

Thermoplastic Labyrinth Seals in Centrifugal Compressors - 15 years of experiences

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⁵⁵⁴Thermoplastic Labyrinth Seals

- n Thermoplastics used in compressors for over 20 years now.
 - n The two most common thermoplastic materials used are:
 - q PolyAmide-Imide (PAI) – trade name Torlon
 - q Polyetheretherketone – trade name PEEK
-

⁵⁵⁵Thermoplastic Labyrinth Seals

- n **Benefits of Thermoplastic Seals**
 - q **Efficiency**
 - n Design with reduced clearances
 - q **Reliability**
 - n Maintain clearance during “transient” rubs
 - n Forgiving during hard rubs (gall resistant)
 - n Can be more corrosion resistant
 - q **Ease of installation**
-

Introduction

n Labyrinth Seals

- q Basics, leakage, use in centrifugal compressors

n Thermoplastics

- q Types, properties, use in centrifugal compressors

n Upgrade payback calculations

n Case Histories

- q Canadian ethylene plant

- q Texas ethylene plant

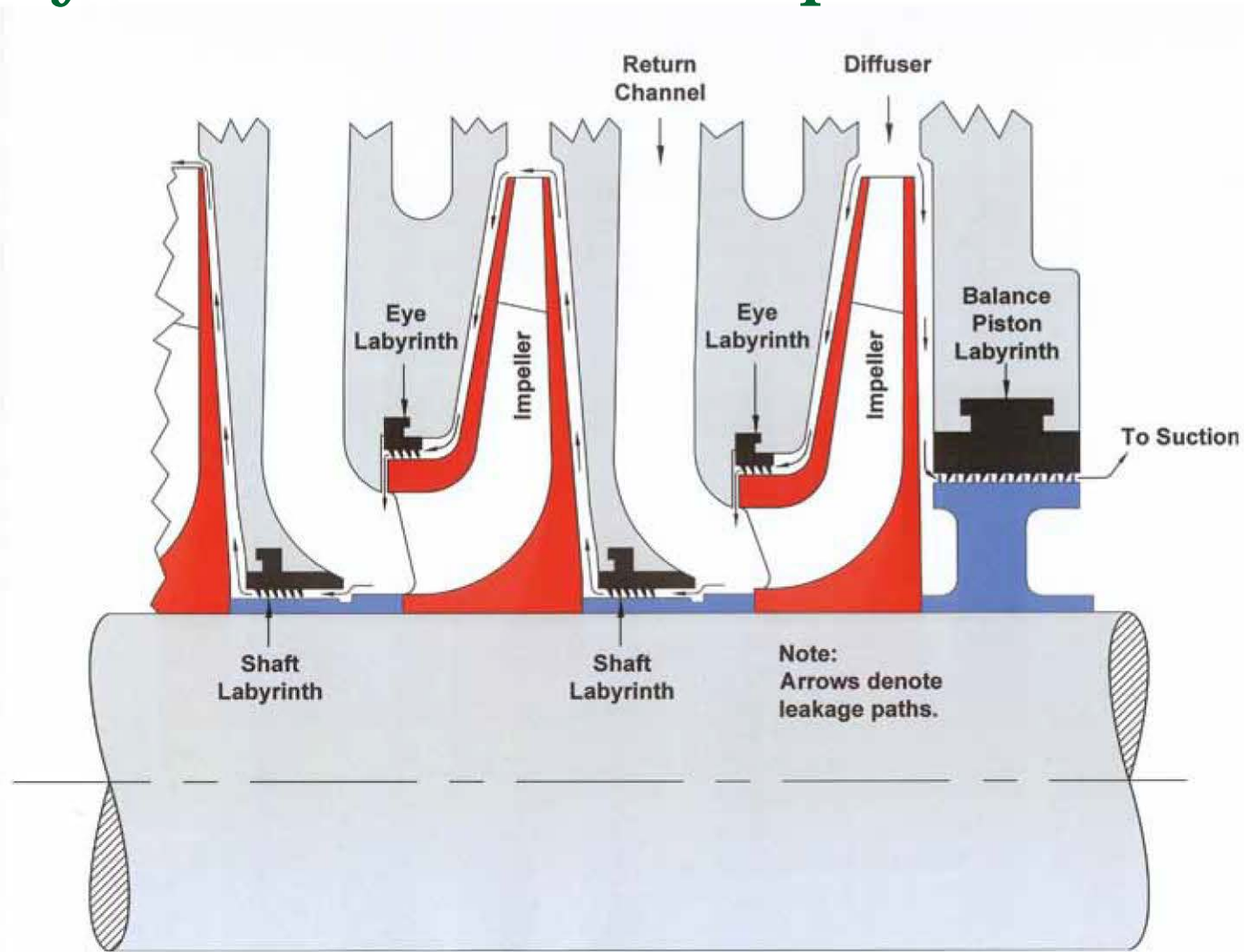
n Conclusions

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Labyrinth Seals

- n Seal an area of high pressure from an area of low pressure
 - n Clearance seals – they do leak
 - n Seals typically upgraded in a centrifugal compressor
 - q Eye
 - q Shaft or Hub
 - q Balance piston
-

Labyrinth Seals – Compressor Seals



⁵⁵⁹Labyrinth Seals

- n Centrifugal compressor seal impact on efficiency.
 - q Assume leakage is linear with clearance.
 - q Assume 4% of the compressor efficiency loss is attributable to internal labyrinth seals.
 - q If we reduce clearance to $\frac{1}{2}$ then leakage will reduce to $\frac{1}{2}$ --> 2% efficiency gain.
 - q If all major compressors in a 2 billion lb/yr ethylene plant are upgraded this can save \$700,000 per year in energy savings.

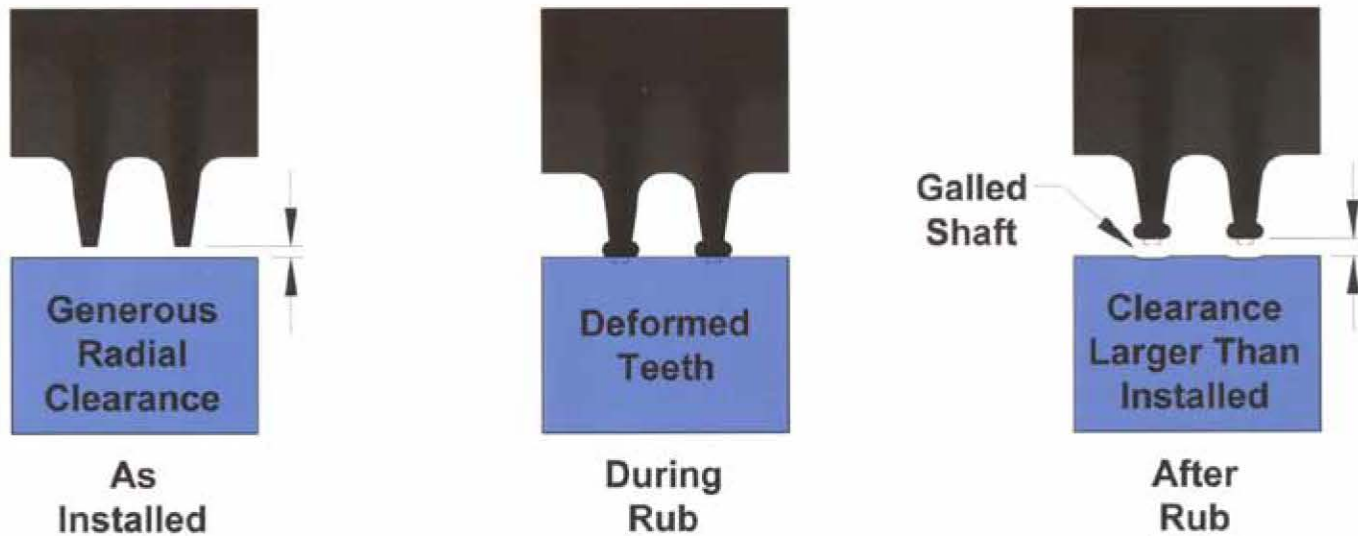
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Labyrinth Seals

- n How to reduce seal leakage
 - q Reduce clearance and ensure it stays reduced
 - q Metallic seal rub can cause problems
 - n Open seal bore
 - n Vibration
 - n Rotor damage (galling)
 - q Polymer seal rubs are “forgiving”
 - n Clearance integrity
 - n Not likely to induce rub related vibration
 - n Typically do not damage rotor
-

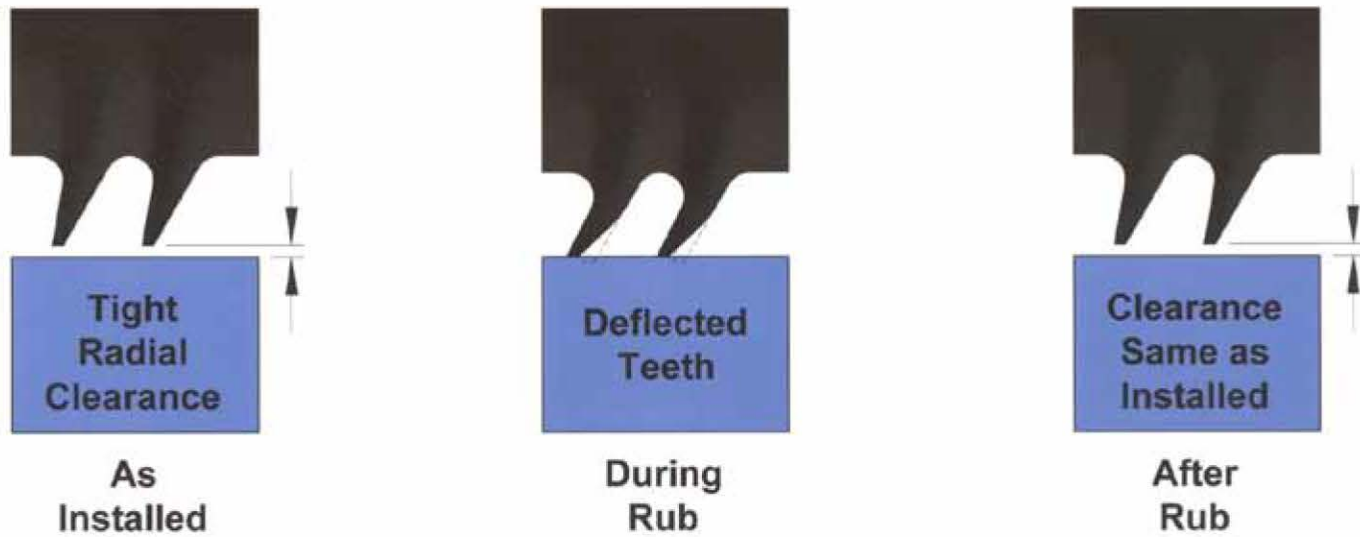
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Metallic Seal Rubs



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Polymer Seal Rubs



⁵⁶³Thermoplastics

- n Define Thermal Property Terms
 - n Polymer Types
 - q Thermosets
 - q Thermoplastics
 - n Amorphous
 - q Torlon®
 - n Crystalline
 - q PEEK
-

⁵⁶⁴Thermoplastics

n Thermal Properties

- q Tg – Glass transition temperature
 - q Tm – Melt temperature
 - q CUT – Continuous Use Temperature
 - q HDT – Heat Deflection Temperature
 - q DMA – Dynamic Mechanical Analysis
 - q CLTE – Coefficient of Linear Thermal Expansion
-

⁵⁶⁵Thermoplastics

- n Tg – Glass transition temperature
 - q Temperature at which the polymer softens
 - q Below Tg polymers are rigid
 - q Above Tg polymers are “rubbery”
 - q At Tg CLTE increases significantly
 - q Above Tg strength and modulus drop off
 - q Loses “memory”
 - q For labyrinth seals operation at or above the Tg should be avoided.
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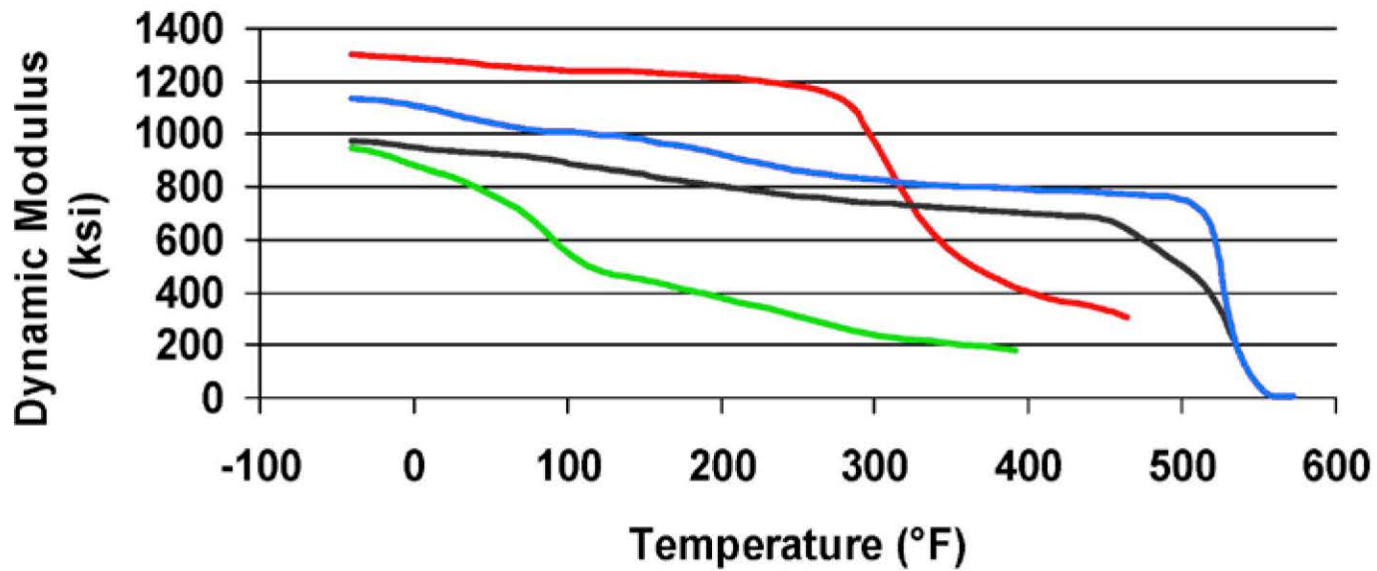
⁵⁶⁶Thermoplastics

- n CUT – Continuous use temperature
 - q Based upon UL tests
 - q Temperature a polymer can be exposed to for 100,000 hours before losing ½ its strength.
 - q Accounts for thermal aging
 - q Increases brittleness
 - q Does not impact installed seal performance
 - q Only a concern in high temperatures (300-350 °F)
-

⁵⁶⁷Thermoplastics

- n HDT is the Heat Deflection Temperature
 - q Per ASTM D-648, the temperature at which a standard test specimen (typically 0.5" W x 5" L x 0.5" Thick) under a load of 264 psi will deflect 0.010" or 5%
 - q Essentially the HDT is the temperature at which the flexural modulus of the polymer is reduced to 100,000 psi.
 - n DMA (Dynamic Mechanical Analysis) is a measure of the stiffness at temperature.
-

⁵⁶⁸ DMA Plot for Various Thermoplastics

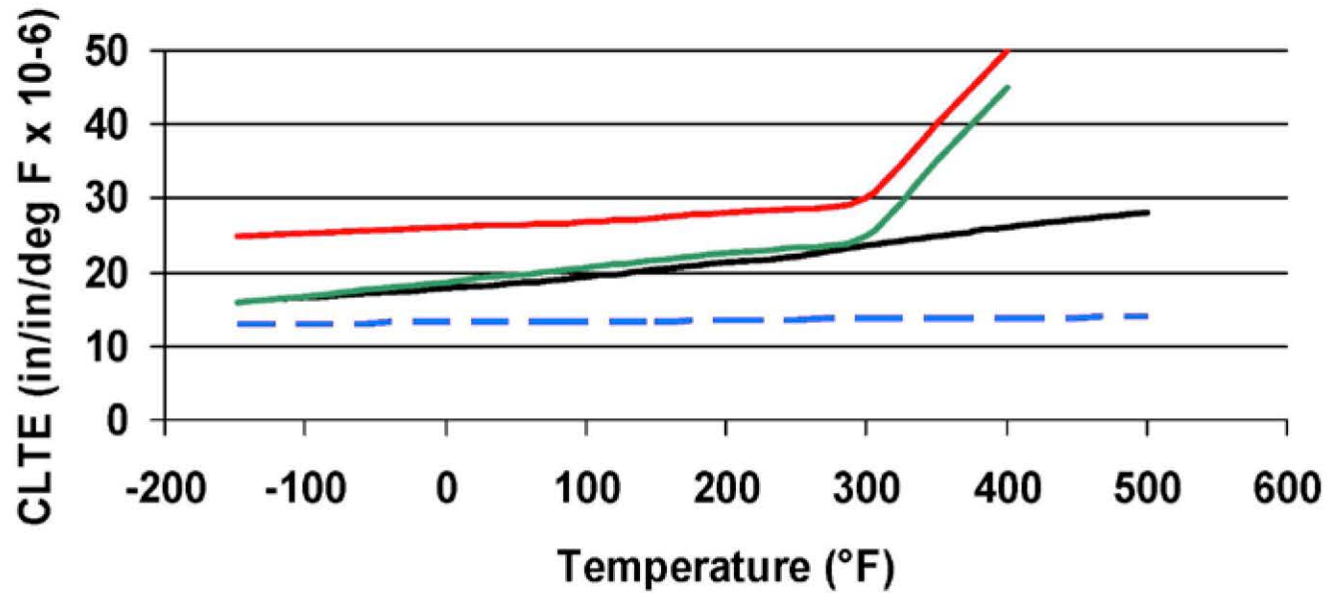


— PEEK (15% CF) — Torlon (0% CF)
— Torlon (30% CF) — Fluorosint

⁵⁶⁹Thermoplastics

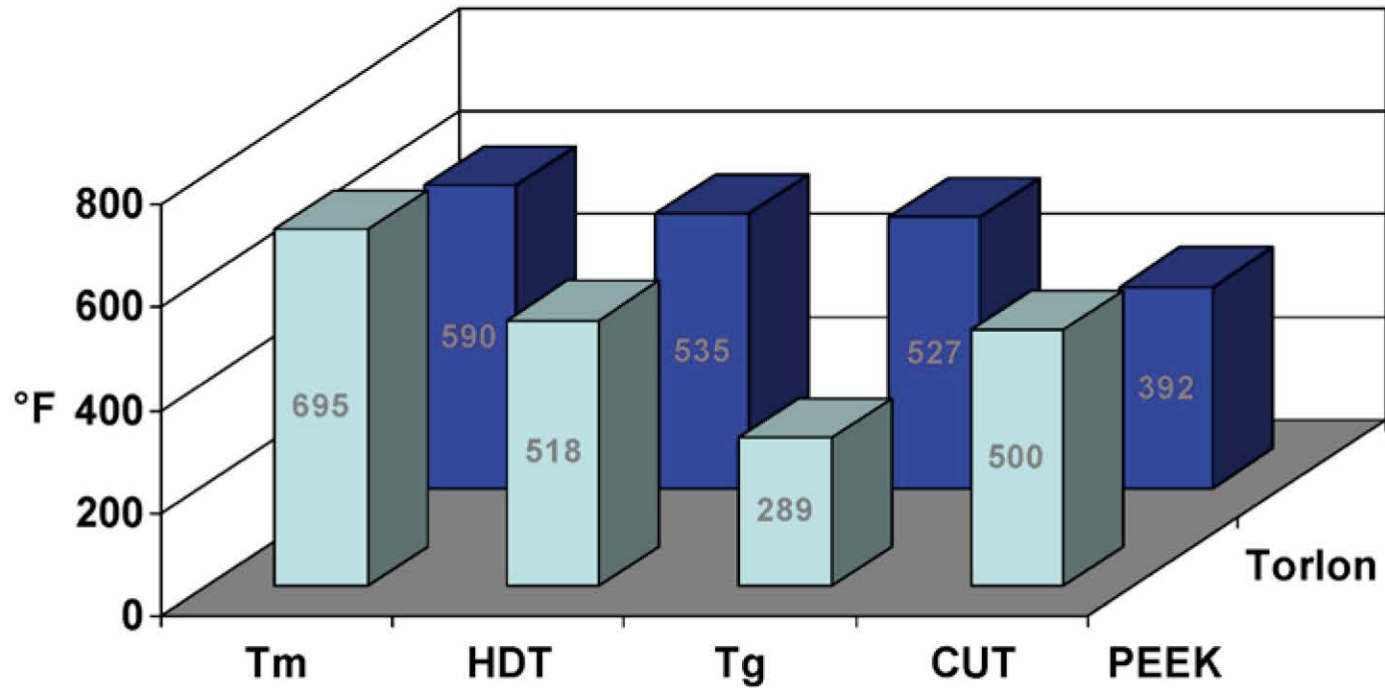
- n CLTE (Coefficient of Linear Thermal Expansion)
 - q Describes how the size of a part will change with changes in temperature.
 - q The smaller the material's CLTE, the more dimensionally stable a part made from that material will be as temperatures are varied
 - q For most polymers the CLTE increases with temperature
 - n Must be accounted for in close tolerance applications
-

570 CLTE Plot



— Torlon - - Aluminum — PEEK (30% CF) — PEEK (15% CF)

571 Relative Thermal Properties



⁵⁷²Thermoplastics

- n Chemical Attack Depends on
 - Temperature
 - Concentration
 - Pressure
 - Time
-

⁵⁷³ PEEK Chemical Resistance

As a Semi crystalline polymer, PEEK is highly resistant to chemical attack **BUT** will be attacked by concentrated (over 30%) strong acids at high temperature:

Sensitive to:

Chromic Acid

Hydrofluoric Acid

Nitric Acid

Sulfuric Acid

Chlorine Dry & Wet

Unaffected by:

Acetic Acid, 10% Conc

Amines

Hydrocarbons

⁵⁷⁴Torlon Chemical Resistance

As an amorphous polymer, Torlon is less chemically resistant than PEEK.

Sensitive to:

Amines (-NH₂)
Ammonia (-NH₃)
Oxidizing Acids
Strong Bases (OH)
Chlorine Dry & wet
Saturated Steam
> 300F

Unaffected by:

Automotive Trans. Fluids
Aliphatic Hydrocarbons(Butane)
Aromatic Hydrocarbons (Toluene)
Halogenated Hydrocarbons
such as: Methylene Chloride

⁵⁷⁵Engineering

- n Data required includes:
 - q Process make up for compatibility analysis
 - q Suction and discharge temperatures and pressures
 - q Speed – for centrifugal growth calculations
 - q Cross sectional drawing of compressor showing impeller and seal arrangement
 - q Actual sealing diameters, from recent inspection report
 - q Sample seals or seal drawings
 - q Bearing clearance

⁵⁷⁶Engineering

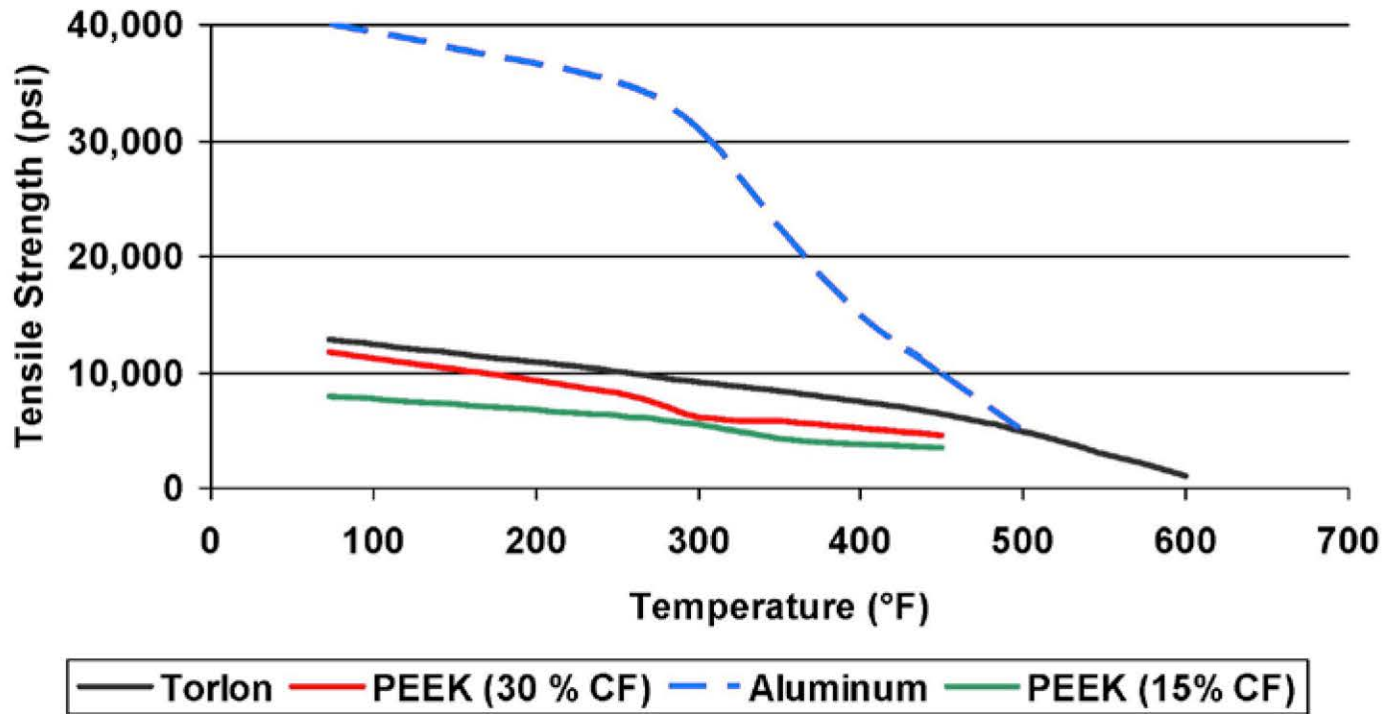
n Calculations performed:

- q Polymer properties at operating temperature
- q Thermal expansion of impeller, seal, and diaphragm
- q Centrifugal growth of sealing surface
- q Resulting operating seal clearance
 - n Size operating clearance equal to bearing clearance
 - n For barrel compressor use 1.5 times bearing clearance

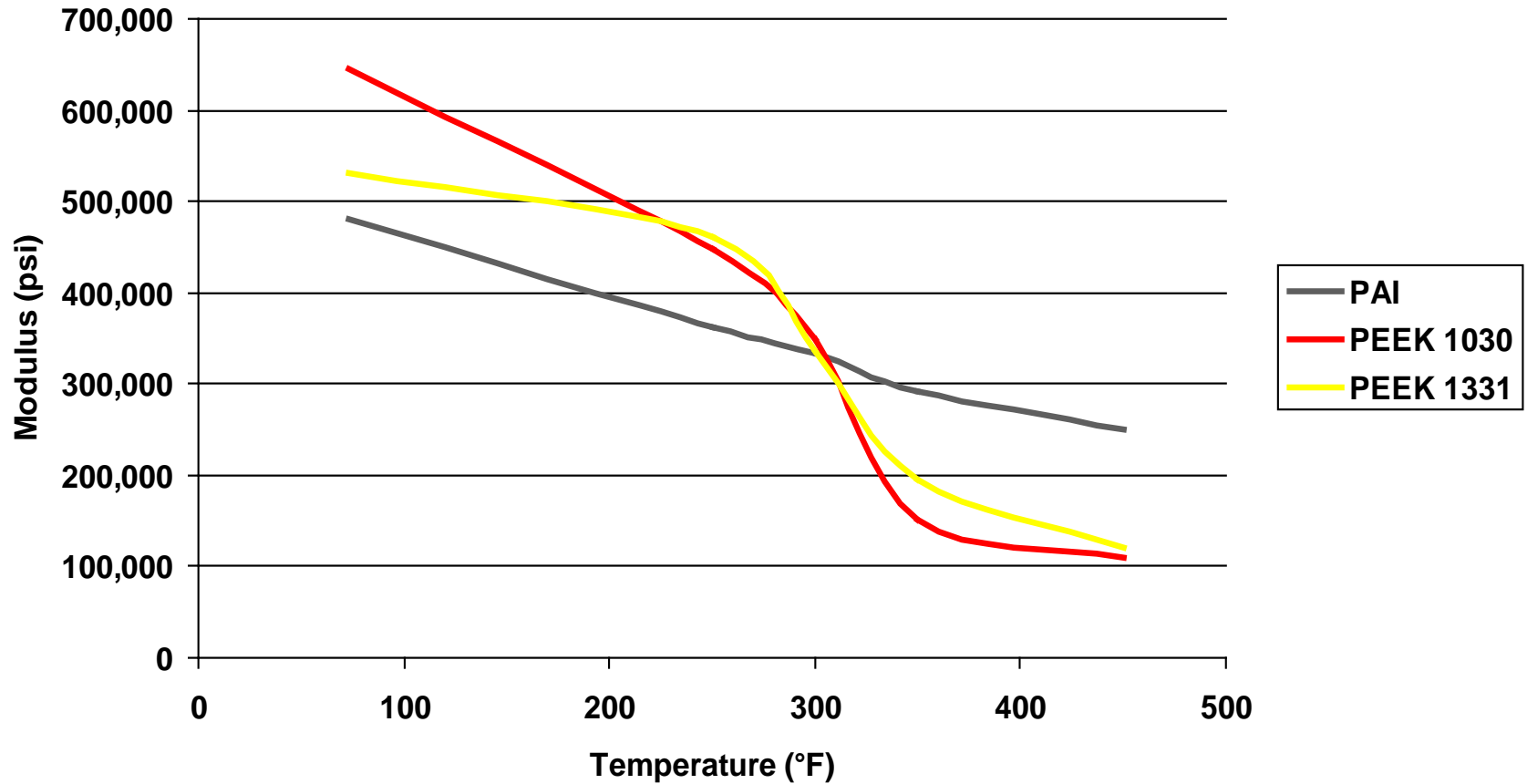
n Low temperature applications

- q Since CLTE is high the seals will contract more than surrounding components – this must be accounted for.
- q Must ensure “hook” will not bind up in diaphragm.
- q Successfully applied by authors at negative 150 degrees F suction temperature.
- q Extrapolate mechanical properties.

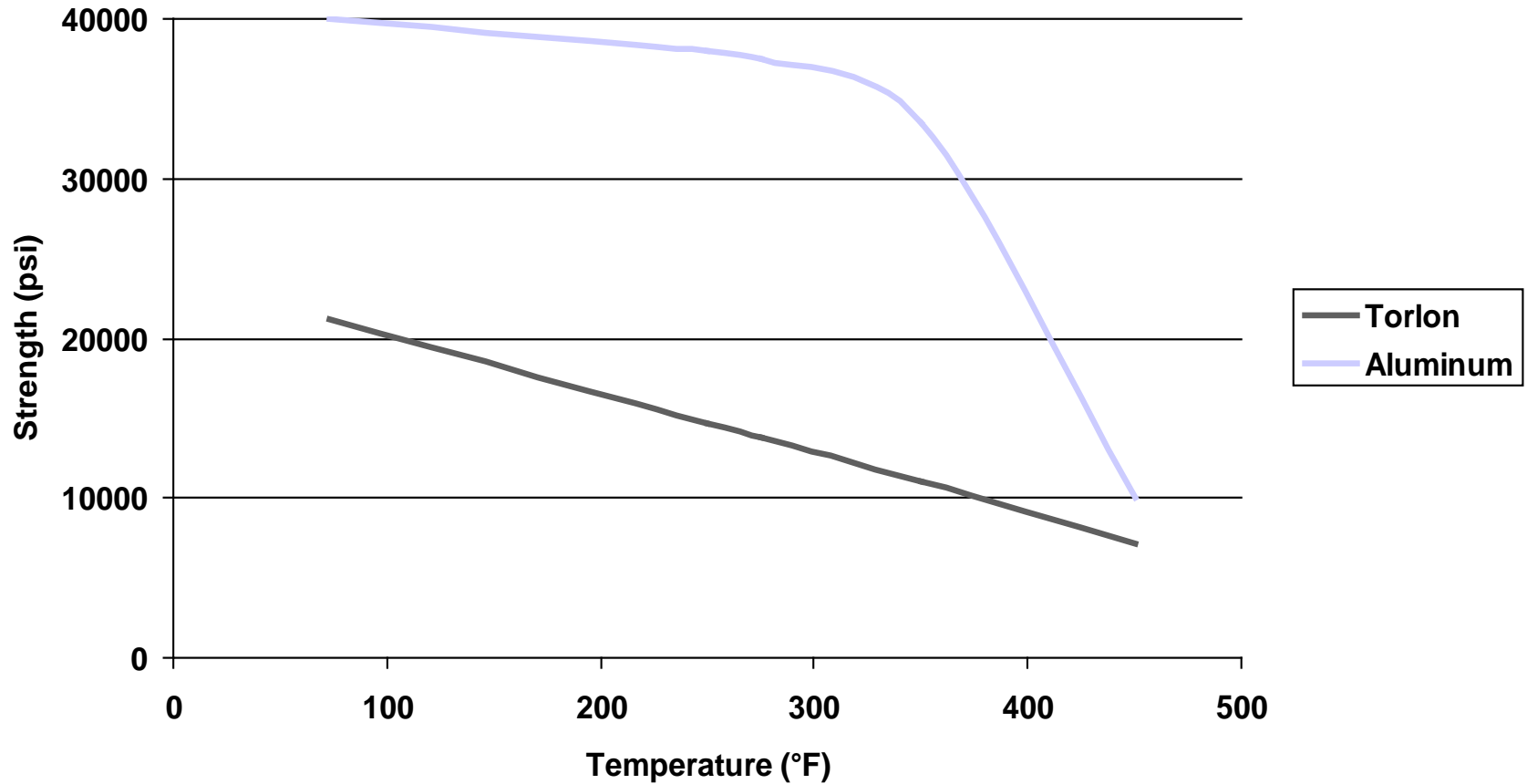
578 Tensile Strength vs. Temperature



579 Tensile Modulus vs. Temperature



580 Compressive Strength vs. Temperature



⁵⁸¹Upgrade Payback Calculations

- n A common “rule of thumb” for estimating compressor performance gains is to use $\frac{1}{4}$ to $\frac{1}{2}$ % per impeller.
 - n Based upon experience this is conservative
 - n Use the $\frac{1}{2}$ % number if the balance piston seal is included in the project
-

582 Upgrade Payback Calculations

- n Items brought up during this discussion;
 - q “I **expect** to see efficiency gains after a turnaround.”
 - q How to break out overall gains when several things were done that should improve efficiency.
 - q “I can’t measure my compressor efficiency accurately enough to quantify the gains.”
 - n Use past experience
 - q See the two case histories that follow.
-

⁵⁸³Case Histories

n Case 1: Canadian Ethylene Plant

q Chow and Miller: “Optimizing performance of an ethylene plant cracked gas compressor train.”

n 10th Ethylene producers conference

q Whalen and Miller: “An ethylene plant benefits from polymer labyrinth seals.”

n Turbomachinery International, 1998

n Case 2: Texas Ethylene Plant

q Whalen and Dugas: “Upgrading centrifugal compressors with polymer seals in an ethylene plant – a case history.”

n 29th Turbomachinery Symposium, 2000

584 Canadian Ethylene Plant

- n 1996 Outage – Ethylene 1
 - n Installed Torlon in two cracked gas compressors and the propylene compressor
 - n Propylene seals are very large
 - q 45” bore 1st stage eye, 36 ½” bore balance piston
-

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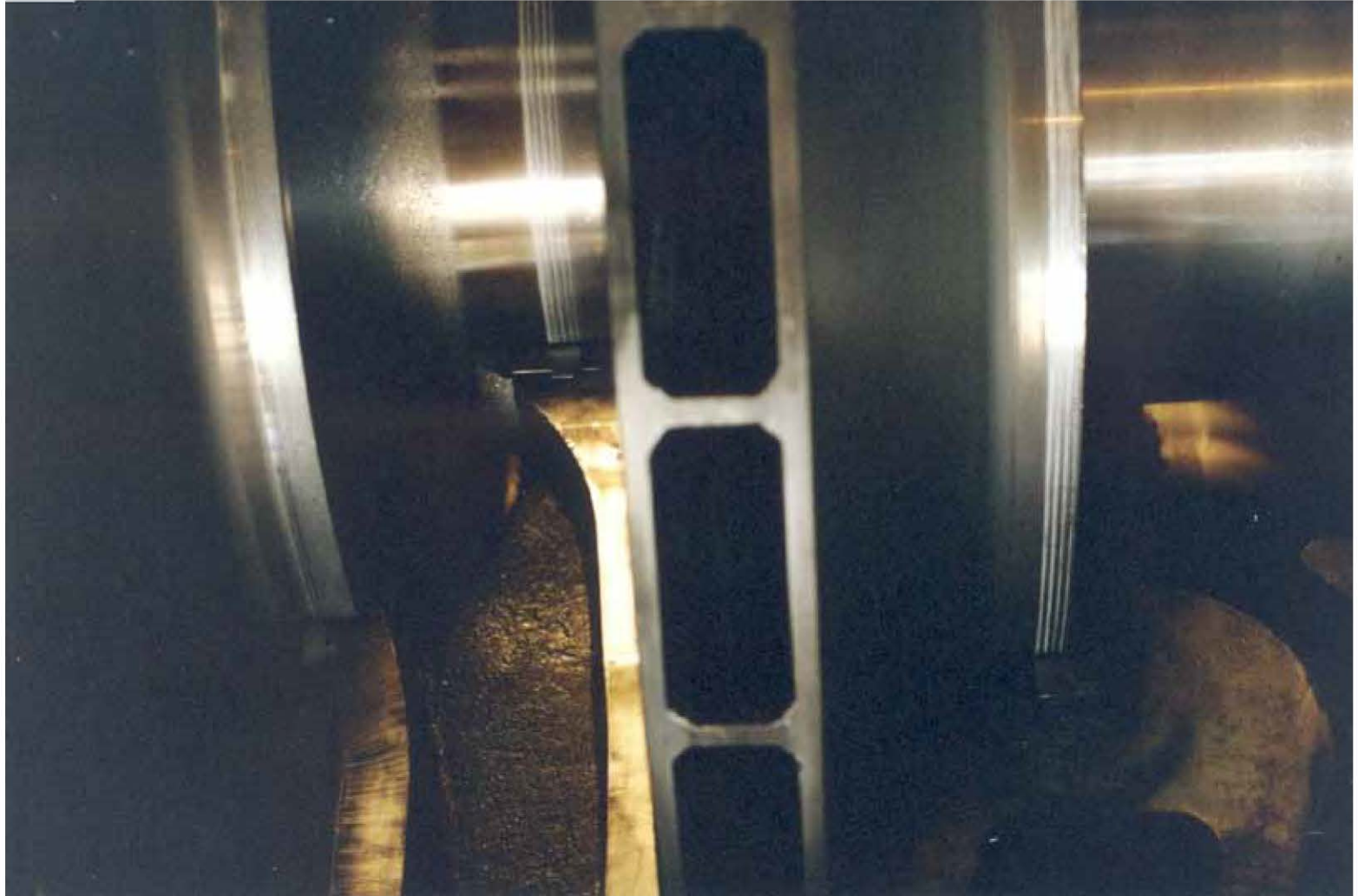
Canadian Ethylene Plant

- n Ran 4 years - to 2001
 - q Checked clearances in one machine – still in spec
 - q Buttoned up and running today
 - n Ran 5 years - to 2006
 - q Checked clearances – still in spec
 - q Buttoned up and running today
 - q Expect to run for 6 years
-

⁵⁸⁶
Canadian Ethylene Plant

- n 1998 Outage – Ethylene 2
 - n Installed Torlon in all three cracked gas compressors and the ethylene compressor
 - n 2002 outage – still in spec
 - n 2007 outage – still in spec
 - n All major compressors in both units are now running polymer seals.
-

587
Canadian Ethylene Plant 1996 outage



588
Canadian Ethylene Plant 1996 outage



589 Canadian Ethylene Plant

- n Historical trouble fitting the babbitt lined balance piston seal
 - q Machined teeth off balance piston
 - q Went with Torlon stationary teeth
 - n Significant reduction in installation time
 - n No drop in performance
-

⁵⁹⁰
Torlon Tooth Scrapping Tool



Relatively clean
service but some
seals were fouled



⁵⁹¹ Shaft Seal as removed after 4 and 5
year runs – 9 year total run time –
reinstalled will run another 6 years



⁵⁹² Eye Seal as removed after 4 and 5 year runs – 9 year total run time



593 Canadian Ethylene Plant

- n Some seals were damaged when removed
 - n These (5) were sent to vendor for analysis
 - q All from charge gas service
 - n Vendor found very little drop off in properties
 - q Seals ran for 9 years
 - q Visually looked good
 - q Slight embrittlement
 - q Tg constant – no polymer degradation
-

594 Canadian Ethylene Plant

n Reported:

- q "...2-3% increase per compression stage with the installation of thermoplastic seals."
 - q "The rotating equipment specialists at the Joffre site believe that the use of thermoplastics is important in optimizing performance, increasing run lengths, and reducing turn around costs."
-

Texas Ethylene Plant

- n Major ethylene producer
- n Has six primary compressor trains
 - q Booster
 - q Charge gas (3 bodies)
 - q Propylene refrigeration (2 bodies)
 - q Ethylene refrigeration
 - q Purge propylene
 - q Methane (2 bodies)

596

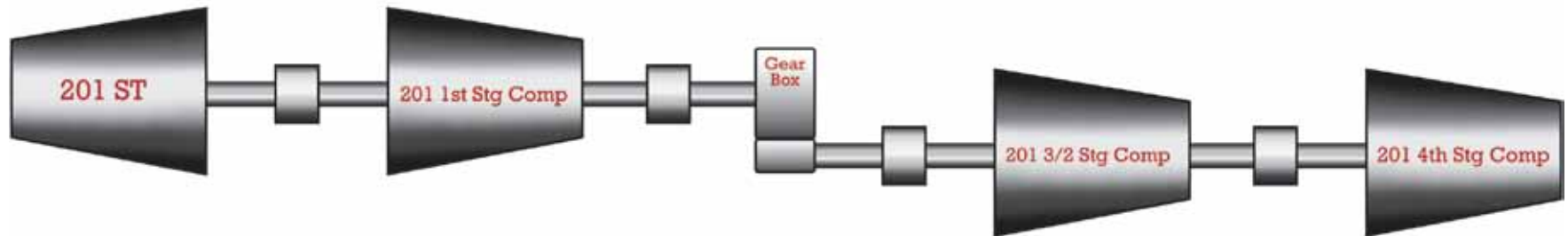
DuPont Cracked Gas Train



⁵⁹⁷DuPont Cracked Gas Train

36,000 hp turbine driving
three compressor bodies

Upgraded last
case in 2005



Upgraded 1st stage and 2nd/3rd stage
compressors in 1999

Also upgraded both propylene, the
ethylene, and the purge propylene
compressors in 1999

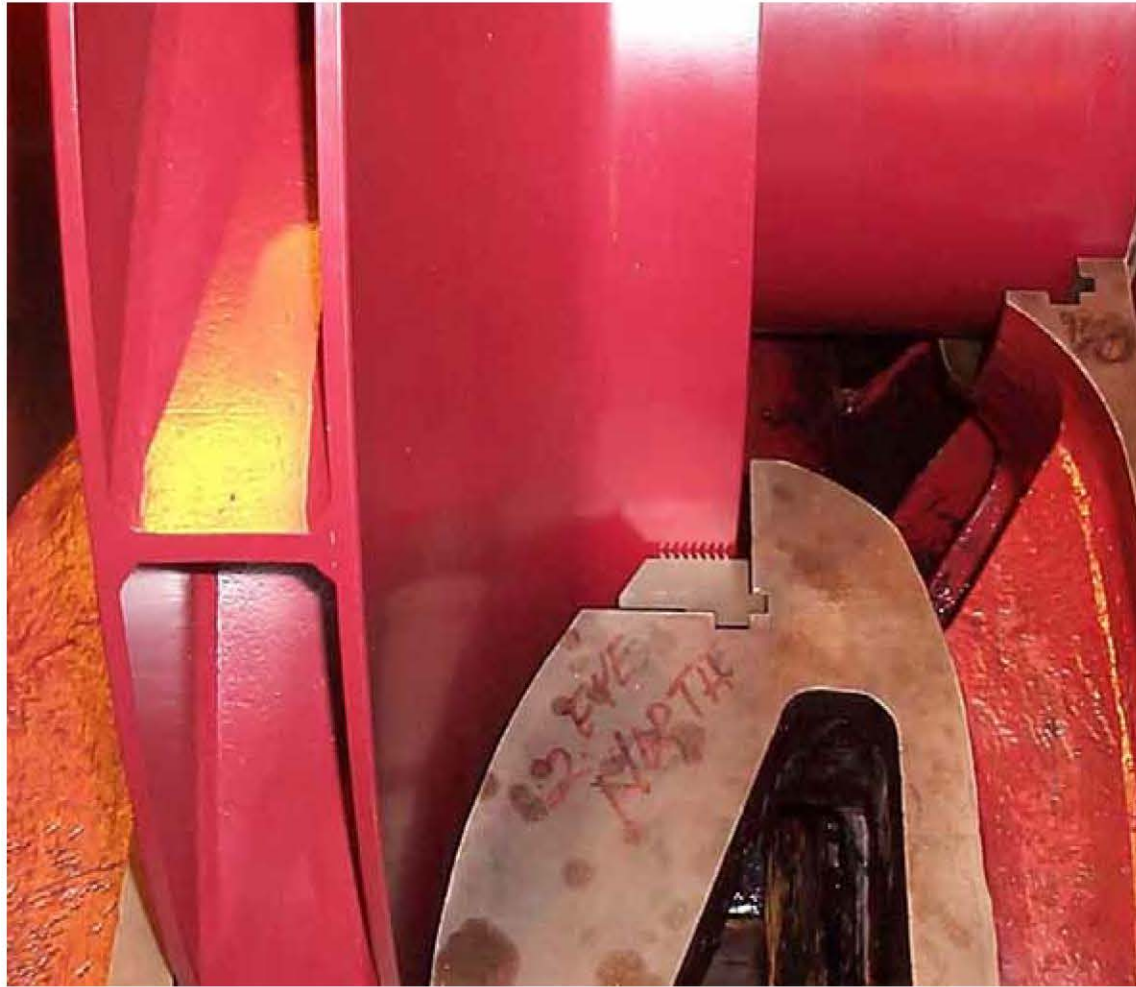
Texas Ethylene Plant

- n Introduction to polymer seals
 - q Started investigating early 1990's
 - q Talked to several users
 - q Decided to upgrade and evaluate one compressor
 - n 10,000 hp booster
 - n Upgraded in 1997

Texas Ethylene Plant

- n Booster compressor
 - q Plant can run w/o booster
 - q Used 3% efficiency upgrade for justification
 - q Installation went smoothly (only real work performed that would effect efficiency)
 - q After upgrade realized:
 - n 3.1% flow increase
 - n 2.7% steam flow reduction
 - q Decided to upgrade remaining compressors

⁶⁰⁰ New Polymer Seal–Newly Coated Rotor

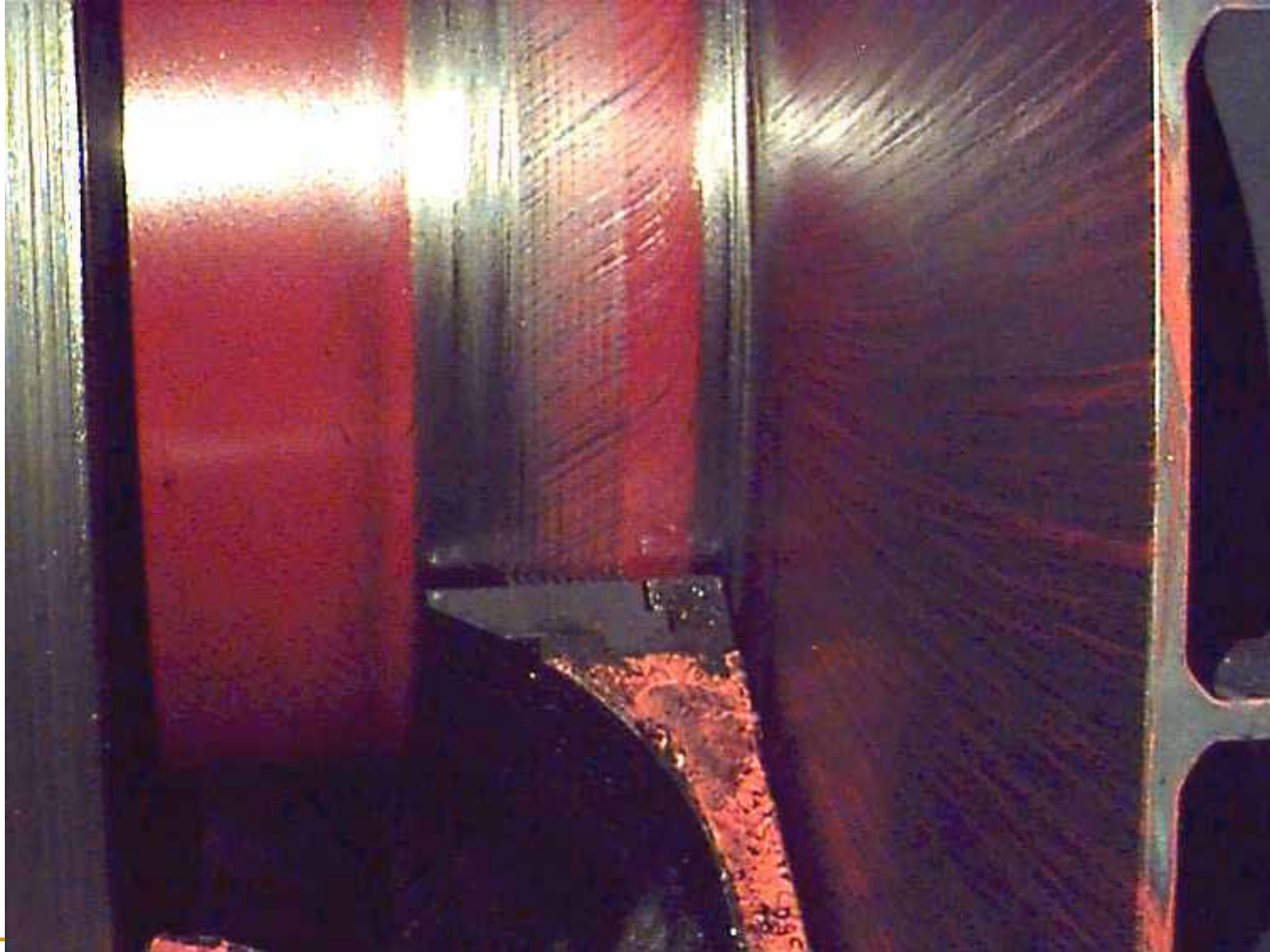


⁶⁰¹ New Polymer Seal–Newly Coated Rotor



Texas Ethylene Plant

Used Booster Compressor Shaft Seal



Texas Ethylene Plant

Used Charge Gas Compressor eye Seal



⁶⁰⁴Texas Ethylene Plant

- n Fouling more of an issue at this facility
 - n Replaced charge gas seals in 2003 and 2008
 - q Too fouled and could not clean
 - n Inspected and reused refrigeration compressor seals in 2008
 - q Very clean service
 - q 9 year run (since 1999)
 - q Seals “in spec”
-

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Texas Ethylene Plant

Conclusions

- n It is estimated that overall plant capacity increased 5% due to the polymer seal upgrades
 - n Reliability increased due to forgiveness of polymer seals compared to aluminum
 - n Plant is extremely pleased with this upgrade project
-

606 Conclusion

- n The cases presented here represent up to 15 years of experience running polymer seals in critical turbomachinery.
 - n Analysis of material removed from service after 9 years demonstrated very low levels of material degradation.
 - q Indeed other seals were reinstalled and will run for another 6 years or longer before being reevaluated.
-

⁶⁰⁷Thermoplastic Seals

- n Labyrinth Seals
 - n Thermoplastics
 - n Engineering an Upgrade
 - n Upgrade payback calculations
 - n Case Histories
 - q Canadian ethylene plant
 - q Texas ethylene plant
 - n Conclusions
-

**DISCUSSION GROUP T1
ON
TURBOMACHINERY OPERATION AND MAINTENANCE**



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Dr. Kurz attended the University of the German Armed Forces, in Hamburg, Germany, where he received the degree of a Dipl.-Ing., and, in 1991, the degree of a Dr.-Ing. He was elected as an ASME Fellow in 2003.

Joe Moreno, Coordinator



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