



TURBOMACHINERY LABORATORY TEXAS A&M ENGINEERING EXPERIMENT STATION

Optimizing Compressor Packing Designs by Predicting Rod Temperatures

Andreas Brandl, John Ladd, Karl Markey



Author Bios

Andreas Brandl is the Engineering Manager at HOERBIGER Service Inc. in Houston TX. His work focuses on Reciprocating Compressors for the Oil & Gas and Chemical/Petrochemical industry. Before coming to Texas he was working in the corporate R&D department for HOERBIGER in Austria. Andreas

earned his Master's degree in mechanical engineering at the Vienna University of Technology and his MBA at the Jones Graduate School of Business at Rice University.

John Ladd is a Solutions REE Engineer and Compressor Analyst at HOERBIGER Service In. in Houston, TX. His primary role is conducting comprehensive technical evaluations of reciprocating compressors to identify and quantify unit improvements in reliability, efficiency, and environmental soundness. Prior to his current role John earned his Master's in mechanical engineering at Colorado State University with a focus on legacy integral pipeline compressors.

Karl Markey is the R&P Engineering Team Manager at HOERBIGER in North America. His team focuses on product design and support for compressor OEM's and end users in a variety of industries. Karl has 15 years of experience in the Rings and Packing business and he has additional prior experience with product design and development outside the oil and gas industry. Karl has a Bachelor of Science degree from Massachusetts Institute of Technology and a Master of Engineering Degree from Rensselaer Polytechnic Institute.



Abstract

Current compressor rod packing engineering standards rely on rule of thumb methods and selection tables. This lecture presents a method to maximize the packing run time by optimizing the performance determining parameters of the packing. By predicting the rod temperature distribution, the performance of different packing layouts (case length, number of rings, backup ring material, ring design, case ID) can be compared and a relative run time prediction can be given. The lecture describes the model details, discusses the heat transfer correlation assumptions and deducts general packing design guidelines based on the model results. Several packing optimizations have been performed using this approach and two case studies are discussed in this lecture.

Agenda

1 Introduction and Motivation

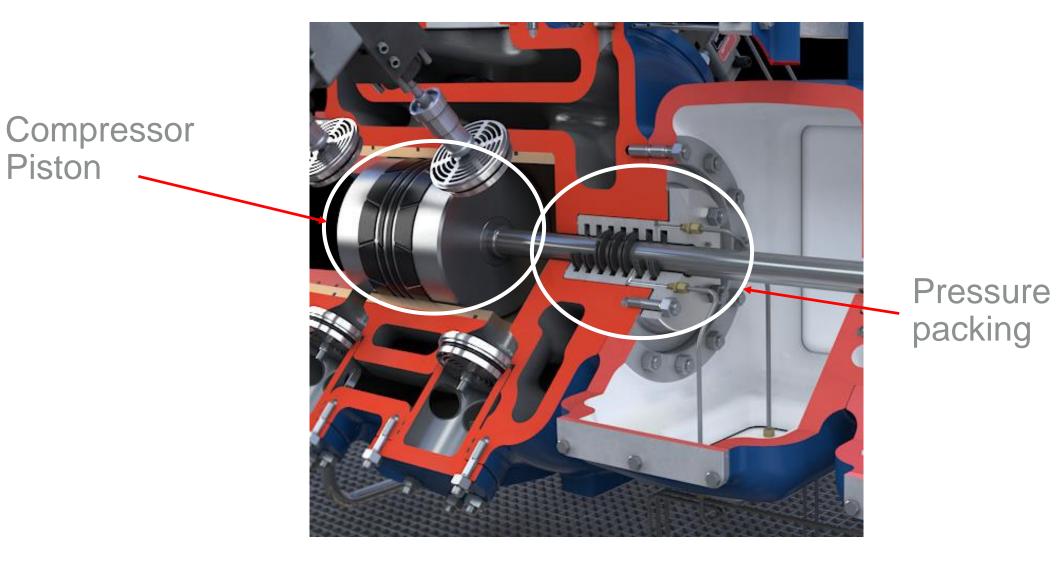
- 2 Description of the Rod Temperature Model
- **3** Optimization examples

4 Summary



Seal System – Piston & Pressure Packing

Piston

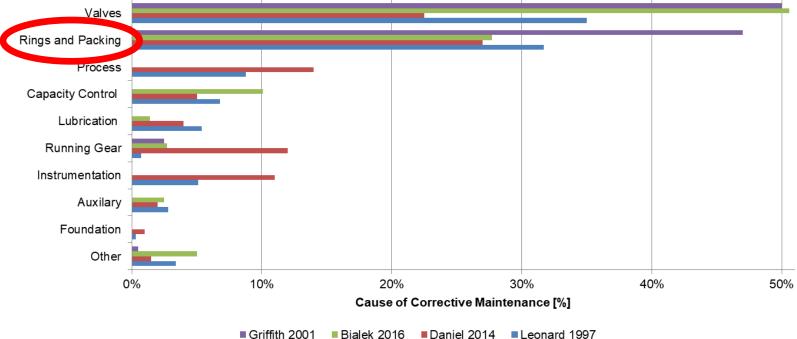




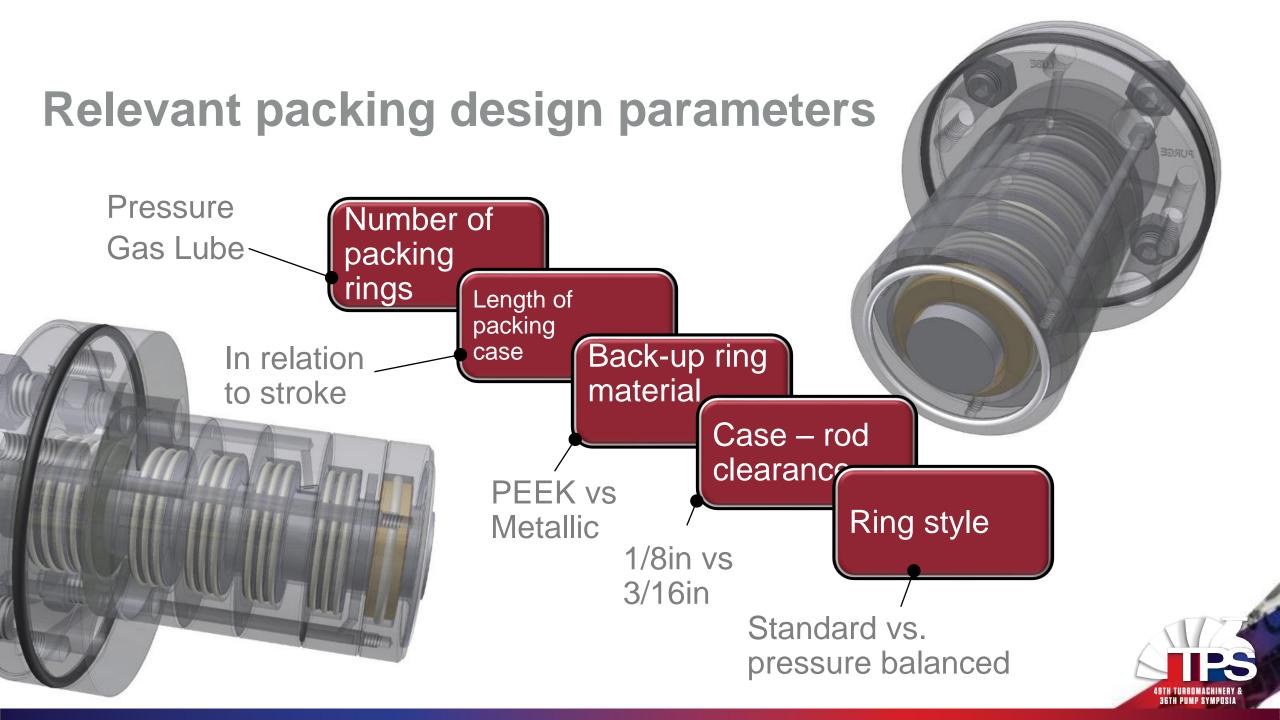
Seal system = Rings and Packing

27% - 47% of corrective maintenance events!



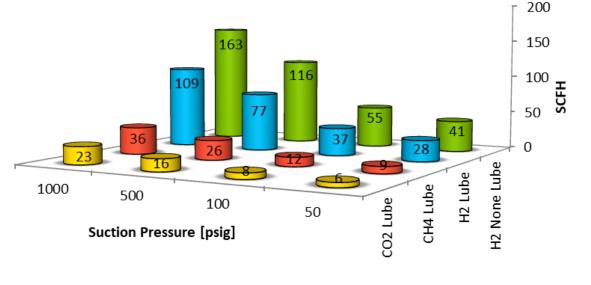






Typical leakage rates and heat removal

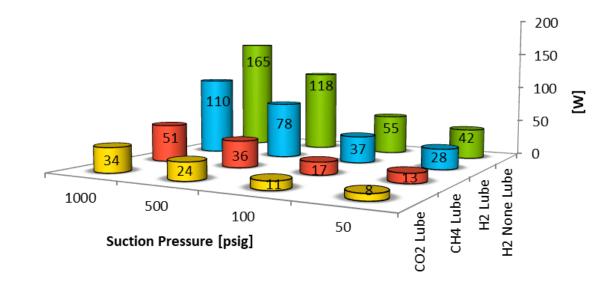
Expected Packing Leakage Rates (Based on empirical data)



H2 None Lube H2 Lube CH4 Lube CO2 Lube

Assumptions: Compression ratio of 2.5, 2in rod dia, 9in stroke

Expected Heat Removal From Rod via Gas Leakage



■ H2 None Lube ■ H2 Lube ■ CH4 Lube ■ CO2 Lube

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Assumptions: Compression ratio of 2.5, 2in rod dia, 9in stroke, temperature rise of gas of 180°F

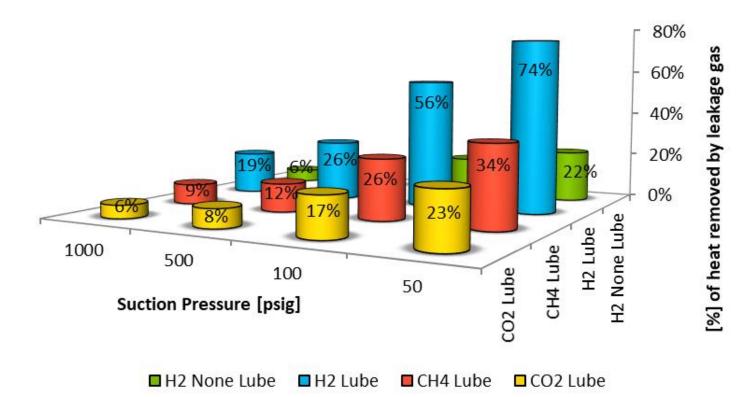
The leakage gas removes only a small fraction of the generated heat

Assumptions

- Compression Ratio: 2.5
- Rod dia: 2in
- Stroke: 9in
- Temperature rise: 180°F
- Frictional coefficient:
 - 0.2 (none-lube)
 - 0.04 (lube)

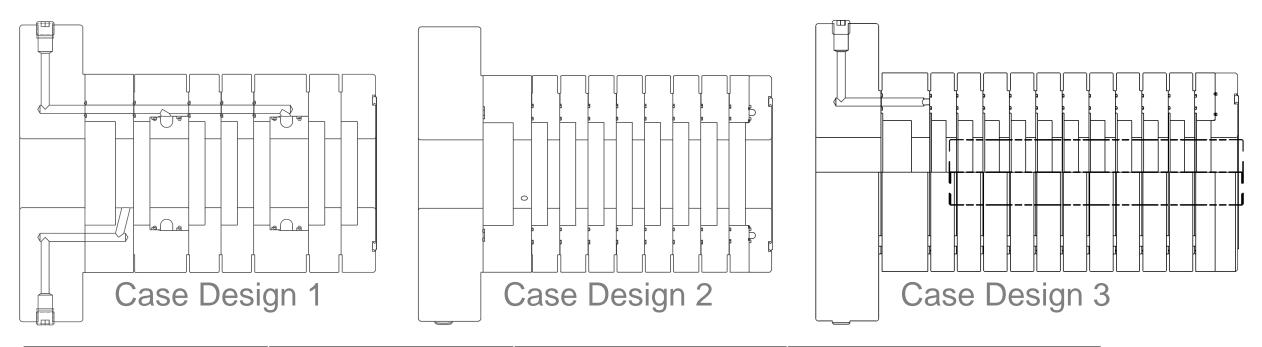
Lube oil

Heat removal from packing lube oil is negligible





Ideal Packing Case – Rod Temperature is a key parameter



Case Design 1	Case design 2	Case design 3	
6	8	11	
9	9	11	-
?	?	?	E
	Case Design 1 6 9 ?	Case Design 1Case design 26899??	Case Design 1Case design 2Case design 368119911???

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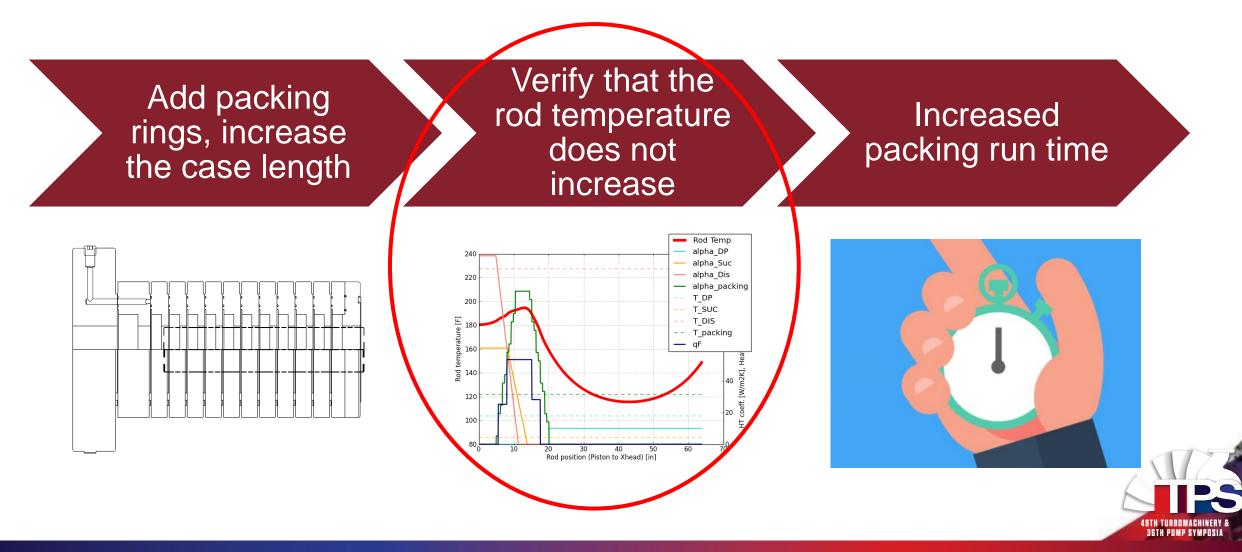
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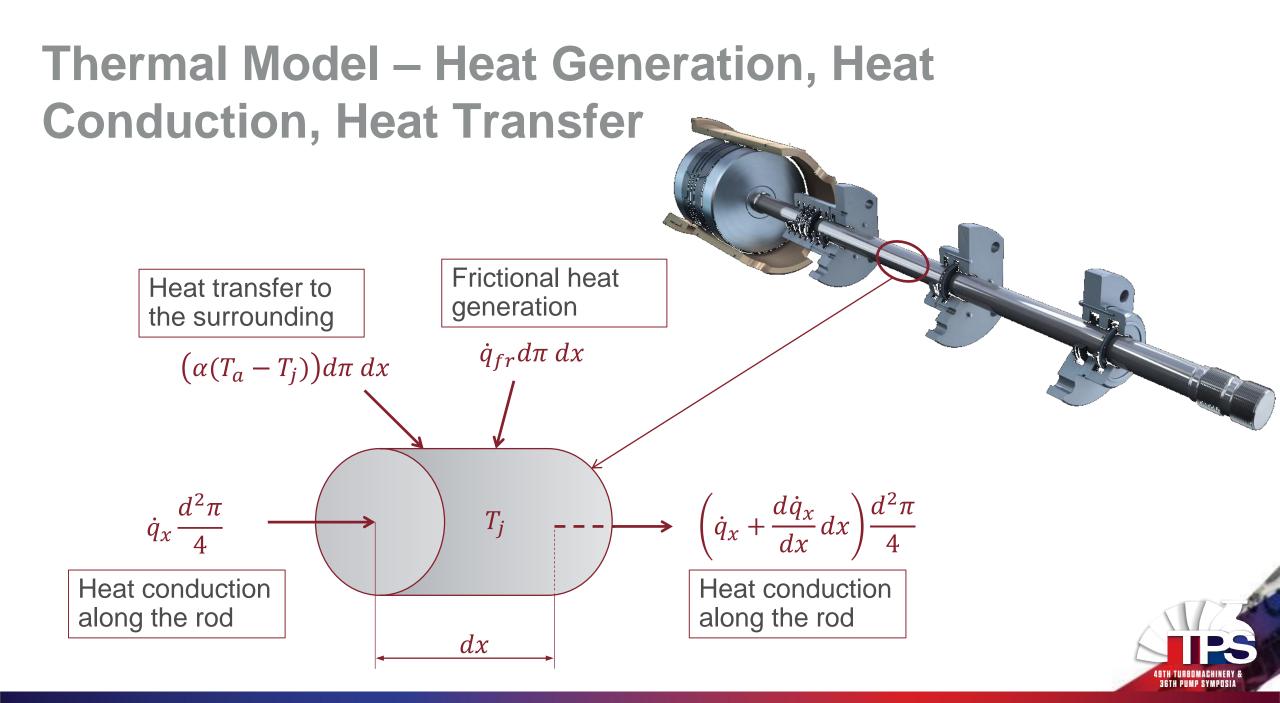
3 Optimization examples

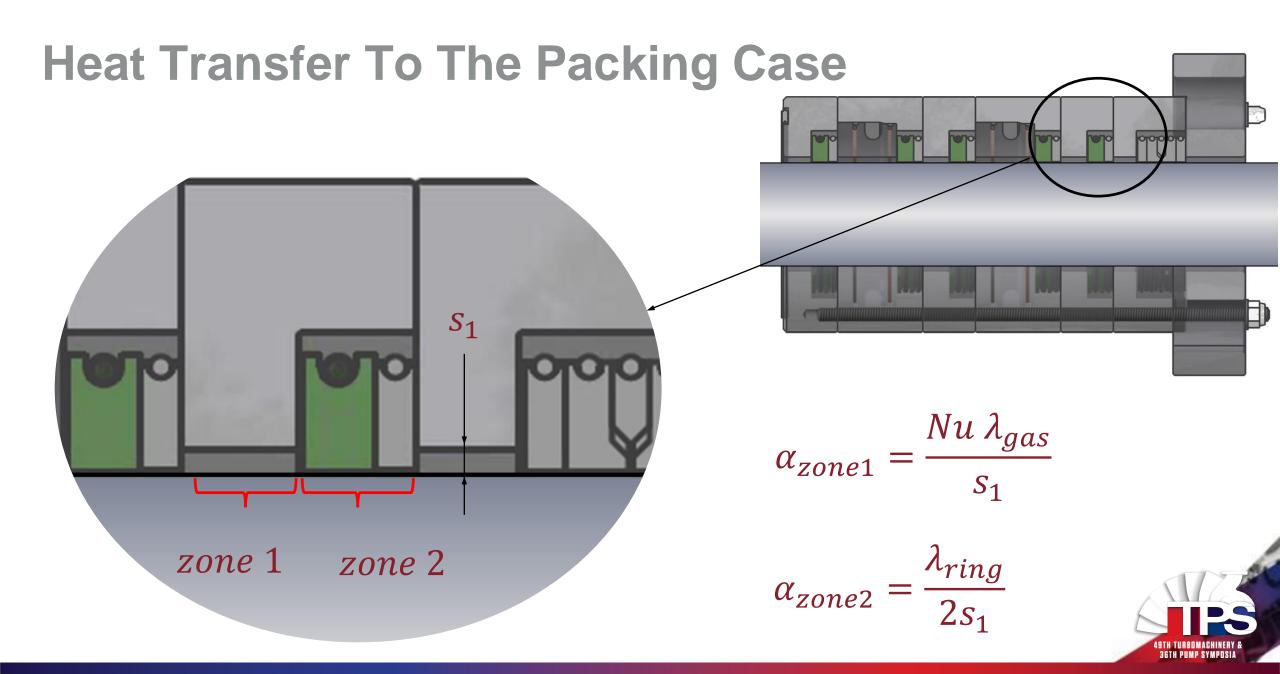
4 Summary



Optimization Process – Increase the ring count without increasing the rod temperature







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2 **Description of the Rod Temperature Model**

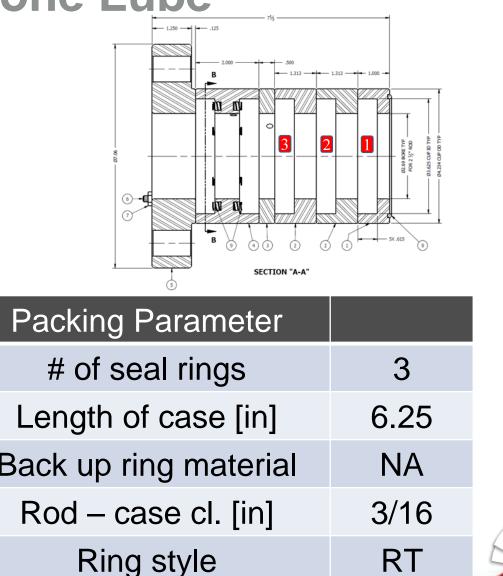
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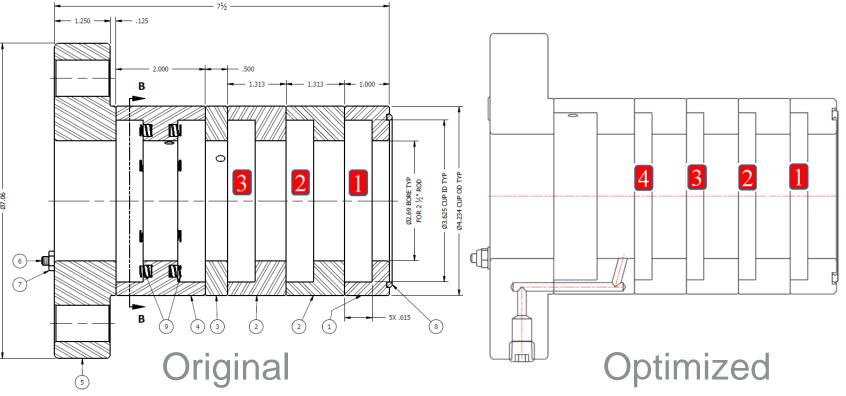
Low Pressure, Ethylene, None Lube

440	
16.5	
9	
660	
2.5	
1.29	
25.8	
None Lube	E
14	
65	
	16.5 9 660 2.5 1.29 25.8 None Lube 14



9TH TURBOMACHINERY 36TH PUMP Symposia

Packing Optimization



¹⁾Radial / Tangential cut ring ²⁾Pressure balanced ring

Packing Parameter	Existing	New	Impact
# of seal rings	3	4	Increased wear life
Length of case [in]	6.25	6.25	NA
Back up ring material	NA	NA	NA
Rod – case clearance [in]	3/16	3/16	NA
Ring style	RT ¹⁾	PB ²⁾	Reduced heat generation

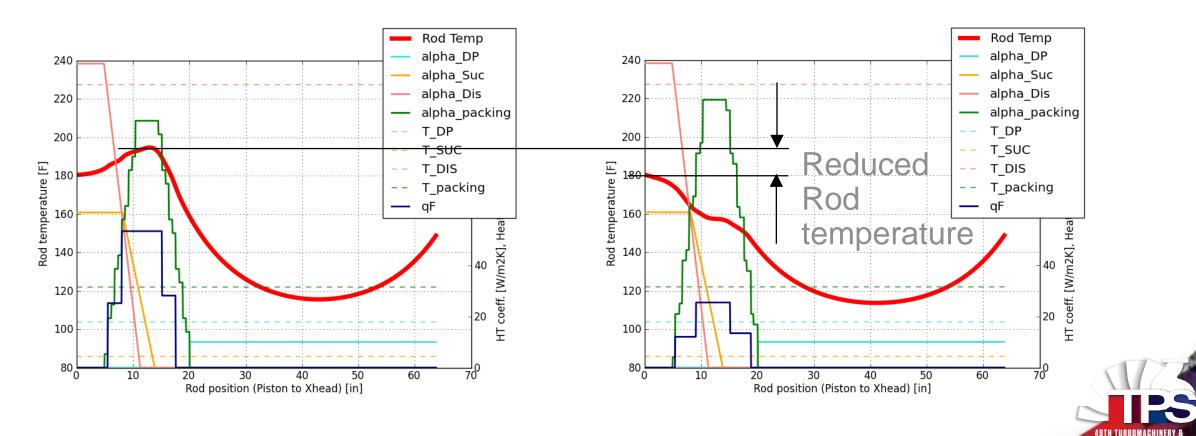


Increased number of ring + Reduced Rod Temperature

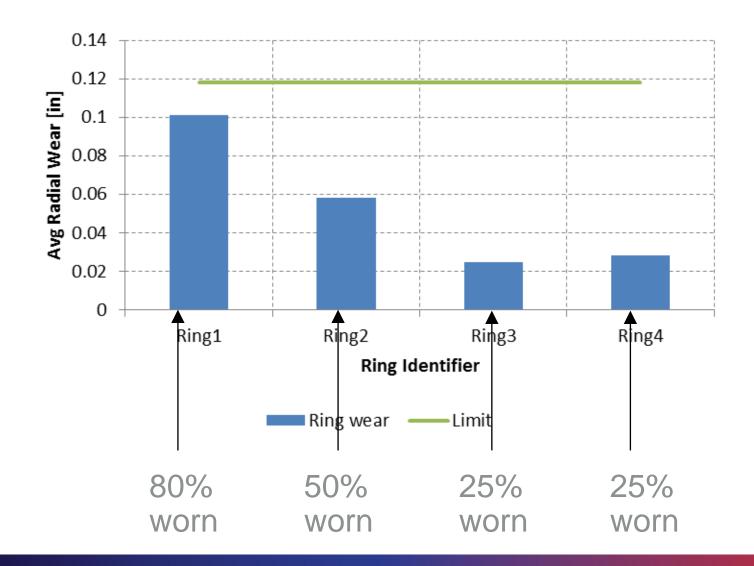
Increased number of rings

- Pressure balanced packing rings

36TH PUMP SYMPOSI



50% wear progress after 14 months of run time









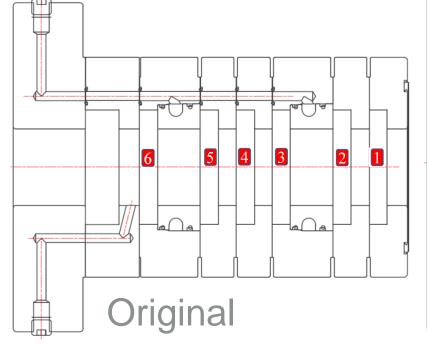
Medium Pressure, Hydrogen, None Lube

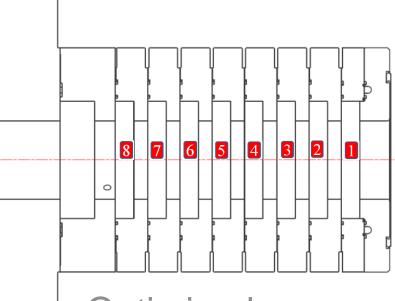
Parameter			
Speed [rpm]	396		
Cylinder dia [in]	4.75		
Stroke [in]	9		
Avg. P. speed [ft/min]	593		
Rod dia [in]	2	Packing Parameter	
Isentropic Exp. []	1.4	# of seal rings	6
Molar mass [kg/kmol]	2	Length of case [in]	9
Cylinder Lubrication	None Lube	Back up ring material	PEEK
p _{suc} [psig]	920	Rod – case cl.[in]	1/8
p _{dis} [psig]	1530	Ring style	RT

36TH PUMP SYMPOS

Packing Optimization

¹⁾Radial / Tangential cut ring ²⁾Pressure balanced ring





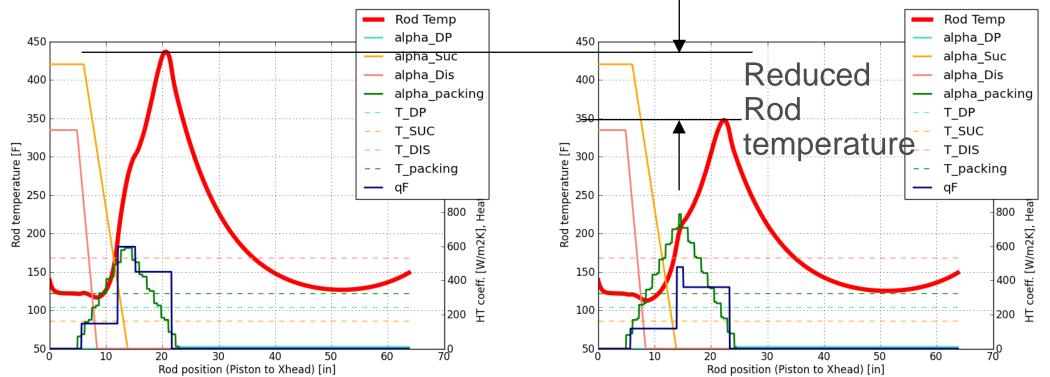
Optimized

Packing Parameter	Existing	New	Impact
# of seal rings	6	8	Increased wear life
Length of case [in]	9	9	NA
Back up ring material	PEEK	Bronze	Better heat transfer
Rod – case clearance [in]	1/8	1/8	NA
Ring style	RT ¹⁾	PB ²⁾	Reduced heat generation



Rod Temperature Distribution

- Increased number of rings
- Pressure balanced packing rings
- Metallic back-up ring



19TH TURBOMACHINERY 36TH PUMP SYMPOSIA

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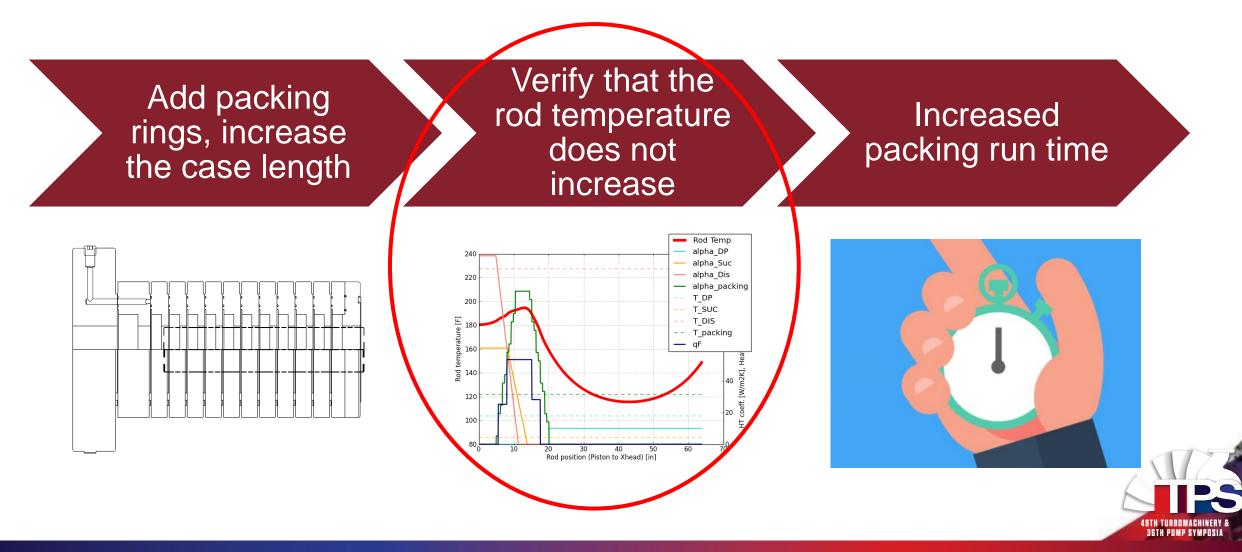
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Making Pressure Packings more Reliable by Taking the Rod Temperature into Consideration

