAGE, FDENT, HUANTH, TASINI
       COMMON /BLK3/HTDTAL(30), FEMRGN, SPROUT, RCOUNT(30), FLEAF(30),
                      PDAY, PDAYS (30), DLA (500), DLAI (500), PAREA, SDEPTH, IDAY0
      ε
       COMMON /BLK4/EDS, EO, SWLAYR (20), SW, DLLAYR (20), UL, UL1, SUMET, SMI,
                      LAYRS, DLAYR (20), RTDEP, RTDEPM, ASDILT
       COMMON /BSDIL/ CN2, SL, PWC, W1, W2, SSW, Q, IOPT, IDB, IDE, S1
        DIMENSION STOR (20)
        DATA DELT, CF/15., 2.54/
IF(I.GT. IBEGIN) 60 TO 110
```

```
1=0.
      SMI=SWLAYR(1)/ULLAYR(1)
      IF(SMI-0.9) 101,102,102
      SUMES1=UL1
      SUMES2=2.5-2.78*SMI
      60 TO 110
 102
      SUMES1=10. -SMI +10.
      SUMES2=0.
      RAINSI = RAIN(I) / 10
 110
       IF (RAINSI.LE.2.5) Q=0.
C
C
       IF (RAINSI.LE. 2.5) GO TO 111
       STORE *0.
Ċ
       DO 113 L=1, LAYRS
       STOR(L) = (ULLAYR(L) -SWLAYR(L)) *DLAYR(L)
C
       STORE=STORE+STOR(L)
C
 113 CONTINUE
       Q=(ABS(RAINSI-0.2*STORE))**2./(RAINSI+0.8*STORE)
C
      RAINEF=RAINSI-Q
 111
      IF(SUMES1-UL1) 1,2,2
      IF (RAINSI-SUMES1) 3, 4, 4
 3
      SUMES1=SUMES1-RAINŚI
      60 TO 5
      SUMES1=0.
 5
      SUMES1=SUMES1+EOS
      IF (SUMES1-UL1) 6,6,7
 6
      ES=EOS
      GD TD 24
 7
      ES=EOS-0.4*(SUMES1-UL1)
      SUMES2=0.6*(SUMES1-UL1)
       T=(SUMES2/.35) **2
      60 TO 24
       IF (RAINSI-SUMES2)9,8,8
       RAINSI=RAINSI-SUMES2
       SUMES1=UL1-RAINSI
       T=0.
       IF(RAINSI-UL1) 5,5,4
 9
       T=T+1.
       ES=. 35*T**@. 5-SUMES2
       IF (RAINSI.GT. 0.) 60 TO 10
       IF(ES.GT.EOS) ES=EOS
       60 TO 11
  10
       ESX=0.8*RAINSI
       IF(ESX.LE.ES) ESX=ES+RAINSI
       IF(ESX.GT.EOS) ESX=EOS
       ES=ESX
  11
       SUMES2=SUMES2+ES-RAINSI
       T=(SUMES2/.35) ++2
       IF (ES.LT. 0.) ES=0.
  24
       IF(DLAI(I).GT.3.) GO TO 26
       EP=.53*DLAI(I)**.5*ED
       GO TO 27
  26
       EP=EO-ES
  27
       IF (EP.LT. 0.) EP=0.
       ET=ES+EP
       IF(E0-ET) 39,41,41
  39
       ET=EO
       EP=ET-ES
       CONTINUE
       EP=EP*WATCO(SMI,.40,0.)
       ET=ES+EP
       IF (I.LE. IDAY@) SUMET=@.
       SUMET=SUMET+ET
       IF(SPROUT.EQ. 0.) GO TO 200
       IF (IDAY7. NE. 0) GO TO 200
       RTGROW=HUNITS(I)*(0,2-0,0008*RTDEP)*WATCB(SMI,.15,0.)
       RTDEP=RTDEP+RTGROW
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IF (RIDEP. GI. RIDEPM) RIDEP=RIDEPM
     DELTSW=RAINEF-ET
200
     DO 300 L=1,LAYRS
      IF(DELTSW.ED. 0.) 60 TO 301
     SWLR=SWLAYR(L) +DLAYR(L) +DELTSW
      SWMAX=ULLAYR(L) *DLAYR(L)
      IF (SWLR.GE. 0.) GD TO 210
      DELTSW=DELTSW+SWLAYR(L) +DLAYR(L)
      SWLAYR(L)=0.
      GO TO 300
      IF (SWLR. LE. SWMAX) GO TO 220
      DELTSW=DELTSW-SWMAX+SWLAYR(L) *DLAYR(L)
      SWLAYR (L) =ULLAYR (L)
      GO TO 300
      SWLAYR(L)=SWLR/DLAYR(L)
929
      DELTSW=0.
      CONTINUE
 300
      DEPTH#0.
 301
      SW≖Q.
      UL=0.
      DO 400 L=1, LAYRS
      DEPTH=DEPTH+DLAYR(L)
       IF (I.LT. IDAY@) DEPTH=@.
       IF (RTDEP.LE. DEPTH) GO TO 410
       UL=UL+ULLAYR(L)#DLAYR(L)
       SW=SW+SWLAYR(L) *DLAYR(L)
 400
      CONTINUE
       SW=SW+SWLAYR(L) + (RTDEP+DLAYR(L) -DEPTH)
 410
       UL=UL+ULLAYR(L) + (RTDEP+DLAYR(L)-DEPTH)
       SWI=SWLAYR(1)/ULLAYR(1)
       IF(DLAYR(1).GE.30.) 60 TO 450
       SWI=(SWI+DLAYR(1)+(SWLAYR(2)/ULLAYR(2))+(30.-DLAYR(1)))/30.
       SMI=AMAX1 (SW/UL, SWI)
       RETURN
       FND
SUBROUTINE PHOTO(I)
       COMMON/BLK1/ALAT, TEMPMX (500), TEMPMN (500), SOLRAD (500), RAIN (500), CMAX, CAVG, DAYLN, HUNITS (500), SUMHU, IBEGIN, IEND
       COMMON/BLK2/MCLASS, XMAX (30), XN, NEARIN, FTASIN, FANTH, FSILK, FBLIST,
                      IDAY1, IDAY2, IDAY3, IDAY4, IDAY5, IDAY6, IDAY7, IDAY8, IDAY9, ISTAGE, FDENT, HUANTH, TASINI
        COMMON /BLK3/HTOTAL (30), FEMRGN, SPROUT, RCDUNT (30), FLEAF (30), PDAY, PDAYS (30), DLA (500), DLAI (500), PAREA, SDEPTH, IDAYO
        COMMON /BLK4/EDS, ED, SWLAYR (20), SW, ULLAYR (20), UL, UL1, SUMET, SMI,
        LAYRS, DLAYR (20), RTDEP, RTDEPM, ASOILT
COMMON /BLKS/DRIWT, TOTWT, RSRVS, GRNWT, TOTGRN, GRNMST, KRNLS, IPAR
       2
        REAL IPAR
        EXTINC#0.65
        IPAR=0.5*SOLRAD(I)*(1.~EXP(-EXTINC*DLAI(I)))
        ALPHA=3.2
        IF(ISTAGE. SE. 5) ALPHA=2.57
        DRIWT=4.2E-6*ALPHA*IPAR*PAREA*WATCO(SMI,.40,0.)
        IF (I.GT. IDAY9. AND. IDAY9. NE. 0) DRIWT=0.
         TOTWT=TOTWT+DRIWT
         RETURN
        END
  COMMON/BLK1/ALAT, TEMPMX (500), TEMPMN (500), SOLRAD (500), RAIN (500),
         SUBROUTINE EAR(I)
                       CMAX, CAVG, DAYLN, HUNITS (500), SUMHU, IBEGIN, IEND
         COMMON/BLK2/MCLASS, XMAX (30), XN, NEARIN, FTASIN, FANTH, FSILK, FBLIST,
        2
                        IDAY1, IDAY2, IDAY3, IDAY4, IDAY5, IDAY6, IDAY7, IDAY8,
        2
                        IDAY9, ISTAGE, FDENT, HUANTH, TASINI
         COMMON /BLK3/HTOTAL (30), FEMRGN, SPROUT, RCOUNT (30), FLEAF (30),
         PDAY, PDAYS (30), DLA (500), DLAI (500), PAREA, SDEPTH, IDAY
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CUMMUN / BEK4/EDS, EU, SWEAYK(20), SW, DEEAYK(20), DE, DE1, SUME1, SMI,
     LAYRS, DLAYR (20), RTDEP, RTDEPM, ASDILT
COMMON /BLKS/DRIWT, TOTWT, RSRVS, GRNWT, TOTGRN, GRNMST, KRNLS, IPAR
    2
     REAL KRNRED
     IF (IDAY6. EQ. IDAY5. AND. I. EQ. IDAY6) GO TO 9
     GO TO (900,900,900,6,8,10,15,20,25), ISTAGE
     IF(1-IDAY4) 900,7,14
     KRNRED=1.
     GO TO 14
IF(I-IDAYS) 900,9,14
8
     RSFRAC=0.20
     DMANTH=TOTWT
10
     IF(I-IDAY6) 900.12.14
12
     K=0
     GRNWT1=0.
     GRNRED=1.
14
      KRNRED=KRNRED-(1.-WATCD(SMI,.50,0.))+0.04
      IF(ISTAGE.EQ.4) GO TO 900
     GO TO 30
15
      IF(I-IDAY7) 900,17,30
17
      RSRVS=RSFRAC*TOTWT
      GRNMST=90.
      GO TO 30
      K≖K+1
20
      GRNRED=0.5+TANH (2.4-0.4+K)+0.5
      GO TO 30
25
      GRNRED=0.
      GO TO 100
      IF(CMAX.LT.30.) CMAX=30.
30
      IF (I.GE. IDAY7. AND. IDAY7. NE. 0) GO TO 31
      RSFRAC=RSFRAC+(1.-(CMAX-30.)/50.)
      60 TO 900
      RSFRAC=1-(CMAX-30.)/50.
31
      RSRVS=RSFRAC+RSRVS
32
      IF (DMANTH. GT. 160.) 60 TO 35
      KRNLS= (5. *DMANTH-50. ) *KRNRED
      GO TO 40
      KRNLS=750. +KRNRED
35
      GRNWT=0.00065*HUNITS(I)*KRNLS
 40
      IF (RSRVS.LE. 0. AND. GRNWT.GT. DRIWT) GRNWT=DRIWT
      RSRVS=RSRVS+DRIWT-GRNWT
      IF (RSRVS.GE. 0.) GO TO 100
      GRNWT=GRNWT+RSRVS
      RSRVS=0.
      GRNWT=GRNRED+GRNWT
       IF (ISTAGE. EQ. 8) RSRVS=RSRVS+GRNWT/GRNRED-GRNWT
       TOTGRN=TOTGRN+GRNWT
       IF(ISTAGE.EQ.9) 60 TO 210
       IF (GRNWT1.LT. 0.1. AND. GRNWT.LT. 0.1) IDAY9=I
       IF(I.EQ.IDAY9) ISTAGE=9
       GRNWT1=GRNWT
       GMSTLS=60. *HUNITS(I)/(0.75*(HUANTH-85.))
       GO TO 220
 210 GMSTLS=ED/.4
 220 IF (RAIN(I).GT. 0. AND. ISTAGE.GT. 8) GMSTLS=0.
       GRNMST=GRNMST-GMSTLS
 900
       RETURN
       END
       REAL FUNCTION WATCO (C1, C3, C5)
       C4=1.0
       IF(C1.LT.C3) GO TD 100
       WATCO=C4
       RETURN
  100 WATCD=C1*(C4-C5)/C3+C5
       RETURN
       FND
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SUBROUTINE RNF
       COMMON/BLK1/ALAT, TEMPMX (500), TEMPMN (500), SOLRAD (500), RAIN (500),
       CMAX, CAVG, DAYLN, HUNITS (500), SUMHU, IBEGIN, IEND
COMMON/BLKZ/MCLASS, XMAX (30), XN, NEARIN, FTASIN, FANTH, FSILK, FBLIST,
IDAY1, IDAY2, IDAY3, IDAY4, IDAY5, IDAY6, IDAY7, IDAY8,
      2
                      IDAY9, ISTAGE, FDENT, HUANTH, TASINI
      3
       COMMON /BLK3/HTOTAL (30), FEMRGN, SPROUT, RCOUNT (30), FLEAF (30),
                      PDAY, PDAYS (30), DLA (500), DLAI (500), PAREA, SDEPTH, IDAYO
      2
       COMMON /BLK4/EOS, EO, SWLAYR(20), SW, ULLAYR(20), UL, UL1, SUMET, SMI, LAYRS, DLAYR(20), RTDEP, RTDEPM, ASDILT
       COMMON /BLK5/DRIWT, TOTWT, RSRVS, GRNWT, TOTGRN, GRNMST, KRNLS, IPAR
       COMMON /BSOIL/ CN2, SL, PWC, W1, W2, SSW, Q, TOPT, IDB, IDE, S1
       SUL=0
       DO 100 N=1, LAYRS
       SUL#SUL+ULLAYR(N) *DLAYR(N)
       CONTINUE
  100
       C=100-CN2
       D=C+0.063
       E=2.533-D
        F=EXP(E)
        G=C+F
        H=(20*C)/6
        CN1=CN2-H
        CN3=CN2*EXP(.00673*(100-CN2))
        IF(SL.EQ. 0.05) GO TO 150
        CN2A=(CN3-CN2)*((1-2*EXP(-13.86*SL))/3)+CN2
        CN2=CN2A
        C=100-CN2
        D=C*0.063
        E=2.533-D
        F=EXP(E)
        G=C+F
        H=(20*C)/G
        CN1=CN2-H
        CN3#CN2*EXP(.00673*(100-CN2))
   150 S1=254*((100/CN1)-1)
        S3=254*((100/CN3)-1)
        FC=SUL #10
        ULM=PWC+10
        0=2.54/S1
         P1=1-P
         P2=ULM/P1
         P3=P2-ULM
         @1 =S3/S1
         Q2=1-Q1
         Q3=FC/Q2
         Q4=Q3~FC
         Q5=ALOG (Q4) -ALOG (P3)
         W2=05/(ULM-FC)
         W1=ALDG(Q4)+(W2*FC)
         RETURN
         END
  SUBROUTINE RUNOFF(I)
         COMMON/BLK1/ALAT, TEMPMX (500), TEMPMN (500), SOLRAD (500), RAIN (500),
                        CMAX, CAVG, DAYLN, HUNITS (500), SUMHU, IBEGIN, IEND
         COMMON/BLK2/MCLASS, XMAX (30), XN, NEARIN, FTASIN, FANTH, FSILK, FBLIST,
                         IDAY1, IDAY2, IDAY3, IDAY4, IDAY5, IDAY6, IDAY7, IDAY8,
                         IDAY9, ISTAGE, FDENT, HUANTH, TASINI
         COMMON /BLK3/HTOTAL (30), FEMRGN, SPROUT, RCOUNT (30), FLEAF (30),
         PDAY, PDAYS (30), DLA (500), DLAI (500), PAREA, SDEPTH, IDAYO COMMON /BLK4/EOS, EO, SWLAYR (20), SW, ULLAYR (20), UL, UL1, SUMET, SMI,
         ٤
                         LAYRS, DLAYR (20), RTDEP, RTDEPM, ASOILT
          COMMON /BLK5/DRIWT, TOTWT, RSRVS, GRNWT, TOTGRN, GRNMST, KRNLS, IPAR
          COMMON /BSOIL/ CN2, SL, PWC, W1, W2, SSW, Q, TOPT, IDB, IDE, S1
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ションション
      DO 100 N=1, LAYRS
SSW=SSW+SWLAYR(N) #DLAYR(N)
100 CONTINUE
       SSW=SSW+10
      S=S1*(1-(SSW/(SSW+EXP(W1-(W2*SSW))))))
      IF (S .LE. 0.01) S = 0.01
CN=25400/(S+254)
       R=RAIN(I)
      T=0.2*S

IF(R.LT.Z) GD TD 200

Q=(R-0.2*S)**2/(R+0.8*S)
       Q=Q/10
       IF (IOPT. NE. 3) GO TO 230
       IOP#IOPT
       IF(I.T.IDB) IOP=1
IF(I.GE.IDB .AND. I.LE.IDE) IOP=2
IF(I.GT.IDE) IOP=1
       IF (10P.EQ.2) Q=0
GO TO 240
230 CONTINUE
       IF(IOPT.EQ.2) Q=0
240 SSW#SSW/10
       CONTINUE
       GO TO 250
200 G=0
       55W=S5W/10
250 RETURN
       END
```