

**EXPERIMENTAL STUDY ON SUPPRESSION CHAMBER THERMAL-
HYDRAULIC BEHAVIOR FOR LONG-TERM REACTOR CORE ISOLATION
COOLING SYSTEM OPERATION**

A Dissertation

by

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ABSTRACT

In current Station Blackout analyses for Generation II Light Water Reactors, battery failure in 4-8 hours is expected to result in the failure of the Reactor Core Isolation Cooling System. The RCIC System, which uses a steam-turbine driven pump to pump cooling water to the reactor, theoretically requires DC power for the controller to operate. However, in the Fukushima Daiichi accidents at Units 2 and 3, the RCIC System performed for much longer than expected. It managed to continue working long after the loss of critical DC power, even without operator intervention.

In order to better understand the RCIC System and Suppression Pool in long-term system operation, a model of the system was constructed at the Laboratory for Nuclear Heat Transfer Systems at Texas A&M University. This experiment investigated the thermal hydraulic limitations of the RCIC System, focusing on the Suppression Pool. In 32 individual tests, several parameters were varied; these included the steam flow rate, the steam quality, the sparger design, and the pressure conditions in the Suppression Chamber.

It was found that the Suppression Pool, with a strong dependence on conditions, can experience a great deal of thermal stratification resulting from RCIC System operations. Such stratification can be both beneficial and limiting; pump suction from the bottom of the pool will be cooler when stratified, protecting the pump, while at the same time containment pressurization will be accelerated. Chugging at the beginning and bubbling later on tended to enhance pool mixing while calm conditions in the

intermediate period tended towards stratification. A chugging correlation has been adapted and modified to describe the state of mixing in the scaled pool.

The SRV-analog tests had little to no effective thermal stratification in the Suppression Chamber, whereas every RCIC-analog test had some. Pressure in the Suppression Chamber in particular was strongly associated with the degree of stratification; one pressurized case had >65 °C of thermal separation, while a similar but fully-vented atmospheric case saw only 13 °C. While steam quality and steam flowrate affected the thermal stratification, their effects were neither as pronounced nor as simple as those of the pressurization conditions.

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NOMENCLATURE

AP	Absolute Pressure
β_p	Vapor Pressure Ratio, = $(P_{\text{vap}} / P_{\text{tot}})^{0.5}$
BWR	Boiling Water Reactor
DAQ	Data Acquisition [System]
DCC	Direct Contact Condensation
DI	Deionized/Deionization [Water]
DP	Differential Pressure
Fr_s	[Steam Injection] Froude Number
Ja_{TP}	Two-Phase Jakob Number
KP	Key Point [#]
NPS	Nominal Pipe Size
NRC	[United States] Nuclear Regulatory Commission
RCIC	Reactor Core Isolation Cooling [System]
RHR	Residual Heat Removal [System]
SBO	Station Blackout
SRV	Safety/Relief Valve
TDP	Turbine Driven Pump

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1. INTRODUCTION

On March 11, 2011, the Great East Japan Earthquake struck off the eastern coast of the Japanese island of Honshu. The magnitude 9.0 temblor spawned a massive set of tsunamis; the earthquake and tsunami officially resulted in 15,889 dead, 6,152 injured, and 2,598 missing people [1]. The immediate damage has been estimated to be \$300 billion, with significant long-term ramifications [2]. Also severely damaged was the Fukushima Daiichi nuclear power plant, which suffered widely-publicized accidents. The tsunami cut off all offsite electrical power and caused most of the on-site emergency diesel generators to fail; this, in turn, led to the failure of cooling systems and eventual core damage at Units 1, 2, and 3. Unit 4 suffered major damage as well [3].

In the course of events during the accident, one emergency cooling system applicable only to Units 2 and 3 functioned for time periods much longer than had been predicted in earlier analyses: the Reactor Core Isolation Cooling (RCIC) System [4]. The RCIC system is a turbine-driven system that takes steam from the reactor and passes it through said turbine to generate sufficient mechanical power to drive a pump; the pump sends water back to the reactor to maintain core cooling. While the system does not require large amounts of electric power for pumping, the system's controller does require some small amount of power. In current analyses, when the controller loses all electrical power, the RCIC system is assumed to fail. This is expected to happen in 4-8 hours in short-term station blackout scenarios as the station batteries are depleted and Suppression Pool temperatures rise; normally, “one should not expect the RCIC system

to run much beyond 8 hours in a station blackout (SBO)” [4]. However, the RCIC system in Unit 3 performed its duty for 19.5 hours before finally going offline; in Unit 2, the system ran for nearly 3 days, long after the station's batteries went offline [3]. It is not clear how or why the systems performed so well.

1.1 PROBLEM STATEMENT

The goal of this research is to investigate parts of a genericized RCIC system to gain insight into extended operations. In at least some cases, as evidenced by the Fukushima events, the system can perform much longer than anticipated. The focus will be on the thermal-hydraulic behavior of the Suppression Pool as it relates to RCIC System operation.

1.2 TECHNICAL APPROACH

This research intends to establish some of the physical thermal hydraulic limitations of the RCIC System, with a highlight on the interplay between the Suppression Pool and RCIC System. It will examine potential thermal stratification in the Suppression Pool, pump inlet conditions, and two-phase steam/water injection through the RCIC Sparger. While neither the control system nor an actual turbine will be examined, these tests are expected to yield certain phenomena that affect system operability. Once known, such data can be used in plant safety analyses to gain a greater understanding of the system, assist in the development of procedures in off-normal or accident conditions, and to inform decisions about modifications to improve overall plant safety.

The data gathered in the experimental tests will be subject to further analysis focusing on key locations. Their time-dependent conditions shall be examined and the evolution of their thermal-hydraulic profiles investigated. Ultimately, a correlation will be developed to relate the overall mixing state of the Suppression Pool, a key interfacing system affecting RCIC System operability.

2. BACKGROUND

The Reactor Core Isolation Cooling System is found in some, but not all, GE Boiling Water Reactors with the Mark I Containment. It was originally designed to ensure adequate cooling water is supplied to the reactor in isolation events; i.e., when the isolation valves are closed for the steam lines and feedwater. This results in the reactor, which produces significant amounts of decay heat long after shutdown, being isolated from the outside world – and its primary ultimate heat sink. In such an isolation event, the RCIC system is engaged. It draws steam from the reactor via the in-containment portion of the Main Steam Line, passes it through the RCIC Turbine's governor valve and then the turbine, and exhausts it through a sparger into the Suppression Pool [5]. The Suppression Pool in a BWR with the Mark I containment partially fills the torus, and can store a large volume of water – 76,000 cubic feet at Monticello [8], and more than 125,000 cubic feet at Peach Bottom [9]. It is inside the containment boundary. An illustration of the BWR Mark I Containment can be seen in Figure 1.

[5]. As there is no control valve past the pump to regulate water flow, regulation is performed by controlling the turbine speed with the throttling governor valve. In addition to these main flowpaths, there are several others for system support – system cooling, lubrication, hydraulics, etc. The cooling function is noteworthy, as cooling water is the same water supplied by the RCIC Pump [5].

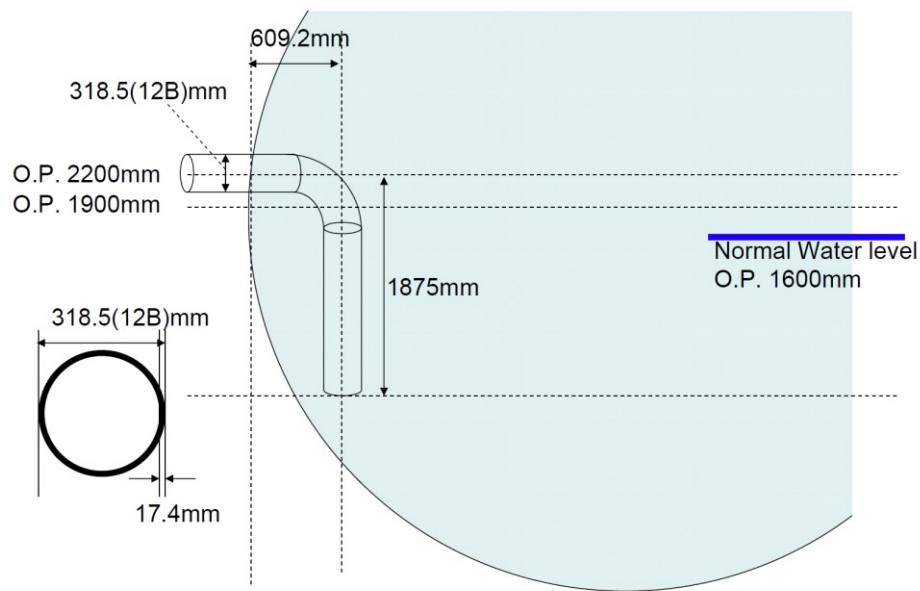


Figure 2: RCIC Turbine Vent Line from Fukushima Daiichi Unit 2 [6]

The outlet into the Suppression Pool is a sparger that appears to be unique for each plant. Based on information made public by TEPCO, the sparger design may even differ from unit to unit at the same plant; this was the case at Fukushima Daiichi. There do, however, appear to be generic classes of design employed. The simplest is a vertical pipe, open at the end, pointed downwards and depositing steam well below the surface

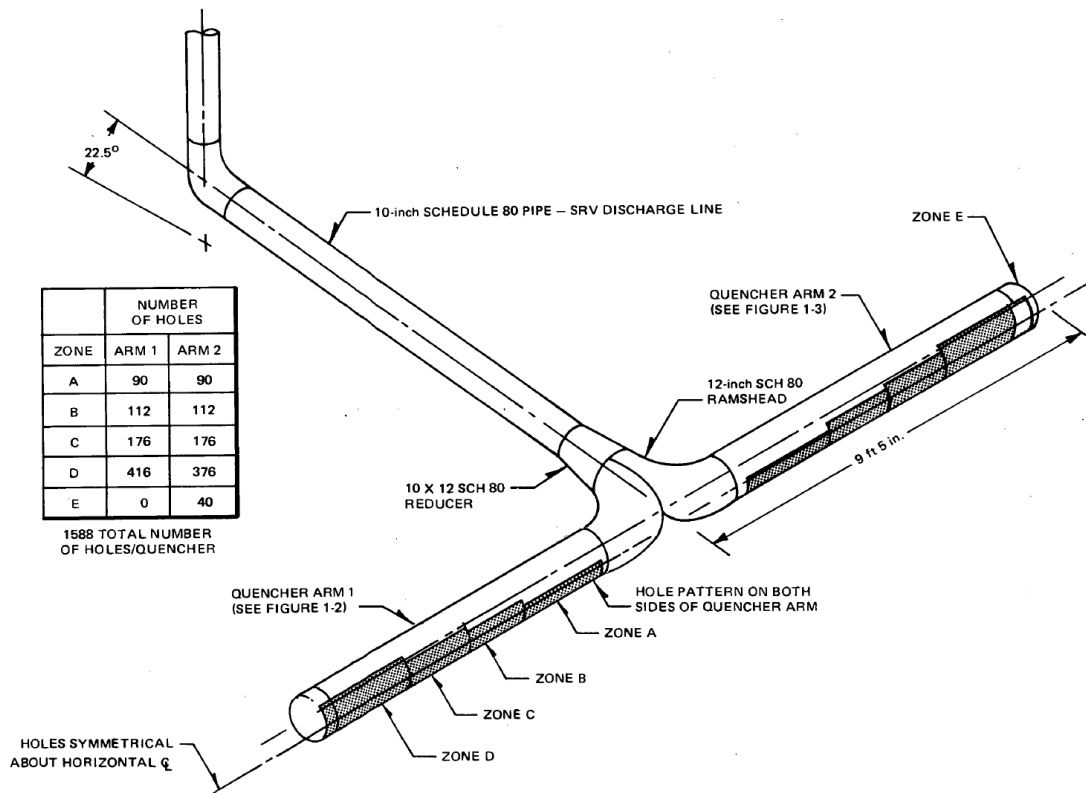


Figure 4: Monticello T-Quencher [8]

In addition, the relative positions of spargers and suction inlets in the Suppression Pool are unclear, and may have a high degree of plant dependency. If, for example, the RCIC suction draws from a part of the Suppression pool in the immediate vicinity of the SRV T-Quencher with the lowest opening setpoint, then it may attempt to draw water into the pump from a localized hot spot. Other thermal stratification issues may come in to play as well.

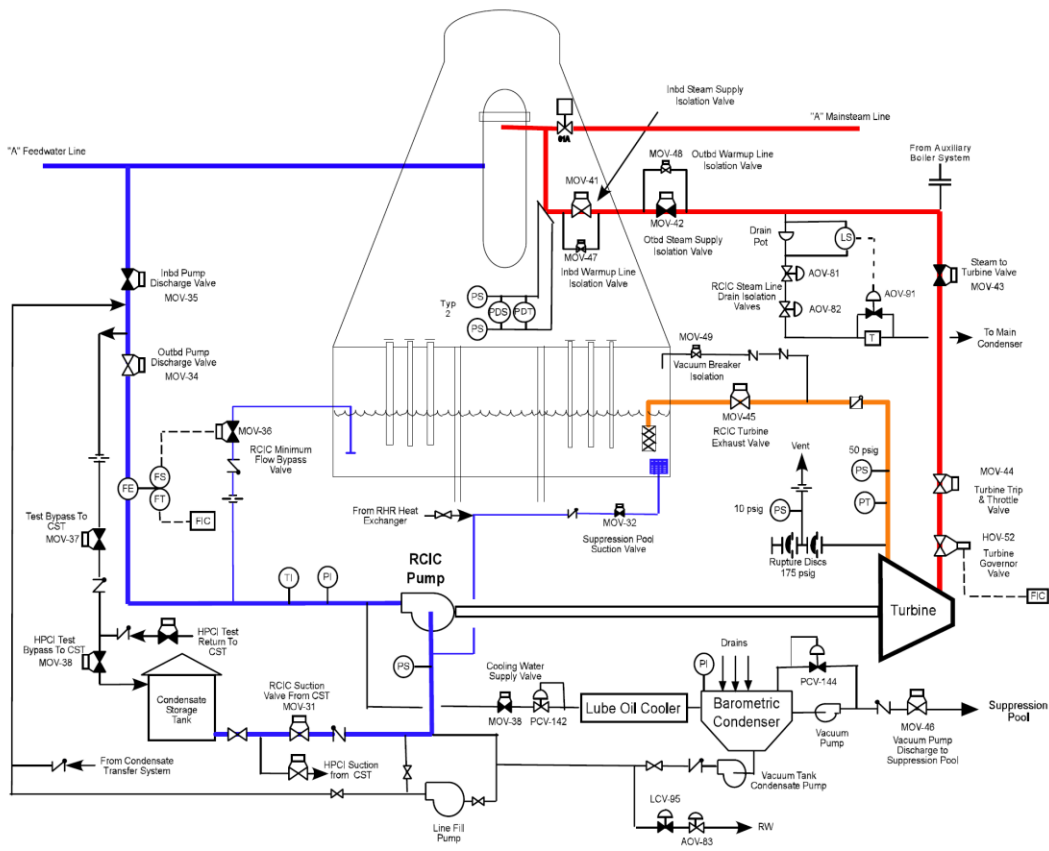


Figure 5: RCIC System in a BWR Mark II Containment [12]

No AC power is required to start or operate the system; only DC power is necessary to operate the system controller [10]. Without DC power, the controller is expected to cause the turbine governor valve to open fully. Given sufficient steam pressure, this would result in the turbine accelerating until an overspeed condition is reached. At the turbine overspeed setpoint, a mechanical turbine trip system is actuated, which shuts off flow into the turbine. The mechanical overspeed trip does not reset itself; once it trips, an operator needs to physically reset it [10]. In existing analyses, this is a

major limiting condition. In station blackout (SBO) scenarios, the station batteries are predicted to be depleted in 4-8 hours after the loss of all AC power; this will leave the RCIC controller without a viable source of DC power.

There are two major capacities for RCIC systems installed in existing plants, and between them 400 to 800 gpm of makeup water can be supplied [10]. Both small and large sizes are designed to be able to supply sufficient cooling water to the reactor from shortly after reactor trip when the system is at high pressures and temperatures (1150 psi at saturation temperature) down to much cooler, lower pressure states (150 psi, saturated) [5].

2.1 RCIC CONTROL LOGIC

The RCIC System control logic is described here because it influences experimental facility operational procedures. The system, by design, will automatically start when a reactor vessel low-low water level signal is received after a reactor shutdown is initiated [5]. It can also be started manually from the control room, or physically by operators acting directly on the equipment using “blackstart” (system startup through the manual/physical alignment of valves and direct local control of system components by operators in the absence of electrical power) procedures.

Operation of the RCIC system will generally be expected to continue until a trip signal is sent to the turbine. There are 5 such automatic signals that come in to play: high reactor vessel water level, turbine overspeed, low pump suction pressure, high turbine exhaust pressure, and an Auto Isolation Signal [5]. Each of these signals require DC power to operate correctly. The overspeed trip can occur as a control signal that

closes a steam valve with the ability to remotely reactivate the system, or as a mechanical overspeed trip (at a higher setpoint) that, once actuated, requires operators to physically reset the trip on the turbine after actuation before the system can start once again. All the remaining trips, with the exception of the high reactor water signal, will require operators to reset the system before it restarts. The high reactor water level signal allows the system to automatically restart once the level again drops to the low-low mark without any operator intervention [5].

In addition to the automatic signals, operators can take more direct control of system operation. They are given controls to manually set a desired output flowrate or turbine speed; not only can they control the system from the control room, but a local hand wheel on the trip and throttle valve for the turbine allows operators to physically control the steam flow into the turbine [10].

The ability for such manual, physical control can be an important feature, especially when electrical power sources are unavailable. The governor systems appear to have been designed with this in mind, and upon loss of electrical power is set to have the governor valve open fully. At that point, it is intended for an operator to locally take over the control functions using the trip and throttle valve if an overspeed trip is to be avoided [10]. This is achieved in the way the electro-hydraulic control system is designed. A certain non-zero voltage (-.75 to -1.00 V DC) is required to be present on the actuator terminals in order to maintain the pilot valve at its centered, steady-state position. When the voltage disappears, springs move it slightly to allow oil to flow to the remote servo, opening the governor valve; eventually, it will open fully [10].

2.2 TERRY TURBINES

The RCIC system employs a non-condensing Terry turbine as produced by Dresser-Rand, formerly the Terry Steam Turbine Co. A Terry turbine resembles a simple water wheel or Pelton wheel, and was developed in the very early 20th Century. It is an impulse-type turbine with jet and reversing chambers mounted on the casing, and “buckets” milled into the outer end of a rotating wheel [10].

2.2.1 Terry Turbine Design

Steam passes through the turbine's governor valve, and proceeds to enter the turbine assembly. It is accelerated through a nozzle, transforming some of its enthalpy into kinetic energy. Almost the entirety of the pressure drop in the turbine is across the nozzle; the more it accelerates the flow, the more efficient the turbine becomes. A converging-diverging nozzle designed to accelerate steam to supersonic conditions is, therefore, well suited to the turbine. The nozzle directs the flow to be nearly tangential to the rotating wheel and into U-shaped buckets milled into it. The flow imparts energy to the wheel as it is redirected at the bottom of the bucket and turned around. Upon departing the bucket, the flow enters a series of one or more reversing chambers on the stator assembly. The reversing chamber redirects the flow back towards the wheel, and into a subsequent bucket [10]. After the set of reversing chambers, the steam is released into the casing space, and exhausted from the turbine. Historically, there were usually four reversing chambers for each nozzle assembly, and 4 to 8 nozzle assemblies in the turbine [13]. Terry turbines are illustrated in Figure 6 and Figure 7.

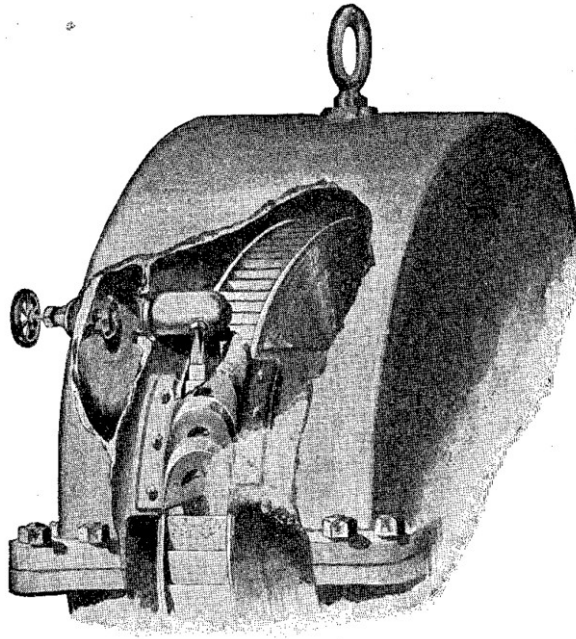


Figure 6: Terry Turbine with Steam Jet [13]

Non-condensing turbines such as the Terry turbine are not efficient turbines; they do not take advantage of the massive amounts of energy stored in steam's latent heat. In emergency systems such as the RCIC system, efficiency is not an important characteristic, and constitutes a lower priority than ruggedness or functionality. It does not initially consume a large fraction of the steam generated by the reactor; the majority of the generated steam will be dumped by the relief valves into the Suppression Pool. The RCIC system is sized to provide sufficient makeup water to replace that which boils off; it is not intended to maintain reactor water levels when significant leakage (pipe breaks) is present [5], [10].

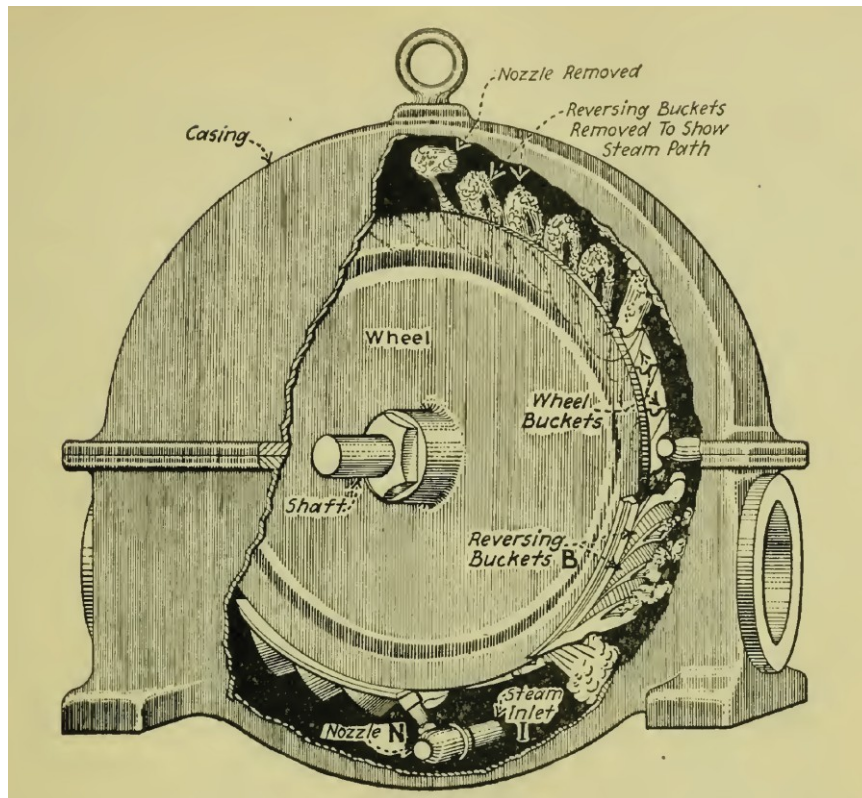


Figure 7: Terry Turbine Steam Path [14]

2.2.2 RCIC Turbine

The RCIC Turbine is designed to operate across a wide range of input conditions. The turbine wheel has a nominal diameter of 24 inches [10], and has different numbers of steam inlets and jet/reversing chamber assemblies based on the required power output. The two different RCIC size classes use the same turbine wheel, but different casings. The smaller casing allows for up to five jet-reversing chamber assemblies, while the larger casing allows for up to ten [10]. The wide operating range places high demands on the controller; successful operation of the system requires the controller to be responsive and well-maintained [10]. This is the result of significant amounts of excess

mechanical power supplied by the turbine under some conditions; the turbine is designed to supply sufficient pump power from inlet steam pressures of 100 to 150 psi. When greater pressures are supplied, up to more than 1150 psi, “the turbine is capable of several times the rated horsepower” [10], and therefore the controller must be well-designed in order to maintain system operability and stability. Startup transients are an important consideration in the design, as the system must go from stopped to full rated flow in 30-90 seconds.

Documentation shows that the valve for the turbine's mechanical overspeed trip can double as a throttling control valve; it is a trip and throttle valve independent of the governor valve. However, based on Electric Power Research Institute (EPRI) diagrams of the mechanical overspeed trip system, it would appear that the mechanical trip cannot provide regulating functions. It instead appears to be a two-state system: ready, and tripped [10], [11]. Rather, the throttling function is provided by a local valve hand wheel on all systems, as well as an electric motor on some [10].

2.3 RCIC SYSTEM RELIABILITY

The RCIC system has limitations beyond DC power failure. Some potential limitations may not be immediately apparent. One potential avenue of interest, not actively pursued here, involves the system's lubrication oil. The RCIC turbine-driven pump (TDP) assembly and associated plumbing constitutes a containment boundary, and sits in a shielded room in the reactor building. Cooling to that room may be limited in some scenarios. In prolonged operation of the system, the ambient temperature may rise to a high enough temperature that the lubrication cooling is insufficient (if cooling is

based on room temperatures; in Peach Bottom, cooling is based on pump inlet water [5]); the lubricant would then heat up. If hot enough, it could be unable to perform its functions correctly. As a result, the bearings and seals could fail, halting operation of the system.

As the heart of the system is the RCIC Turbine and Pump assembly. It can logically be expected to have limitations similar to other TDP systems: valve misalignments, pump cavitation or deadheading, turbine damage, lubricant problems, seal failure, air ingress, etc. The turbine, a Terry turbine, is considered to be very robust; however, even without damage, the system may not perform in severely off-normal conditions.

In fact, the system may have difficulties performing in relatively normal conditions. In 2000, a study was published examining the performance of TDP systems in nuclear power plants. It found that, in the 1987-1998 period, RCIC turbine driven pumps in BWR plants had a mean probability of failure on demand of 2%; from 1987-1995, the mean failure rate was $1.3E-5$ /hour [15]. The vast majority of failures, 70%, were in the governor. The turbine accounted for 27%, and the remaining 3% was in the pump. Overall, the causes of the majority of failures were age/wear (30%) and maintenance/procedures (27%). A significant (23%) fraction of failures had undetermined/unknown causes. The remainder of the causes of failure were dirt/contamination (7%), design defects (10%), and other (3%) [15].

The high proportion of failures related to the turbine is somewhat surprising, given that the Terry turbines are designed to be very robust. Testing has been performed

in the past, and they were found to be fairly rugged. When high fractions of water are injected into the steam flow, a condition that can damage turbines not built to withstand it, the water spraying out of the Terry turbine exhaust made an impressive display for the investigators. However, the turbine itself, in post-excursion disassembly and inspection, was found to be completely unharmed [16].

Mechanical and power failures are not the only adverse conditions facing RCIC systems; operational conditions should be considered as well. These include out-of-bounds or incorrect control signals from the control room (for example, incorrect start/stop signals) and hostile inlet/outlet conditions for both the turbine and pump. For example, the switchover from the Condensate Storage Tank to the Suppression Pool for pump suction may fail, and there may be insufficient net positive suction head or vapor could then be drawn into the pump. The pump suction may draw water at temperatures too close to saturation, either from a localized hot spot in the pool or an overheated pool, and then give rise to pump cavitation. Alternately, there may be too little driving pressure for the turbine, too much back pressure, or liquid may enter the turbine inlet. This is not expected to damage the turbine, but its performance may suffer.

If water slugs are present, the governor may be unable to compensate for rapid speed changes fast enough, and the turbine could experience an overspeed trip; the controller has historically had difficulties with more than 1% moisture content [10]. At higher moisture contents, the performance of the nozzles can be expected to suffer; they are not jet ejectors intended to operate with two-phase flow. Interestingly, two-phase flow through jet ejectors is under consideration to *enhance* the efficiency of refrigeration

cycles [17], which might provide some insight into the two-phase behavior of traditional nozzles. In addition, conditions in the turbine exhaust sparger in the Suppression Pool may generate hot spots in the pool, or possibly cause flow disruptions. Rapid condensation in the exhaust line may have only limited impacts in system operation, as there are both check valves and vacuum breakers installed to prevent the development of major vacuum conditions in the line [5].

2.4 DIRECT CONTACT CONDENSATION

When steam comes into contact with subcooled water, it will tend to condense. Given sufficient water subcooling and steam purity, the steam can condense very rapidly, even violently. This method of condensation, called Direct Contact Condensation (DCC), has been employed by the nuclear industry in a number of safety systems, including the RCIC System. As a result, interest in the subject has been more than simply academic; comprehending the complex phenomena that can present in it is important for a complete understanding of the operation of such systems, making it important for plant safety.

A number of efforts have been made to classify, categorize, and correlate the phenomena seen in DCC systems. Some treatments, both experimental [18] and analytical [19], have examined stratified/separated flows, while others have investigated vapor injection into pools. With steam injection into a pool, published results tend to find it “difficult to analyze the DCC phenomena around the sparger by simple analyses due to its geometrical complexity and complicated flow patterns” [20]. There is an apparent sensitivity to the design of experimental facilities in the results relating not just

to the sparger design and orientation, but also to the steam injection feedback (a “hard” steam injection rate being fixed, while “soft” steam injection responds to pressure transients); some systems can experience severe water hammer issues [21]. Some tests have focused on pressure pulses from violent condensation and their potential effects on structures, such as those in [22]. A common line of inquiry involves the effective heat transfer coefficient. Others involve pool circulation patterns (such as [23]), and some explore steam plumes from a variety of outlet sizes and orientations as in [24].

Upon inspection, a number of DCC regimes have been identified by researchers in the field. Notably, these studies have limited to no examination of the effects of system pressurization (limited rather than nonexistent; for example, Celata et al. did investigate pressurization [18]), saturated two-phase steam-water injection, or extensively superheated steam injection in DCC systems. In the de With study [25], it was reported that 15 different regimes have been identified, and for the sake of simplicity were grouped into seven regimes. Each regime is identified by broadly similar shapes, locations, and behaviors of the steam/water interface. In traditional regime maps, the key variables are steam mass flux and bulk water subcooling; the de With maps add the diameter of the steam injector as a third variable; this showed the transitions between often significantly different regime maps and resolved some of their noncorroborating features.

The regimes include variants of chugging, bubble, and jet regimes. In the traditional regime map established by Chan and Lee (presented in Figure 8) [26], seven separate regimes were established; one, the chugging regime, was further subdivided

into three regions. At high steam fluxes, they identified two jetting regimes; one at low pool temperatures which was unstable and showed steam bubble detachments, and another at high pool temperatures which showed no bubble detachment. At sonic conditions, the steam jet was very stable. When they reduced the steam mass flux, the conical jet shape of the steam bubble at the exit of the vent tube (vertically downward in their tests) became more bubble-shaped, resembling ellipsoids, and had frequent detachments and oscillations in both warm and cool pool temperatures. Even lower steam mass fluxes demonstrated chugging:

“Further reduction in the steam mass flux caused the point of detachment to occur closer to the pipe exit and ultimately right at the exit. This was taken as the boundary for the steam chugging regime, because the vapor region could only exist periodically in the pool, and the pool water would periodically enter the pipe” [26].

Chugging was noted to cease as the pool warmed up; at that point, an oscillating bubble formed around the pipe exit. Greater pool temperatures, as it approaches saturation, limits condensation and allowed steam to escape from the pool surface [26].

Chugging is associated with (sometimes large) rapid drops and subsequent rises in pressure in and in the immediate vicinity of a submerged vent tube. Damped “ringout” oscillations follow the initial spikes; these are associated with the presence and radius oscillation of small gas bubbles in the pool [27].

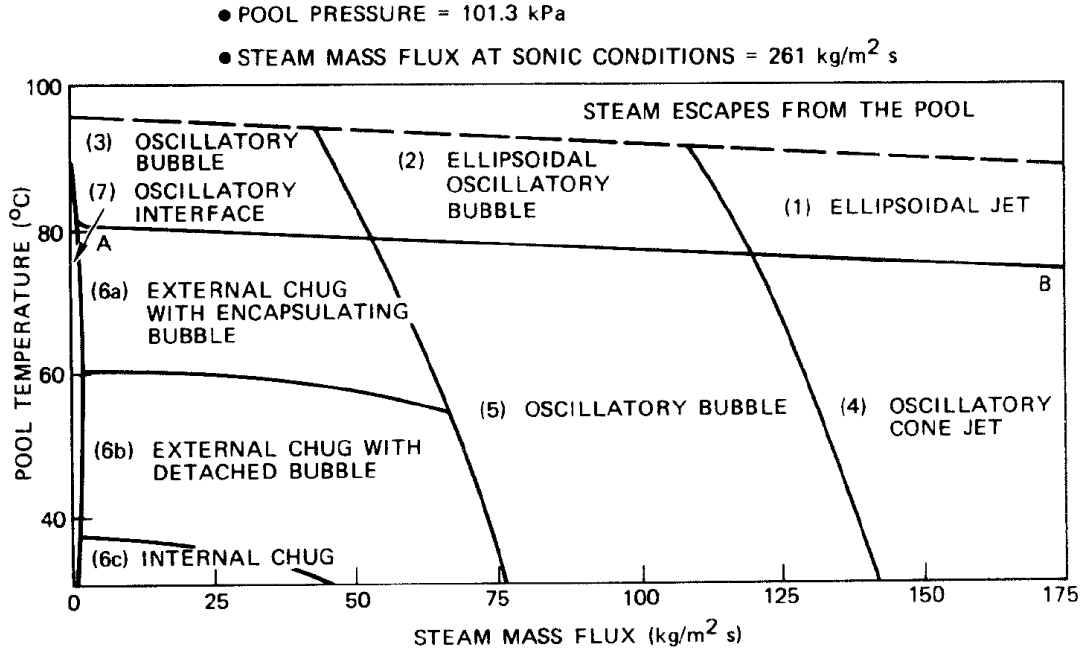


Figure 8: Chan and Lee DCC Regime Map [26]

Another DCC regime map was assembled by Aya and Nariai [28]. In conjunction with their experiment, they developed correlations defining the boundaries of the regimes in their map. Their proposed analytical approach produced regime boundaries that, in some parts of the map, began to diverge from the experimental results. Further complicating matters is their use of a significant header volume between the main flow restriction and the vent tube; this volume appears in the correlation, and the correlation is resultingly unclear in its applicability to systems without such a header. The correlations presented tended to be complicated; the boundary between condensation oscillation and chugging was given as Eq. (1) [28] in terms of pool subcooling, where the Hodgson Number in the experiment, N_H (a derived time constant

for oscillating bubbles divided by the measured pulsation period), was determined to be 0.44. Thermal conductivity was expressed as λ , and ξ expresses a coefficient of flow resistance. It was based on a previous empirical correlation involving oscillating condensing bubbles. The regime map is given in Figure 9.

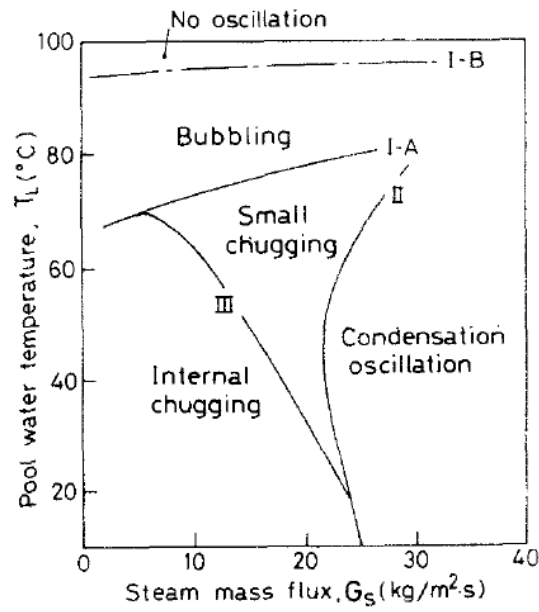


Figure 9: Aya and Nariai DCC Regime Map [28]

$$\Delta T_T^{2/3} = K \left(\frac{\rho_s}{G_s} \right)^{1.3}$$

where

$$K = \frac{N_H}{1.54 \xi \{ \}^{1/3}} \quad (1)$$

$$\{ \} = \frac{C_{PL} \lambda_L \rho_s^{0.9} \left(\frac{\partial \rho_s}{\partial p} \right)^2 \left(\frac{V_D}{\frac{\pi}{4} d_V^2} \right)}{L^2 \nu_L^{0.9} \rho_L^{1.9} d_V^{2.1}}$$

Liang and Griffith [29] produced a DCC regime map with correlations as well. In comparison with other regime maps, the Liang and Griffith maps were largely expressed in terms of the analytical correlations produced in their research. The presented relationship for the transition between chugging and bubbling/jetting was remarkably different from that of Aya and Nariai; it was much simpler and expressed in terms of (not entirely standard uses of) standard thermofluid nondimensional numbers.

The Liang and Griffith expression for the chugging regime is given in Eq. (2) [29], and expanded/restated in Eq. (3) at the regime boundary in terms using definitions of the nondimensional numbers compatible with those herein, and was based on a transient conduction model. It was noted that the model applies to horizontal injection, and that vertical downward injection, owing to the effects of buoyancy, required less steam to transition past the chugging regime. They also investigated the effect of noncondensables in the steam, and found that even small amounts were effective at preventing chugging; this can be seen in Figure 10 [29].

$$0.06 \text{Re}_{sw}^{\frac{1}{2}} \text{Pr}_w^{\frac{1}{2}} \text{Ja}_{dens}^{-1} \leq 1 \quad (2)$$

$$0.06 \text{Pr}_w^{\frac{1}{2}} \left(\frac{\mu_s}{\mu_w} \right)^{\frac{1}{2}} \left(\frac{\rho_s}{\rho_w} \right)^{\frac{1}{2}} \text{Ja}_w^{-1} \text{Re}_s^{\frac{1}{2}} = 1 \quad (3)$$

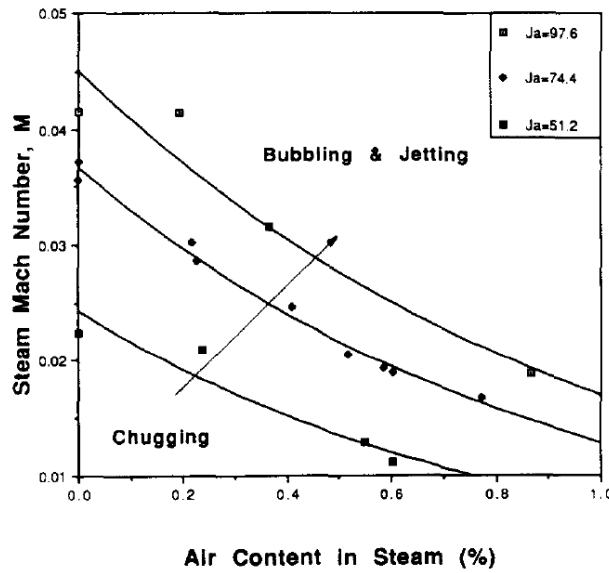


Figure 10: Influence of Noncondensibles on Chugging [29]

From these previous efforts, it can be seen that system differences can play a major role in the resultant DCC regime map. This can limit the applicability of the maps to systems that have a great deal of similarity, including scale. This is a disappointing result, as the chaotic fluid motions chugging can be very effective at dispersing material.

2.5 THERMAL STRATIFICATION IN THE SUPPRESSION POOL

Thermal stratification in the Suppression Pool may or may not be a problem from the consideration of plant operations; this has yet to be determined. There is, however, some evidence that it can exist [8], [30]. It is more than the presence of hot or cold spots in the pool; it is the bulk presence of significantly different temperatures over significant regions in the pool. For the purposes of this research, it can be said to be expressed vertically, horizontally/laterally, or in any irregular shape. Due to the difference in density between warm and cold water, vertical stratification is expected to be more stable than longitudinal expressions. However, that does not preclude the potential for such stratification; the pool is a very large body, and transient conditions may persist for long periods.

Stratification may be an issue for several reasons. If, for example, pumps draw water from the warmer regions, then they may exceed their inlet constraints earlier than expected from a consistent bulk pool temperature. Conversely, if they draw from relatively cool regions, they may operate longer than expected. Furthermore, when heat is injected into a stratified, warm region, the heat is effectively being absorbed by a smaller volume of water than anticipated. The parts of the pool that remain cool essentially do not participate as much or, in severe cases, at all in the thermal loading. It may seem as if large parts of the pool are absent. In such cases, it may fail to fulfill its pressure suppression/steam condensing functions early as uncondensed steam would begin to escape from the pool surface, and lead to pressurization of containment much quicker than predicted in analyses. In addition, attempts to condense steam in regions

with out-of-specification temperatures may lead to instabilities and large, potentially damaging, vibrations as in the 1972 Wurgassen incident [31].

There have been some investigations that shed light into stratification in the Suppression Pool. Tests at the Monticello Nuclear Generating Station were conducted circa 1978 to examine pool mixing with and without modifications to T-quencher devices and to RHR lines. Monticello has a single 2004 MWth BWR/3 reactor with the Mark I containment [32]. Its Suppression Pool has a limiting water volume of 76,000 cubic ft; tests were performed with 69,000 cubic feet [8].

Without RHR operation, it was found that steam flow through unmodified T-quenchers resulted in significant vertical pool thermal stratification; a temperature difference from pool top to bottom of 52 °F was observed at the end of the steam injection [30]. When the RHR was engaged, the pool's thermal stratification disappeared.

Further testing used modified T-quenchers. These had holes bored into one end with the aim of inducing circulating currents in the Suppression Pool from SRV discharges; modifications with the same end goal were made to the RHR system as well. Test results found that, without the RHR, the modifications to the T-quenchers was sufficient to cause a degree of pool circulation after a few minutes. Tests with the modified RHR system revealed that the modifications induced “considerable pool mixing” [8]; it was so significant that within 6 minutes of the end of steam injection, the pool came to an essentially uniform temperature.

These full-scale tests demonstrate the effects of injector geometry for steam injection into the Suppression Pool. Given an appropriate injector/sparger design, the Suppression Pool can be thoroughly mixed in all directions via steam injection.

2.6 FUKUSHIMA DAIICHI RCIC PERFORMANCE

The RCIC systems in Fukushima Daiichi Units 2 and 3 performed their duties in a very challenging situation. They both operated much longer than expected, and did so without any electrical power or operator intervention for a prolonged period.

In Unit 2, the RCIC system initially started and stopped as designed on reactor water levels. The tsunamis generated by the earthquake began to reach the plant 41 minutes after the earthquake; by 55 minutes after the quake, parts of the building had flooded. This resulted in the eventual loss of all AC power as diesel generators went offline, and most DC power as the distribution system was damaged. The RCIC system had been restarted by operators about the time the first tsunami hit the plant, and subsequently continued operating until its ultimate failure. Workers were sent to the RCIC room to verify operation on multiple occasions, but were unable to examine the RCIC system in detail or even approach the equipment as the room itself was partially flooded. After a number of hours, the RCIC source was realigned from the Condensate Storage Tank to the Suppression Pool. Eventually, the Suppression Pool's indicators revealed that it had reached saturation. By 70.5 hours after the earthquake, trends in reactor water levels revealed that the RCIC had failed. All told, it operated for nearly three days, and did so largely without available DC power or operator direct intervention

[3]. In addition, the reactor had not depressurized; it remained at high pressure until it was depressurized manually to initiate seawater injection [4].

The RCIC system in Unit 3 initially behaved as in Unit 2. It started and stopped normally as the designated water levels in the reactor were reached. However, not all DC power was lost after tsunami inundation; there was sufficient power and connectivity that operators were able to start RCIC operation after the tsunamis struck; the system was restarted 1.3 hours after the earthquake. The RCIC System shut down 20.8 hours after the earthquake after running for 19.5; operators were then unable to restore it [3]. Investigations have concluded that the system likely tripped on a high turbine exhaust pressure signal; sufficient DC power was available (albeit becoming unstable) for such signals [33]. As in Unit 2, the reactor in Unit 3 did not depressurize in the period of RCIC operation.

It is not clear why the RCIC Systems performed as they did, or what eventually caused the Unit 2 failure. It has been speculated that the Unit 2 reactor overfilled, and that spillover into the then-unregulated turbine provided an unintentional yet beneficial feedback control mechanism. The water injected into the turbine would degrade its performance, slow it down, and lead to less water being injected into the reactor. In turn, this would limit the spillover into the Main Steam Line and from there to the RCIC turbine. So long as any transients were slow and stable, this could potentially reach a stable operating point.

2.7 RECENT EXPERIMENTS

Testing has been done at the Lappeenranta University of Technology to explore the phenomena associated with a condensation pool, especially one of the type employed in the Olkiluoto BWR containment. A number of these POOLEX tests were performed, where the facility consisted of a vertical cylindrical vessel filled with water, into which steam is injected downward through a vertical tube open at the bottom. In the blowdown tests, full condensation in the blowdown pipe was observed at very low temperatures, which transitioned through chugging to condensation oscillation as the pool temperatures were increased [34]. Water hammer was observed in the tests, and stresses severe enough to cause plastic deformation in some components were estimated for some pulses.

Further POOLEX testing was done to study thermal stratification in the facility [35]. Strong vertical thermal stratification was observed in the water in the STB-20 test, peaking at a difference of 37 °C difference from pool top to bottom when the steam was shut off. The steam flow was not constant during the test, but gradually reduced to maintain condensation within the pipe rather than outside it in the pool. The pool temperatures are illustrated in Figure 11 [35].

POOLEX data have been used as benchmarks. Test STB-31, for example, was simulated in CFD to compare different codes and DCC models, finding differences of a full order of magnitude for the condensation rate [36].

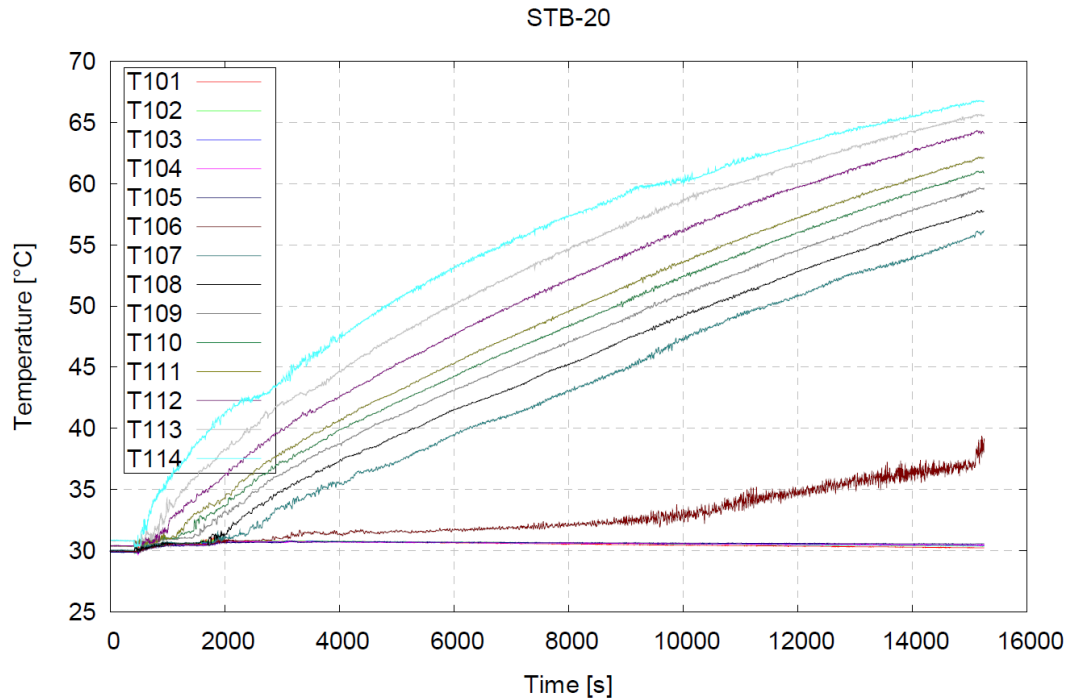


Figure 11: POOLEX STB-20 Stratification Test Pool Temperatures [35]

More recent testing at the Lappeenranta University of Technology has used the PPOOLEX facility [37]. It shares some similarity to the POOLEX facility, but models more features of containment. Notably, the vessel is separated into a drywell and wetwell, and the drywell is vented to the wetwell through the blowdown line. Thermal stratification was found to be significant, but had a slightly different development than the most comparable of POOLEX stratification tests [37].

Additional recent studies in Japan at the University of Tokyo demonstrated the potential for transient thermal stratification in the Suppression Pool with spargers based on the RCIC turbine exhaust discharge. These, however, were conducted in a scaled facility rather than a full-size power plant. Numerical and experimental data showed a

fair amount of vertical stratification near the injection point [38]. Early on during steam injection, low points in the pool maintain a near-constant temperature. With a more pronounced vacuum and varying flow rates, the thermal stratification profile changes. A high steam flow rate produced little stratification in the test chamber. At a more moderate rate, stratification only appeared after a fair amount of thermal energy had been injected into the pool; it later vanished as the bulk temperature increased. At low injection rates, stratification was apparent from almost the beginning of the test. Then, towards the end of the test, the stratification disappeared in stages: first, the higher-elevation temperatures jumped to the top-level temperatures, then, progressively, the lower-level temperatures did the same [39].

Another set of experiments has been performed at the Società Informazioni Esperienze Termoidrauliche (SIET) laboratory in Italy. Those tests focused, among other (less-related to this work) areas, on the RCIC sparger designs rather than the complete system and Suppression Pool, and explored the effect of the presence of noncondensibles in the exhaust flow. The open-bottom (Fukushima Daiichi Unit 2-style) sparger had a diameter of 20 cm (vs. 28.3 in Unit 2), and the tube was large when compared to the pool. The multiple-hole (Unit 3-style) preserved the hole sizes of the plant system, but reduced their number; the tube was similarly large when compared to the pool [40]. Those tests have an admitted distortion for pool circulating currents due to the limited pool dimensions and its shape.

Both sparger types in the SIET tests produced a measurable vertical dependence for the pool temperatures [40], [41]. The open-bottom type produced some stratification,

which was eliminated by the addition of 3% air to the steam flow [41]. The more complex (multiple holes with differing diameters venting solely from the side of the sparger) design produced significantly more thermal stratification. Chugging was found to end as the pool warmed up beyond 45 °C, at which point stratification began. Even as the pool (open to the atmosphere) approached saturation, the lowest portions of the pool in the SIET facility appeared to remain unmixed [40].

3. EXPERIMENTAL FACILITY DESIGN AND CONSTRUCTION

In order to investigate the operation of the RCIC System in BWR units with the Mark I containment, an experimental facility was designed and constructed at the Laboratory for Nuclear Heat Transfer Systems at Texas A&M University. In the RCIC System, steam from the reactor is drawn off of the Main Steam Line, directed through the RCIC Turbine, and exhausted into the Suppression Pool. The turbine, in turn, drives a pump on their common shaft. This RCIC pump draws water either from the Condensate Storage Tank or from the Suppression Pool and pumps it back to the reactor. This maintains the reactor's water level as decay heat in the core boils it off.

In the experimental facility, the alignment to draw water from the Condensate Storage Tank will not be explored in this endeavor; only the pump suction's alignment to the Suppression Pool will be considered. The experiment, therefore, is analogous to a RCIC system operating in its closed-loop mode in the long-term. The role of the reactor will be played by the laboratory's steam generator, which directs steam through a manual control valve (an analog to the RCIC Turbine's governor valve), through an analog to the RCIC turbine (currently an orifice), and through a sparger in a large pressure vessel analogous to the RCIC sparger in the Suppression Pool. A second sparger setup performs as an analog to an SRV. The Suppression Chamber analog and proximate equipment are shown in Figure 12.



Figure 12: Completed Suppression Chamber and Nearby Plumbing

Water from the analog to the Suppression Pool is drawn into a centrifugal multistage pump, analogous to the RCIC pump. Here, the pump will not be directly connected to the turbine analog, and instead will be fully separated from it. This allows for independent investigation of both the pump and turbine sides of the system. From the pump, water will be returned to the steam generator to complete the closed loop. In addition to recirculation lines, there is an injection line to the steam path upstream of both the RCIC and SRV sparger analogs. This will allow the investigation of potential water carryover into the Main Steam Line from an overfilled reactor. The recirculation

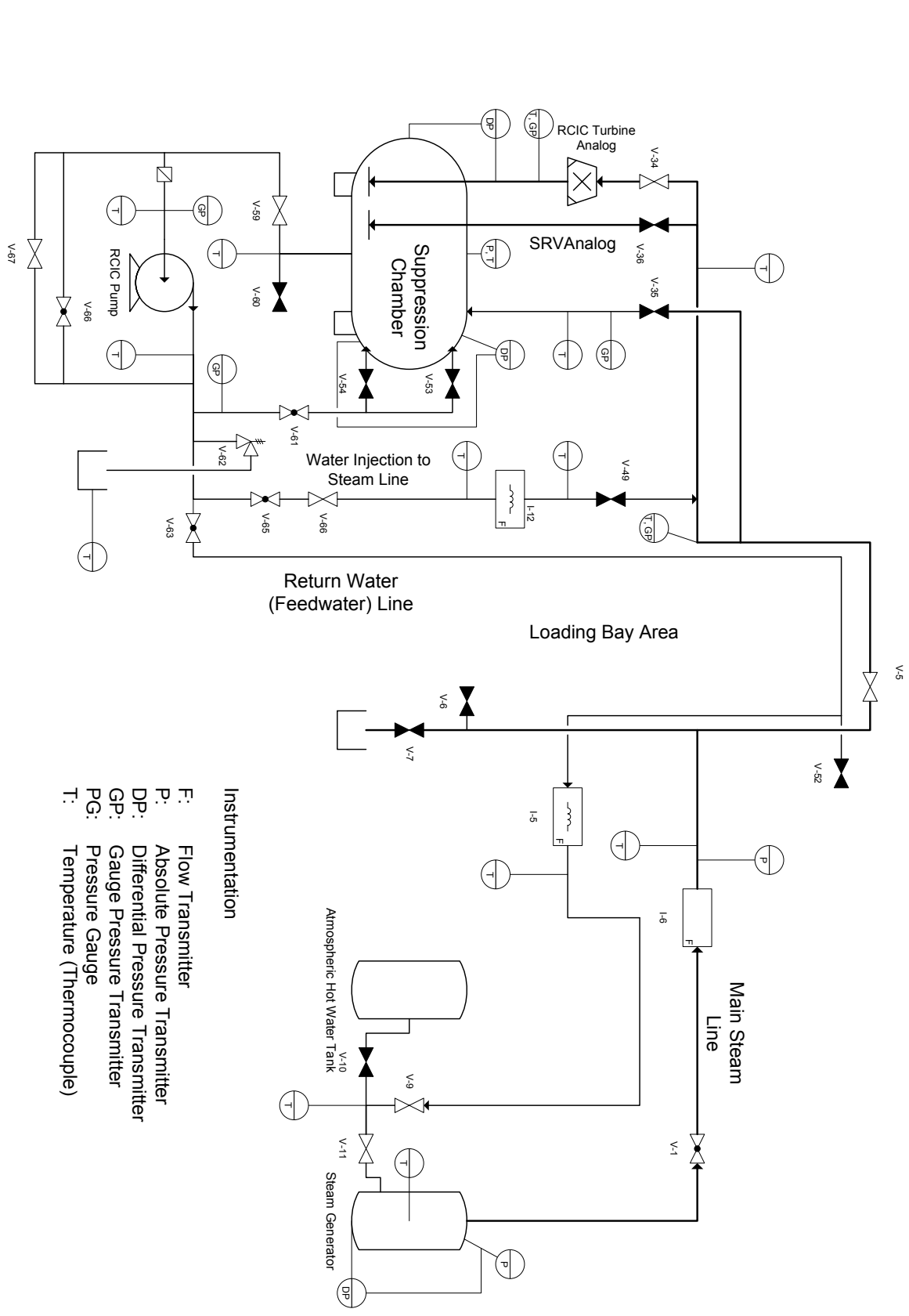
flow is used to prevent deadheading the pump as well as to assist in preventing overpressurization of the downstream lines. It can also be used to circulate the water in the Suppression Chamber Analog.

The experimental system uses deionized water throughout, and is thoroughly instrumented to examine all variables of interest.

3.1 EXPERIMENTAL EQUIPMENT

In the standard alignment, steam is directed from the outlet of the steam generator system to the manual steam control valve. This is entirely in standard-wall (Schedule 40) 1.5-inch NPS Stainless Steel 304 piping, and the entirety of the steam piping is covered with 2-inch thick rigid fiberglass pipe insulation. From the control valve, the steam continues in a straight horizontal path through the Foxboro vortex flowmeter and past its associated pressure and temperature taps until it encounters the liquid trap and facility branch-off point; this consists of a tee where liquid in the line drains downward to the trap valve and the steam flows vertically until it reaches the appropriate height. The branch-off, not used in this experiment during data collection but used for cooldown operations, is located near the bottom by the liquid trap valve. The change in elevation is due to physical limitations of the laboratory space; the plumbing must be directed up and over a region that cannot have permanent installations blocking access. Once the requisite elevation is achieved, the steam line returns to a horizontal path, and encounters a block valve. From the block valve, the piping is directed over the clear area to the Suppression Chamber Analog area, where it is turned downward until it meets the various branches of the Suppression Chamber Analog

assembly. The top branch connects to the top 1.5-inch flange on the Suppression Chamber Analog through a normally-closed ball valve. The lower branch flows contains the water injection point, and downstream of that point the line branches off once again to two ball valves; one for each sparger assembly. Pressure and temperature are monitored at the bottom of the vertical section of the steam line, right at the lower (second) branch off point upstream of the water injection. One of the sparger lines, analogous to an SRV, aligns the steam line directly to the SRV sparger when its ball valve is opened. The other, a RCIC analog, passes the steam through the RCIC Turbine analog and then to the RCIC sparger analog. Both spargers deposit their steam below the surface of the water in the Suppression Chamber Analog, which contains a major support structure for the spargers as well as internal instrumentation. A simplified P&ID of the experimental system, omitting some components, is given in Figure 13. Complete P&IDs for the entire system are given in Appendix A.



- Instrumentation**
- F: Flow Transmitter
 - P: Absolute Pressure Transmitter
 - DP: Differential Pressure Transmitter
 - GP: Gauge Pressure Transmitter
 - PG: Pressure Gauge
 - T: Temperature (Thermocouple)

Figure 13: Simplified Experiment P&ID

The water line consists of several pipe sizes. All are Schedule 40, and the majority is 0.75-inch NPS. All of the water lines are insulated, largely with 1.5-inch thick rigid fiberglass pipe insulation. The water is drawn from the outlet of the Suppression Chamber Analog (the bottom-most flange) through a 0.75-inch line that immediately becomes a 1-inch line. The water temperature at the vessel outlet is measured by a thermocouple. From there, the line traverses a block valve and joins with recirculation flow coming from the pump outlet through stainless steel tubing. It then goes past a thermocouple and pipe size reduction to 0.75-inches to enter the pump inlet. From the outlet of the pump, the water temperature is again measured with a thermocouple and then the pipe size is expanded to 1-inch. This 1-inch segment handles the major branch-offs: a 0.5-inch recirculation line to an upper and lower flange on the front of the Suppression Chamber Analog, the aforementioned stainless steel tubing recirculation lines back to the pump inlet, a visual pressure gauge and relief valve, the injection line, and the return flow (to the steam generator) control valve.

From the return flow control valve, the flow is directed vertically and the pipe size is reduced to 0.75-inch NPS, and it travels horizontally alongside/slightly below the steam line until it too crosses the reserved/clear area. It then drops down and enters a length of 0.5-inch NPS pipe for the Yamatake magnetic flowmeter. From the flowmeter and its associated thermocouple, there is a short vertical segment of 1-inch pipe to provide a U-trap meant to keep the meter full of water at all times. The size is then reduced back to 0.75-inch NPS, horizontally, until it reaches the vicinity of the steam generator. There, it drops to near the level of the bottom of the steam generator, and

encounters a block valve. From there, the pipe size is reduced to 0.5-inch NPS and there is a visual pressure gauge and a branch point with a thermocouple. Both branch points have block valves; one connects to the hot water tank, and the other connects to a low penetration in the steam generator to complete the loop.

The injection line to the main steam line takes water from the pump's branching outlet and passes it through a control valve and a block valve. Then, it reduces the pipe size down to 0.25-inch NPS. The flow encounters a thermocouple, passes through a Badger M2000 magnetic flowmeter, encounters a second (downstream) thermocouple, and then hits another block valve. From the block valve, the water injection flow is directed to a tee in the steam line, where the steam and water mix.

The relevant process variables, i.e., pressures, temperatures, and flows, are measured by appropriate instruments. These include flowmeters, pressure transmitters, and thermocouples. Their measurements are then processed and recorded by a data acquisition system. More detailed information on the subsystems and components in the experimental facility are given in the following sections.

3.1.1 Water Deionization System

The entirety of the water used in the RCIC experimental facility is deionized water. This DI water is provided by passing city water through a Culligan ® mixed bed system consisting, in order of the flow, an activated charcoal filter, a cartridge filter, two mixed bed resin tanks in series, and a final cartridge filter. An indicator lamp turns from green to red when it senses that the resin needs regeneration. Due to the level of

dissolved material in the supply water, the DI system can only purify about 350 gallons of water between regenerations.

In order to fill the system with DI water, the valve connecting the DI system to the hot water tank is opened, as are the valves between the hot water tank and steam generator. Then the hot water tank is filled, which drains into the steam generator. Once the steam generator is filled, all of the valves on the steam generator and DI system are closed. Next, using the laboratory's air compressor, the steam generator is pressurized to a moderate level with air. Slowly, the valves aligning the return water line from the Suppression Chamber Analog to the steam generator are opened, allowing the pressurized water to flow in reverse through the water line back to the Suppression Chamber Analog. In turn, valves for the branching lines are opened and closed to purge all the air from the lines. Before the water level in the steam generator drops too low, the block valves are closed to trap the water in the lines, and the steam generator is depressurized. The valves are then realigned, opening up flow through the DI system to the hot water tank and steam generator. In addition, the valves on the return water line from the Suppression Chamber Analog to the steam generator are reopened. The water in the steam generator and hot water tank can then siphon over into the Suppression Chamber Analog as the DI system adds water to the vessels. This is a slow process, as the DI system processes 1 to 2 GPM. Filling approximately 700 gallons into the Suppression Chamber Analog, as well as any additional necessary fill for the steam generator and hot water tank, takes a minimum of two complete regeneration cycles and more than 7 hours of fill time.

3.1.2 Flowmeters

There are three primary flowmeters used in the experiment; a vortex flowmeter is on the steam line, and two magnetic flowmeters are on water lines. An additional magnetic flowmeter was used for monitoring flows while cooling the system down, but is not available in the actual tests' alignment.

3.1.2.1 Vortex Flowmeter

The vortex flowmeter on the steam line is a Foxboro 83W wafer-style meter in the 1.5-inch steam line nearly 100 inches downstream of the main steam control valve. It uses a standard analog 4-20 mA signal to the DAQ, and can register saturated steam flow at atmospheric pressure up to nearly 96 g/s when properly configured. At higher fluid densities, the maximum measurable mass flowrate increases. At 6 and 8.25 inches downstream of the meter are pressure and temperature taps, respectively, for use in calculating the correct flow value from the signal generated by the meter.

A vortex flowmeter, as implied by its name, measures fluid flow by utilizing vortices; these vortices are generated as fluid flow past an engineered obstruction in the flow path. The meter measures the frequency of vortex shedding, which is directly related to the flow rate. This is achieved by the use of a small piezoelectric differential pressure sensor near the obstruction; the shedding of vortices alternates from side to side of the obstruction and generates time-varying differential pressures across the sensor at the frequency of the shedding [42]. When combined with the fluid's thermophysical conditions as measured near the meter i.e., pressure and temperature in a pure superheated steam system to determine density and the meter's correction factors, the

flow can be fully characterized. The equations for the flow characterization and correction factors appear in Eqs. (4), (5), (6), and (7) [42].

$$URF = CRF \cdot CF \cdot \frac{URV}{Time} \cdot \frac{1}{\rho_f} \quad (4)$$

$$CRF = BCF \cdot K_{ref} \quad (5)$$

$$BCF = TCF \cdot MCF \cdot UCF \quad (6)$$

$$TCF = 1 - 3 \cdot \alpha \cdot (T - T_0) \quad (7)$$

In the equations, URF is the upper range vortex shedding frequency while URV is the upper range value of the flow, i.e., kg/s. K_{ref} is the reference K-factor characteristic of the meter, which needs to be corrected for changes in temperature, pipe wall thickness and nearby disturbances. Only the temperature correction factor given in Eq. (7) will be nonunity in Eq. (6); it corresponds to thermal expansion in the meter material (expansion rate of α) at fluid temperatures T other than reference T_0 . Both CF and Time are used as unit scaling factors.

3.1.2.2 Magnetic Flowmeters

A magnetic flowmeter works by passing a conductive liquid through a magnetic field. By the laws of magnetic induction, this generates a voltage perpendicular to both the magnetic field and the flow of the conductive liquid; it is picked up by electrodes in proper locations. With a known electrode spacing and magnetic field, the voltage will be directly proportional to the flow velocity [43].

Of the two magnetic flowmeters, one is a Yamatake MagneW 3000 PLUS system with a 0.5-inch NPS wafer-style detector. The system consists of an MGG18

detector connected to a remote MGG14C converter. It can measure flowrates up to 28.01 gpm with an error of $\pm 0.2\%$ to 0.5% , given a minimum liquid conductivity of 3 micromhos/cm [43]. The range, however, is set to 0-5 gpm on its analog 4-20 mA output. Liquid temperature is measured a few inches downstream of the meter to assist in fully characterizing the mass flow. This meter is situated to measure the flow from the Suppression Chamber Analog back to the steam generator.

The second magnetic flowmeter is a Badger M2000; it is used for measuring the liquid injection flow into the steam line. It uses a 0.25-inch flange connection, and can register flowrates from 0.02 to 5 GPM; its accuracy can be better than $\pm 0.25\%$ [44]. In addition, it can handle process fluid temperatures of up to $150\text{ }^{\circ}\text{C}$, and requires a minimum fluid conductivity of 5 micromhos/cm [44]. Temperatures are measured 6 inches upstream and 2 inches downstream.

3.1.3 Pressure Transmitters

Four different primary models of pressure transmitter are used in the RCIC facility: one Dwyer 682-3, four Dwyer 673-7 gauge pressure transmitters, three Honeywell ST3000 STA940 absolute pressure transmitters, and three Honeywell ST3000 STD924 differential pressure transmitters. In addition to the electronic pressure transmitters, there are a number of simple visual pressure gauges placed throughout the facility. These, however, are not intended for any actual measurement and are present only for operator convenience as well as sanity checks.

The Dwyer 673-7 pressure transmitters are factory set to a fixed range from 0 to 100 psig (the 682-3 goes up to 250), and transmit on an analog 4-20 mA line. No end-

user adjustments are possible, and they do not communicate with a Honeywell Smart Field Communicator. The 673-7 transmitters have a maximum case pressure of 200 psig, and therefore can survive exposure to pressures beyond their ability to communicate. This is an important feature, as one was originally installed on an outlet to a high-pressure multistage centrifugal pump; that line may see pressures approaching 150 psi before the relief opens.

Four such Dwyer gauge pressure transmitters are deployed in the experimental facility: one on the RCIC pump analog's discharge (originally, it was later upgraded to the 682-3 and moved to the pump suction), another on the outlet to the RCIC turbine analog, a third on the Suppression Chamber Analog's top vapor space, and a fourth on the Main Steam Line on the branch-off point in proximity to the Suppression Chamber Analog, far downstream of the vortex flowmeter. Especially in light of the age and calibration difficulties for these transmitters, their transmitted data are not considered high-quality for the purposes of this experiment and are therefore seen as rough monitors rather than as accurate measurements.

Both of the Honeywell models can be used with a Honeywell Smart Field Communicator. This allows for fast and simple connections to the transmitter, quick adjustments to the output ranges, simplified calibration procedures, and in general they are easier to work with than if they did not have that capability. With the communicator, reading and adjusting ranges is a matter of connecting the leads and pressing a short sequence of buttons. No potentiometers need to be adjusted. In addition, the output can

be directed to hold at specified values to assist in calibrating the 4-20 mA analog current loop.

The STD924 model can measure differential pressures ranging from -20 to +400 inH₂O. This range may seem limited in higher-pressure situations, such as high-pressure choked flow through a restriction, but combined with a capability for withstanding a high common-mode case pressure, these transmitters are very useful for measuring liquid levels in pressure vessels. Two of them are used for exactly that: one on the steam generator to measure its water level, and another on the Suppression Chamber Analog to measure its level. The third is installed to measure the differential pressure from the RCIC Turbine Analog's outlet to the Suppression Chamber Analog's bulk vapor space pressure, which is not expected to be large.

The STA940 model can measure absolute pressures ranging from 0 to 500 psia; however, none of the three used here are set to such a broad range. One measures the pressure in the steam generator, a second measures the pressure in the vapor space of the Suppression Chamber Analog, and a third measures the pressure in the Main Steam Line at the appropriate location shortly downstream of the vortex flowmeter. The widest range is set for the transmitter on the steam generator, transmitting from 0 to 150 psia; the narrowest set range is on the Suppression Chamber Analog, being 0 to 100 psia. The main steam line pressure transmitter's range is set to 0 to 130 psia.

3.1.4 Thermocouples

In this experimental facility, a total of 44 thermocouples are used to measure temperatures at various locations. Of them, 24 are installed in the interior of the

Suppression Chamber Analog proper, with an additional 25th that can effectively be considered to be internal much of the time. The remainder are distributed throughout the system; near the Suppression Chamber Analog, one is on the vessel's outlet, one on the RCIC pump analog's inlet, another on its outlet, one is on the Main Steam Line at its branchoff point, another near 6 feet downstream of the water injection point in the steam line, another on the outlet of the RCIC Turbine Analog, one is immediately upstream and another immediately downstream of the Badger M2000 magnetic flowmeter on the water injection line to the steam line, and one even monitors the bottom temperature of the blowdown drum. Four monitor temperatures inside the steam generator, another measures the temperature on the water return line to the steam generator at the point of injection, another on that line is immediately downstream of the Yamatake magnetic flowmeter, one measures the steam temperature at an appropriate location downstream of the vortex flowmeter, and one even monitors the room temperature of the laboratory.

All of the thermocouples used in this experiment are Omega type T (copper-constantan) thermocouples with special limits of error for accuracy within 0.5 °C [49]. They are all of the ungrounded type, with stainless steel sheathing. However, they do not have the same lengths nor do they have the same sheath diameter. The lengths range from 12 inches to 120 inches, and the diameters range from 0.032 inches to 0.062 inches. With the exception of the room temperature thermocouple, all the loop resistances are well below 100 ohms.

The SCXI-1102/b/c modules used in conjunction with SCXI-1303 terminal blocks on the Data Acquisition System are built to enable open thermocouple detection.

This uses high resistances to pass a very small current through the thermocouple; when the thermocouple is disconnected or damaged, it will result in a (safe) offscale high voltage on the positive terminal. However, with long extension wires, high thermocouple loop resistances, or when very high accuracy is desired, it is recommended that such detection be disabled, as it can result in measurement errors [45]. As a result, it has largely been disabled in this experimental facility.

Additionally, as the thermocouples used here are universally of the ungrounded type, it is recommended that they be ground referenced on one terminal (the negative terminal). The SCXI-1303 terminal blocks make this a simple matter, and such ground referencing has been enabled for all of the thermocouples.

3.1.5 Pump

The pump used in this experiment is a five-stage centrifugal pump, and should provide a reasonable analog to the multistage centrifugal RCIC pump. It is a Dayton 5UXF5 with a 0.75 HP electric motor running off of 115 VAC, and can produce up to 93 psi of boost pressure; the performance curve is shown in Figure 14. Both the inlet and outlet of the pump are 0.75-inch NPT connections. The speed of the motor, nominally 3450 rpm, is not controlled by the user; as a result, any pressure and flow regulation must be done using valves connected to the system.

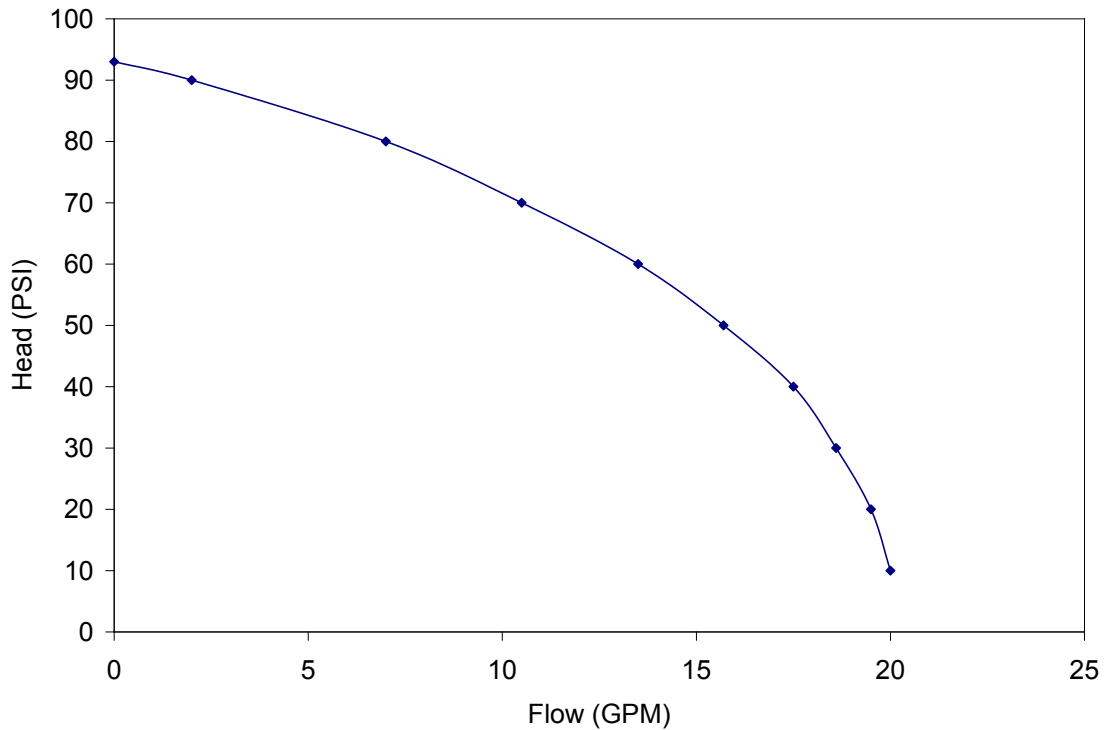


Figure 14: Pump Performance Curve (Data from [46])

While some of the wetted materials on the pump are cast iron and the listed maximum liquid temperature is 194 °F [46], it was predicted that corrosion would not be a major issue for the duration of the experiment. It was also assumed that the liquid temperature limit could be exceeded at elevated inlet pressures without causing significant damage to the pump for the duration of the experiment. In the event that damage does occur, all of the components of the pump are serviceable/replaceable.

3.1.6 Steam Generator

The steam generator pressure vessel used in this experiment is a Kennedy Tank and Manufacturing Co., acquired in the past for use on other experiments; it has a

capacity of 130-135 gallons and limits of 135 psig and 350 °F. It can be represented as a vertically-mounted cylinder, with a diameter of 24 inches and a height of 60 inches; the top and bottom both have curved heads that bring the height to approximately 72 inches in addition to the legs below and the equipment mounted above. It was made out of schedule 10 stainless steel 304 pipe. The entire assembly is wrapped in two-inch thick rigid fiberglass insulation. The steam generator pressure vessel and associated equipment is shown in Figure 15.



Figure 15: Steam Generator System

The steam is generated by six strategically placed electric immersion heaters; they are wired for 3-phase 480 VAC, and can produce a grand total of 157 kW of heat nominal. They are submerged beneath the water level in the main vessel, and heat the water to boil it. The heaters are not all of the same size; two are two kW in capacity (screw-in type), one is three kW (screw-in type), and the remaining three are fifty-kW heaters (8-inch flanged type). Of the fifty-kW heaters, two can be powered in 25-kW intervals, while the third has 6.25-kW intervals. This allows for a staggered resolution of available heating powers by using different combinations of heaters: 2, 3, 4, 5, 6.25, 7, 8.25, 9.25, 10.25, 11.25, 12.5, 13.25, ..., 157 kW. The heaters and electrical control panel were manufactured by Watlow Process Systems.

As it was originally wired, a total of 6.25 kW from the 7th and 8th circuit of the third 50-kW heater were unavailable. This brought the total available power down to 150.75 kW at 480 VAC 3-phase. This was rectified after shakedown testing.

In addition to the main vessel, there is a smaller separator attached to the main steam output line. It is a separate pressure vessel manufactured by Clark Reliance and is connected to the main steam line upstream of the control valves. Both it and the steam generator are ASME-code rated. Wet steam from the steam generator flows into it through a 1.5-inch line, it removes entrained liquid from the output flow, and the liquid is returned to the steam generator while the exiting steam continues its journey; thus, the steam exiting from the overall steam generator system is nearly dry saturated steam.

There are a number of instruments that monitor the steam generator. For bulk temperature measurements, there are four thermocouples placed at different vertical

locations penetrating the vessel; these give the DAQ the temperature readings from the cooler water near the bottom of the main vessel to the steam space near the top. The DAQ also monitors two pressure transducers on the steam generator: an absolute pressure meter connected to the top for pressure determination, and a differential pressure meter tapped to the top and bottom of the main vessel for water level determination.

In addition to the instruments connected to the DAQ, there are visual gauges attached to the system: pressure gauges at the top and bottom of the main vessel, and a magnetic float-based level indicator. The level indicator is also used by the interlock circuitry for the heaters; the heater interlock cuts power when a thermal overload is detected in the heaters or when the level float falls below the cutoff level, triggering a reed switch.

There are several lines that connect to the steam generator: the main steam line, two Kunkle relief valves, a manual blowdown line, a vacuum breaker line, an air line featuring a pneumatic quick-connect fitting, a drain line, and a fill/return water line.

The Kunkle relief valves are ASME-code rated, each set to lift at 115 psi. They both open to a large atmospheric blowdown drum partially filled with water to condense any escaping steam during their operation. This prevents hot steam from being ejected directly into the laboratory space. The blowdown line, however, does not direct steam into the drum. Instead, it directs the steam to an outdoor location away from laboratory personnel.

The vacuum breaker is meant to prevent a significant vacuum from developing in the steam generator when it is shut off and cools down. It consists of a ball valve, a check valve, and a filter. The ball valve should be closed when the system is under pressure to prevent leakage back through the check valve. At any other time, it should be open, allowing one-way airflow through the check valve into the steam generator. The inlet has a filter on it to prevent dust or other contaminants from entering the system. When used properly, this system should prevent a vacuum from developing in the steam generator, and thus preventing vacuum damage to the vessel.

3.1.7 Suppression Chamber Analog

The Suppression Chamber Analog is, in this experiment, the analog to the Torus/Suppression Chamber in BWR plants with the Mark I containment. Unlike the actual Suppression Chambers, it is in the shape of a cylinder rather than a torus. It is a large (approximately a 1,400 gallon capacity and empty weight of near 3,000 pounds) pressure vessel originally constructed in 1952 by Wyatt Metal & Boiler Works. It is made of 304 Stainless Steel, and has a pressure rating of 88 psi with a temperature rating of 400 °F. It is a horizontally-mounted cylinder with an inner diameter of 59 inches and a length of 96 inches from head weld to head weld; from each head weld, each head extends out approximately 3 inches before the curvature changes, extending the cylindrical section to approximately 102 inches total. The longest length is from head to head through the centerline; this length is about 122 inches internally. The vessel's legs near either end elevate the bottom center 18 inches above the surface beneath it. For reference here, the front face will be deemed the head with the ASME-API stamped

plate, and the right-hand side will be the right-hand side of the vessel when facing toward the front head from the rear head. It has a number of useful penetrations, including a 6-inch NPS flange underneath at the front end where it feeds the pump suction. In addition, the front face has four 0.75-inch NPS flanges arranged rectangularly about the head. The centers of these four flanges are spaced 17 inches horizontally and 52.25 inches vertically, and extend several inches out from the head. The rear face has a 6-inch NPS flange near the top center. The top of the tank has four penetrations, in order from front to back: nearest the front, a 1.5-inch NPS flange without pipe significantly extending past the inner weld; a 20-inch manhole at the top center giving personnel access to the interior of the pressure vessel; a 2-inch NPS flange with tubing extending several inches into the interior, and a 4-inch NPS flange near the back end, also without tubing extending into the vessel. In Figure 16, the vessel can be seen during the construction phase of the experiment.



Figure 16: Suppression Chamber Analog During Facility Assembly

3.1.7.1 Vessel Internals

The vessel is heavily instrumented, and has 24 thermocouples placed strategically throughout its interior. In order to position the thermocouples and provide support for the sparger systems, a support structure was assembled inside the vessel. The support structure system was pieced together out of stainless steel channel strut and stainless steel fasteners. It has four feet made out of heavy stainless steel blocks to weigh down and secure the entire assembly; there are no mechanical attachments to the vessel itself. Instead, the feet have silicone rubber pads adhered to their edges with JB

Weld to provide a cushion and dampening where the blocks sit on the bottom of the vessel's interior. Some of the internals can be seen in Figure 17.

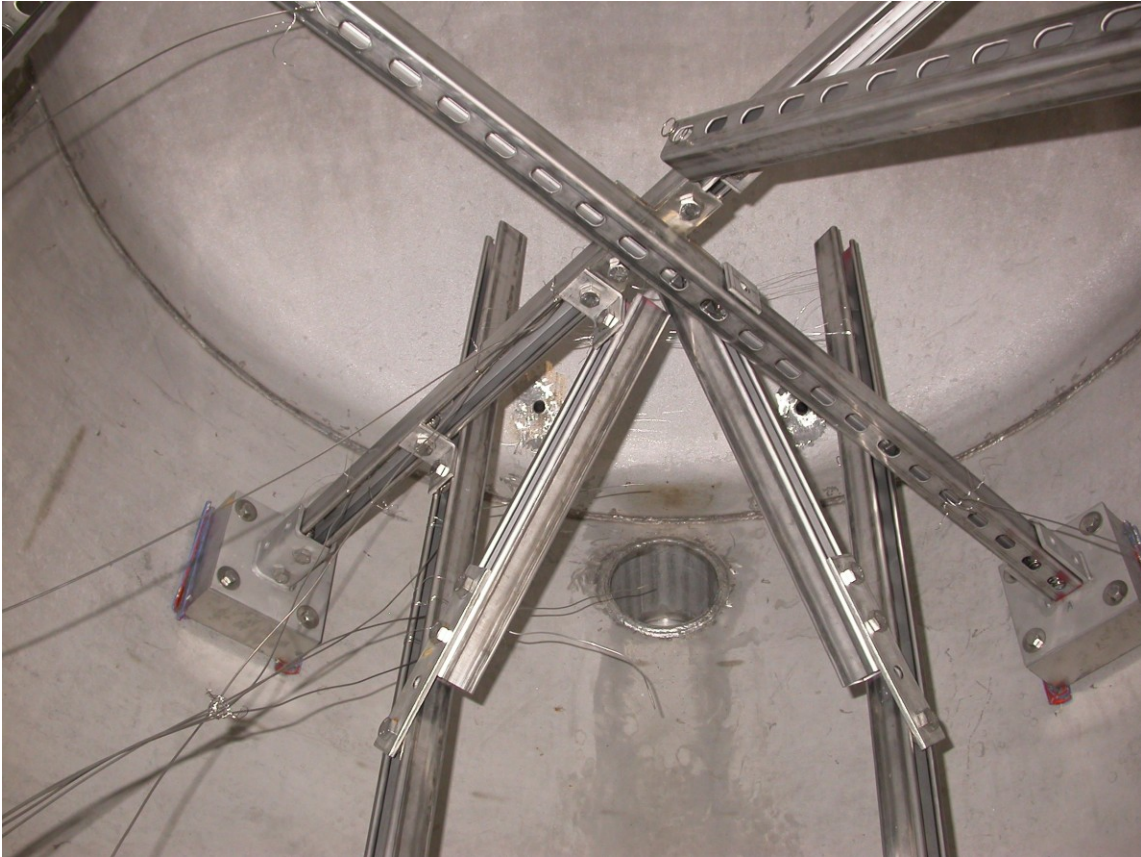


Figure 17: View of Vessel Internals Near Front Head

The feet are connected to channel strut pieces that, when attached, form an “X” shape; there are two such assemblies, each with feet only on the bottom of the X. They are roughly positioned to be above the vessel's legs at either end, and have channel strut pieces run lengthwise along the vessel attached to each leg of the X. Under normal operating conditions, two of the lengthwise pieces will be below the water's surface and

two above it. The lower two pieces sit roughly 16.75 inches above the very bottom center of the cylindrical portion of the vessel, and span 102 inches. The lengthwise gap between them is roughly 16 inches. In addition to these major elements, there are a number of minor pieces bolted to them to increase the structure's overall strength and rigidity, and to provide mounting points to anchor the sparger systems.

There are two separate sparger systems in the vessel: one for the RCIC line, and one for the SRV line. Only one is intended for operation at any given time. Both spargers are anchored to the support structure within 12 inches of their outlet ends. The SRV line comes in through an adapter on the 2-inch pipe flange on the top of the vessel, and drops straight down through a length of 1.25-inch pipe, which is then reduced to 1-inch for half of the vertical drop. It then meets a 1-inch tee that is 3 inches wide, and each end of the tee has an additional 2 inches of 1-inch pipe extending from it. These outlets are aligned to be pointed lengthwise along the vessel toward either head, and their centers are 7 inches above the vessel's bottom. The alignment of the vertical section is not perfect, however, and the tee actually sits almost 2 inches off-center towards the right when viewed from the front head looking toward the back. It is 24.5 inches from the back head weld.

The RCIC sparger system uses a simpler sparger type: a single open pipe end. The pipe enters through an adapter on the rear side 6-inch flange and proceeds horizontally to an elbow, which angles the pipe down vertically. After the adapter, the pipe expands to a 1.5-inch line, and stays that size. Shortly before the outlet, there is a 1.5-inch tee in the line used to insert a thermocouple into the flow, which goes straight

through the tee without bending. A pipe stub of less than two inches extends past the tee; the thermocouple is therefore less than 4 inches from the outlet. The outlet end itself, still pointing vertically towards the vessel bottom, sits 11 inches inward from the back head weld and 15 inches above a jet shield intended to protect the vessel wall from any steam jet and violent phenomena associated with it. The shield is made from a 6-inch long piece of 6-inch schedule 10 stainless steel pipe cut in half lengthwise. This is kept a small distance above the vessel bottom by using silicone rubber feet adhered to the shield with JB Weld as well as bolts mounting it to the main support structure. Both the SRV and RCIC analog spargers can be seen in Figure 18; the RCIC sparger analog is in the foreground along with its jet shield, and the SRV sparger analog is in the background.

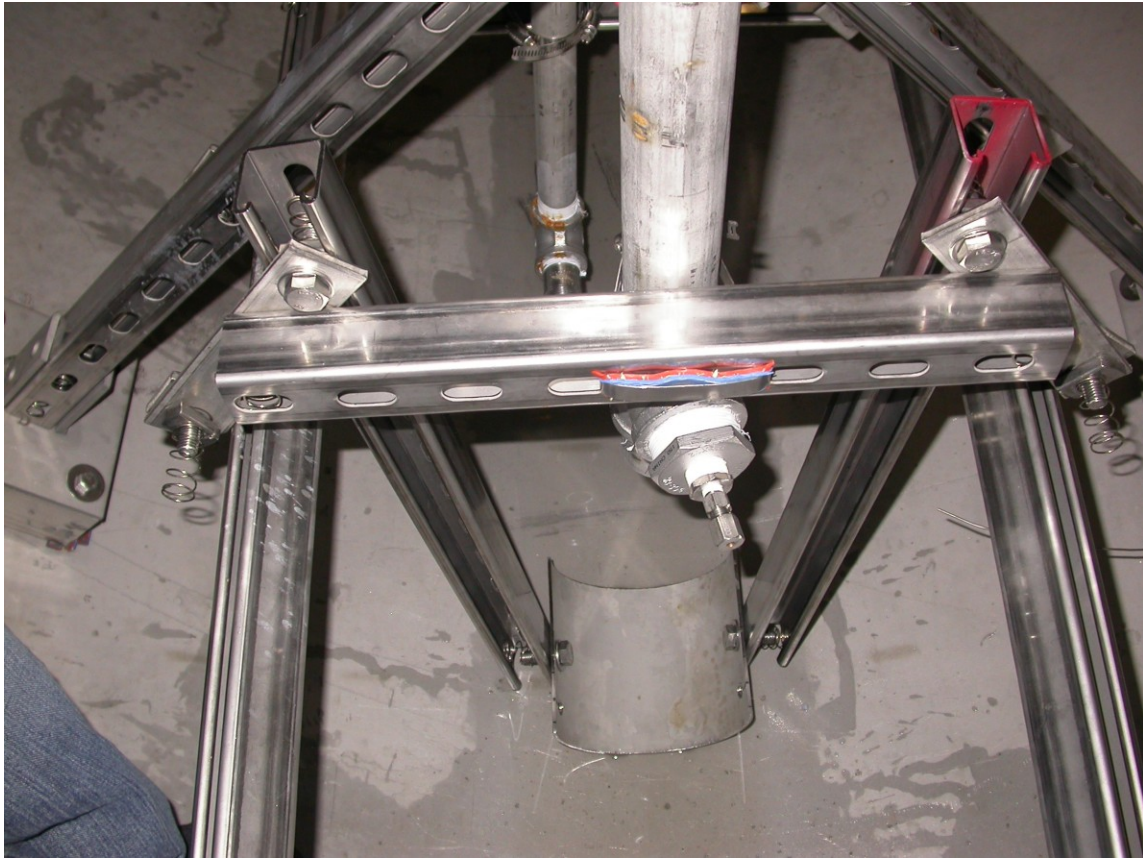


Figure 18: View of Spargers from Vessel Rear Head

Aside from the thermocouple in the RCIC sparger, there are 23 other thermocouples spaced throughout the vessel to examine any thermal stratification that may appear. A 24th, while not in the vessel proper, can be considered to be in the vessel under the valve alignments for most operating conditions. It sits in a pipe attached directly to the 1.5-inch top flange just a few inches from the flange, and the valve between it and the main steam line is normally closed. The internal vessel thermocouples enter through two multiconductor feedthroughs installed in the four-inch

flange on the top of the vessel; they have 120 inch leads, allowing their sensitive ends to be placed relatively far from their entry points.

Table 1: Vessel Internal Thermocouple Positions

<u>SP Thermocouple</u>	<u>x-position</u>	<u>y-position</u>	<u>z-position</u>
SP 1	Inside RCIC Sparger		
SP 2	0	0	58
SP 3	0	0	22
SP 4	0	0	15
SP 5	0	0	8
SP 6	0	12	15
SP 7	0	-12	15
SP 8	12	0	15
SP 9	24	0	15
SP 10	36	0	15
SP 11	48	0	22
SP 12	48	0	15
SP 13	48	0	8
SP 14	48	12	15
SP 15	48	-12	15
SP 16	60	0	15
SP 17	72	0	15
SP 18	84	0	44
SP 19	84	0	22
SP 20	84	0	15
SP 21	84	0	8
SP 22	84	12	15
SP 23	84	-12	15
SP 24	96	0	15

With an expected water level near half-full, there are two thermocouples in the tank proper to measure vapor space temperatures: one close to the top of the tank just

below the back head weld, and a second roughly 12 inches back from the front head weld, 15 inches below the top of the tank. The remaining internal thermocouples are spaced throughout the liquid space. A line of 9 thermocouples is set up along the vessel axis, 15 inches above the bottom and spaced 12 inches apart. As a result, they span from the back weld to the front weld. At three points along that thermocouple line, there are an additional 4 thermocouples offset from the line: one 7 inches above, a second one seven inches below, a third at the same height and axial location but 12 inches to the left (toward the side wall), and a fourth similarly situated, but 12 inches to the right instead. These sets are placed such that one is, axially, at the back head weld, the second is in the middle between the welds, and the third is 12 inches back from the front head weld. This should be sufficient to give at least a minimal indication of thermal gradients in three dimensions in the liquid pool, and to highlight potential hot spots within it. The internal x,y,z positions of the thermocouple ends in the vessel are given in Table 1 and depicted in Figure 19. The positions are given in inches; the x-position is measured from the rear head weld pointing toward the front head, the y-position is from the center of the vessel pointing to the right as one looks towards the front head from the rear, and the z-position is the height measured from the bottom centerline inside the vessel.

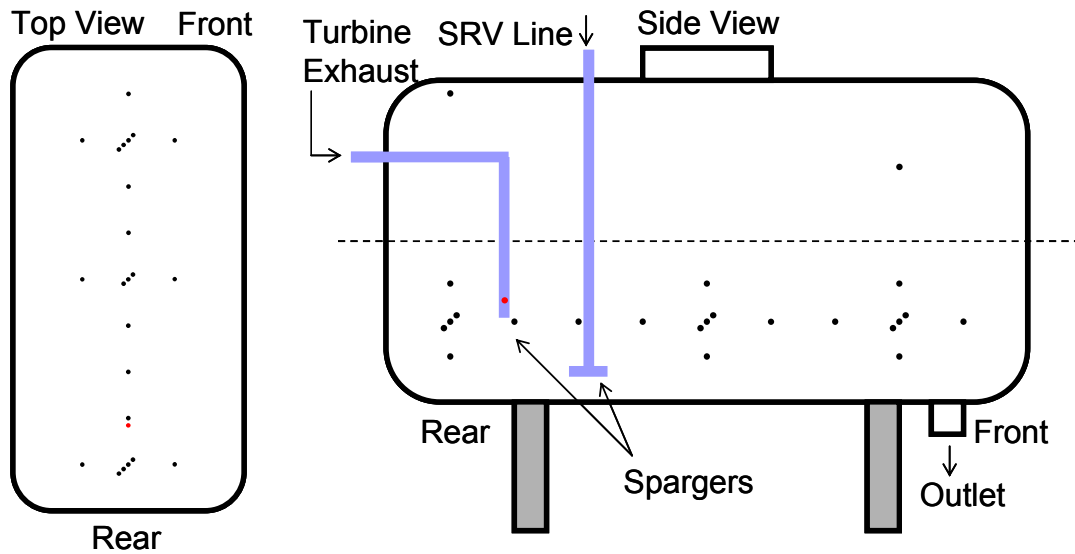


Figure 19: Thermocouple Layout

3.1.7.2 External Instrumentation

Besides the thermocouples inside the vessel, several instruments positioned externally monitor vessel conditions. An Orion magnetic level indicator, very similar to the one used in the steam generator system, is mounted to the front head to give a visual indication of the vessel's water level. In addition, a Honeywell DP transmitter is used to formally measure the liquid fill level and log it in the data acquisition system. It has the high pressure side connected to a column of water terminating at the top of the vessel, open to the vessel's internal pressure in the upper vapor space. The low pressure side is connected to the liquid space, and measures the hydrostatic head of the water fill above it. The head difference between the two depends on the fill level, and can be easily calculated under standard conditions.

A second Honeywell DP transmitter is connected across the RCIC Turbine Analog outlet and the bulk vessel vapor space. This allows monitoring of pressure fluctuations appearing in the RCIC sparger, especially those that can be expected to occur in a chugging regime or when liquid is injected through the turbine analog.

A third Honeywell pressure transmitter, an absolute pressure transmitter, is connected to the top of the vapor space in the vessel and observes the bulk pressure in the vessel.

In addition, there is a Dwyer gauge pressure transmitter installed on the 1.5-inch flange that monitors vessel/flow pressure at that point. However, it is of lower quality and precision than the Honeywell transmitters. While its data does get recorded by the data acquisition system, it is used more as a monitor of general conditions than as a full-fledged measurement.

3.1.7.3 Pressure Relief, Vacuum Breaking, and Blowdown

The aforementioned 1.5-inch flange on the top front of the vessel serves a number of functions. Besides the pressure and temperature readings taken there, it feeds the relief, vacuum breaking, blowdown, and generic main steam line functions. On the 1.5-inch pipe, a cross piece branches components out onto a number of lines. With everything attached, it resembles a crown or antlers on the pressure vessel. The top line is connected to a valve, normally closed, that opens into the main steam line. This can be used to pressurize the vapor space, or alternately, to depressurize it by running the main steam line in reverse. Both the left and right branches then tee off to connect to the relief valves. There is a total of two relief valves, each a 0.5-inch Kunkle spring-

operated ASME relief set to 88 psi. They are, with the exception of the pressure setting, identical to those on the steam generator. They open to an atmospheric blowdown drum, somewhat smaller than that of the steam generator system, also partially filled with water to condense any steam present in the release. In addition, a manual blowdown line drains to the drum. This line comes from the tee on one of the vessel's relief valve lines. There is also a line draining to the drum from a non-code relief valve on the outlet of the RCIC Pump analog, set to keep the pump's maximum case pressure (150 psi) from being reached. The tee on the other line, past the relief valve, connects to a check valve aligned to allow flow into the vessel. Much like the steam generator, this is set up as a vacuum breaker, except that it does not have the shutoff valve and it is much larger – the full 1.5-inch pipe size. It too is fed from a filter, again scaled up in size. This is arranged so that a surprise vacuum condition will not damage the vessel; it is possible to align the pump to spray water into the vapor space in the vessel. It is conceivable that this could cause a rapid steam void collapse even under pressure; therefore, there is no operating condition in which the vacuum breaker should ever be closed off from the vessel.

3.1.7.4 Insulation

The vessel and the attachments, aside from the blowdown drum, are all well-insulated. This is intended not only to protect laboratory personnel from potentially high temperatures, but to thermally isolate the system as well. A layer of 2-inch thick fiberglass tank wrap insulation was applied around the pressure vessel, not without difficulty. Both heads and all the penetrations are insulated. The vessel's legs are

insulated as well, but only part of the way. It was assumed to be sufficient to insulate them only part of the way down below the vessel, as they are carbon steel (limited thermal conductivity) and beyond insulating a few inches the marginal additional heat retention is not expected to be high.

3.1.8 RCIC Turbine Analog

The turbine in the RCIC system of BWR plants with the Mark I containment is a non-condensing Terry Turbine as described earlier. The analog to this in the current experimental setup is an orifice followed by a loop. The orifice consists of a 7/16" (originally 0.348-inch) hole drilled in the center of a 0.25-inch thick stainless steel disc. The edges of the hole are chamfered at 135° (67.5° with respect to the axis). The disc itself is sandwiched into a 1-inch NPS Class 150 flange. Downstream, the flange has a 6-inch length of 1-inch Schedule 80 pipe connecting to an even thicker elbow. This elbow, in turn, is connected to a 3-inch length of 1-inch Schedule 80 pipe that connects to another (standard) elbow; two more 3-inch pipe lengths and elbow complete the loop (here, closer to a rounded square). From the final elbow, there is a 6-inch length of 1-inch Schedule 80 pipe connected to an end flange; this pipe is parallel to the first 6-inch length with flow in the same direction, but shifted to be below the first length.

While not an ideal representation of the turbine, the orifice was deemed to be sufficient for the purposes of this experiment. It preserves a choke point as would exist in the nozzles of the real turbine, and provides some swirl in the flowpath downstream of the choke point. As a result, the upstream flows into the turbine analog are isolated from downstream conditions when there is a sufficient pressure drop across the turbine analog

to result in choked flow, and the outlet conditions are very turbulent; both are expected from the genuine article. Although no work is done in the analog, the low efficiency of Terry turbines means the work done in a real system is itself limited. In addition, while the transient dynamics of the turbine are not preserved, the steady-state operations considered here do not involve transient responses.

The use of thick-wall rather than standard pipe as well as the more robust first elbow downstream of the orifice is a response to potential erosion issues. As the experiment expects some two-phase choked flow through the orifice, erosion from sonic velocity droplets impacting the first elbow and the pipes to a lesser extent, was expected. While thicker walls will not prevent such erosion, it does provide a more robust barrier and resulting additional operating time before replacement would become necessary.

3.1.9 Data Acquisition System

The Data Acquisition System consists of the collection of both hardware and software that combine to interpret and record all the relevant data produced during operation of the experiment. This includes each of the 44 thermocouples as well as the 16 4-20 mA pressure and flow transmitters.

3.1.9.1 Hardware

The primary hardware consists of a National Instruments SCXI system connected to a PC. This is the nerve center of the data acquisition system, and is shown in Figure 20. The SCXI system itself consists of an SCXI-1000 chassis with four modules installed: two SCXI-1102 modules, one SCXI-1102B module, and one SCXI-1102C module. The primary difference between the 1102, 1102B, and 1102C is the specific

lowpass filter specified for each one; the 1102 has a bandwidth of 2 Hz, while the 1102B and 1102C have bandwidths of 200 Hz and 10 kHz, respectively [47]. These modules each have 32 nominal voltage/thermocouple inputs in addition to a cold junction sensor input from the attached terminal block, and each channel has an independent amplifier and filter [47]. Each module in use is connected to its instruments via an SCXI-1303 terminal block and appropriate wiring; one of the SCXI-1102 modules is unused in this setup.

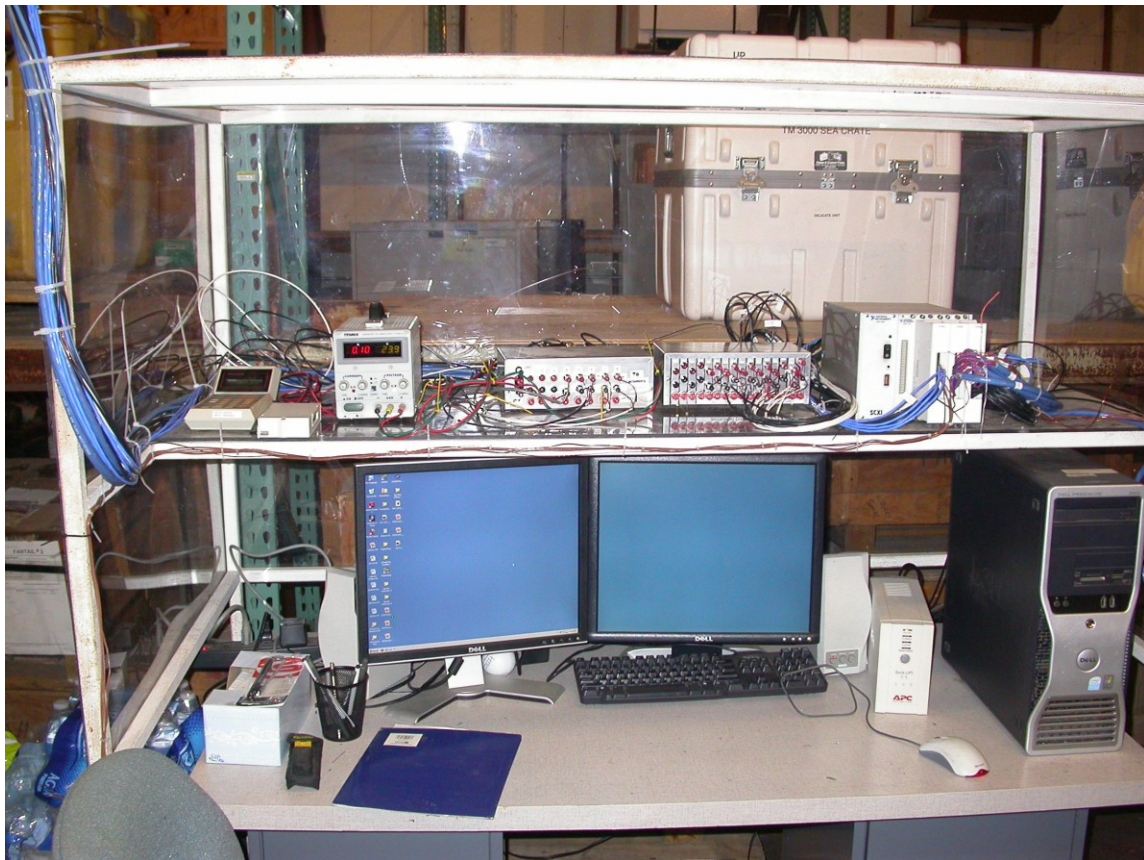


Figure 20: Data Acquisition System

The PC is connected to the SCXI-1000 chassis through a shielded cable connected from the back of one of the SCXI-1102 modules to an NI PCIe-6341 card in the PC. The analog input signals are multiplexed onto a single channel between the chassis and PC; when using LabVIEW software with the DAQmx drivers, much of the multiplexing and demultiplexing is invisible to the end user. However, care should still be taken in signal configuration to reduce the effects of sometimes unexpected or unclear phenomena such as extra settling time due to channel-to-channel gain transitions, as recommended by NI [48]. Essentially, signals of certain type and expected level should be clustered together physically on the terminals; for example, one would group channels 0-15 for one class of signal, and channels 16-31 for another in an SCXI-1303 terminal block. One would want to avoid putting a small signal on channel 0, a large one on channel 1, a small one on channel 2, etc.

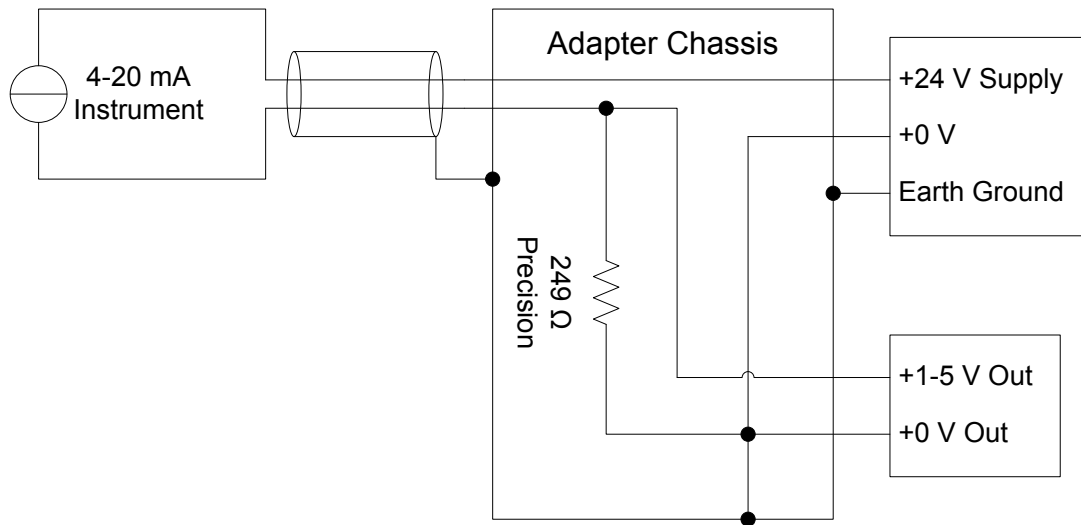


Figure 21: Current to Voltage Signal Conversion

While thermocouples can be connected directly to the terminal blocks with the current hardware, current loops cannot. Therefore, in order to use instruments with 4-20 mA analog outputs, some intermediate hardware is needed. For each channel, this consists of little more than a 249-Ohm precision resistor in the loop as illustrated by Figure 21 (only one channel is shown; the chassis contains multiple identical channels). Nominally, a 250-Ohm resistor would be used to convert the signal to 1-5V; here, the use of 249 Ohms gives a little bit of additional headroom for offscale high signals, and is what would be used internally in the 1102 module to permanently make it a 4-20 mA channel [47]. The instrument's current is passed through its connected downstream resistor, and the voltage drop across said resistor is measured by the SCXI system by

connecting both ends of the resistor to the input terminals for that specific channel. This generates a voltage signal slightly less than 1-5 V, depending on calibrations.

3.1.9.2 Software

The primary software environment is 32-bit LabVIEW 2012 SP1 running under 64-bit Microsoft Windows 7 Enterprise with SP1. The DAQmx drivers are more recent, being version 14. As the system is limited in its CPU resources (Pentium D 930), care was taken in designing the LabVIEW VI (Virtual Instrument, stored in a .vi file) to reduce CPU utilization while still maintaining functionality. Figure 22 shows the user interface for the data acquisition program.

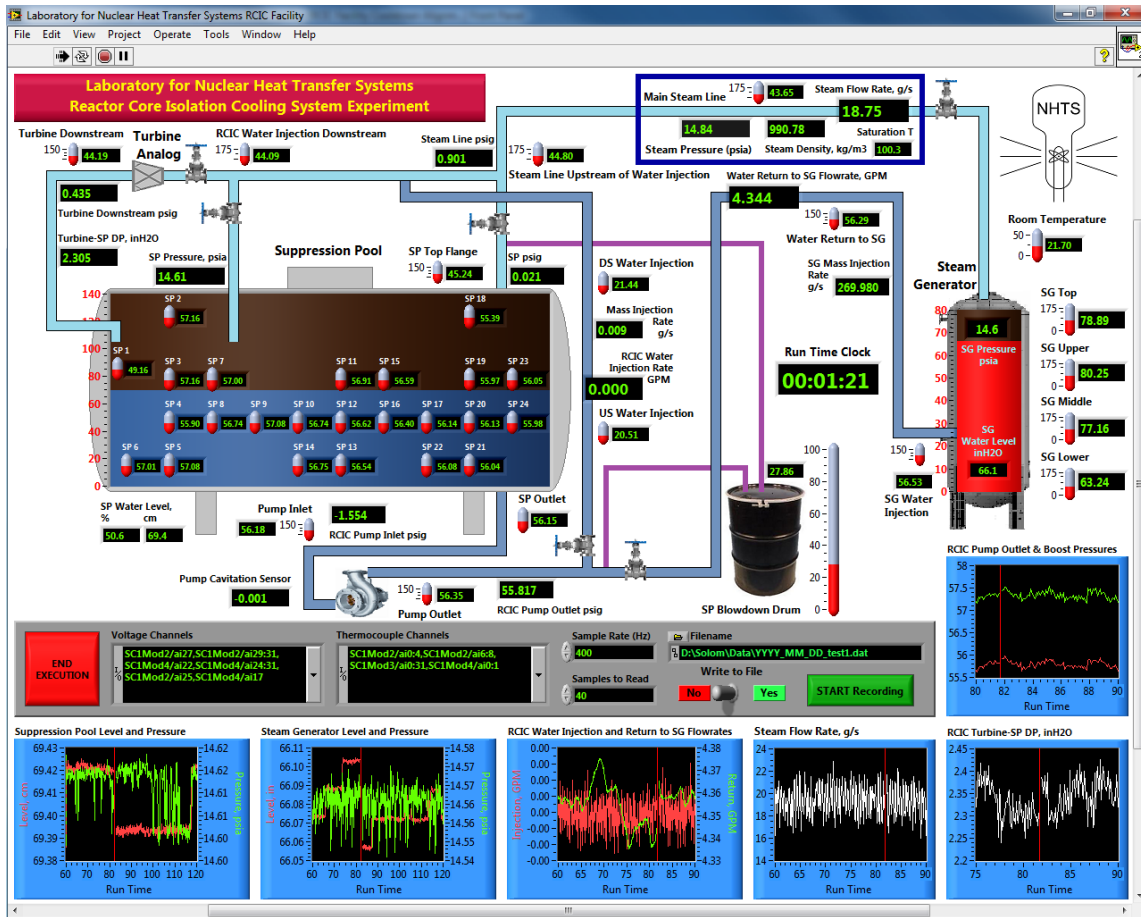


Figure 22: Data Acquisition Program UI

The LabVIEW VI produced for this experiment was based off of those for earlier experiments performed in the Laboratory for Nuclear Heat Transfer Systems, primarily the earlier Counter-Current Flow Limitation experiments. It uses similar conventions in both the User Interface and data logging output. However, it does some processing that was not done in earlier experiments. Most notably, in its averaging scheme, it not only logs the raw mean value for the channel (either raw voltage or internally determined temperature, depending on whether the channel is for general voltage or for a

thermocouple) but the standard deviation in the averaged sample set as well. This can assist not only in determining aspects of a channel's uncertainty, but can also assist in characterizing the amount of rapid fluctuations occurring in a channel that happen on timescales between those of the sample rate and the logging rate.

Each channel's processing follows a similar path. A collection of samples is taken and then passed on to the averaging scheme, which reports both the mean and standard deviation in either the temperature (thermocouples) or voltage (other instruments). Both the mean and standard deviation are recorded. Then, the mean value is passed on to a block that contains a calibration profile for that particular signal, transforming the raw voltage to a fraction from 0 to 1 of the instruments full scale (0 corresponding to 4 mA, 1 corresponding to 20 mA). This value, in turn, is passed to a block transforming it with the instrument's set range, thereby reporting the value determined by the instrument (i.e., 20 psia, 0.5 gpm, etc.). For some instruments, that is all that is needed. For thermocouples, such processing is done internally by DAQmx and is unnecessary downstream. For others, however, additional processing may be needed. For example, to transform the differential pressure readings into levels, the reported value must be subtracted from a reference level as the DP transmitters are set up to read the level on the low pressure side. Unit conversions may also need to be done, especially when the values for one instrument are used as part of another's calculations. The final computed value for each instrument is recorded as well.

This is very important for the vortex flowmeter. Both pressure and temperature compensations are applied, and steam density is actively computed using a dll from the X Steam Tables. In such cases, some of the intermediate values are recorded as well.

Besides logging all the relevant data, the LabVIEW VI presents much of it to the operator in the form of numerical indicators and charts. The indicators are overlaid on a simplified graphic of the RCIC System Experiment. This allows the operator not only to observe the live data, but also provides critical information enabling the determination of valve positions and any other relevant manual control.

All of the 4-20 mA instruments used by the data acquisition software for this experimental facility are given in Table 2; it gives the address/channel occupied in the data acquisition system as well as each instrument's basic information. The same is done in Table 3, except that it does so for the thermocouples in the system.

Table 2: Current Loop Instruments

<u>Model</u>	<u>Range</u>	<u>Purpose</u>	<u>DAQ Channel</u>	<u>P&ID Label</u>
Honeywell ST3000 STA940	0 - 150 psia	Steam Generator Pressure	SC1Mod2/ai27	I-1
Honeywell ST3000 STD924	0 - 110 inH2O	Steam Generator Level (DP)	SC1Mod2/ai29	I-2
Honeywell ST3000 STD924	1 - 80 inH2O	Suppression Pool Level (DP)	SC1Mod2/ai30	I-3
Honeywell ST3000 STA940	0 - 100 psia	Suppression Chamber Pressure	SC1Mod2/ai31	I-4
Yamatake MagneW 3000 PLUS	0 - 5 GPM	Water Return to Steam Generator	SC1Mod4/ai22	I-5
Foxboro 83W	0 - 2400 Hz	Main Steam Flowrate	SC1Mod4/ai24	I-6
Honeywell ST3000 STA940	0 - 130 psia	Main Steam Line Pressure	SC1Mod4/ai25	I-7
Honeywell ST3000 STD924	-20 - 400 inH2O	RCIC Turbine Exhaust to Suppression Chamber DP	SC1Mod4/ai26	I-8
Dwyer 682-3	0 – 250 psig	Pump Discharge Pressure Monitor	SC1Mod4/ai27	I-9
Dwyer 673-7	0 - 100 psig	Suppression Chamber Pressure Monitor	SC1Mod4/ai28	I-10
Dwyer 673-7	0 - 100 psig	RCIC Turbine Exhaust Pressure Monitor	SC1Mod4/ai29	I-11
Badger M2000	0 - 1.0 GPM	Water Injection to Steam Line Flowrate	SC1Mod4/ai30	I-12
Dwyer 673-7	0 - 100 psig	Steam Line Pressure Monitor	SC1Mod4/ai31	I-13
Dwyer 673-7	0 - 100 psig	Pump Inlet Pressure Monitor	SC1Mod4/ai17	I-14
Omegadyne PX309-005G5V	0 - 5 psig	Hot Water Tank Level	SC1Mod2/ai28	I-15
Yamatake MagneW 3000 PLUS	0 - 15 GPM	HX Hot-Side Flowrate	SC1Mod4/ai23	I-16

Table 3: Module 3 Thermocouples

<u>Thermocouple</u>	<u>DAQ Channel</u>	<u>P&ID Label</u>
SP 24*	SC1Mod3/ai0	T-9
SP 23*	SC1Mod3/ai1	T-10
SP 22*	SC1Mod3/ai2	T-11
SP 21*	SC1Mod3/ai3	T-12
SP 20*	SC1Mod3/ai4	T-13
SP 19*	SC1Mod3/ai5	T-14
SP 18*	SC1Mod3/ai6	T-15
SP 17*	SC1Mod3/ai7	T-16
SP 16*	SC1Mod3/ai8	T-17
SP 15*	SC1Mod3/ai9	T-18
SP 14*	SC1Mod3/ai10	T-19
SP 13*	SC1Mod3/ai11	T-20
SP 12*	SC1Mod3/ai12	T-21
SP 11*	SC1Mod3/ai13	T-22
SP 10*	SC1Mod3/ai14	T-23
SP 9*	SC1Mod3/ai15	T-24
SP 8*	SC1Mod3/ai16	T-25
SP 7*	SC1Mod3/ai17	T-26
SP 6*	SC1Mod3/ai18	T-27
SP 5*	SC1Mod3/ai19	T-28
SP 4*	SC1Mod3/ai20	T-29
SP 3*	SC1Mod3/ai21	T-30
SP 2*	SC1Mod3/ai22	T-31
SP 1*	SC1Mod3/ai23	T-32
RCIC Turbine Analog Outlet	SC1Mod3/ai24	T-33
Steam Line 6-ft Post-Water Injection	SC1Mod3/ai25	T-34
Pump Inlet	SC1Mod3/ai26	T-35
Pump Outlet	SC1Mod3/ai27	T-36
Suppression Chamber Outlet	SC1Mod3/ai28	T-37
Steam Line Upstream of Water Injection	SC1Mod3/ai29	T-38
Water Injection Line Pre-Flowmeter	SC1Mod3/ai30	T-39
Water Injection Line Post-Flowmeter	SC1Mod3/ai31	T-40

*Location given in Table 1

Table 4: Module 2 and 4 Thermocouples

<u>Thermocouple</u>	<u>DAQ Channel</u>	<u>P&ID Label</u>
Room Temperature	SC1Mod2/ai0	T-1
Steam Generator Top	SC1Mod2/ai1	T-2
Steam Generator Upper	SC1Mod2/ai2	T-3
Steam Generator Middle	SC1Mod2/ai3	T-4
Steam Generator Lower	SC1Mod2/ai4	T-5
Steam Generator Water Injection	SC1Mod2/ai6	T-6
Suppression Chamber Top 1.5-inch Flange	SC1Mod2/ai7	T-7
Suppression Chamber Blowdown Drum	SC1Mod2/ai8	T-8
Main Steam Line Near Vortex Flowmeter	SC1Mod4/ai0	T-41
Water Return to Steam Generator Line Near Flowmeter	SC1Mod4/ai1	T-42
Hot Water Tank Outlet	SC1Mod2/ai5	T-43
Auxiliary Hot Water Pump Inlet	SC1Mod4/ai13	T-44

3.1.9.3 Cable Shielding and Grounding

Proper cable shielding is a paramount issue when assembling an instrumentation system. While current loops have some immunity to noise that is lacking in pure voltage transmission, such immunity is not absolute. In addition, with weak voltage signals such as those generated by thermocouples, noise picked up in long cable runs can swamp the signal. Therefore, in order to obtain high quality data, the transmission paths must be protected from noise – the cables must be properly shielded and all grounds set up correctly.

In this facility, all cables save five are shielded. The five unshielded cables connect to the four thermocouples in the steam generator and the one room temperature

thermocouple. Each of these was installed in earlier experiments, uses relatively short cables, and functioned well in previous endeavors.

The other cables are shielded, and connect their shields to ground only at one end in order to prevent ground loops. For the cables carrying the 4-20 mA signals, they all ground on the chassis to the converter box containing the instrument's 249-ohm resistor. The thermocouple cables land their grounds on the ground connector in their respective SCXI-1303 terminal blocks. While some of the thermocouple cables bundle eight twisted pairs into a single shielded cable, crosstalk between pairs is not expected to be an issue. The short unshielded distances at some of the cables' connector ends is also not expected to cause any appreciable noise injection.

3.1.10 Calibrations

In order to have any confidence in the recorded data, all the instruments must have some sort of calibration. Therefore, where applicable, calibrations have been carried out.

The Honeywell ST3000 Series 900 transmitters were calibrated in two phases: sending them out to calibrate their pressure readings, and a signal calibration on their 4-20 mA outputs to implement in the data acquisition software. Of the six shipped to a calibration service, two of the existing transmitters were found to have defective electronics in need of replacement. Once their measurements were calibrated, signal calibration profiles could be developed as well. The signal calibration profiles were developed in the same way for the pressure transmitters as for the magnetic flowmeters. Using a small LabVIEW VI developed for this particular task, two-point calibration

profiles can be easily computed. With the Honeywell Smart Field Communicator or (if present) a built in menu system, the transmitters were set to output their full-scale (100%, 20 mA) signals. These were recorded by the software and time-averaged over a period of at least 100 seconds. Then, they were each set to output their low-end (0%, 4 mA) signal. Again, the signal was recorded and time-averaged for a minimum of 100 seconds. Assuming full linearity straight through from the measurement to the analog output to the analog to digital conversion in the DAQ, such two point calibrations are sufficient to fully derive the curve.

Not all of the instruments could be so easily calibrated. Each of the gauge pressure transmitters, unable to connect with a Smart Field Communicator, had to have a more creative approach. Some of them, easily disconnected from the system, were able to follow a similar paradigm (a two-point, low-pressure and high-pressure, approach). Their low-end (0% of full scale) points were developed from exposure to atmospheric pressure. The high-end points, however, were somewhat different. By connecting an Omega DPI 603 calibrator (last calibration date: July 19, 2005), and holding at 90.00 psig, points for 90% of full scale (18.4 mA nominal) were found and two-point calibration profiles were estimated. Since the last known calibration date for the calibrator is so far in the past, is not considered reliable. However, it is not expected to have drifted very far.

The remaining two Dwyer gauge pressure transmitters were not easily removed from the system for calibration. For them, a sort of point-and-a-half technique was employed. By measuring the height of the water column above them, a low-end

pressure can be estimated. For the transmitters in question, this is between 0.05% and 1.5% of full scale. The high points were estimated with a bit of a creative leap. It was assumed that their nominal 20 mA output actually corresponds to a 20.00 mA current at 100% full scale output. An additional assumption was that the measured current on the DPI 603 calibrator was accurate. Then, the transmitter was disconnected from the circuit and the calibrator wired in with its ~12 mA current generator enabled. The result was scaled to 20 mA, and assumed to correspond to the nominal 20 mA signal from the transmitter. As this is not expected to be a very accurate technique, the resulting data from the Dwyer transmitters are not expected to be of high quality and are not used analytically.

The most intricate calibration technique used in this experimental facility may belong to the Foxboro vortex flowmeter. As documented in the manual, the procedure involves the calculation of an expected upper range frequency, the temporary setting of DIP switches, the removal of the electronics unit from the flowmeter body, disconnecting the sensor unit and in its place connecting a function generator, and operating the function generator at the predetermined upper range frequency and then at zero while adjusting the appropriate potentiometers. Once complete, the temporary connections must be disconnected, the electronics returned to the housing and the DIP switches set appropriately [42]. For this setup, an upper range frequency of 3000 Hz was used (later reduced to 2400 Hz), as it is the maximum that the flowmeter can handle, and the calculated result for an absolute limiting flowrate was close to it. In addition, the function generator available does not isolate its signals as required by the transmitter but

rather ground-references them. Therefore, in order to provide the requisite isolation to allow the signals to float, the function generator was plugged into a UPS; the UPS was then unplugged from the wall to remove the ground reference during operation.

Furthermore, the frequency was monitored by an oscilloscope to verify that the reported frequency on the function generator was indeed within tolerance.

Profiles for reading thermocouples are built in to the LabVIEW packages, and the thermocouples themselves are assumed to have maintained their “Special Limits of Error” [49] tolerances with little drift or degradation. There is little to do other than to ensure that the electrical connections are sound and that the DAQ hardware on the receiving end is reading the signals correctly. The current DAQ card, where the actual measurements take place, is an NI PCIe-6341 X Series data acquisition card. It replaced an older NI PCI-6034E DAQ card that would no longer accept a calibration or produce consistent, high quality data. The new card was procured with a two-year calibration compliant to ANSI/NCSL Z540-1-1994 (the NI “Compliant Calibration” calibration service level), and is therefore believed to have excellent accuracy.

3.2 SHAKEDOWN TESTING

After the loading of DI water into the system, two major shakedown tests of the experimental facility were performed. The first aligned the system to the SRV sparger analog, and warmed the system up to a relatively mild degree when compared to later tests (final pool temperatures near 63 °C for the SRV-alignment shakedown test). The second test aligned the system to the RCIC analog, and warmed the system up to near saturation conditions.

3.2.1 Liquid Fill

A full complement (half of the Suppression Chamber's capacity) of DI water was filled into the system prior to the major shakedown tests. The Suppression Chamber Analog had previously been filled to capacity with clean city water, which was fully drained before the DI water was added. An attempt was made to do some flushing with DI water to remove contamination in the system, but it was minimal and as a result there is expected to be some degree of residual salts, particulates, etc. from the city water. During the fill, it was discovered that the high purity of the DI water was such that the water's conductivity dropped below the point at which the empty pipe detection circuitry in both the Yamatake and Badger magnetic flowmeters would function correctly. This led to a small bit of unmonitored flow into the system, but further examination of other instruments led to the conclusion that total volume injected in that period was somewhat more than one gallon. The empty pipe detection circuitry was subsequently disabled in both flowmeters. Across the three days in which system filling was conducted (two resin bed regeneration cycles were necessary), the Suppression Chamber Analog was supplied with nearly 768.6 gallons, bringing the water level in the vessel to slightly higher than the halfway mark (31.8 out of 59 inches).

3.2.2 SRV Shakedown

The first shakedown test performed was a primary alignment with the SRV sparger analog. At certain points, operational verification of most of the flowpaths was ascertained. The pump and recirculation paths were found to be operational, as was the

water injection into the steam line. The RCIC turbine and sparger analog alignment was not tested, as this was planned for a second shakedown test.

During this test, it was determined that the wiring connecting the Yamatake magnetic flowmeter's detector to the converter had an easily resolved problem: on one end, two of the wires were connected to each other's terminals. This resulted in the flow being measured in reverse, and indicated as such on the converter. As there is a limit to how much reverse flow can be transmitted on the 4-20 mA line (roughly 5%), the flow back to the steam generator recorded by the DAQ is not correct; the limit had been exceeded by a fair amount, according to the converter. This issue was quickly and easily resolved.

A second issue, perhaps more serious than the first, was identified as well. Based not only on indications from the vortex flowmeter assembly, but by a rough heat balance on the temperature rise in the Suppression Chamber Analog pool, the steam generator was not providing as much heating power as it should have. It was set at full power; every heater was turned on for a nominal power of 157 kW. However, at the full delivered power, steady state output (without makeup water from the return line being injected) was near 50 g/s; this was equivalent to roughly 109 kW based on steam table data. Further investigation revealed 5 blown fuses in the main electrical control panel, disabling 50 kW of heater power. It is not known why 5 of the fuses blew; examination revealed no problems on those circuits. It was in those examinations that it was discovered that two of the 6.25 kW heater circuits were wired to only operate at half power. It is not known why those heaters were wired in that manner. Even with the

fuses replaced, this brings to total nominal power of the steam generator to 150.75 kW. After shakedown testing, an electrician restored full operating power (157 kW) to the steam generator

With a steady state steam flow around 50 g/s, intermittently lower when water was pumped back into the steam generator, the bulk water temperature in the Suppression Chamber Analog pool went from an initial temperature of 24 to 63 °C. The entire test lasted nearly 2.5 hours, but heat (steam) was only injected into the Suppression Chamber Analog for a little more than half that time.

The test itself was not quiet, even with 2-inch thick fiberglass insulation surrounding the Suppression Chamber Analog. There were sounds emanating from within the vessel that seemed to be produced by violent void collapse near the sparger. This is not a surprise, as the bulk water temperature was highly subcooled.

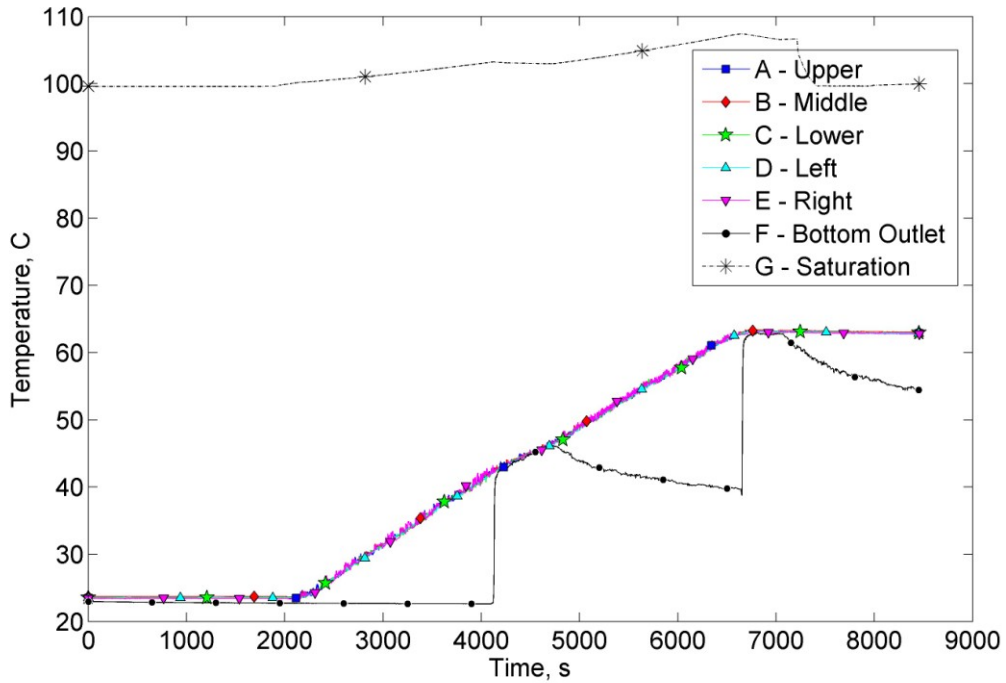


Figure 23: SRV Shakedown Pool Thermal Progression

From the beginning of the shakedown test to its end, the Suppression Chamber Analog pool temperatures seem to have been remarkably even; very little thermal stratification appears to have been present. The pool appears to have been well-mixed; a thermal profile for the test is given in Figure 23. The only deviations are at the pool outlet; due to intermittent operation of the RCIC Pump, water in the line at the measurement point was able to cool down between pumping operations. Whether or not this mixing would be maintained through increased final temperatures was left undetermined at shakedown; such a test was conducted in the data-gathering tests.

3.2.3 RCIC Shakedown

The second shakedown test aligned the facility to the RCIC sparger analog. Before the test, the blown fuses in the steam generator were replaced and the miswiring in the Yamatake magnetic flowmeter was corrected. Several days had passed since the first shakedown test, and yet the bulk pool temperatures were still significantly higher than room temperature. After using the pump in recirculation mode to thoroughly mix the pool, the temperatures were near 48 °C; the room temperature of the lab was 21 °C. Some time was allowed to pass before proceeding with the test in order for the circulation currents in the vessel to die down. For comparison to the earlier shakedown test, a target steam flow rate of roughly 50 g/s was chosen. The steam generator started with a full water load, and the return flow was not engaged until the level had dropped sufficiently for makeup water to be necessary for continued operation. The steam and makeup water flow rates can be seen in Figure 24.

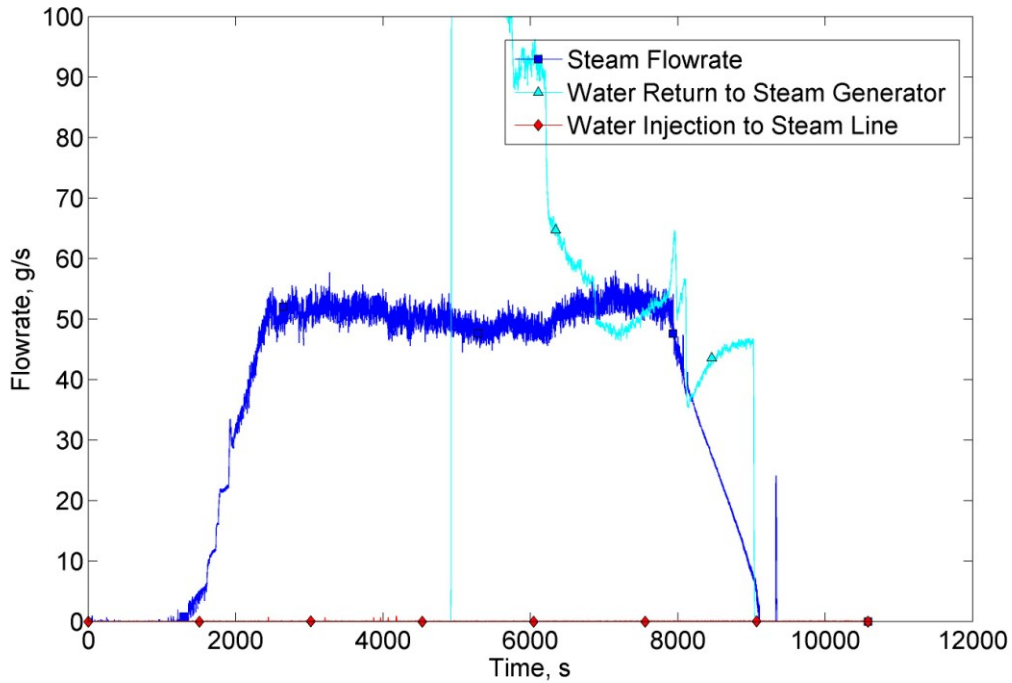


Figure 24: Shakedown Steam and Water Flowrates

This test seemed to be louder than the first, and the void collapses sounded to be more violent as well. As there are additional instruments in this alignment, they may be able to shed some light on the phenomena occurring in the sparger. Major (audible through earplugs) violent events seem to have some recorded presence in the data; they seem to produce spikes appearing in both the sparger’s internal temperature as well as in the differential pressure reading from the Suppression Chamber Analog to the turbine analog’s outlet. An example of this can be seen in Figure 25. The largest spikes occurred roughly every 2-5 seconds; smaller events (still audible to operators) seemed to be occurring more frequently.

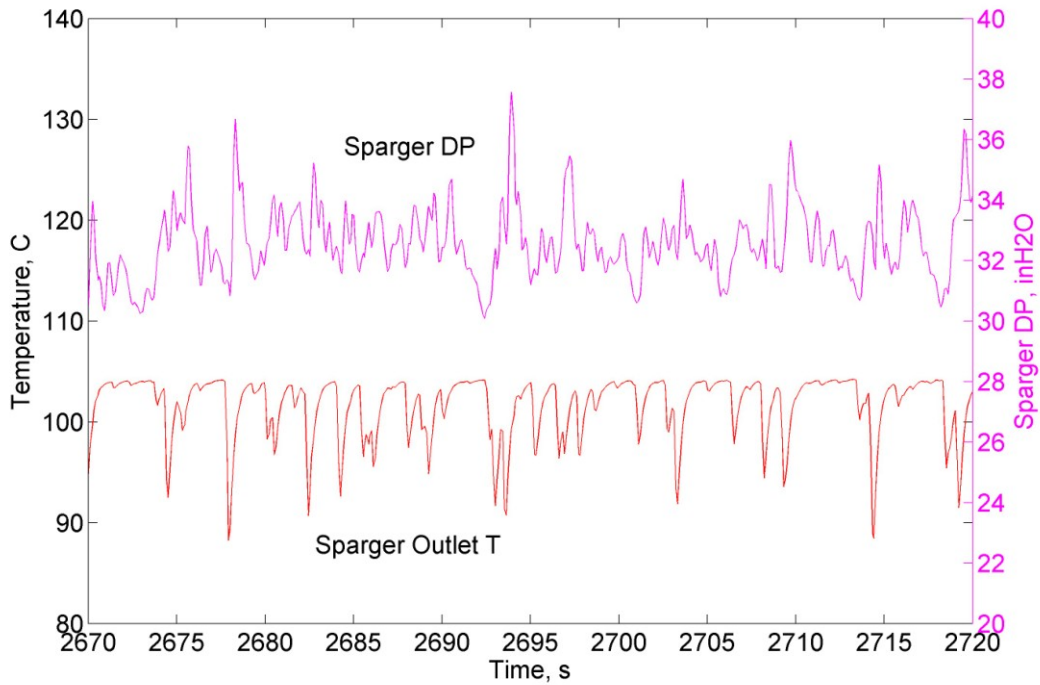


Figure 25: Steam Chugging Spikes

After some time, major chugging events appeared to cease as the pool temperatures warmed up. At the time period in the test focused on in Figure 25, the bulk pool temperatures were between 50 and 60 °C. Later in the test, when they were in the vicinity of 70 °C, corresponding spikes in both the differential pressure and sparger temperature vanished; Figure 26 (with the pool mid-level near 90 °C) has a distinct lack of corresponding spikes on both measurements. However, other phenomena of interest were taking place. While the lateral pool temperatures were very close to each other throughout the test (seen in Figure 27), vertical stratification appears to occur.

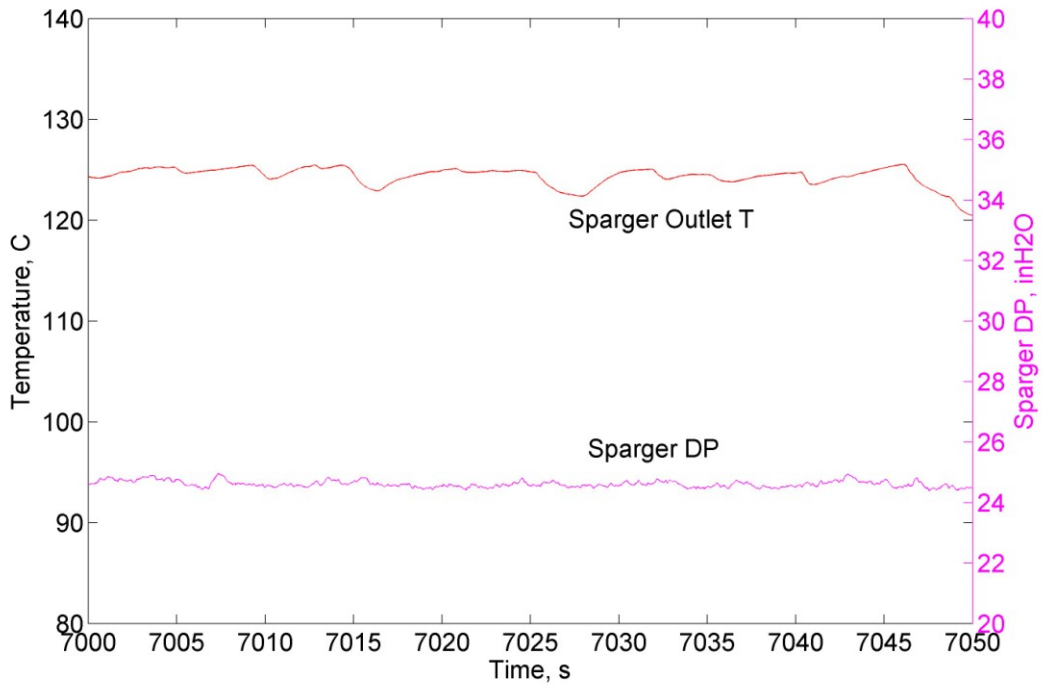


Figure 26: Stable Flow without Chugging

The thermocouples near the mid-level of the pool ($z = 15$ inches in Table 1), with the notable exception of Thermocouple SP8, are all very consistent. Thermocouple SP8, which in Figure 27 reads much higher than the others and appears very noisy, is rather close to the outlet of the RCIC sparger analog. It would appear to be picking up very local disturbances near the sparger's outlet.

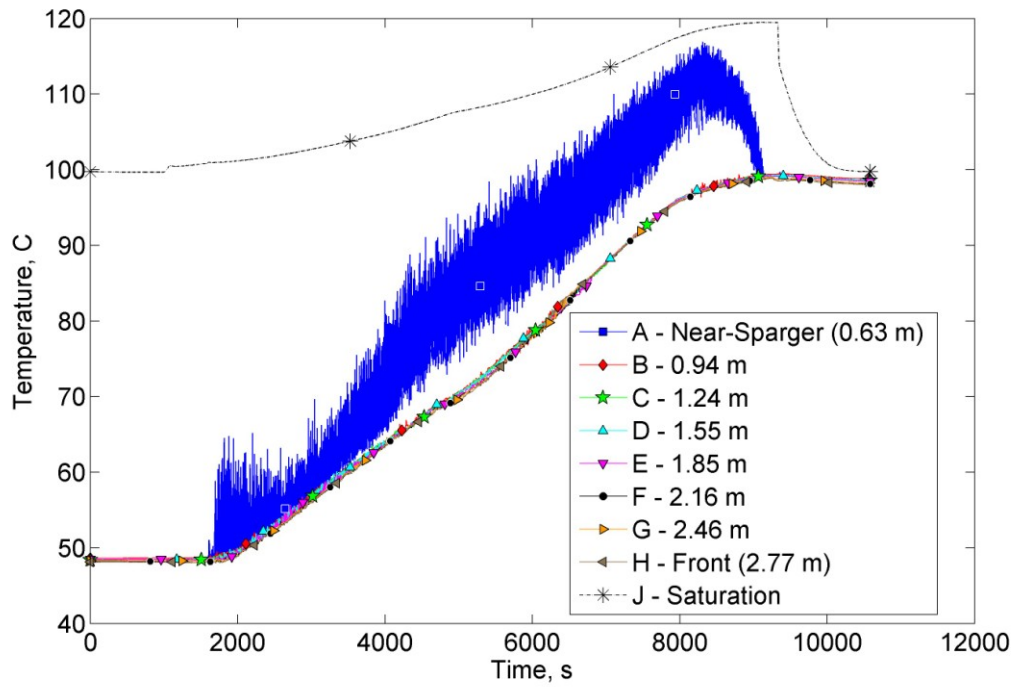


Figure 27: Lateral Pool Temperatures

The thermal profiles appear somewhat different when looking at a comparison of vertical thermocouples. This is seen in Figure 28. Readings from the five submerged thermocouples at the $x=0$ inch position are compared.

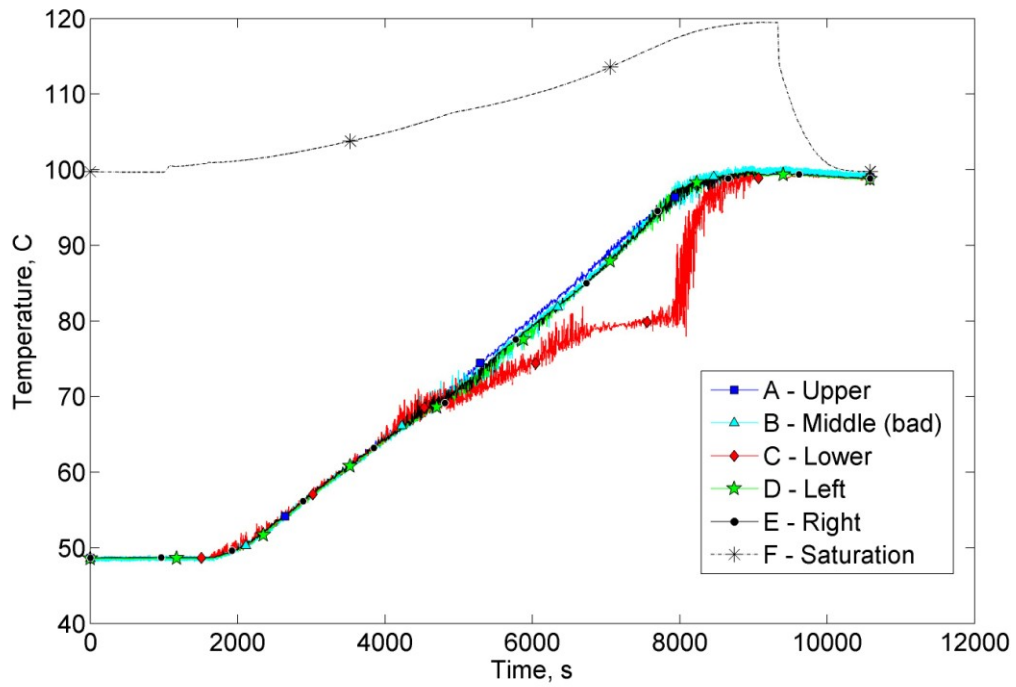


Figure 28: Sparger-End (Rear, x = 0 Inches) Temperature Profile

The vertical stratification is not seen only at the sparger end of the vessel; it appears in the middle as well as the front end. If anything, the vertical stratification is more pronounced in the x=48 inch position than at x=0; this is depicted in Figure 29.

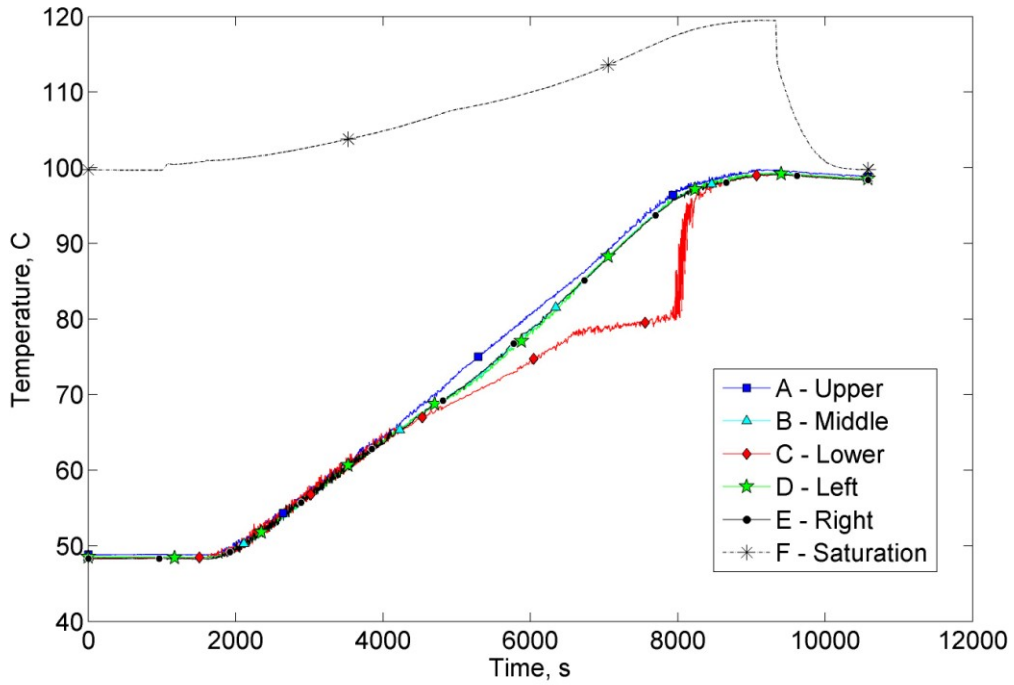


Figure 29: Pool Temperatures, Pool Center (x = 48 Inches)

Separation between top, middle, and bottom-level temperatures is clear in the front end of the vessel as well. These temperatures, measured at the x=84 inch position, show the same appearance and disappearance of vertical stratification as the others. They are shown in Figure 30, along with the vapor space temperature at that axial location.

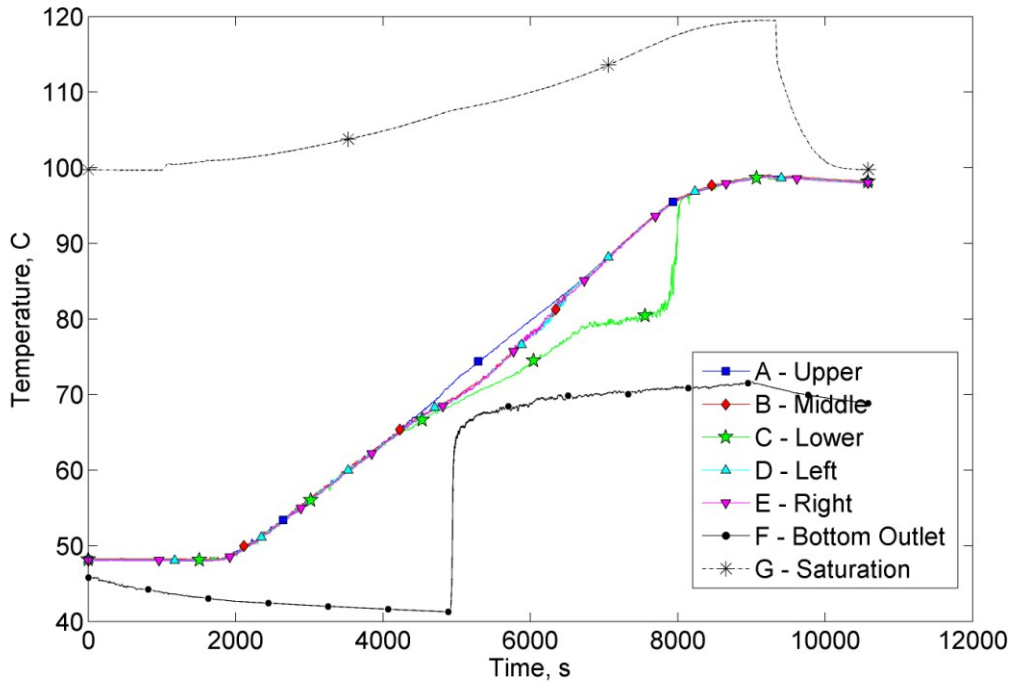


Figure 30: Pool Temperatures, Vessel Front (x = 84 Inches)

The most interesting feature of the vertical temperature comparisons is the appearance and sudden disappearance of vertical thermal stratification. It appears that early in the test, at cooler pool temperatures, the apparent chugging in the sparger was an effective method for agitating the pool and maintaining uniformity. Once the chugging largely ceased, a significant amount of pool mixing would therefore end as well. With stabilized condensing flows through the sparger, if a jet does not traverse much below the outlet, the bottom of the pool may remain relatively stagnant and cool. However, it is not permanent; at some point, there appears to be a remarkably sudden rise in the lower pool temperatures. The reason behind this was at first unclear, but based on subsequent testing, the condensation rate around the sparger would tend to decrease as

pool temperatures increase. Steam bubbles would then emerge from the sparger and rise towards the pool surface until they either reach it or condense, producing currents that would tend to agitate the pool. They would therefore mix the water and bring the temperatures back to uniformity.

3.3 IDENTIFIED ISSUES

Several, mostly minor, issues arose during the operation of the experimental facility.

3.3.1 Pump

The pump employed in these tests experienced multiple, independent failures and had somewhat misleading characteristics given in its data sheet. The original seal installed in the pump is a Buna-N mechanical seal, which failed with a large tear through the rubber on the shaft side during the first attempt at Test #1 (later completed as Test #15). Upon replacement, it was discovered that the seal itself is rated for much lower temperatures than those listed for the pump as-delivered; therefore, SEAL FAILURE IS TO BE EXPECTED WHEN OPERATING THE PUMP AT HIGHER TEMPERATURES STILL WITHIN ITS GIVEN LIMITS. As a result, the failed seal was not replaced in-kind but rather was upgraded to a Viton seal, with a listed temperature limit of 250 °F.

During the pump disassembly, it was found that significant corrosion had already begun attacking the cast iron components. This was not surprising, as the system at the beginning of testing can be expected to have significant oxygen in the water. Furthermore, the pump contains the only cast iron in a largely stainless steel system;

given the difference in galvanic potentials between the materials, corrosion is to be expected. This results in the pump being a potential source of water contamination if the water is not re-purified in long-term reuse schemes.

Later on during testing, the pump developed an unrelated failure between Test #4 and Test #5. During a period of lower-temperature cooldown operations, the centrifugal switch in the motor shattered, and the motor became completely inoperable. Pieces were found embedded in the stator coils, and the motor was deemed unfit for repair due to the potential electrical hazards. As the pump is relatively inexpensive, instead of replacing only the motor, a brand new replacement pump (including the motor) was procured. Since it was the same pump model, the seal was immediately replaced with a new Viton version to prevent premature failure.

3.3.2 Air Compressor Oil

The air compressor employed in this experiment for both system air pressurization as well as air purging is a reciprocating type. Even with significant filtration, lubrication oil from the compressor made its way into the test facility. This is evident based upon the characteristic oily odor it gave the Suppression Chamber volume; facility operators found the odor to be present when decompressing the Suppression Chamber. It was stronger when significant amount of air had been pumped into the system through the compressor. As a result, the compressor can contribute to system contamination.

3.3.3 Thermocouple SP4

During shakedown testing, it was found that Thermocouple SP4 read with greater noise than any of the others installed in the system, and the noise was found to not be an issue with the wiring but with the thermocouple itself. The noise appeared to be centered around the correct reading, and it may be possible to filter most of it out in post-processing. Furthermore, the correct reading can be inferred from the nearby lateral thermocouples. Therefore, due to the inherent difficulty and risk of damage to other components in replacement operations, it was decided to leave the thermocouple in place and label it as an 'unreliable' source of data.

3.3.4 Magnetic Flowmeter Failure

Near the end of the testing program, the magnetic flowmeter measuring feedwater flow to the steam generator began producing wildly erratic and incorrect results. Experimental testing was immediately aborted, and the flowmeter was removed from service. Diagnostics revealed that one of the electrodes was no longer electrically connected to its terminal inside the detector head, necessitating manufacturer service and repair. In order to continue the testing program with the little time left, an alternate flowmeter was installed. It too is a Yamatake MagneW 3000 PLUS; however, it has a lower labeled temperature limit of 120 °C. As a result, care must be taken by operators to ensure that its thermal limits are not exceeded until the original meter can be repaired and reinstalled.

3.3.5 Limit for Vortex Flowmeter

The noise issue with the vortex flowmeter necessitating the use of a flow silencer was resolved for the primary power levels employed in the tests performed for this research (see Section 3.4). However, extended very-low-power (32 kW) testing revealed that it could still be an issue. It was only observed to be a problem at the end of testing in the standard alignment, when the steam density is greater and the velocity resultingly lower. It is also approaching the lower limit for the flowmeter's accurate Reynolds number range. Problems did not occur until the vortex shedding frequency was below 200 Hz (between 150 and 200 Hz); it is advisable for future efforts to either avoid this operating range or to make alterations to the system to address it.

3.3.6 Level Indication

Level indication in both the Suppression Chamber and the Steam Generator was performed by using differential pressure measurements with Honeywell STD924 transmitters. Observation during system operation, and by specific testing of the issue, found a common mode pressure dependency. When a common pressure, i.e., system pressurization, appeared on both the high pressure and low pressure ports on the transmitters, the differential pressure reading was altered. Ideally, the measured differential pressure does not have any dependence on common pressures appearing on both ports, only the pressure difference, but this was found to not be the case. As pressures changed, the level readings were seen to vary by several centimeters, even though the actual water levels were not changing. While this could correspond to incorrect volume readings of 100 gallons in the 1,400 gallon vessel (when the level is

near the middle of the vessel), the error is still on the order of 1% for the full range of the transmitter. The change in reading (offset) for the Suppression Chamber is shown in Figure 31, where the system pressure was increased and then decreased without any changes in pool inventory.

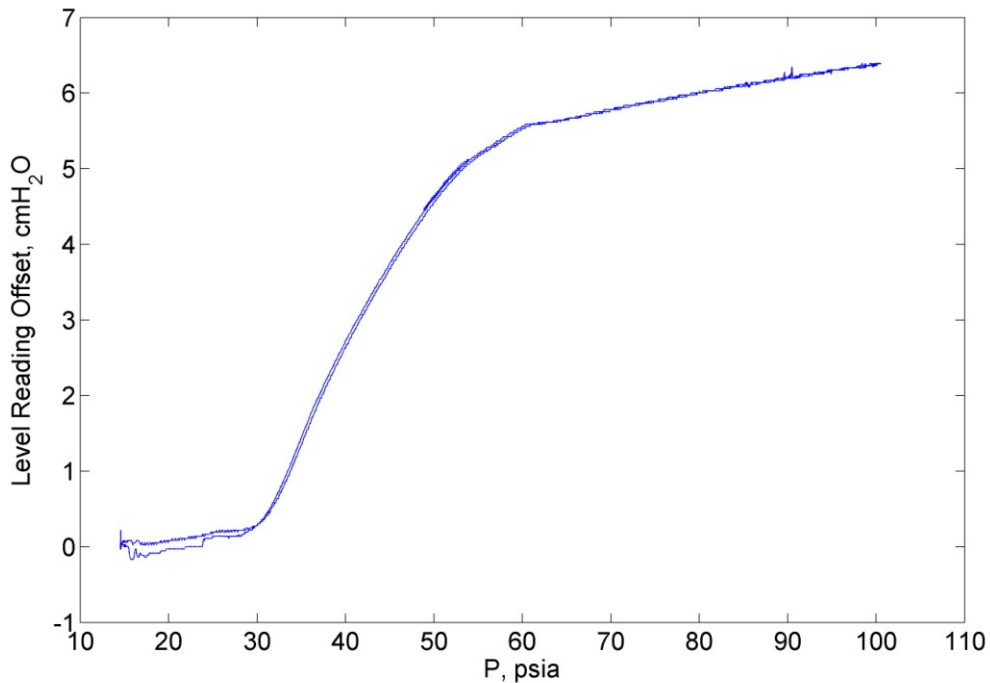


Figure 31: Common-Mode Pressure Level Reading Offset

Such an issue could be the result of bubbles in the instrument pressure reading lines. Indeed, if installed according to the manual, the particular transmitter model employed in this experimental facility may permanently trap air bubbles within the meter body without the ability to bleed them off. However, such bubbles are not expected to be large enough to account for the observed degree of pressure dependence.

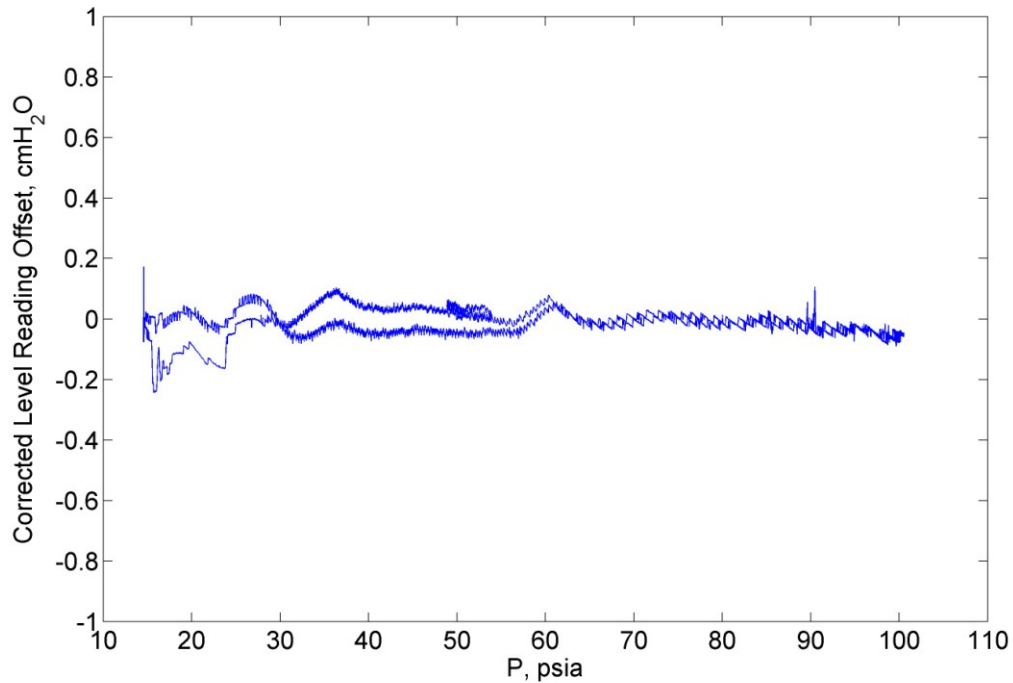


Figure 32: Level Offset after Correction

Fortunately, the common mode pressure dependencies were found to be consistently repeatable. While they did not match each other for the different transmitters (the Suppression Chamber level vs. the Steam Generator level), the profiles were found to have very little variation with time. Therefore, a correction profile for the level reading in the Suppression Chamber was developed and applied in the data processing script to correct the common mode pressure issue. It uses a polynomial (a function only of the Suppression Chamber's pressure) to compute an absolute offset (the shift was taken to be absolute rather than relative/fractional) and subtract it from the

originally indicated reading. The offset in the level reading with the correction term applied is shown in Figure 32.

3.4 POST-SHAKEDOWN REPAIRS

Further shakedown testing revealed other latent issues in the experimental facility. Significantly, the low conductivity present in the water required large time constants ≥ 10 s to be set in the magnetic flowmeters to smooth out the resulting unrealistic fluctuations in the reported flow measurements. However, this also has the impact of reducing measurement responsiveness; high-speed flow transients will not appear correctly in the readings, if at all. Fortunately, the test conditions are not such that the water flowrates would be rapidly changing, and such time constants are therefore acceptable.

A more insidious and difficult to resolve issue revolved around the vortex flowmeter. Close attention to steam generator power levels and fluid flowrates (after the resolution of the steam generator's electrical problems) revealed discrepancies that were not constant in time. It appeared that the vortex flowmeter would sometimes transmit flow rates that were well in excess of 150% of their proper values. This was especially noticeable at lower flowrates/power levels with higher pressures in the steam generator.

After thorough investigation, it was determined that the likely culprit was excess noise in the steam flow; in the flowmeter employed, gas flows, especially at lower flowrates, produce a relatively weak acoustic signal at the transducer element, and noise at similar frequencies may be difficult or impossible for the electronics package to discriminate from the vortex shedding signal. The result is significant misreading.

The determination was done by connecting the sensor element to an oscilloscope and running various flows through the meter as installed in the system. Under the conditions that tended to produce the most severe misreading, the waveform read by the oscilloscope was severely distorted; the expected readout in a trouble-free system is a relatively pure sine wave at the vortex shedding frequency. This came as a bit of a surprise, as the flowmeter was installed with careful attention to its given requirements, and had L/D ratios both upstream and downstream well in excess of the minimum given values.

Further probing with a stethoscope revealed that the likely source of the noise was the main steam control valve. Under the most troublesome conditions, the valve is near closed. Such shallow valve angles are known to produce noise. In addition, the valve may encounter moisture. While the separator in the steam generator system can effectively remove the vast majority of entrained moisture, it is not perfect. As the system up to the valve is at saturation, any heat losses would work to condense small fractions of the steam. Such condensate would naturally flow to the valve. As it passes through the valve into the lower-pressure downstream piping, any moisture left in the steam would tend to flash; this can also be expected to add noise to the flow.

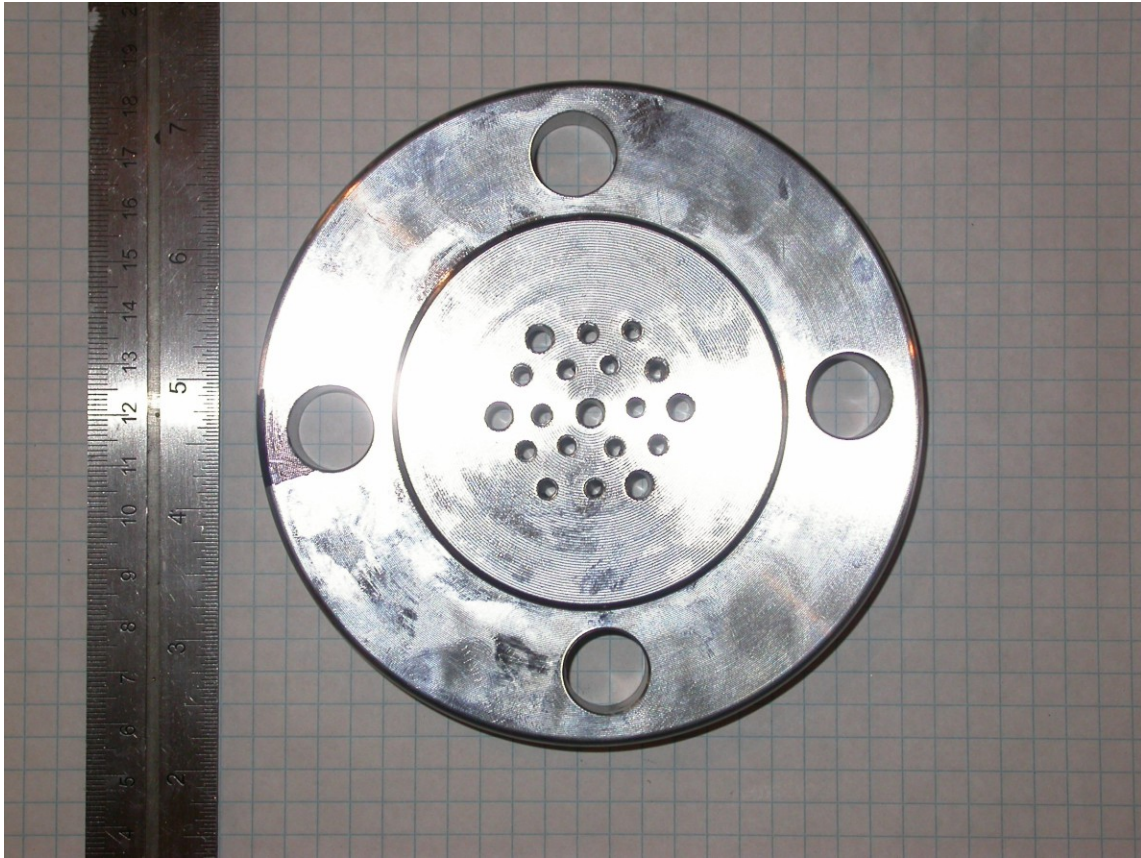


Figure 33: Silencer Plate

In order to limit the noise found in the flow to more tolerable levels, a thick multi-orifice plate was produced (Figure 33) and inserted into the steam line six inches downstream of the main steam control valve. It consists of a 1.5-inch NPS CL150 stainless steel flange blind with 19 holes bored through it in a hexagonal array. Of these holes, 5 have a diameter of $3/16$ " , while the remaining 14 have a diameter of $1/8$ " ; all are chamfered on both sides of the plate. Once installed, this silencer plate appeared to function well; the distortions and fluctuations present before installation largely disappeared. While it adds a flow restriction/head loss to the system, it has the effect of

staging the loss from the control valve and allows the valve to be opened further than it otherwise would have been. Not only does it limit the downstream propagation of valve noise, it also allows for less to be generated in the first place.

3.5 SYSTEM MODIFICATIONS AND ENHANCEMENTS

After the shakedown tests and repairs, some enhancements were made to the system as well as other modifications. The original orifice plate in the RCIC Turbine analog was found to be too small to allow full-power testing under reasonable conditions, and was therefore modified between Test #1 and Test #2. Its original 0.348" bore diameter was enlarged to 7/16", and Test #1 was repeated with the new orifice as Test #2.

In addition to the adjustments to the orifice, modifications were made to the pump and connected equipment. A heat exchange system was added as well in order to reduce the cooldown period to reasonable timeframes as well as to conserve deionized water by reducing the demand for Suppression Chamber atmospheric blowdown operations.

3.5.1 Pump and Related Equipment

A further enhancement came after the second major failure of the original RCIC pump (between Test #4 and Test #5). A strainer was added upstream of the pump to prevent debris from accumulating in the impellers, which was discovered during post-failure examination of the first RCIC pump.

Based on the experimental system's performance through Test #10, it was determined that additional capacity on the RCIC Pump Recirculation Line was needed to prevent pump case overpressure during certain tests. To that end, the original

recirculation line (with RCIC Pump Recirculation Valve V-67) was supplemented with a higher-capacity controllable recirculation line (containing recirculation globe valve V-66) before Test #11. This allowed the operator to shunt enough additional pump flow to direct pump outlet-inlet recirculation to shift the operating position on the pump curve (limiting boost pressure) without changing net system flow rates. This is especially important near the end of pre-pressurized tests, where the pump head in addition to the pressurized inlet conditions could easily exceed the pump's casing pressure limit.

Between Test #11 and Test #12, RCIC Pump-side instrumentation was upgraded. The original Dwyer 673-7 gauge pressure transmitter used for I-9, with a 0-100 psig range, was replaced with a Dwyer 682-3 with a 0-250 psig range. This allows for operators to electronically monitor the outlet pressure on the RCIC pump over its full range up to the casing pressure limit, rather than a subset of it. In addition, a Dwyer 673-7 gauge pressure transmitter was installed immediately before the pump inlet on the suction line as I-14. With the two new instruments, the data acquisition software was updated, and significant additional pump performance parameters could be inferred. Some of the updates to the data acquisition software were operational in nature – alarms were added to alert operators to conditions in the facility that approach design limits.

3.5.2 Heat Exchange System

While not a modification to the system during experimental runs, a heat exchange system added to the facility greatly enhanced the ability to run multiple tests in a week, as such was previously hindered by low cooldown rates. It provided sufficient cooling to allow for three tests per week.



Figure 34: Heat Exchanger Tubing

The centerpiece is an ad hoc heat exchanger. It was assembled from spare parts in the NHTS Laboratory, including 0.5” stainless steel tubing (many short lengths connected together as shown in Figure 34), a 55-gallon drum, and pumps. Due to the potential pressures in the Suppression Chamber as well as the flow restriction of the tubing, more than one pump was needed to provide adequate head for reasonable flow rates through the tubing (the hot liquid flows through the tubing and is cooled by the pool of cooler city water in the drum). The tubing sits inside the drum, below the

waterline. The pool of water in the drum was rapidly circulated by a circulation pump as well as the flows of incoming (cold) and outgoing (heated) city water.

Figure 35 depicts the heat exchange system as aligned during cooldown operations. Hot water from the Suppression Chamber flows into the atmospheric hot water tank through the main water lines and V-10. From there, the hot water is pumped through a magnetic flowmeter and the heat exchange drum. It then flows into the repurposed Main Steam Line as cooled water through V-6, through V-5 and then back to the Suppression Chamber through the RCIC and SRV spargers.

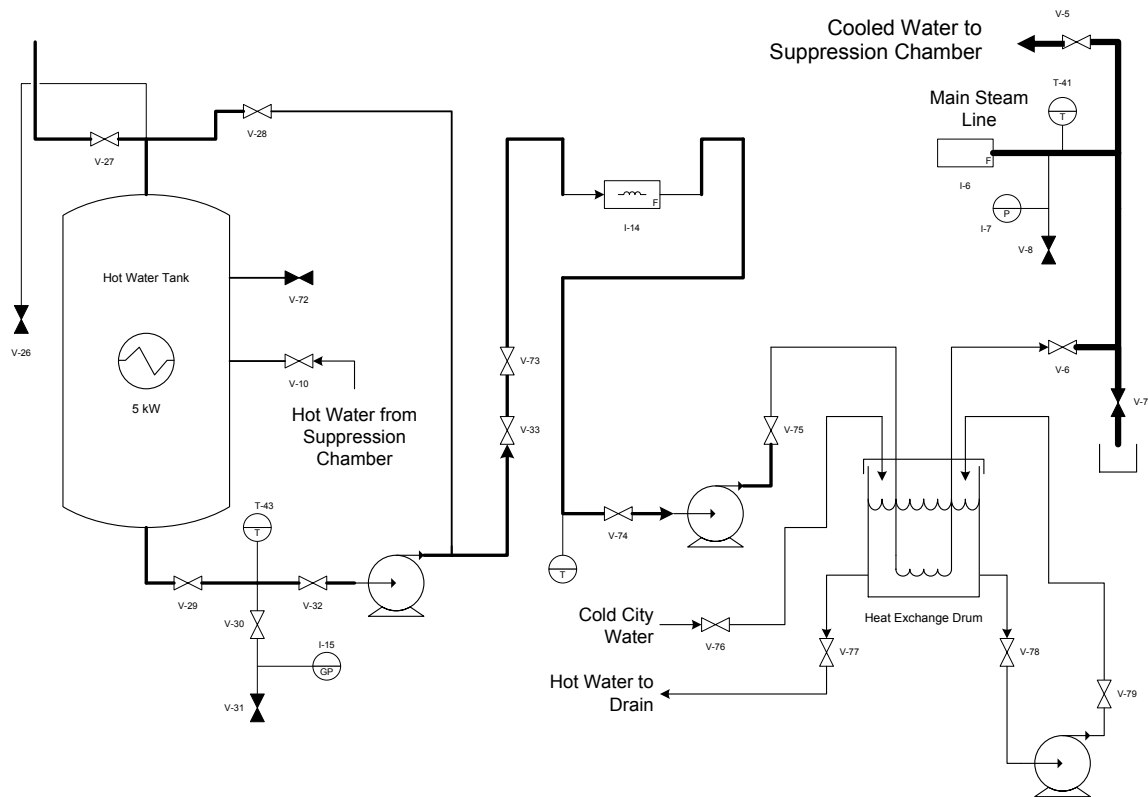


Figure 35: Heat Exchange System

4. EXPERIMENTAL FACILITY OPERATIONS

After shakedown testing and problem corrections, the experimental facility was operated in a data gathering mode. Given a set of testing objectives, a set of variable parameters was determined and procedures were developed to meet the objectives. Copious amounts of resultant data were collected, and general trends could then be identified.

4.1 TESTING PLAN

There are two primary alignments for system operation: steam discharge through the RCIC sparger analog, and discharge through the SRV analog. For each primary alignment, the steam can flow with or without active water injection that produces two-phase injection through the sparger. In addition, the flow rates are continuously variable, within reason. Furthermore, tests can be conducted to stay at low temperatures, or extended to go to higher temperatures, which could conceivably result in the premature failure of the pump. Therefore, there are a multitude of combinations of alignment, steam flow, and water injection rates. The variability of the water flow rate to the steam generator is lower, as it needs to balance the steam removal rate to ensure long-term steam supplies in the testing. Pre-pressurization and venting conditions can be added to the mix as well, very effectively increasing the potential number of unique combinations.

The overall testing plan focuses on examining the time-based thermal profiles developed in each test. These profiles will be compared across tests with different combinations of test parameters.

4.2 VARIED PARAMETERS

The experimental runs conducted varied several parameters. The parameters varied were steam generator heater power (steam flow rate), Suppression Chamber pressurization conditions, water injection rate into the steam line, and sparger type. Variations were considered not just on one parameter at a time, but also for the compounding effects of multiple parameters. While a very wide range of potential parameters can be tested, time constraints limited the total number of tests performed to 32. The parameters for each test are shown in Table 5.

Table 5: Test Parameters

Test #	Sparger/System	Power Level	Pressurization	Water Injection to Steam
1	RCIC*	57 kW	Standard	None
2	RCIC	57 kW	Standard	None
3	RCIC	157 kW	Standard	None
4	RCIC	107 kW	Standard	None
5	SRV	157 kW	Standard	None
6	RCIC	107 kW	Atmospheric	None
7	RCIC	107 kW	Atmospheric	0.4 gpm
8	RCIC	107 kW	Standard	0.4 gpm
9	RCIC	107 kW	14 psig Start	None
10	RCIC	157 kW	10 psig Start	None
11	RCIC	107 kW	15 psig Start	0.4 gpm
12	RCIC	107 kW	5 psig Start	None
13	RCIC	157 kW	Standard	0.6 gpm
14	RCIC	157 kW	Atmospheric	None
15	SRV	107 kW	Standard	None
16	SRV	107 kW	15 psig Start	None
17	SRV	107 kW	Standard	0.4 gpm
18	RCIC	107 kW	5 psig Start	0.4 gpm
19	RCIC	157 kW	10 psig Start	0.6 gpm
20	RCIC	57 kW	Atmospheric	None
21	RCIC	57 kW	Standard	0.2 gpm
22	RCIC	57 kW	5 psig Start	None
23	RCIC	57 kW	5 psig Start	0.2 gpm
24	RCIC	107 kW	15 psig Start, Vented	None
25	SRV	57 kW	Standard Atmospheric, Vent	None
26	RCIC	107 kW	Closed	None
27	RCIC	107 kW	Standard	0.8 gpm
28	RCIC	107 kW	Constant 2 atm	None
29	RCIC	107 kW	Constant 2 atm	0.4 gpm
30	RCIC	57 kW	Standard	0.8 gpm
31	RCIC	32 kW	Standard	None
32	RCIC	107 kW	Standard	None

*Used smaller orifice in RCIC Turbine analog

Steam generator power levels through each of the tests remained set at a constant value for the test duration. To limit the number of tests, only 3 primary power levels were examined: full power (157 kW), standard power (107 kW), and low power (57 kW). A special-case very low power test (32 kW) was performed as well. The 157, 107, and 57 kW power levels provided test-average steam mass flowrates near 66, 45, and 24 g/s, respectively. Without water injection to the steam line, these correspond to mass fluxes through the RCIC Sparger of 50, 34, and 18 kg/m²s. Feedwater flowrates to the steam generator were kept as close to the steam flowrate as achievable to maintain a balance between the two as well as a constant inventory in the steam generator.

Tests used either single-phase or two-phase steam/water injection. For most of the two-phase tests, water injection into the steam line was selected based on the steam generator power level to target 55-60% quality in the steam line. At 157 kW, the standard injection rate was 0.6 gpm, while the flowrates were 0.4 gpm and 0.2 gpm for 107 kW and 57 kW, respectively. In addition, 0.8 gpm testing was done for two tests (power levels of 107 and 57 kW), producing lower steam qualities. The use of volumetric rather than mass flowrates or other derived quantities was due to operational simplicity: the control valve is next to the Badger magnetic flowmeter, which actively displays flow in GPM and can be read directly by operators while correcting the position of the control valve. Due to the thermal expansion of water, the mass flowrate of the water injected into the steam line will tend to slightly decrease in time with increasing pool temperatures; this is the opposite trend of the steam mass flow, which slightly increases over the test duration due to constant heater power and increasing feedwater

temperatures. As a result, the expected trend is a slight increase in steam quality as the test progresses; this can, however, be complicated in tests where high initial steam superheat drops significantly over the test duration.

Pre-pressurization testing included a wider variety of conditions: the Suppression Chamber fully vented to the atmosphere through the test, a 2-atm constant pressure by pre-pressurizing with air and maintained by a backpressure regulator, the “Standard Alignment” in which the Suppression Chamber starts at atmospheric pressure and is isolated from the outside (builds up pressure as the pool heats up), and pre-pressurized variants of the Standard Alignment where the test starts with additional air pressures of 5, 10, or 14-15 psig and continues to pressurize as the pool warms. The pressurization tests were performed at numerous combinations of other parameters.

There were only two options for sparger type: SRV and RCIC Sparger analogs. More tests were performed with the RCIC than SRV sparger analogs, and no test was performed with both simultaneously or both alternated; each test was only performed with one sparger, and the same sparger, for the duration of the test.

4.3 PROCEDURES

Procedures were developed to safely operate the system and collect quality data. Here, they are divided into the relevant operational modes for the system (startup, shutdown, etc.). Each test will progress through several modes; some, such as pressurizing the Suppression Chamber with air, are not relevant for certain tests and are therefore omitted. The basic steps are:

1. Pre-Startup
2. Verify Suppression Chamber and Steam Generator Levels
3. Pressurize the Suppression Chamber
4. Agitate and Ensure Temperatures Meet Requirements
5. Start the Steam Generator
6. Warm the System
7. Maintain Stability for Data Operations
8. System Shutdown
9. System Cooldown
10. Securing at Cold Shutdown

More detailed procedures for each of the operational modes follow. The valve numbers are shown on the P&IDs in Appendix A. In addition, basic tables for primary valve alignments are included. The baseline valve alignment (used for Cold Shutdown) is given in Table 6; it is the starting point for valve realignments.

Table 6: Baseline/Cold Shutdown Valve Alignments

Valve	Position	Valve	Position	Valve	Position
V-1	CLOSED	V-28	OPEN	V-55	CLOSED
V-2	CLOSED	V-29	OPEN	V-56	OPEN
V-3	N/A	V-30	OPEN	V-57	CLOSED
V-4	N/A	V-31	CLOSED	V-58	CLOSED
V-5	OPEN	V-32	OPEN	V-59	OPEN
V-6	CLOSED	V-33	OPEN	V-60	CLOSED
V-7	CLOSED	V-34	OPEN	V-61	CRACKED
V-8	CLOSED	V-35	OPEN	V-62	150 PSIG
V-9	OPEN	V-36	OPEN	V-63	CRACKED
V-10	CLOSED	V-37	OPEN	V-64	OPEN
V-11	CLOSED	V-38	OPEN	V-65	CLOSED
V-12	N/A	V-39	OPEN	V-66	CLOSED
V-13	OPEN	V-40	CLOSED	V-67	OPEN
V-14	OPEN	V-41	CLOSED	V-68	CRACKED
V-15	CLOSED	V-42	CLOSED	V-69	OPEN
V-16	CLOSED	V-43	N/A	V-70	OPEN
V-17	CLOSED	V-44	N/A	V-71	CLOSED
V-18	CLOSED	V-45	N/A	V-72	CLOSED
V-19	CLOSED	V-46	CLOSED	V-73	OPEN
V-20	OPEN	V-47	CLOSED	V-74	OPEN
V-21	CLOSED	V-48	OPEN	V-75	OPEN
V-22	CLOSED	V-49	CLOSED	V-76	CLOSED
V-23	CLOSED	V-50	CLOSED	V-77	CLOSED
V-24	OPEN	V-51	CLOSED	V-78	OPEN
V-25	CLOSED	V-52	CLOSED	V-79	THROTTLE
V-26	CLOSED	V-53	CLOSED		
V-27	OPEN	V-54	CLOSED		

4.3.1 Pre-Startup

Cold Start - Everything powered off

1. Ensure all cables are appropriately connected

2. Plug in and power on the Data Acquisition Computer (including the speakers), SCXI chassis, 24V supply, and remaining instruments
3. Once startup has completed, log into the Data Acquisition Computer and load the appropriate LabVIEW program ('RCIC Facility v2.vi' for running a test, 'RCIC Facility Cooldown Alignment v1c.vi' for cooldown mode)
4. Enter the output datafile information, and begin running

Warm Start - Everything powered on

1. Power cycle instruments as necessary
2. Stop any programs using the data acquisition hardware
3. If necessary, reset the Data Acquisition Card driver. Necessary when the SCXI chassis has been power cycled, instruments are misreading, the system has been operating for long periods, significant noise has been injected into the electrical mains (i.e., thunderstorms), etc.
 - a. Open the Windows Device Manager
 - b. Under "Data Acquisition Devices", disable the "PCIe-6341" adapter
 - c. After a few moments, re-enable the adapter
 - d. Close the Device Manager

4. Load the appropriate LabVIEW program (“RCIC Facility v2.vi” for running a test, “RCIC Facility Cooldown Alignment v1c.vi” for cooldown mode)
5. Enter the output datafile information, and begin running

Stopping:

1. Click the red “End Execution” button in the LabVIEW program, and give it a few moments to complete its end tasks
2. Close the LabVIEW program

If another test/data acquisition operation is forthcoming, the DAQ System can be left as-is for a warm start. Otherwise, power off the instruments, 24 V supply, SCXI chassis, and Data Acquisition PC (unless needed for other tasks).

4.3.2 Water Level Verification/Fill

Check the indicated water levels on both the Steam Generator and Suppression Chamber magnetic float indicators; verify against the transmitted values read by the DAQ

TO FILL THE HOT WATER TANK FROM THE DI WATER SOURCE:

1. Start the DAQ system in Cooldown Mode
2. Ensure that the outlet/drain valves V-10, V-31, V-33, and V-72 are closed
3. Open Culligan DI system valves V-24 and V-26 to begin filling

4. Close Culligan DI system valve V-26 when fill is completed

TO FILL THE HOT WATER TANK FROM THE SUPPRESSION CHAMBER

1. Start the DAQ in Cooldown Mode
2. Ensure the vapor space pressure in the suppression chamber is atmospheric and that the water is subcooled, and open the valves connecting them (V-9, V-10, and V-63)
3. Align the RCIC Pump to the hot water tank (Closed: V-1 and V-11; Open: V-9, V-10, and V-63)
4. Start the RCIC Pump and regulate flow to the hot water tank at a reasonable rate by throttling V-63
5. Once in range, stop the RCIC pump
6. Close the applicable valves (V-10)

TO FILL THE HOT WATER TANK FROM THE STEAM GENERATOR

This is the reverse of filling the steam generator from the hot water tank. The alignment is the same, but the water level in the steam generator needs to be greater than that of the hot water tank for reverse flow

TO FILL THE STEAM GENERATOR FROM THE SUPPRESSION
CHAMBER

1. Start the DAQ in either Cooldown or Test Operation Mode
2. Ensure the vapor space pressures in the steam generator and suppression chamber are equal, and open the valves connecting them (V-9, V-11 and V-63; open V-16 if at atmospheric pressure)
3. Align the RCIC Pump to the steam generator (Closed: V-1 and V-10; Open: V-9, V-11, and V-63)
4. Start the RCIC Pump and regulate flow to the SG at a reasonable rate
5. Once in range, stop the RCIC pump
6. Close the applicable valves (V-11)

TO FILL THE STEAM GENERATOR FROM THE HOT WATER TANK

1. Start the DAQ in Cooldown Mode
2. Ensure that the Hot Water Tank has sufficient water. Concurrent filling of the hot water tank and steam generator is permissible.
3. Ensure that the steam generator is depressurized before filling. Open the blowdown valve (V-16)
4. Open the valves between the steam generator and hot water tank (V-10 and V-11; V-9 is nominally closed)
5. Close V-10 and V-11 when the steam generator is filled to the appropriate level, and open V-9

4.3.3 Suppression Chamber Pre-Test Pressurization

If pre-pressurization of the Suppression Chamber is needed, perform these steps.

1. Ensure that all atmospheric connections are closed
2. Open the Suppression Chamber Airspace Steam Line Connection Valve V-35
3. Open wide the Main Steam Line Control Valve V-1
4. Connect the air compressor hose to the air line quick connect on the steam generator, and power on the compressor
5. Open the steam generator air inlet valve V-17 and allow the system to begin pressurizing
6. Carefully monitor the Suppression Chamber pressure, and allow it to rise to the target pressure
7. Close the steam generator air inlet valve V-17
8. Shut down the compressor
9. Allow the system pressure to stabilize, and add more air via the inlet valve V-17 as necessary; close the valve when complete
10. Close the Suppression Chamber Airspace Steam Line Valve V-35, and ensure that the SRV Block Valve V-36 and RCIC Block Valve V-34 are closed
11. With all personnel safely clear of the vent area, open the steam generator blowdown valve V-16 to depressurize the steam generator

12. When fully depressurized, tightly close the steam generator blowdown valve V-16 and the Main Steam Control Valve V-1

4.3.4 Agitation

To ensure a uniform-temperature pool

1. Ensure that the vessel water levels and all electrical connections are suitable, and power cycle/turn on the instruments as necessary
2. Enter the test (especially the parameters/conditions) into the logbook, and make notes as milestones are reached
3. Start the RCIC Pump cooling fan on maximum speed
4. Start the data acquisition computer in test/experiment mode, and enter in the correct output file information – record everything
5. Set/ensure the following valve alignment: Open: V-53 or V-54 (alternate), throttle V-61; Closed: V-10, V-11
6. Start the RCIC pump and allow it to agitate the tank; continue agitation for several minutes after all submerged thermocouples come to uniform values
7. Close the recirculation block valves V-53 and V-54, then stop the RCIC Pump. Sufficient time needs to pass between the end of pumped agitation and the start of the data period after warmup to allow for the water motion to cease.

8. Ensure that the bulk pool temperatures are within range. If agitation is concurrent with subcooled Steam Generator warmup, it needs to be terminated before the Steam Generator is purged of air to allow for sufficient pool calming time.

4.3.5 Steam Generator Startup

Suppression Chamber agitation may continue into the early part of the Steam Generator warmup, while the Steam Generator temperatures are still below 100 °C.

STEAM GENERATOR STARTUP SEQUENCE

1. Close the vacuum breaker block valve V-13
2. Ensure that valves V-1 and V-11 are closed
3. Turn on the breaker and main power switch for the steam generator
4. Power on the applicable heaters. In warmup, all may be run.
5. If heaters do not power on, and the level is appropriate, bump the water level interlock reed switch with a magnet to unstick it
6. When the steam generator temperatures are above 105 °C, purge the air from the steam generator. SUPPRESSION CHAMBER AGITATION SHOULD HAVE CEASED BY THIS POINT.
7. Make sure no personnel are near the steam blowdown exhaust point
8. Open the Steam Generator blowdown line V-16, and wait until the sound changes to indicate steam rather than air flow

9. After a few moments of pure steam flow, close the blowdown valve V-16
10. Wait until the steam generator pressure rises above 40 psia, then set the power level to that of the test

4.3.6 System Warmup

Operators should exercise caution during system warmup procedures to maintain safety and to prevent damage to the system.

1. Close the steam line block valves V-34, V-35, and V-36, and open (with a partly-filled water bucket underneath) the main steam line condensate drain valve V-7. Be sure to catch any draining water with the bucket
2. SLOWLY open the main steam control valve V-1 until a VERY LOW steam flow passes through it
3. Condensate will begin draining out the open steam condensate drain line.
4. When the condensate draining out the condensate line becomes steam, CAREFULLY close the condensate drain valve V-7 and allow the steam line to pressurize and warm up. Adjustment of the steam flow rate may be necessary
5. If the steam generator pressurizes too fast, turning off some heaters may be necessary. The heaters should be re-energized before steam is

injected into the Suppression Chamber to ensure that the correct heater power level is maintained throughout the test period.

6. Once the steam line has pressurized, drain any new condensate from the line by slowly cracking open the valve V-7 until water slowly flows, and closing it when liquid flow becomes mostly steam. Do not open fully. Caution: HOT!
7. Adjust the main steam control valve V-1 to near the expected position to maintain the pressures and flows during the test
8. Open the appropriate (for the particular test) sparger valve (RCIC/SRV, V-34/V-36) carefully
9. Adjust the steam flow rate to near the target rate with the steam control valve V-1. Typically, steam generator pressures should be maintained to 70 - 90 psia, constant (and well above the steam line pressure) once full-circuit flow is established to ensure superheat through the vortex flowmeter
10. Barely crack open the feedwater control valve V-63
11. Start the RCIC Pump
12. Open the block valves V-9 and V-11 (V-10 closed) to permit feedwater flow to the steam generator, and adjust the control valve V-63 and pump recirculation valve V-68 to attain the correct flow to the steam generator. Note: V-53 and V-54 should both be closed

13. If water injection is directed to the steam line, carefully crack open the injection control valve V-68, and open the block valves V-49 and V-69
14. Adjust the Suppression Chamber Atmospheric block/regulator valve V-50 as determined for the particular test
15. Ensure that the basic valve alignment is appropriate for the current particular test
16. Adjust the control valves V-1, V-63, V-66, and V-68 to bring all the flows into their appropriate ranges for the test
17. Allow the system to heat up/approach the test begin condition, adjusting valves as appropriate and draining any collected steam condensate (through V-7)

4.3.7 Primary Data Operations

Ensure that the valves are correctly aligned for the test during the warmup period.

Once full injection conditions/alignments are met, make only minor adjustments to maintain the correct flowrates and pressure/temperature conditions (i.e., more than the minimum necessary superheat at the vortex flowmeter)

While temperatures are below the test begin condition in the Suppression Chamber, but near the temperature, fully drain any new condensate from the steam line by CAREFULLY cracking open the condensate drain valve V-7 until all the collected

liquid is vented. Limit the flow rate to a slow drain and only open the valve slightly; DO NOT OPEN THE VALVE FULLY DURING TESTING.

Once the test period has begun, only make slight, slow changes to control valve positions to maintain flows/temperatures/pressures

For fine-tuning the flow rate from the RCIC pump back to the steam generator, multiple valves are employed. The main control valve, V-63, can be thought of as a 'rough adjustment'; it is difficult with just that valve to make fine adjustments to the flow. Small adjustments can be made by varying the position of the pump recirculation globe valve V-66; such adjustments will result in a reverse effect as a similar adjustment would have for the main control valve (i.e., opening the control valve will increase flow to the steam generator, while opening the recirculation valve will tend to decrease flow to the steam generator. The gate valve V-67 should ALWAYS BE OPEN to ensure adequate minimum flow through the pump, and should not be used to regulate flow. In addition, the recirculation valve should be opened enough to limit the pump outlet pressure to below its case pressure limit (150 psig) and below the outlet relief valve's (V-62) set point. This can be a concern in the latter stages of a pre-pressurized test.

At the end of the test period, or if any equipment limits have been met/exceeded (or if something unspecified goes wrong), proceed immediately to the shutdown sequence. It should be noted that the data processing scripts look for the termination of steamflow as a flag that the test has been terminated, and define an endpoint as 60 seconds before detection of that signal to allow for beginning shutdown procedures.

A summary of the valve alignments for the data period is given in Table 7. Items in bold differ from their cold shutdown positions.

Table 7: Main Data Period Valve Alignments

<u>Valve</u>	<u>Position</u>	<u>Valve</u>	<u>Position</u>	<u>Valve</u>	<u>Position</u>
V-1	THROTTLE	V-28	OPEN	V-55	CLOSED
V-2	CLOSED	V-29	OPEN	V-56	OPEN
V-3	N/A	V-30	OPEN	V-57	CLOSED
V-4	N/A	V-31	CLOSED	V-58	CLOSED
V-5	OPEN	V-32	OPEN	V-59	OPEN
V-6	CLOSED	V-33	OPEN	V-60	CLOSED
V-7	CLOSED	V-34	TEST	V-61	CRACKED
V-8	CLOSED	V-35	CLOSED	V-62	150 PSIG
V-9	OPEN	V-36	TEST	V-63	THROTTLE
V-10	CLOSED	V-37	OPEN	V-64	OPEN
V-11	OPEN	V-38	OPEN	V-65	CLOSED
V-12	N/A	V-39	OPEN	V-66	THROTTLE
V-13	CLOSED	V-40	CLOSED	V-67	OPEN
V-14	OPEN	V-41	CLOSED	V-68	THROTTLE
V-15	CLOSED	V-42	CLOSED	V-69	OPEN
V-16	CLOSED	V-43	N/A	V-70	OPEN
V-17	CLOSED	V-44	N/A	V-71	CLOSED
V-18	CLOSED	V-45	N/A	V-72	CLOSED
V-19	CLOSED	V-46	CLOSED	V-73	OPEN
V-20	OPEN	V-47	CLOSED	V-74	OPEN
V-21	CLOSED	V-48	OPEN	V-75	OPEN
V-22	CLOSED	V-49	TEST	V-76	CLOSED
V-23	CLOSED	V-50	TEST	V-77	CLOSED
V-24	OPEN	V-51	CLOSED	V-78	OPEN
V-25	CLOSED	V-52	CLOSED	V-79	THROTTLE
V-26	CLOSED	V-53	CLOSED		
V-27	OPEN	V-54	CLOSED		

4.3.8 System Shutdown

IMPORTANT!

FIRST, close the downstream water injection to steam line block valve V-49 to prevent water hammer and steam exposure to the Badger flowmeter.

In rapid sequence, QUICKLY

1. close the main steam control valve V-1,
2. switch off the steam generator entirely,
3. close the feedwater block valve V-9, and
4. switch off the RCIC pump

Allow the system to sit for at least two minutes before proceeding. It is permissible to delay 3 and 4 above to give extra fill to the steam generator if the RCIC pump's limits are not at risk of being exceeded.

5. Open the SRV and RCIC sparger block valves V-36 and V-34
6. Open wide the main steam control valve V-1 to blow down the steam generator to the Suppression Chamber
7. Open the Suppression Chamber blowdown valve V-50 to dump the hot steam-air mixture into the Suppression Chamber Blowdown Drum.
8. Close the Suppression Chamber Blowdown valve V-50 once nearly all the available air from the Suppression Chamber has been vented (sounds of steam condensation rather than air bubbling in the drum's

water volume) or the Suppression Chamber reaches a sustainable atmospheric pressure. Do not allow the drum's water to reach saturation temperatures.

9. Once the steam generator finishes blowing down to the Suppression Chamber, close the main steam line control valve V-1 tightly
10. Ensure that all personnel are clear of the vent area, open the steam generator blowdown valve V-16, and bring the steam generator to atmospheric conditions
11. Operate the air compressor until it has sufficient pressure to fill the steam generator with sufficient pressure to blow air into the Suppression Chamber, and attach the quick connect hose to the air hose connection on the steam generator.
12. Close the steam generator blowdown valve V-16
13. Open the steam generator air inlet valve V-17 and fill it with air until it has sufficient air pressure to purge the steam line all the way to the Suppression Chamber – generally at least 15 psi above the Suppression Chamber's pressure.
14. Close the steam generator air inlet valve V-17
15. Open the main steam control valve V-1 to blow air through the steam line through the spargers until the steam generator pressure drops to that of the Suppression Chamber
16. Tightly close the main steam control valve V-1

17. Close the RCIC Sparger block valve V-34
18. With all personnel clear of the vent area, open the steam generator blowdown valve V-16, and allow the steam generator to come to atmospheric pressure
19. open the steam generator vacuum breaker block valve V-13
20. Close the steam generator blowdown valve V-16
21. End execution of the test-mode LabVIEW VI, and begin execution of the cooldown mode VI
22. Proceed with cooldown procedures. If the pool temperature is still pressurized or above 100 °C, it is in the Superheated Hot Shutdown condition

4.3.9 System Cooldown

Follow these steps to proceed through system cooldown. As a basic reference, the normal operating alignments of the valves are given in Table 8. Items in bold differ from their cold shutdown positions, and items in italics differed from their cold shutdown positions during the main data period.

Table 8: Primary Cooldown Valve Alignments

Valve	Position	Valve	Position	Valve	Position
V-1	CLOSED	V-28	OPEN	V-55	CLOSED
V-2	CLOSED	V-29	OPEN	V-56	OPEN
V-3	N/A	V-30	OPEN	V-57	CLOSED
V-4	N/A	V-31	CLOSED	V-58	CLOSED
V-5	OPEN	V-32	OPEN	V-59	OPEN
V-6	OPEN	V-33	OPEN	V-60	CLOSED
V-7	CLOSED	V-34	OPERATE	V-61	THROTTLE
V-8	CLOSED	V-35	OPERATE	V-62	150 PSIG
V-9	OPEN	V-36	OPERATE	V-63	THROTTLE
V-10	OPEN	V-37	OPEN	V-64	OPEN
V-11	CLOSED	V-38	OPEN	V-65	CLOSED
V-12	N/A	V-39	OPEN	V-66	THROTTLE
V-13	OPEN	V-40	CLOSED	V-67	OPEN
V-14	OPEN	V-41	CLOSED	V-68	CRACKED
V-15	CLOSED	V-42	CLOSED	V-69	OPEN
V-16	CLOSED	V-43	N/A	V-70	OPEN
V-17	CLOSED	V-44	N/A	V-71	CLOSED
V-18	CLOSED	V-45	N/A	V-72	CLOSED
V-19	CLOSED	V-46	CLOSED	V-73	OPEN
V-20	OPEN	V-47	CLOSED	V-74	OPEN
V-21	CLOSED	V-48	OPEN	V-75	OPEN
V-22	CLOSED	V-49	CLOSED	V-76	THROTTLE
V-23	CLOSED	V-50	OPERATE	V-77	OPEN
V-24	OPEN	V-51	CLOSED	V-78	OPEN
V-25	CLOSED	V-52	CLOSED	V-79	THROTTLE
V-26	CLOSED	V-53	OPERATE		
V-27	OPEN	V-54	OPERATE		

From SUPERHEATED HOT SHUTDOWN

1. Ensure that the heat exchange drum is filled with water and that there is sufficient water in the hot water tank to drain a substantial volume

without dropping below the minimum level for operation of the hot water pump

2. Start the heat exchange recirculation pump
3. Open the heat exchange drum outlet valve V-77 fully, and throttle open the cold water inlet valve V-76 to match the drain flowrate in the heat exchange drum. Maintain full levels.
4. Ensure that the Main Steam Control Valve V-1 is tightly closed, the SRV line (V-36) is open, the RCIC and Suppression Chamber Airspace valves V-34 and V-35 are closed, and that the main steam line has been purged with air
5. Ensure that the Cooldown Heat Exchange Auxiliary Pieces are properly connected to the system
6. Fully open hot water valves V-29, V-32, V-33, V-73, V-74, and V-75

In rapid succession, quickly

7. Turn on the hot water pump
8. Turn on the auxiliary hot water pump
9. Open the Cooldown System Block Valve V-6

If additional makeup water is needed in the system, the hot water tank can be simultaneously filled via the Culligan DI system (opening V-26)

Once a substantial amount of water has been added to the bottom of the Suppression Chamber, there should be sufficient thermal stratification that hot subcooled water can be extracted from the bottom and fed to the hot water tank without flashing issues

ALWAYS maintain a MINIMUM of 50 inches of water above the outlet of the hot water tank to ensure sufficient NPSH at the hot water pump

To send hot water to the hot water tank,

1. Close the steam generator feedwater block valve V-11
2. Open the hot water tank feedwater block valve V-10
3. Open the feedwater block valve V-9
4. Open the Suppression Chamber Recirculation Lower Block Valve V-54
5. Fully open the Suppression Chamber Recirculation Control Valve V-61
6. Throttle open the main feedwater control valve V-63 to refill the hot water tank (fill rate greater than water removal rate)

Optimum feedwater temperatures are between 95 and 98 °C to have a high enough ΔT across the heat exchanger to provide for effective heat removal.

Once temperatures at the outlet drop below around 90 °C, open the RCIC Sparger Block Valve V-34 to weaken the thermal stratification layers in the pool

When either the pool's pressure is insufficient to maintain necessary feedwater flow or the outlet temperatures stay below 90 °C, begin forced recirculation:

1. Throttle the main feedwater control valve V-63 and the Suppression Chamber Recirculation Valve V-61 to barely open
2. Start the RCIC Pump
3. Throttle the main feedwater control valve V-63 to provide sufficient feedwater flow to the hot water tank
4. Throttle the Suppression Chamber Recirculation Valve V-61 to provide a small mixing current in the lower regions of the vessel, to maintain outlet temperatures near 95 °C

Continue to maintain flows (all heat exchanger flow rates, balanced flows to the hot water tank, near-saturation water to the hot water tank) until the Suppression Chamber bulk pool temperatures drop several degrees below saturation. NOTE: THESE CONDITIONS MAY BE CONDUCTIVE TO PUMP CAVITATION. Avoid cavitation in the pump, flashing in valves, lines, etc.

Once the bulk pool temperatures drop several degrees below saturation:

1. Provide additional recirculation flow (throttle open V-61) to achieve and maintain pool thermal uniformity.

2. Open the Suppression Chamber Vapor Space Steam Line Valve V-35 to discourage the formation of cool thermal layers on the bottom of the pool

Once the pool is below 100 °C, if operator fatigue becomes an issue, the system can be shut down, depressurized, and allowed to sit safely overnight (Hot Shutdown).

To do so:

1. Close the Suppression Chamber Vapor Space Steam Line Valve V-35
2. Open the Suppression Chamber Blowdown Valve V-50 and vent the remaining pressure through the blowdown drum
3. Once the Suppression Chamber pressure reaches atmospheric pressure, close the Suppression Chamber Blowdown Valve V-50
4. Open the Suppression Chamber Vapor Space Steam Line Valve V-35
5. Shut off all pumps
6. Close the Feedwater Block Valve V-9
7. Close the cooling water supply valve V-76 and the heat exchange drum drain valve V-77
8. Switch off the RCIC Pump Cooling Fan

The Data Acquisition System may be allowed to continue collecting data while the system is left to perform a natural cooldown. To resume active cooldown from the Hot Shutdown state:

1. switch on the RCIC Pump Cooling Fan

2. ensure that the Lower Suppression Chamber Recirculation Block Valve V-54 is open (may alternate with Upper Suppression Chamber Recirculation Block Valve V-53)
3. Throttle open the Suppression Chamber Recirculation Control valve V-61
4. Start the RCIC Pump
5. Open the Heat Exchange Drum Drain Valve V-77
6. Throttle open the Heat Exchange Cold Water Valve V-76 to maintain level in the heat exchange drum
7. Start the Heat Exchange Drum Recirculation Pump
8. Ensure that valves V-6, V-29, V-32, V-33, V-73, V-74, and V-75 are full open and start the hot water pump
9. Start the auxiliary hot water pump
10. Throttle open the Feedwater Control Valve V-63
11. Open the Feedwater Block Valve V-9
12. Regulate feedwater flow with the Feedwater Control Valve V-63 to maintain level in the hot water tank

Maintain levels and flows with cooling until the bulk Suppression Chamber temperatures reach the appropriate cold shutdown temperatures (i.e., cold enough to run another test, typically at or below 37 °C)

If performing another test within the next few days, the overnight shutdown procedures (above) can be applied, and the next test started at some point afterward. Otherwise, follow the long-term Cold Shutdown sequence

4.3.10 Cold Shutdown

To reach Cold Shutdown, start from an appropriate (subcooled, unpressurized) Hot Shutdown at low temperature.

1. Perform an overnight shutdown sequence for Hot Shutdown
2. close the V-6 Cooldown System Block Valve
3. close the hot water tank feedwater block valve V-10 (V-11 still closed)
4. open the feedwater block valve V-9
5. end execution of the cooldown mode VI
6. shut down the instruments
7. switch off the 24V power supply
8. power off the SCXI chassis
9. Back up collected data from the Data Acquisition Computer
10. Shut down the data Acquisition Computer
11. Reached Cold Shutdown

At cold shutdown, all pressures should be atmospheric and all temperatures should be well below saturation. The primary valve alignment in Cold Shutdown should be that of Table 6.

4.4 RESULTS

A total of 32 tests were performed. Each of them will be briefly described in the order in which the tests were performed. Summaries of the tests are given in Table 9 and Table 10.

Test #4 has been used in the past as a baseline reference case. The typical progression of phenomena common in these tests is given in 4.4.4, which discusses Test #4. In addition, only a limited number of thermocouple positions are plotted in these results for simplicity. The typical plot includes the vessel front stratification set, consisting of an Upper (Thermocouple SP19), Middle (Thermocouple SP20), Lower (Thermocouple SP21), Left (Thermocouple SP22, at the same elevation as the Middle), Right (Thermocouple SP23, at the same elevation as the Middle), and a Bottom/Vessel Outlet temperature reading.

Table 9: Mean Measured Flow Conditions

Test #	Steam Flow, g/s	FW Flow, g/s	Water Injection Flow, g/s	Sparger Steam Quality	SC Start P, psia	SC End P, psia	Initial Water Level, in.	Final Water Level, in.
1	23.5	22.2	0.0	1.012	16.2	29.7	28.0	28.8
2	23.5	25.0	0.0	1.012	15.0	30.8	30.8	31.1
3	65.8	65.9	0.0	1.019	15.1	54.3	30.2	30.3
4	45.3	45.1	0.0	1.017	14.7	47.8	29.7	33.9
5	66.4	65.6	0.0	1.017	15.1	32.5	29.6	33.0
6	45.0	43.8	0.0	1.022	14.8	15.6	29.7	30.1
7	45.4	44.0	24.5	0.638	14.7	15.4	30.1	30.4
8	45.5	44.9	24.8	0.625	14.7	42.2	29.9	33.6
9	43.5	43.4	0.0	1.003	29.6	72.3	33.5	33.5
10	65.4	64.2	0.0	1.013	25.9	74.8	32.0	32.8
11	43.7	43.1	24.9	0.585	30.2	100.7	32.7	32.7
12	44.7	43.7	0.0	1.009	20.7	72.1	30.5	32.6
13	66.3	65.9	37.2	0.626	15.1	46.8	30.8	35.2
14	66.8	65.2	0.0	1.028	14.8	16.2	30.4	30.6
15	45.7	45.6	0.0	1.012	15.1	39.0	30.2	31.8
16	45.5	45.4	0.0	1.005	30.2	56.9	30.1	30.2
17	45.4	45.4	25.3	0.623	15.3	39.2	29.7	30.0
18	44.4	44.8	25.3	0.599	20.3	62.4	29.7	29.8
19	66.4	65.7	37.4	0.606	25.1	95.9	30.6	31.1
20	23.9	23.5	0.0	1.017	14.8	15.5	31.0	31.1
21	23.8	23.2	12.5	0.635	15.2	40.7	30.7	31.7
22	23.7	23.5	0.0	1.005	20.2	49.3	30.5	31.2
23	23.3	22.9	12.5	0.618	20.3	48.2	30.4	31.1
24	44.8	44.0	0.0	1.011	30.5	32.3	30.9	31.2
25	23.9	23.7	0.0	1.008	14.9	42.3	30.7	31.6
26	45.6	44.7	0.0	1.019	15.0	35.4	30.6	31.4
27	44.8	44.4	49.9	0.441	15.0	42.7	30.4	31.3
28	44.6	43.9	0.0	1.011	30.1	30.7	31.0	31.3
29	44.4	43.8	25.0	0.606	30.8	30.6	31.3	31.5
30	23.3	23.0	49.8	0.261	14.9	40.8	30.6	31.7
31	13.0	12.9	0.0	1.000	14.6	39.6	30.6	31.6
32	44.7	44.3	0.0	1.015	15.1	49.6	31.1	31.3

Qualities greater than unity are superheated steam

Table 10: Peak Stratification

Test #	Duration, s	Start Pool T	End Pool T	Strat. Period, s	Max Top-Mid DT	Max Mid-Low DT	Max Low-Outlet DT
1*	10368	40	95	6972	2.1	10.8	20.7
2	12878	40	100	8247	1.4	9.3	22.6
3	6678	40	127	3731	2.1	5.5	43.1
4	8917	40	122	5373	3.1	20.9	43.3
5	4710	40	104	0	2.6	2.3	5.0
6	6466	40	99	2846	2.4	5.9	21.0
7	5932	40	94	2809	1.9	3.4	13.2
8	8436	40	117	5206	2.3	11.7	36.8
9*	9336	40	128	8075	5.1	29.4	61.9
10*	6452	40	134	4506	4.0	29.0	55.0
11~	11407	40	146	10381	5.6	28.9	65.1
12~	10942	40	136	7521	4.1	26.9	55.9
13	6361	40	121	2372	2.2	1.9	15.4
14	4542	40	100	1127	2.2	1.5	9.1
15	8081	40	113	0	2.3	2.1	4.1
16	8120	41	112	3859	2.4	3.0	5.5
17	7977	40	113	0	2.2	2.1	4.2
18~	9795	40	129	7111	3.7	25.5	52.6
19~	8367	40	147	6235	2.7	12.0	44.4
20	12992	40	100	6260	1.6	5.8	14.0
21	15915	40	114	8952	1.5	10.6	23.9
22	16254	40	117	10082	1.7	13.2	30.7
23	16122	40	115	10733	1.8	14.4	32.9
24	8209	40	113	5575	5.1	14.6	36.6
25	16930	40	116	10297	1.9	2.3	4.4
26	8602	40	116	3683	2.2	5.8	27.7
27	8705	40	117	4709	1.7	3.7	15.7
28	10221	30	120	7568	4.5	21.0	39.6
29	9483	35	119	7233	4.5	22.9	40.5
30	17979	30	113	7817	1.3	10.1	24.2
31'	31398	35	112	22584	1.0	8.4	27.9
32	9675	41	123	5994	2.8	20.7	43.5

*Stopped before completion

~Destratification did not complete before termination

'Steam Flow Measurement Issues

4.4.1 Test #1

Test #1 was the only test to use the smaller-diameter orifice (0.348”) in the RCIC Turbine analog. It ran at 57 kW in the Standard Alignment – Suppression Chamber isolated with an initial near-atmospheric pressure and no water injection to the steam. This produced main steam line pressures on the order of 10 psi greater than those of Test #2, which was almost identical; the only difference was the use of the larger orifice. Procedurally, the test was terminated earlier than the others. The final pool lower-outlet destratification point was not found, but the others (upper-mid level, mid-lower level) were.

The test ran with steam flowrates of 23.5 ± 0.5 g/s, and feedwater flows were 22.2 ± 0.9 g/s. As with the other tests, chugging was evident and decreased in intensity as the test progressed. Thermal stratification was evident (and can be seen in Figure 36) for most of the test, appearing after about 56 minutes and enduring through the end near 173 minutes; the beginning and end of the stratification period as determined by the data processing script are identified by gray vertical lines, while the vertical dotted gold line indicates plume detection as defined in Section 5.2. The top-mid level stratification peaked at 2.1 °C at 124 minutes, followed by a peak 10.8 °C maximum mid-low level separation at 159 minutes. The low-outlet separation reached 20.7 °C at the very end, and was still growing. Over the test period, the pressure in the Suppression Chamber nearly doubled.

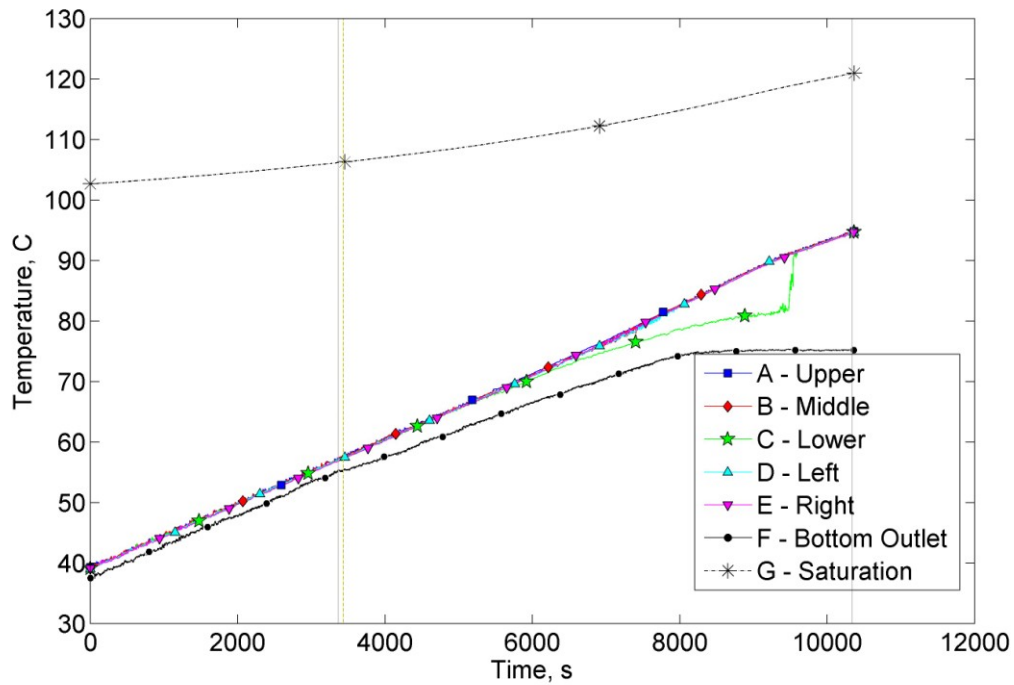


Figure 36: Test #1 Thermal Progression

4.4.2 Test #2

Test #2 was nearly identical to Test #1, with the exception of the larger orifice diameter being used. It too ran 57 kW of heater power in the steam generator with a standard alignment RCIC profile. Unlike Test #1, it was run to completion – the full destratification and reconvergence of all pool temperatures to essentially a uniform bulk temperature was observed. It was also reported in [50].

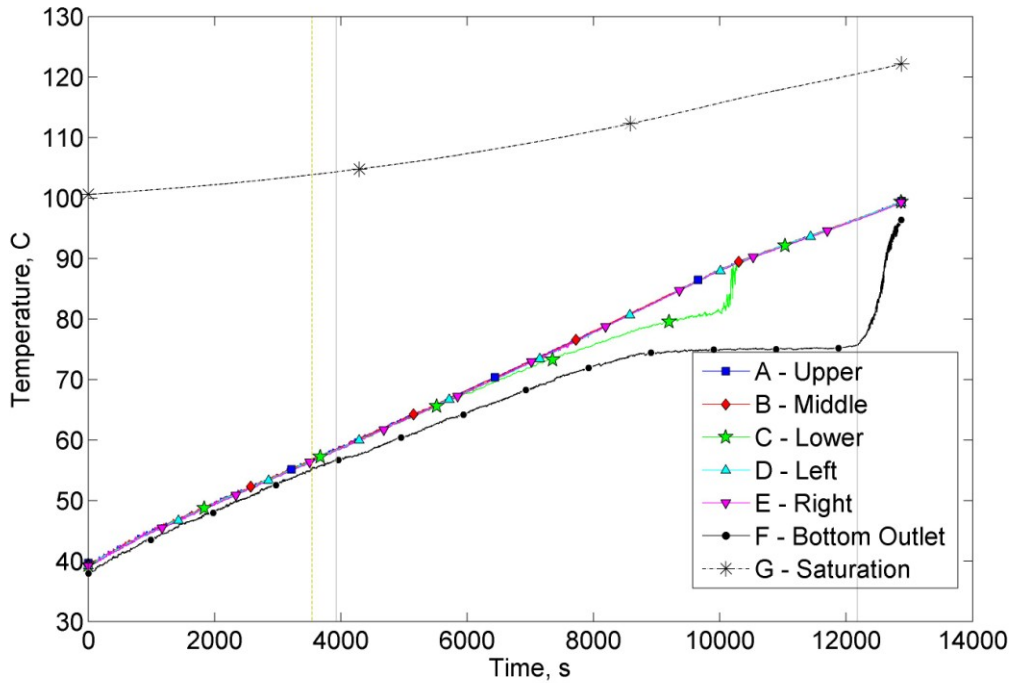


Figure 37: Test #2 Thermal Progression

While not identical, the results and thermal profiles for Test #2 were similar to those of Test #1. Steam and feedwater flowrates were 23.5 ± 1.1 and 25.0 ± 2.2 g/s, respectively. The initial water inventory was slightly greater, and the initial (post-warmup) pressures slightly less than Test #1. Thermal stratification appeared somewhat later, after 65 minutes (see Figure 37), and was slightly, but not significantly when compared to instrument tolerances, lower than Test #1 for the top-mid (1.4 °C) and mid-low regions (9.3 °C). Owing to the run through completion, the peak low-outlet stratification was greater, and measured 22.6 °C.

As was the case earlier, the period of major thermal stratification ran for the majority of the test – more than $2/3$ of a nearly 203 minute period.

4.4.3 Test #3

Test #3 was a full-power (157 kW) standard alignment run. With its nearly triple the heater power of the previous tests, the water in the Suppression Chamber heated up at a much faster rate, and proved somewhat more difficult to control than lower-power tests. This test was also discussed in [50].

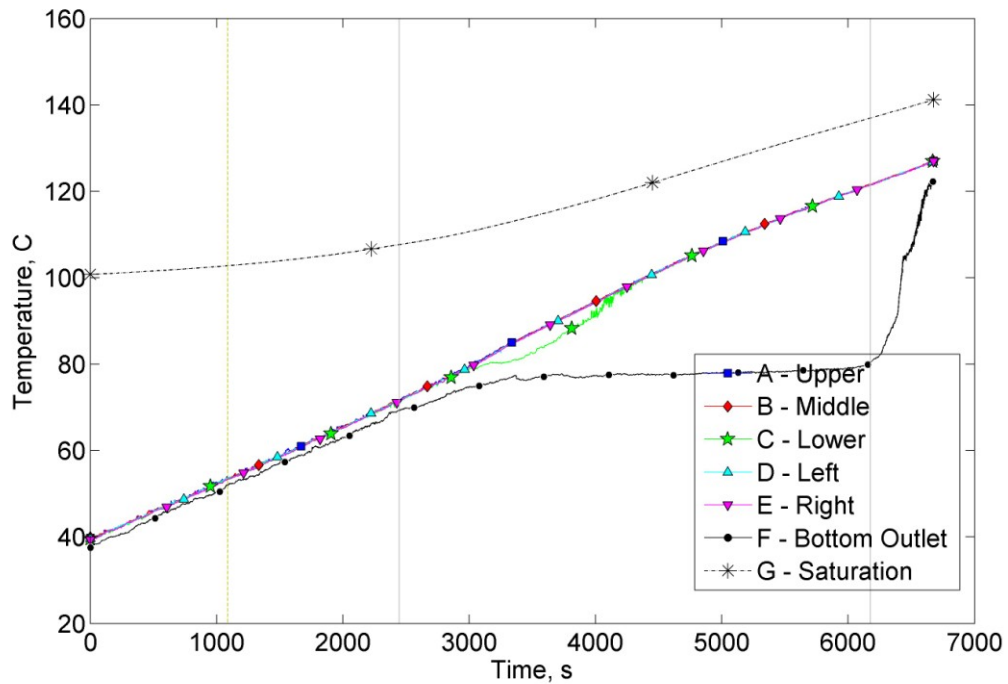


Figure 38: Test #3 Thermal Progression

With 65.8 ± 3.0 g/s of steam flow and 65.9 ± 9.2 g/s of feedwater, there proved to be more variation in steam and water flow rates. In order for the increased flowrate through the orifice, greater upstream pressures were needed in the main steam line. To maintain superheat through the vortex flowmeter, somewhat greater pressures were

needed in the steam generator (~90 psia with a main steam line running ~70-80 psia).

Not only were flows through the main steam control valve no longer choked (it would be choked through the orifice for most of the run), but the high differential pressure between the RCIC Pump and steam generator made it difficult for operators to maintain a stable, balanced flow back to the steam generator.

Thermal stratification (shown in Figure 38) in the upper levels of the pool were similar to those of the earlier low-power tests. The peak separation in the top-mid regions was 2.1 °C, and the mid-low difference peaked at 5.5 °C. The low-outlet stratification, however, was much larger. At 43.1 °C, the difference was more than 20 °C greater, and nearly twice that of Test #2. Destratification occurred later, and the final pool temperature was resultingly greater than earlier tests.

4.4.4 Test #4

Test #4 was a mid-power (107 kW) standard alignment test, and was considered the quintessential/base-case RCIC test in [50] and [51]. It produced some of the clearest stratification and chugging profiles in the basic tests.

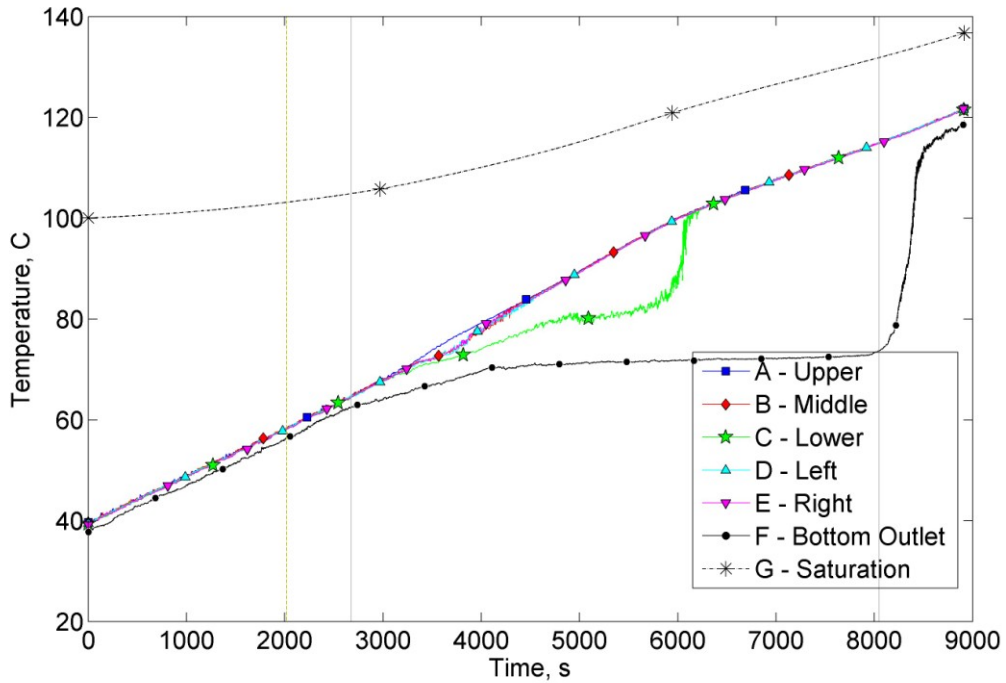


Figure 39: Test #4 Thermal Progression (Vessel Front)

With steam and feedwater flowrates of 45.3 ± 1.3 and 45.1 ± 3.8 g/s, respectively, a peak stratification of 3.1 °C top-mid was produced, only slightly more than the tests at higher and lower powers. The mid-low difference, however, was remarkable: 20.9 °C, the greatest of the standard alignment tests. The peak low-outlet stratification was the greatest of the standard alignment tests as well at 43.3 °C, although that is within instrument tolerance of the same value for Test #3. The thermal profiles can be seen in Figure 39 for the front of the vessel, which shows essentially the same profile as in the (axially) middle region of the pool (shown in Figure 40).

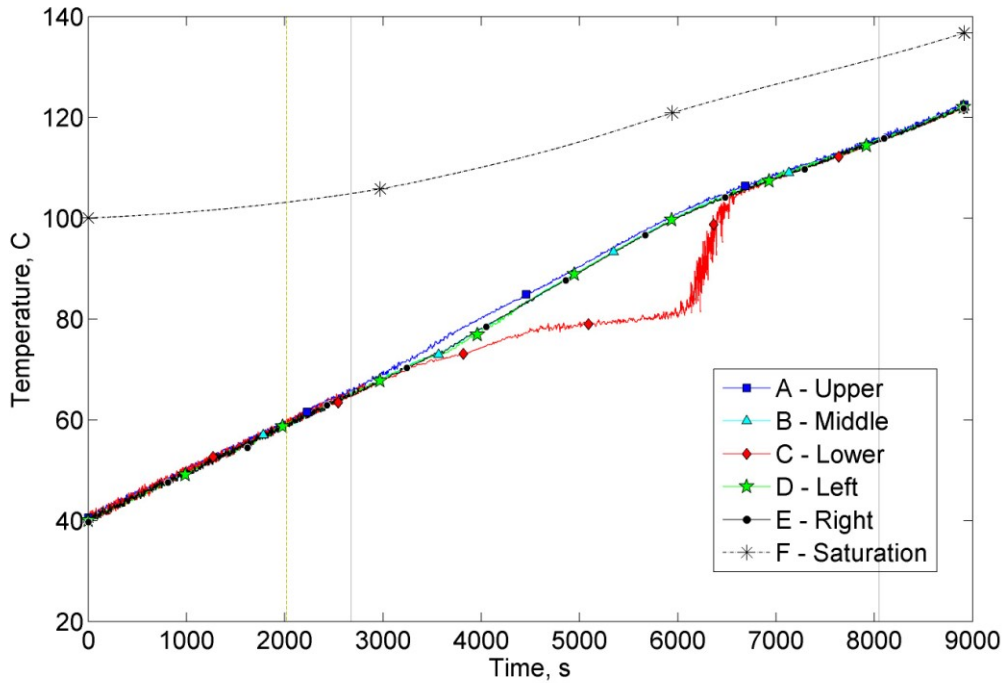


Figure 40: Test #4 Pool Thermal Progression, Mid-Pool

Axial temperatures were very consistent at similar elevations in the pool with one major exception: Thermocouple SP8. It is located very near the outlet for the RCIC Sparger, and displays behavior indicating a somewhat chaotic hot spot. Initially, it matches the others on its elevation, but eventually separates. The separation is an important part of the analysis of the data collected in these tests, and is taken to represent the formation of a thermal plume. The axial profile can be seen in Figure 41.

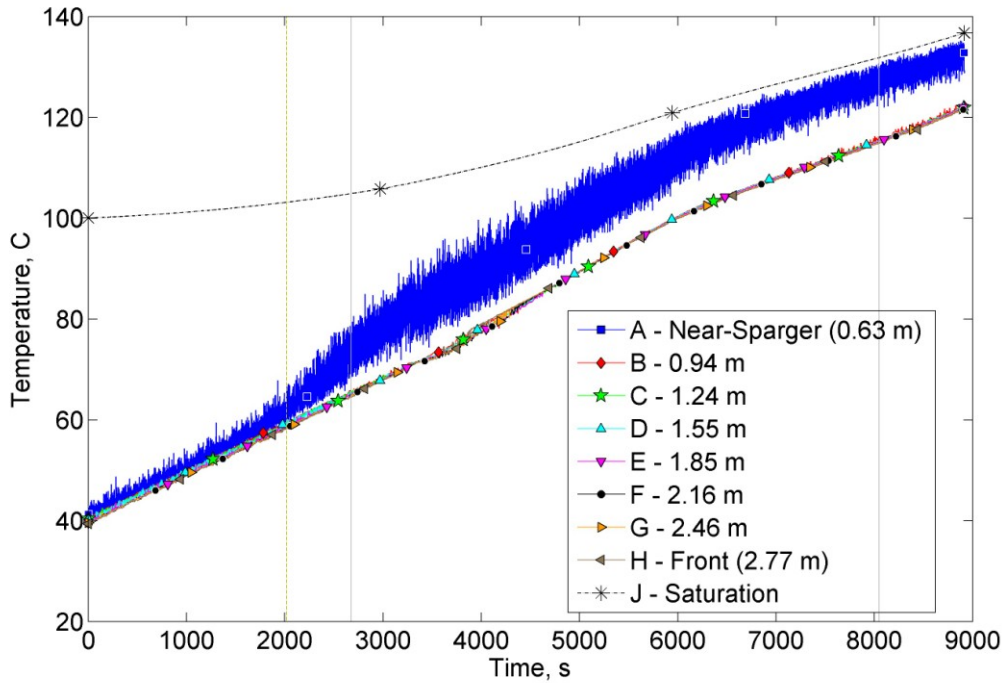


Figure 41: Test #4 Pool Mid-Level Axial Temperature Progression

By about 2780 seconds into the test, operators had noticed that the sounds of violent steam condensation in the Suppression Chamber had begun to die down, and that there had appeared noticeable hesitation in the chugging. This coincides with an apparent transition period starting at roughly 2000 seconds and appearing to end sometime before 3500 seconds in both the sparger DP and sparger outlet temperature data, and can be found in Figure 42. Qualitative reports from operator's notes (regarding the sounds that were being heard by operators) reveal that by 3080 seconds, the acoustic profile had changed significantly, with a longer time between pops. By 3680 seconds, pops were few, far between, and much quieter than before; by 4520 seconds, they had stopped almost entirely. The recorded data shows the largest pressure and temperature

spikes in the sparger occurring approximately once every 7 seconds, with smaller spikes more frequent, similar to the shakedown tests. Similar responses are visible in data from other tests; the temperature and pressure spikes are clear in Test #2, as shown in Figure 43; its largest spikes in the instrument data seemed to occur more frequently, on the order of 1 per second. Test #3 had its largest spikes, appearing somewhat lesser in magnitude than the lower-power tests, occurring on roughly 2-7 second intervals.

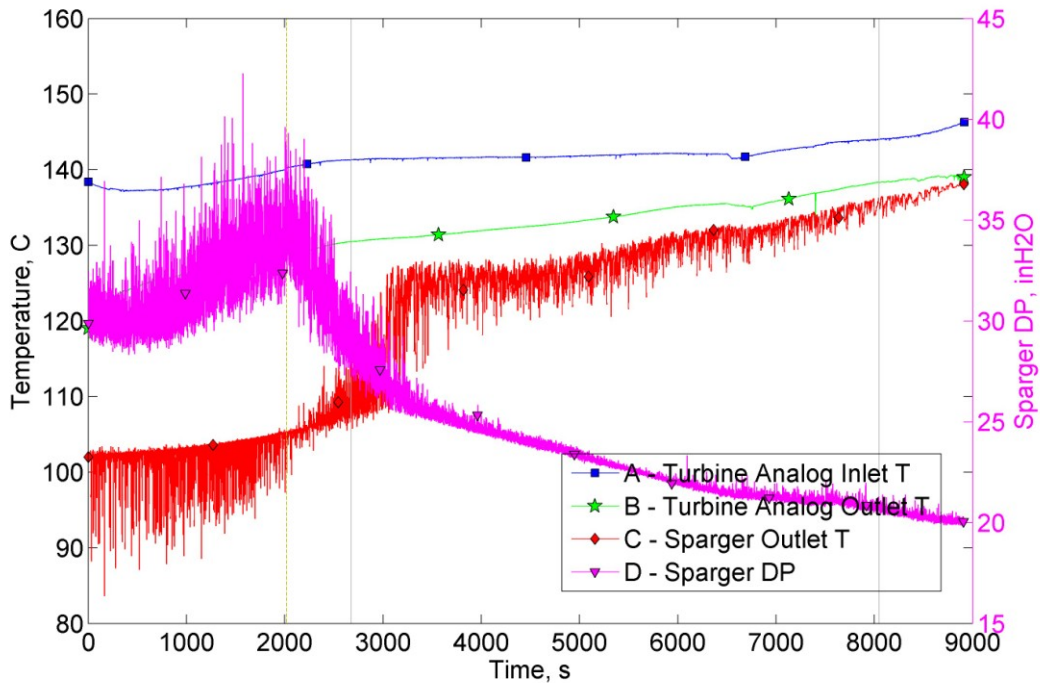


Figure 42: Test #4 Sparger Performance

Long after this test completed, near the end of cooldown operations in preparation for Test #5, the pump motor experienced a catastrophic failure of the centrifugal switch which necessitated replacement of the whole motor. Due to the

relatively small cost difference between a new motor and a completely new pump, a complete replacement pump was procured. In the process of replacement, a Y-strainer was added to the pump inlet to reduce the debris ingestion by the pump.

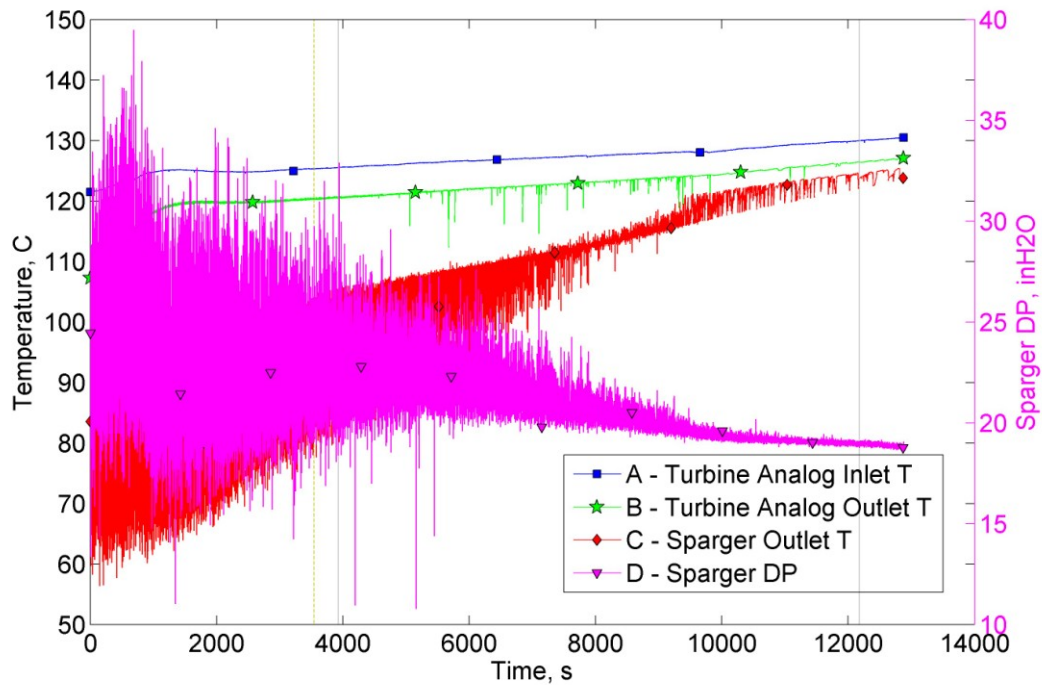


Figure 43: Test #2 Sparger Performance

4.4.5 Test #5

Test #5 was the first of the SRV alignment tests, and has been presented previously in [50]. It was conducted at full power (157 kW), and was like the standard alignment in terms of water injection to the steam line (none) and pressurization conditions (Suppression Chamber isolated from the lab, beginning at atmospheric pressure); the main difference was that instead of the RCIC Turbine analog and sparger,

steam flow was aligned to the SRV sparger. This resulted in reduced main steam line pressures (no orifice to obstruct the steam flow) and a lack of data for DP across the sparger as well as temperatures at the outlet – neither instrument exists on the SRV sparger analog.

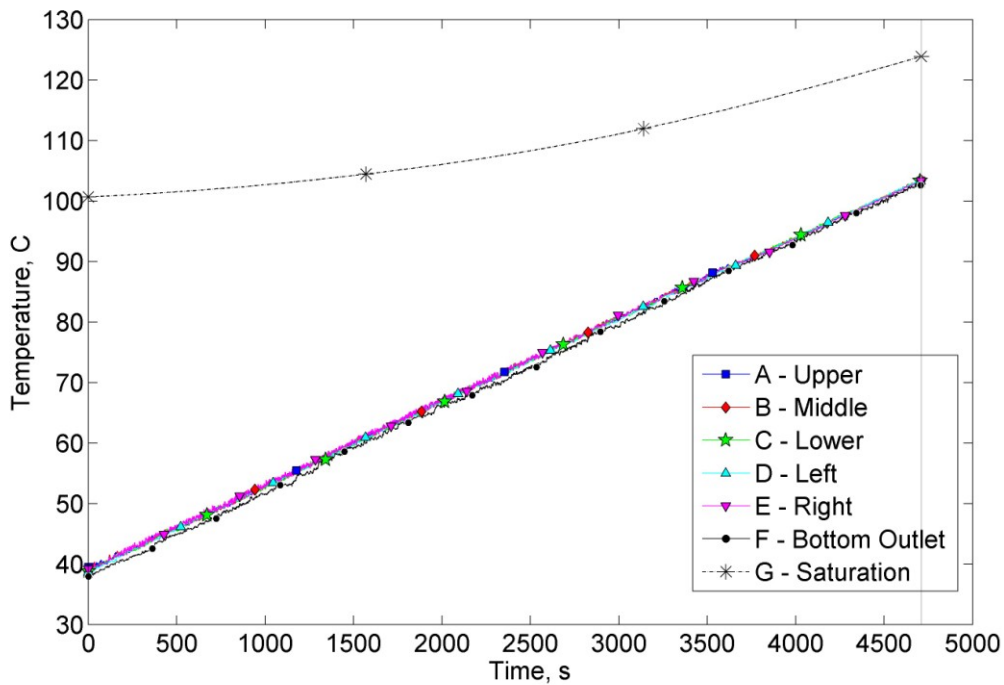


Figure 44: Test #5 Thermal Progression

The test ran with 66.4 ± 2.1 g/s of steam and 65.6 ± 3.5 g/s of feedwater. While it did not run for quite as long as the high power standard alignment test, it ran long enough to go to completion. There were measureable differences in temperature between different locations – a peak of 2.6 °C top-mid, 2.3 °C mid-low, and 5.0 °C low-

outlet (see Figure 44), but that appears to be the result of fluctuating currents within the vessel; no consistent bulk stratification was detected to develop.

Operators did hear what sounded like the violent ‘pops’ and ‘bangs’ of condensation events characteristic of chugging in the RCIC sparger; at the beginning of the test, they were loud, violent, and fast. They lost much intensity by around 3700 seconds, and were quiet and non-violent by the end of the test.

4.4.6 Test #6

Test #6 was a fully-vented medium power (107 kW) RCIC test with no water injection to the steam line. Instead of isolating from the atmosphere, a valve (V-50) to the airspace in the Suppression Chamber was left open for the entire duration of the test, maintaining near-atmospheric pressures in the vessel. This test was discussed previously in [51].

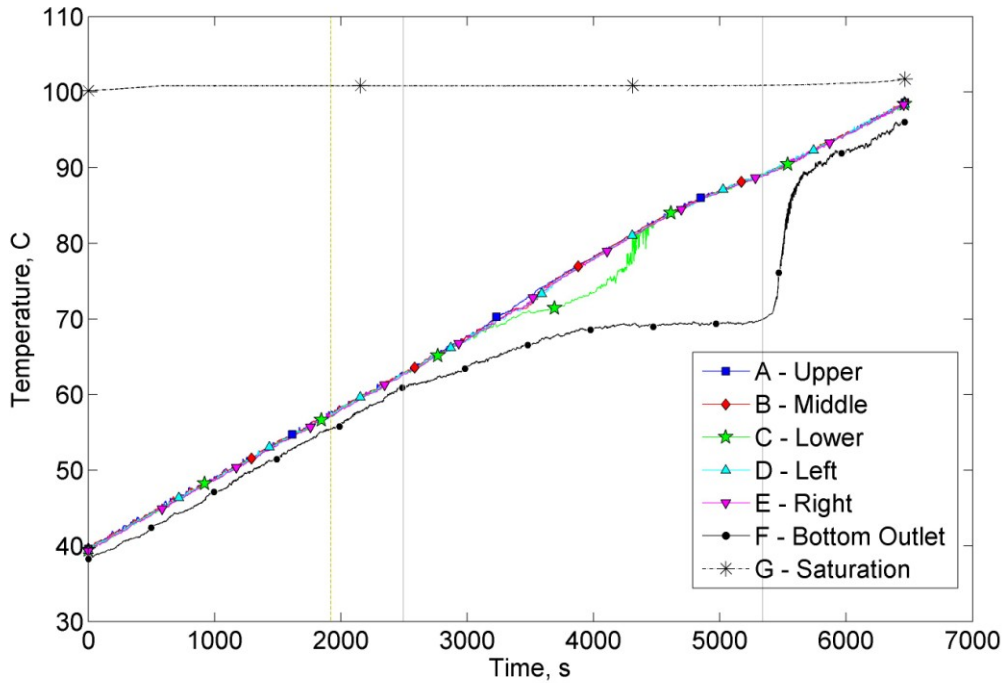


Figure 45: Test #6 Thermal Progression

Steam flow registered at 45.0 ± 1.4 g/s, and feedwater was 43.8 ± 1.9 g/s. This test finished faster than some of the others. The stratification period, at 2846 seconds in duration, was less than half of the test period shown in Figure 45. It also produced weaker gradients than the standard alignment test of the same power (Test #4); the greatest top-mid stratification was 2.4 °C, the mid-low differences were limited to 5.9 °C, and the low-outlet differences peaked at 21.0 °C – a little less than half of the standard alignment value.

The early parts of the test tended to resemble the standard alignment. Pressurization in the standard alignment tends to happen in the latter parts of the test, while the early increases are much smaller. The detected onset of thermal stratification

in the pool only happens about 3 minutes earlier (out of a nearly 108-minute run) in the atmospheric case and has similar bulk pool temperatures. However, in the atmospheric case, the stratification terminates much sooner.

4.4.7 Test #7

Test #7 was a RCIC atmospheric test at medium power with water injection (targeting 0.4 GPM) into the steam line. It was the first of the water injection tests, and was essentially Test #6 run with water injection.

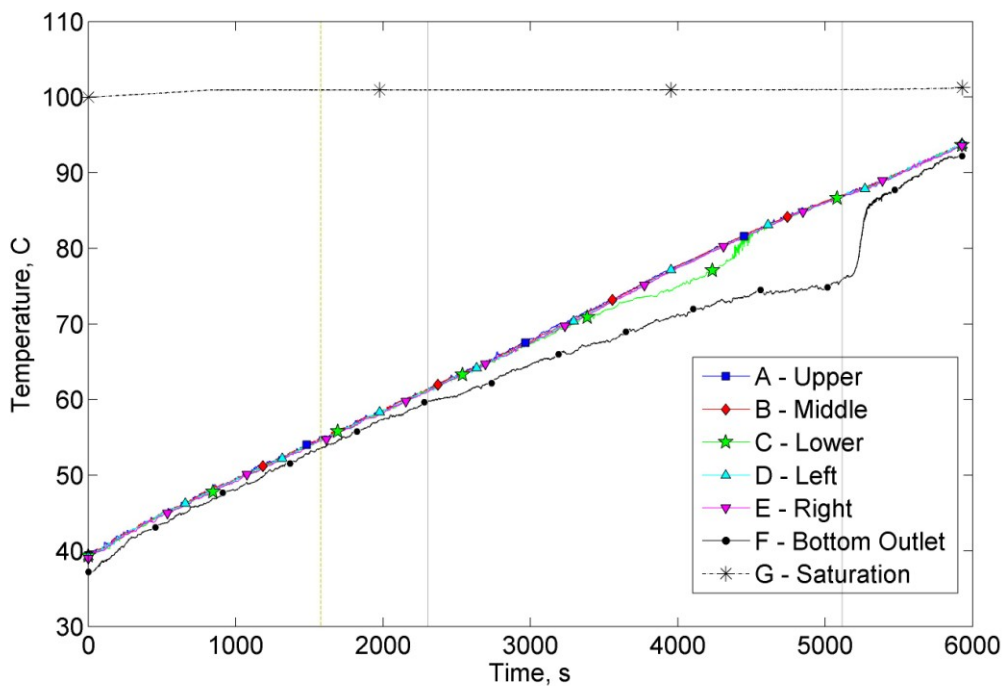


Figure 46: Test #7 Thermal Progression

Steam flow was measured at 45.4 ± 2.3 g/s over the test. Feedwater was 44.0 ± 6.5 g/s, and water injection to the steam line was 24.5 ± 1.9 g/s. The resulting main steam line steam quality was 0.59 ± 0.03 , while post-orifice it was 0.64 ± 0.03 .

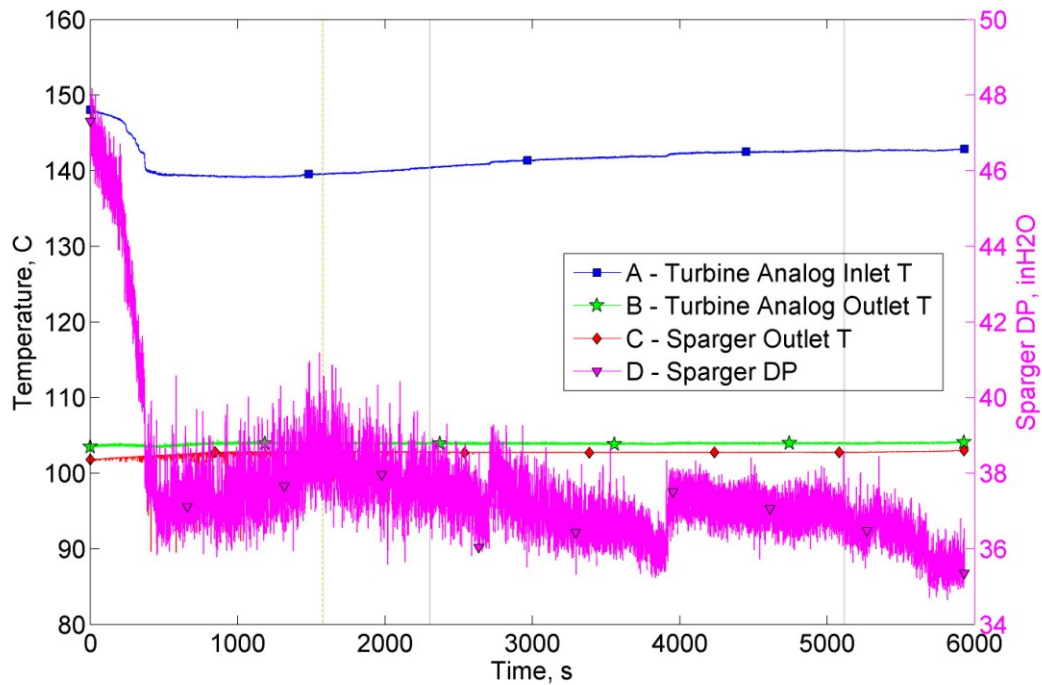


Figure 47: Test #7 Sparger Behavior

The thermal stratification in the Suppression Chamber (shown in Figure 46) was very limited in this test. The top-mid difference peaked at 1.9 °C, while the mid-lower stratification was limited to just 3.4 °C. The low-outlet stratification was less than 2/3 that of Test #6 at only 13.2 °C. The stratification period was similar in duration to that of Test #6, being less than one minute shorter for a nearly 47 minute period. The temperature curves, when compared to Test #4, appear smaller and somewhat distorted.

Even the chugging signatures in the data become much harder to discern; the operator's observations do not line up nearly as well with the sparger outlet temperatures and DP readings (Figure 47) as in other tests.

4.4.8 Test #8

Test #8 was a mid-power (107 kW) RCIC test under standard pressurization with 0.4 GPM of water injection into the main steam line – essentially a standard alignment test with water injection. The results show a somewhat diminished amount of thermal stratification in the Suppression Chamber when compared to the mid-power standard alignment test (Test #4).

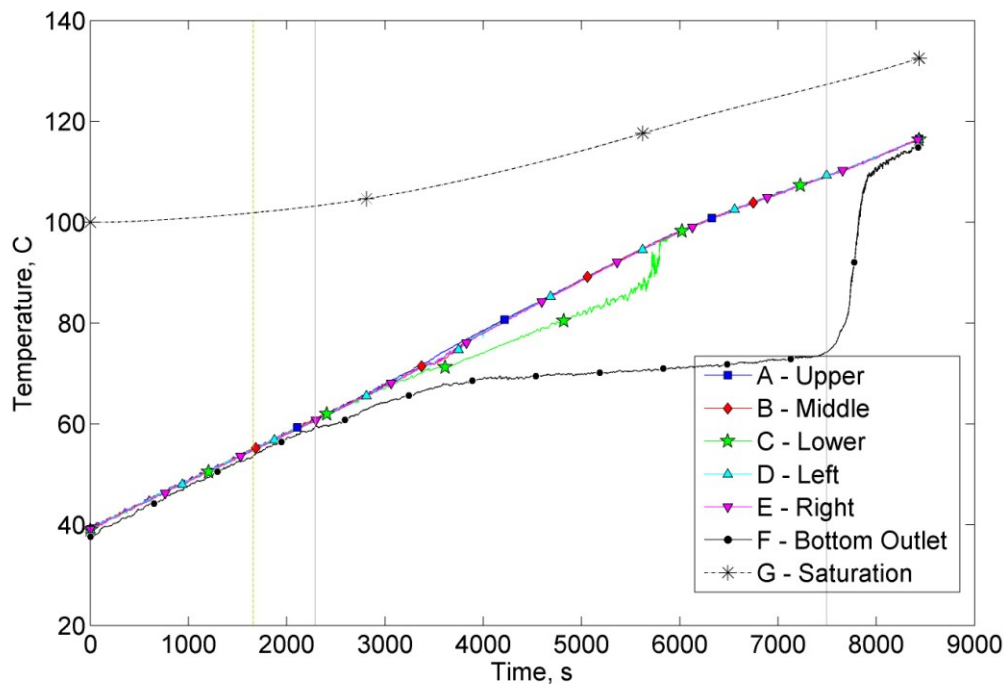


Figure 48: Test #8 Thermal Progression

Steam was injected at a rate of 45.5 ± 1.0 g/s. Feedwater was 44.9 ± 1.3 g/s, and water was injected into the steam line at 24.8 ± 1.1 g/s. This produced a steam quality of 0.59 ± 0.02 , rising to 0.63 ± 0.02 past the orifice.

The resulting thermal stratification in the Suppression Chamber (Figure 48) was below that of Test #4, but was not orders of magnitude less. The top-mid difference peaked at 2.3 °C, while the low-outlet separation was limited to 36.8 °C. The mid-low stratification was the biggest change, both in absolute and relative terms, with a maximum of 11.7 °C (compare to 20.9 °C in Test #4). As with Test #7, the chugging regime was more difficult to distinguish in the recorded data than in the earlier tests. It should also be noted that the pool mid-level thermal profile, while stratified, did not have the same flattening out as displayed in Test #4 ca. 5000 seconds, but instead continued to trend upwards.

4.4.9 Test #9

Test #9 was the first of the pre-pressurized tests conducted, and was previously presented in [51]. It was a mid-power (107 kW) RCIC test, and other than the initial 14 psig of air pressure in the Suppression Chamber it was the same as the standard alignment. It proved challenging on the then-installed equipment, and even had to be terminated early due to reaching the casing pressure limit on the RCIC pump.

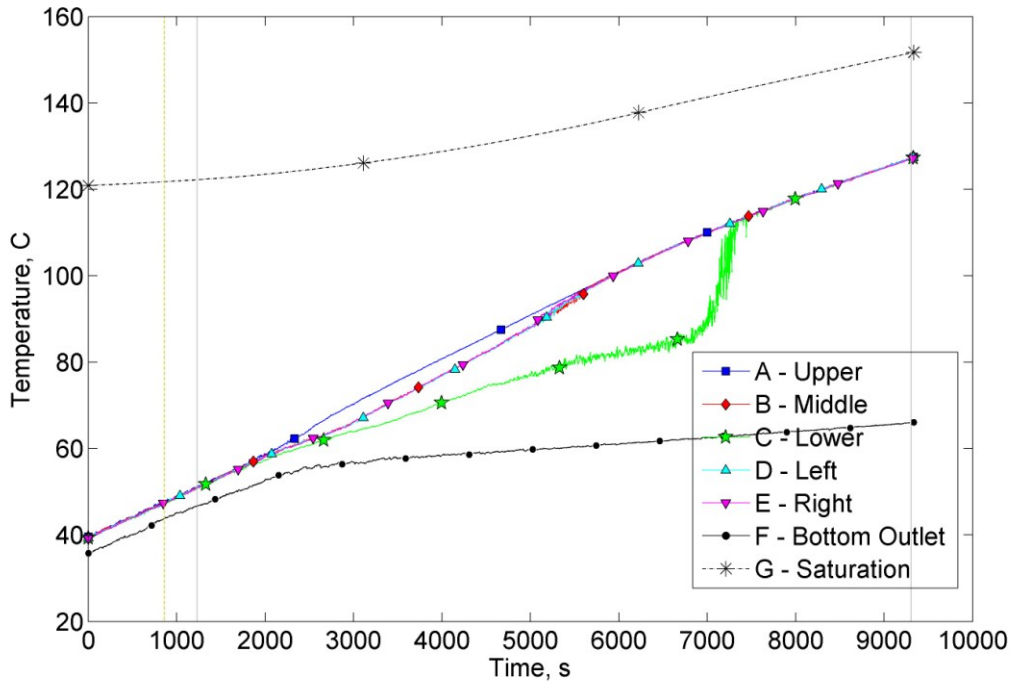


Figure 49: Test #9 Thermal Progression

Steam flow was maintained at 43.5 ± 1.1 g/s, and feedwater flowed at 43.4 ± 1.7 g/s. Over the course of nearly 156 minutes, the pool displayed a remarkable amount of thermal stratification; this is shown in Figure 49. The top-mid stratification peaked at a difference of 5.1 °C, and maintained a clear separation for approximately an hour. The mid-low stratification reached a 29.4 °C difference, the greatest at that location in the entire test series. The low-outlet separation, which was still growing at the termination of the test, reached 61.9 °C.

Not only did the pump outlet pressure limit the test, but it is likely that the relief valve on the line experienced some chattering. The relief's outlet line was observed to be warm to the touch several minutes before the termination of the test. However, the

receiving blowdown drum's temperatures were not observed to be rising significantly; therefore, it is not believed much system inventory was lost through that route.

4.4.10 Test #10

Test #10 was a high-power (157 kW) pre-pressurized RCIC test. With 10 psig of initial air pressure, it behaved in manners similar to both Test #3 and Test #9. As with Test #9, high pump discharge pressures required early test termination.

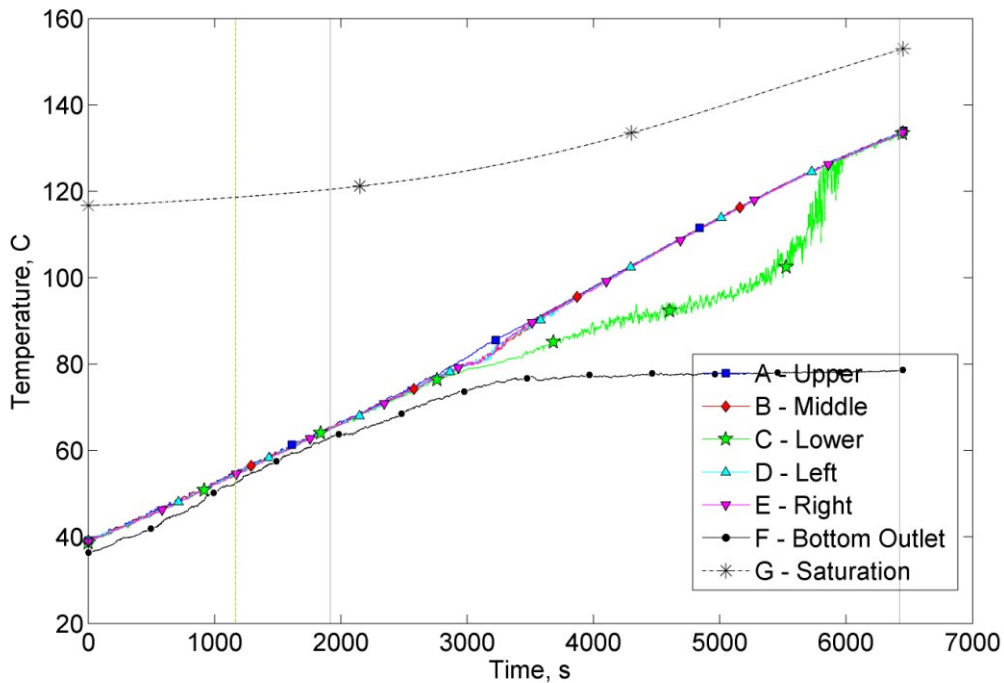


Figure 50: Test #10 Thermal Progression

The steam flowrate was 65.4 ± 3.2 g/s, and feedwater flowed at 64.2 ± 8.5 g/s. Unlike Test #9, which maintained steam generator pressures in the mid to upper 70s psia until late in the test when it was necessary to allow it to rise to provide adequate flow

and superheat in the vortex flowmeter, the steam generator pressure was maintained above 100 psia for most of the test. In addition, early steam flowrates tended to be slightly low as operators slowly worked towards a stable pressure and flow envelope for the entire loop.

The thermal stratification limits in the Suppression Chamber (see Figure 50) were similar to that seen in Test #9. The top-mid difference had a maximum of 4.0 °C, and the mid-low separation reached 29.0 °C. Unlike Test #9, the top-mid profiles did not have such a clear lengthy separation. Similar to Test #9, the low-out stratification was still increasing in intensity at the end of the test, at which point it has reached a difference of 55.0 °C.

4.4.11 Test #11

Test #11 was a mid-power (107 kW) pre-pressurized (15 psig) RCIC test with 0.4 GPM of water injection to the steam line. It was an operationally challenging test, and the first to use the enhanced pump recirculation flow lines (allowing greater flow through the pump to limit the discharge pressure). By the end of the test, much of the equipment was at or fast approaching limiting operational conditions (steam generator, Suppression Chamber, pump discharge). As a result, while the limits of thermal stratification were found, full destratification in the Suppression Chamber was not complete at test termination.

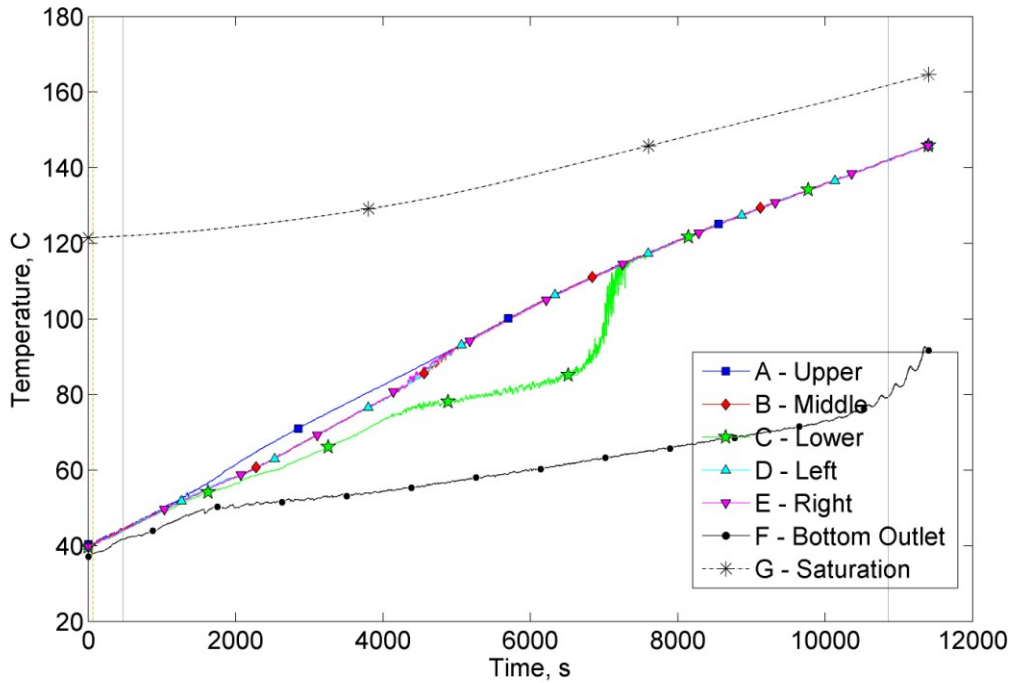


Figure 51: Test #11 Thermal Progression

Steam generator pressures were kept well above 100 psia for the test duration, rising above 120 psia at the very end as needed. For comparison, the Suppression Chamber rose to 100.7 psia at the end – barely 2 psi below the relief valve set point, and its greatest pressure in these tests. This maintained steamflows of 43.7 ± 1.0 g/s while feedwater was 43.1 ± 1.9 g/s. The water injection to the steam line was 24.9 ± 1.5 g/s. The resulting steam quality was 0.57 ± 0.02 , rising to 0.59 ± 0.02 post-orifice.

As with the other pre-pressurized RCIC tests, the thermal stratification in this test was severe; this is revealed in Figure 51. The top-mid differences peaked at 5.6 °C, the greatest in these tests at that location. The mid-low stratification reached 28.9 °C, also one of the highest values recorded at its location. The low-outlet stratification hit its

maximum with a difference of 65.1 °C – not only the maximum recorded for this location, but the maximum one-level separation overall in the entire collection of these tests.

4.4.12 Test #12

Test #12 was a mid-power, moderately pre-pressurized (5 psig) RCIC test – essentially Test #9 with lower start pressurization and abilities to operate the pump longer. It was also documented previously in [51]. In addition, due to the significant fraction of time that the pump discharge pressure monitor was out-of-range high in previous tests, it was upgraded to a higher pressure monitor and the original was instead moved to the pump inlet. This allowed operators better monitoring at the DAQ station of a parameter that had been shown to be limiting for system operation without traveling to the readout gauge.

Flowrates were 44.7 ± 0.8 g/s for steam and 43.7 ± 1.8 g/s for feedwater. As with other pre-pressurized tests, equipment limitations played a major role in the test termination. While it did run to completion, and the destratification was mostly complete, it was not fully complete. The test was terminated when the pump suction temperature approached the thermal limit for the upgraded Viton seal.

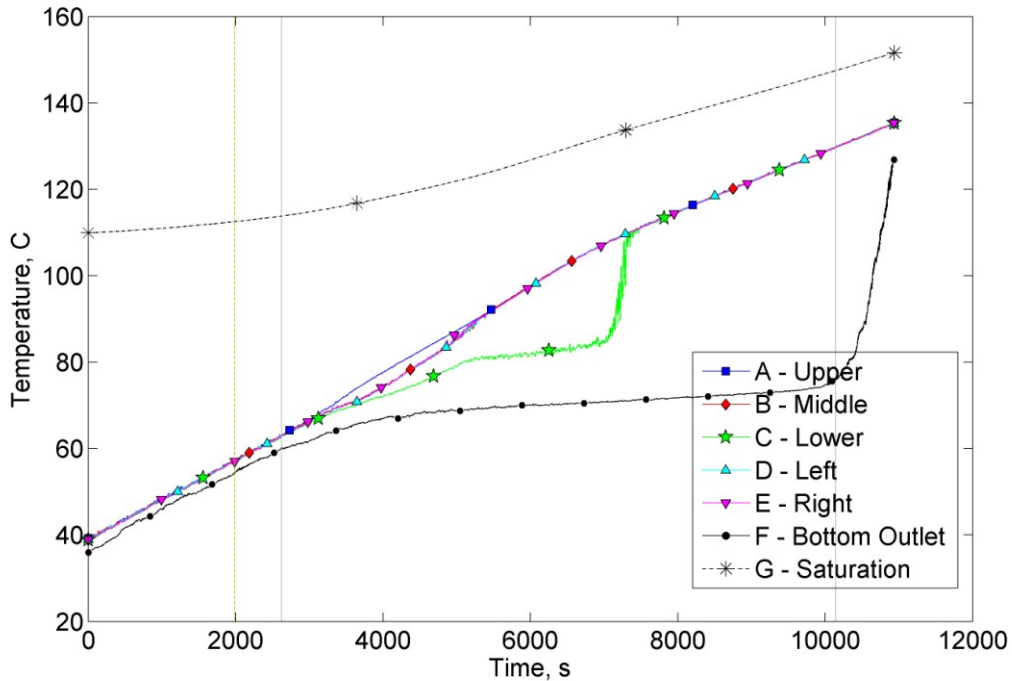


Figure 52: Test #12 Thermal Progression

Thermal stratification in the Suppression Chamber was severe (shown in Figure 52), although not as severe as in other pre-pressurized tests. The top-mid separation reached 4.1 °C, and the mid-low difference peaked at 26.9 °C. At 55.9 °C, the low-outlet stratification limit was well above most other tests.

4.4.13 Test #13

Test #13 was a high-power (157 kW) RCIC test with 0.6 GPM of water injection and standard pressurization – a version of Test #3 with water injection into the steam line. As tended to be the case with other high-power tests with atmospheric pressure in the Suppression Chamber at some point during operation, control was difficult for operators to maintain. In fact, the first attempt at this test went unstable (unable to

balance steamflow with feedwater) and the test had to be aborted at the beginning. The second attempt, however, was successful in collecting data. As a result of the operational demands, superheat in the vortex flowmeter was more limited than in other tests.

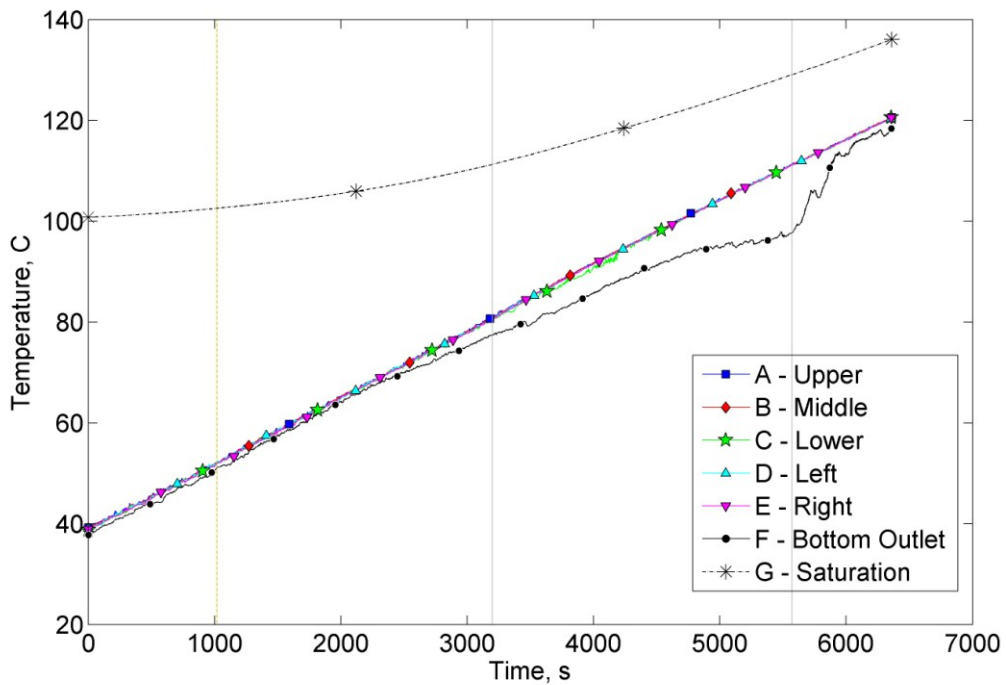


Figure 53: Test #13 Thermal Progression

Steam flow was 66.3 ± 2.9 g/s, and feedwater was maintained at 65.9 ± 5.1 g/s. Water injection to the steam line was 37.2 ± 2.6 g/s. This produced steam qualities of 0.58 ± 0.03 , increasing to 0.63 ± 0.02 downstream of the orifice.

Thermal stratification in this test, depicted in Figure 53, was more limited than in a number of other RCIC tests. The peak top-mid difference was 2.2 °C, while the

maximum mid-low separation was only 1.9 °C. The low-outlet stratification was limited to 15.4 °C, a far cry from the 65.1 °C seen in Test #11.

4.4.14 Test #14

Test #14 was a full-power (157 kW) atmospheric RCIC test with no water injection into the steam line. Due to the number of tests terminated early by equipment limitations, revisions were made to the data acquisition software for this and subsequent tests to notify operators when certain limits are close, and to sound an alarm if conditions get too close to said limits.

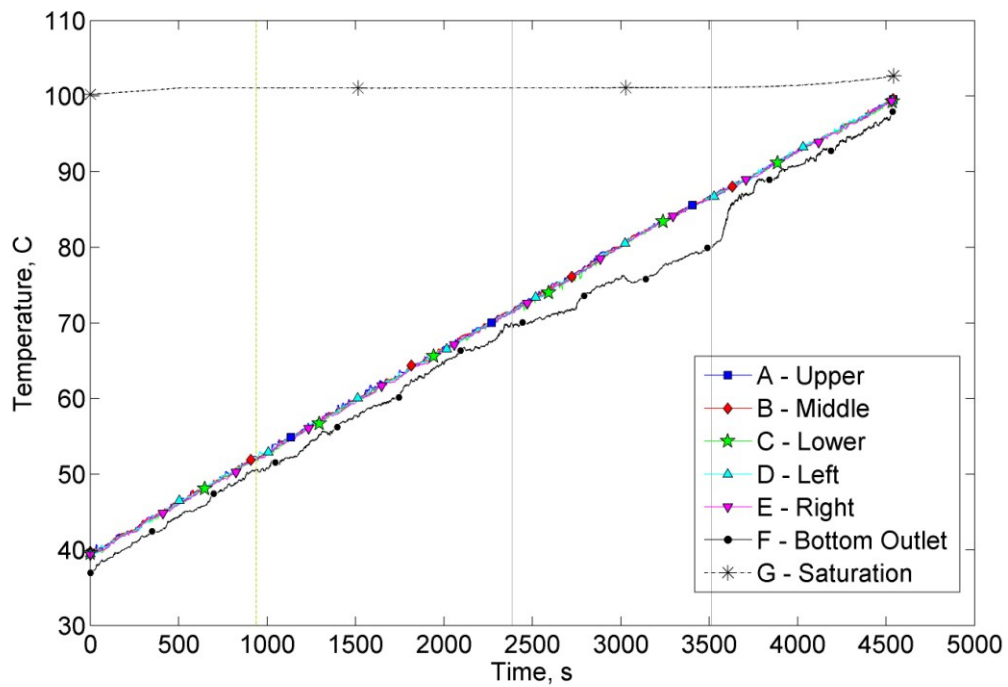


Figure 54: Test #14 Thermal Progression

Steam flow ran at 66.8 ± 2.0 g/s. Feedwater was 65.2 ± 10.6 g/s; as with the other high-power tests, this test was more difficult to keep stable than the mid-power ones. Over the course of this (more than 75-minute) test, pressures in the Suppression Chamber were nearly constant at atmospheric.

The thermal stratification developed in this test, shown in Figure 54, was some of the weakest developed in all of the RCIC tests. Top-mid separation was limited to 2.2 °C, and the mid-low numbers were even less at just 1.5 °C. Even the low-outlet values had a relatively small peak separation, being just 9.1 °C. The profiles themselves were not only weak, the outlet temperature meandered more so than in other tests. It did not develop the clean flattening profile seen in the standard alignment runs.

4.4.15 Test #15

Test #15 was a mid-power (107 kW) standard pressurization SRV test. Over the course of its nearly 135 minute run, no major consistent thermal stratification profile was detected.

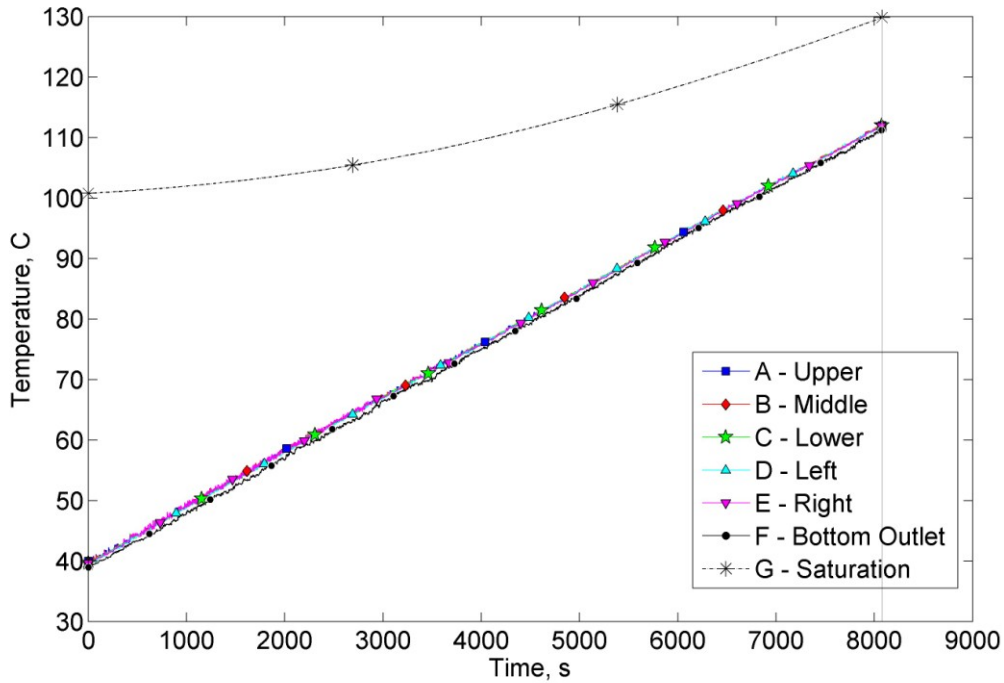


Figure 55: Test #15 Thermal Progression

Steam flowrates were 45.7 ± 1.6 g/s. Feedwater was maintained at 45.6 ± 1.7 g/s.

While a major stratification profile was not detected (see Figure 55), there were still detectable differences in the measured temperatures at different pool elevations. The top-mid difference was limited to 2.3 °C, and the mid-low differences peaked at 2.1 °C. This test had the weakest low-outlet temperature separation at that level for the entire test series, with a maximum of only 4.1 °C.

4.4.16 Test #16

Test #16 was a pre-pressurized SRV test at mid-power (107 kW). It was much the same as Test #15, with the notable exception of starting at 15 psig. An operational

error in the first attempt to run this test resulted in termination at the beginning of the first attempt; after cooling, a second attempt was able to complete successfully.

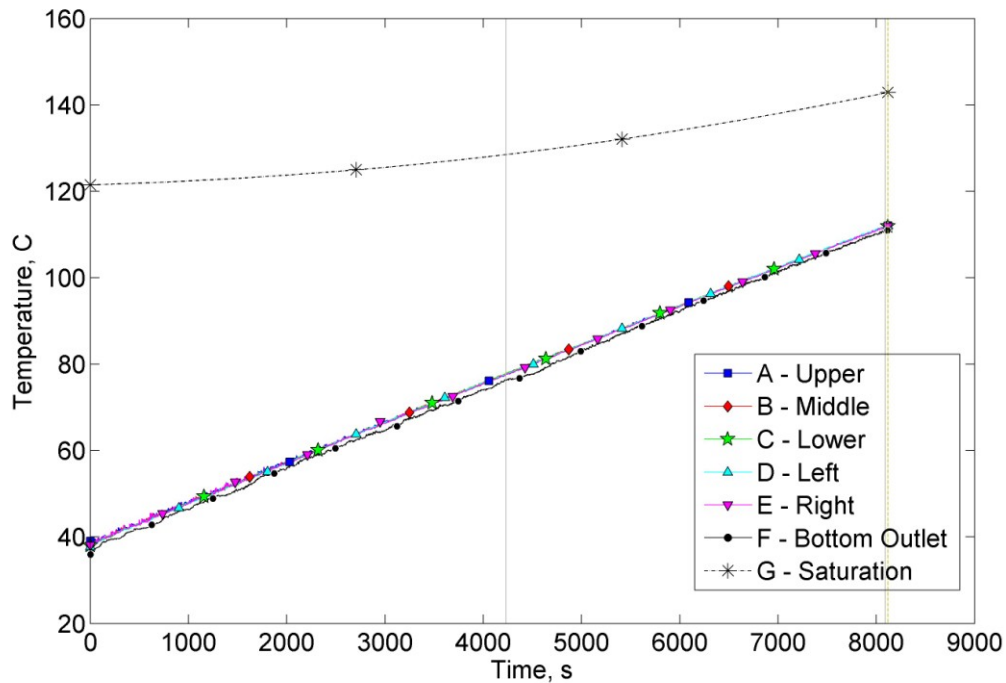


Figure 56: Test #16 Thermal Progression

The test ran for a period of more than 135 minutes. The steam flowrate was 45.5 ± 1.2 g/s, and the feedwater flowrate was 45.4 ± 1.8 g/s.

The stratification detection routines report a stratification period for nearly half the test. Indeed, the outlet temperatures do appear to be measurably lower than those of the higher elevations as depicted in Figure 56. However, they also fluctuate more and are not far below the higher elevation temperatures, making detection problematic. The detected stratification here may be more of an issue with heat loss at the vessel outlet

than inhomogeneous thermal deposition. The top-mid and mid-low differences peaked at 2.4 and 3 °C, respectively; the low-outlet difference reached a maximum of 5.5 °C.

4.4.17 Test #17

Test #17, much like Test #15, was a mid-power (107 kW) standard pressurization SRV test. Unlike #15, this test included water injection into the steam line at a target rate of 0.4 GPM. It remained well mixed, as demonstrated by Figure 57.

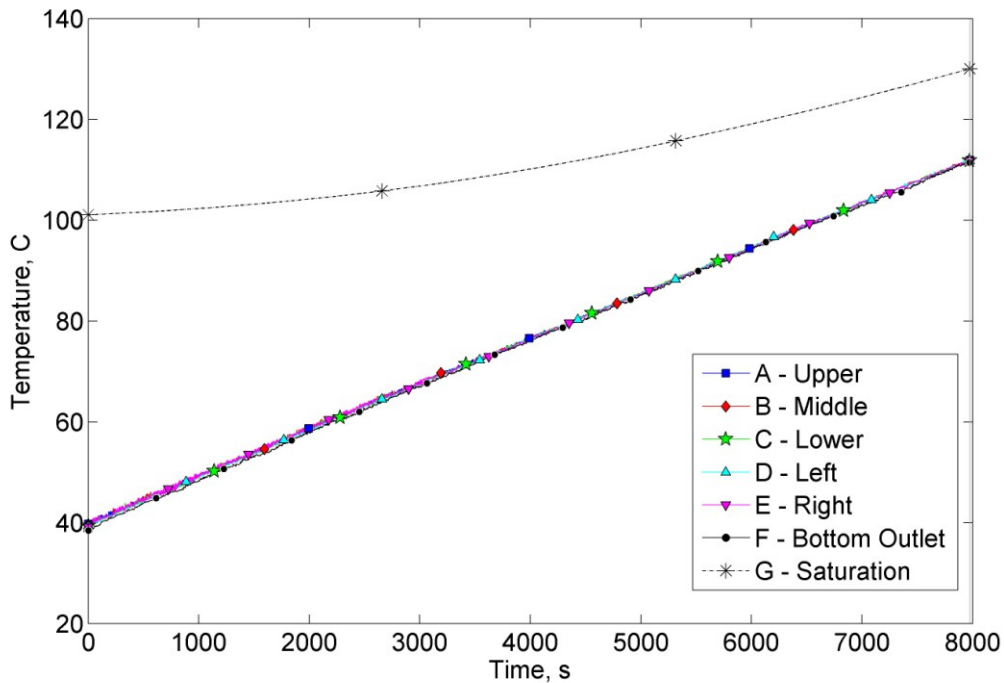


Figure 57: Test #17 Thermal Progression

This test was less than two minutes shorter than Test #15, finishing just short of 133 minutes. It had a steam flowrate of 45.4 ± 1.6 g/s, and feedwater flowed at $45.4 \pm$

1.9 g/s. Water was injected into the steamline at 25.3 ± 1.4 g/s, producing a quality of 0.62 ± 0.02 .

The peak thermal differences in this test were almost identical to those of Test #15, although their times in the test were different. The top-mid and mid-low differences were 2.2 and 2.1 °C (compare to 2.3 and 2.1 °C in Test #15), respectively. The peak low-outlet difference was 4.2 °C (Test #15 showed 4.1 °C).

4.4.18 Test #18

Test #18 a bit of a cross between Test #8 and Test #12. It was a mid-power (107 kW), somewhat pre-pressurized (5 psig) RCIC test with 0.4 GPM water injection into the steam line. As was the case for several other tests, this test was terminated before full destratification was complete to keep the pump's seal within its thermal limits.

Steam flowed at 44.4 ± 0.8 g/s, and feedwater ran at 44.8 ± 1.6 g/s. The water injection rate was 25.3 ± 1.0 g/s, producing qualities of 0.58 ± 0.01 (0.60 ± 0.02 past the orifice). As with other water-injected RCIC tests, the whole chugging period is difficult to identify from instrument data alone.

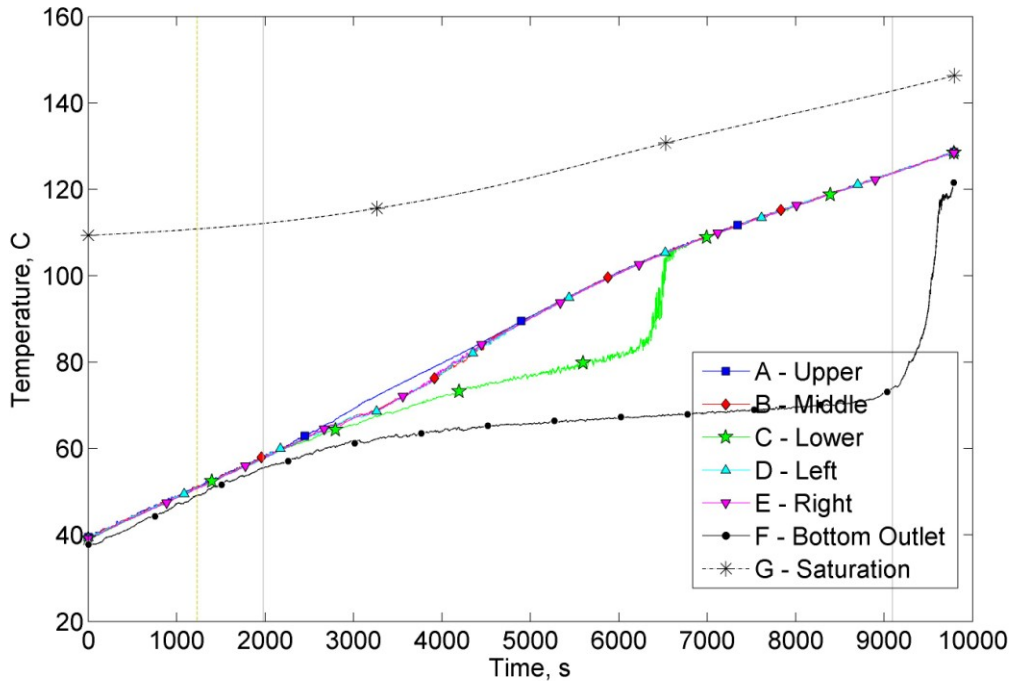


Figure 58: Test #18 Thermal Progression

The thermal profile for this test (Figure 58) followed that of Test #12 more than that of Test #8. The top-mid difference was limited to 3.7 °C. The mid-low and low-outlet separations peaked at 25.5 and 52.6 °C, respectively; these were much closer to Test #12's 26.9 and 55.9 °C than to Test #8's 11.7 and 36.8 °C.

4.4.19 Test #19

Test #19 was another pre-pressurized RCIC test with water injection. In this case, the test ran at full power (157 kW) with 0.6 GPM of water injection into the steam, and had the Suppression Chamber pre-pressurized to 10 psig. Similar in nature to Test #11, the necessary pressures in the steam generator were relatively high; they ran above 100 psia for most of the test, and finished well above 120 psia – at which point the reliefs on

the steam generator, while not lifted, were noticeably leaking steam. Destratification, while detected, once again could not go through to completion in order to protect the pump seal.

Over the course of this nearly 140-minute test, the Suppression Chamber pressure rose to 95.6 psia – the second highest termination pressure in these tests. Steam flowed at 66.4 ± 2.8 g/s, and feedwater fed the steam generator at 65.7 ± 3.3 g/s. Water injection into the steam at 37.4 ± 1.2 g/s produced a quality of 0.58 ± 0.02 , which rises to 0.61 ± 0.02 past the orifice.

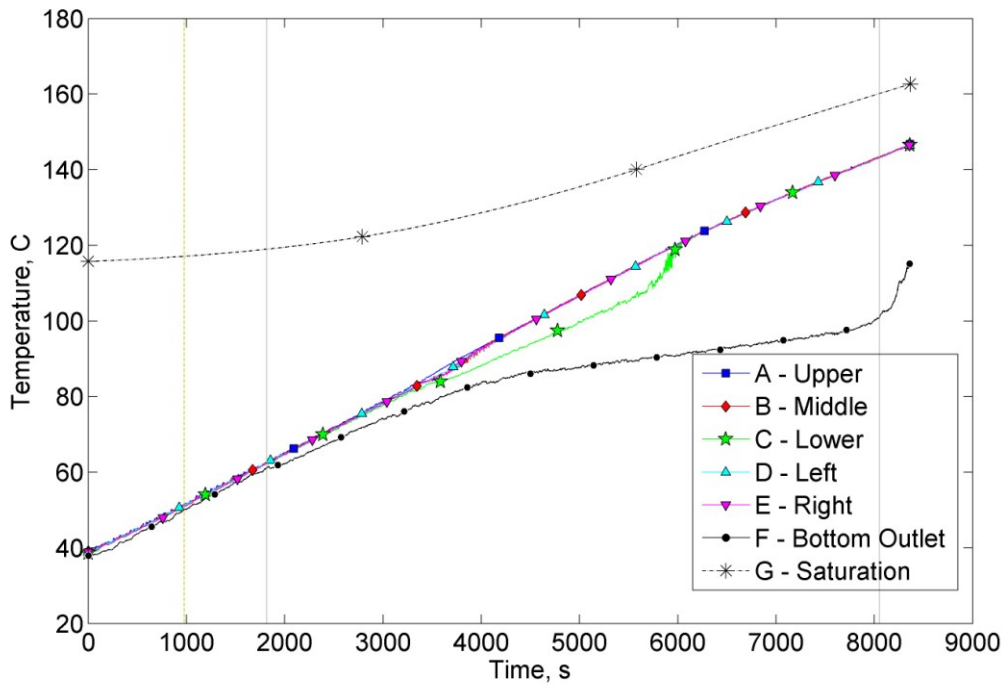


Figure 59: Test #19 Thermal Progression

The stratification profile (Figure 59) did not flatten out as much as in other tests; rather, temperatures separated but kept increasing (albeit at slower rates) as was seen in other water injection tests. The degree of stratification was also lower than seen in other pre-pressurized tests. The top-mid difference was limited to 2.7 °C, and the mid-low values peaked at 12.0 °C. While not small, the maximum low-outlet separation of 44.4 °C here was still only around 2/3 the largest value in these tests.

4.4.20 Test #20

Test #20 was a low-power (57 kW) atmospheric RCIC test with no water injection to the steam line. It ran for nearly 217 minutes.

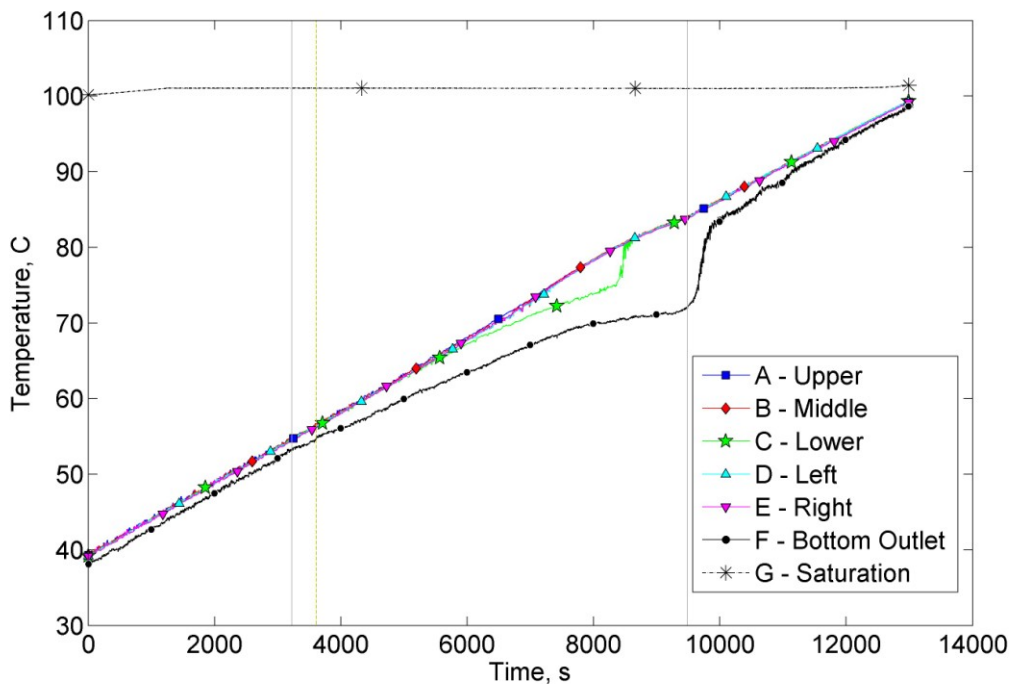


Figure 60: Test #20 Thermal Progression

Steam flowed at 23.9 ± 0.8 g/s, and feedwater to the steam generator ran at 23.5 ± 1.1 g/s. The resulting stratification, shown in Figure 60, was weaker than in many other tests, consistent with the low power and atmospheric conditions. The top-mid profile only saw a peak separation of 1.6 °C, and the mid-low stratification was limited to 5.8 °C. The low-outlet stratification reached a maximum of only 14.0 °C, one of the smaller values in the RCIC tests.

4.4.21 Test #21

Test #21 was a low-power (57 kW) RCIC test with standard pressurization and 0.2 GPM water injection into the steam line. This test was akin to Test #2 with the addition of water injection to the steam. The test ran for more than 265 minutes, well beyond the point of full thermal destratification in the Suppression Chamber.

Steam flowed at 23.8 ± 0.8 g/s, and feedwater sent 23.2 ± 0.9 g/s back to the steam generator. With 12.5 ± 0.4 g/s of water injection into the steam line, the quality was maintained at 0.62 ± 0.02 . This rose to 0.63 ± 0.01 downstream of the orifice.

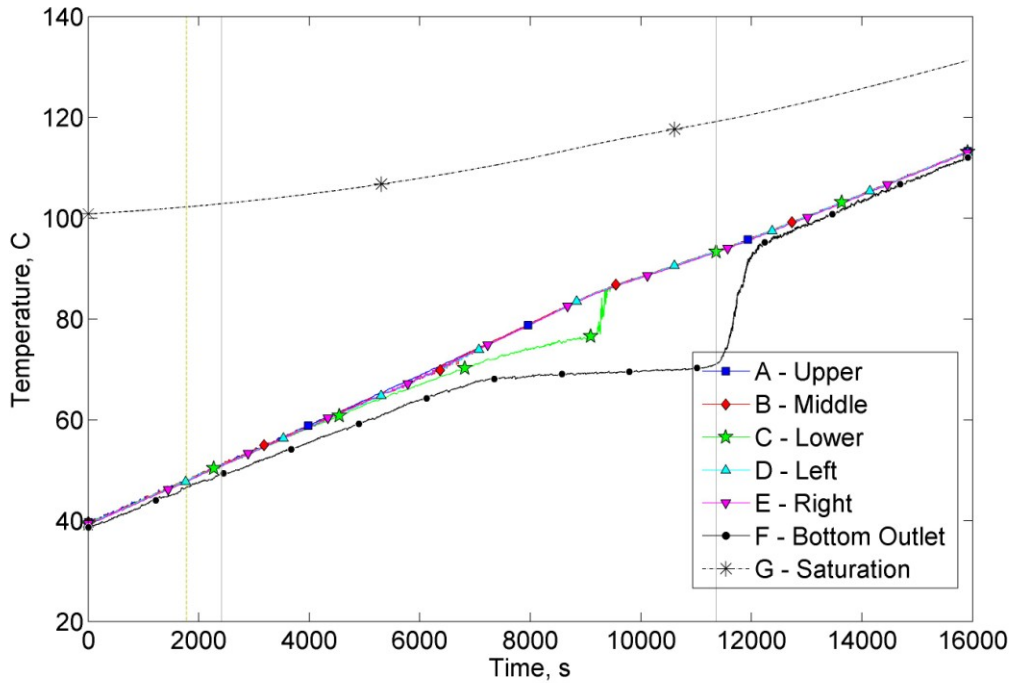


Figure 61: Test #21 Thermal Progression

Interestingly, the resulting thermal stratification in the Suppression Chamber (see Figure 61) tended to be greater than that of Test #2 (although not much greater, and was similar to the results from Test #1). The top-mid separation was 1.5 °C. The mid-low difference peaked at 10.6 °C, on par with the 10.8 °C of Test #1 and more than the 9.3 °C of Test #2. The peak low-outlet stratification was 23.9 °C, more than the 22.6 °C of Test #2; Test #1 terminated before a fully comparable limit was found (terminated at 20.7 °C).

4.4.22 Test #22

Test #22 was a low-power (57 kW) pre-pressurized (5 psig) RCIC test with no water injection to the steam line. At nearly 271 minutes, it was one of the longest tests performed; the thermal profile is shown in Figure 62.

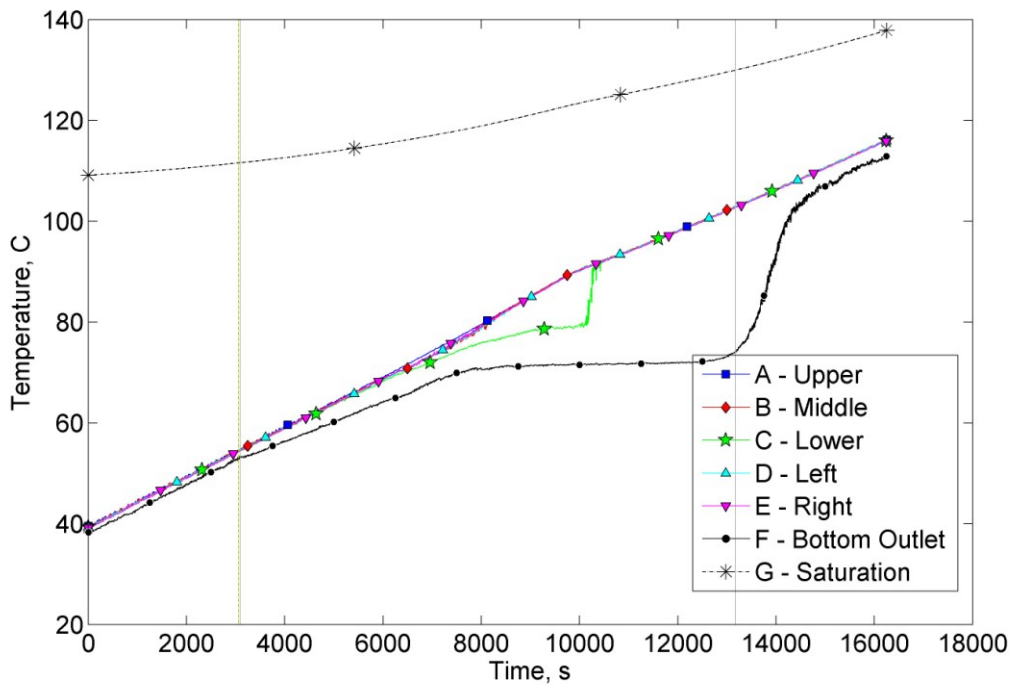


Figure 62: Test #22 Thermal Progression

Steam flowed through the RCIC Sparger at 23.7 ± 0.6 g/s, and feedwater flowed back to the steam generator at 23.5 ± 0.9 g/s. As was the case with other pre-pressurized tests, the resulting thermal stratification in the Suppression Chamber was greater than in the comparable test without pre-pressurization (here, Test #2).

While the stratification limit for the top-mid region had an insignificant difference between this test and Test #2 (1.7 °C here vs. 1.4 °C in Test #2), the lower regions did show greater stratification. The mid-low difference peaked at 13.2 °C, measurably more than the 9.3 °C of Test #2, and the low-outlet separation reached 30.7 °C (more than 8 °C greater than the 22.6 °C of Test #2).

4.4.23 Test #23

Test #23 (profiled in Figure 63) was a low-power (57 kW) pre-pressurized (5 psig) RCIC test with 0.2 GPM water injection into the steam line. It was essentially Test #22 with the addition of water injection, and ran for almost the same amount of time; it was just two minutes shorter.

The steam flowrate was 23.3 ± 0.5 g/s, and feedwater flowed at 22.9 ± 1.2 g/s. The water injection rate to the steam line was 12.5 ± 0.4 g/s, resulting in a steam quality of 0.61 ± 0.01 . Downstream of the orifice, this became 0.62 ± 0.01 .

As was the case with Test #21, the addition of water injection into the steam line seemed to increase the degree of thermal stratification in the Suppression Chamber when compared to a similar water-injection free test (here, Test #22). This appears to be limited to low power tests; higher power levels appeared to experience the opposite.

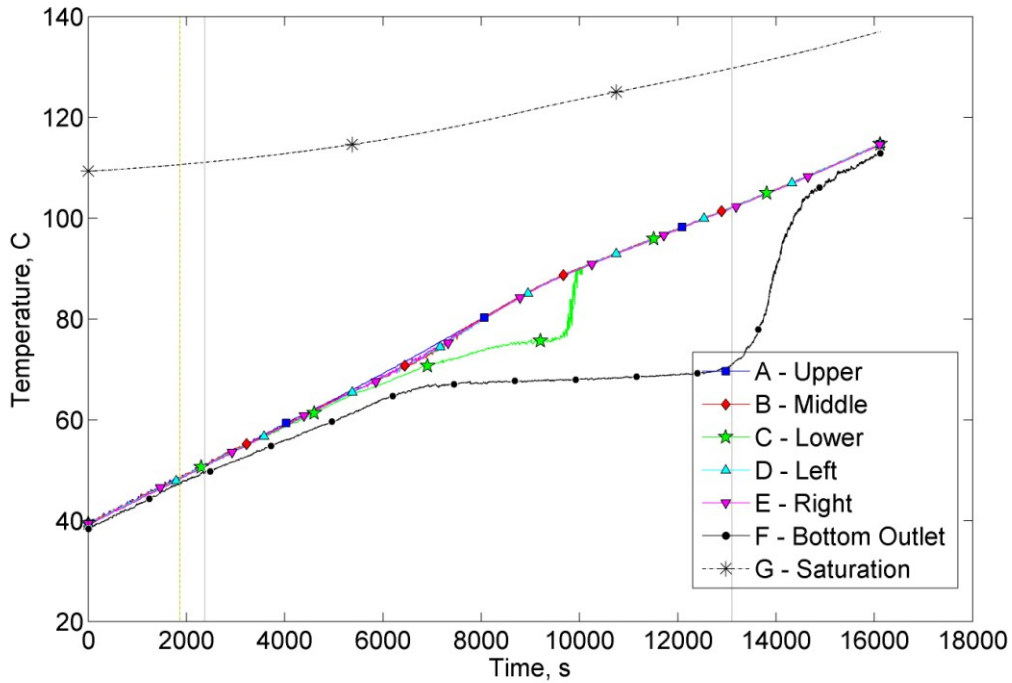


Figure 63: Test #23 Thermal Progression

The peak difference for the top-mid levels was 1.8 °C, not significantly greater than the 1.7 °C of Test #22. The 14.4 °C separation at the mid-lower level was greater than the 13.2 °C at that level in Test #22, but not by much. The greatest increase was seen in the low-outlet region, which experienced up to 32.9 °C of separation; this was a 2.2 °C (~7%) increase from the 30.7 °C of Test #22.

4.4.24 Test #24

Test #24 was the first of two tests (the other being Test #26) which investigated the effects of a simple venting operation. In this test, a mid-power (107 kW) RCIC test with no water injection to the steam line started out with the Suppression Chamber pre-pressurized to 15 psig. Then, when temperatures in the upper middle of the pool (SP 11)

were greater than 86 °C, operators opened a vent line from the vapor space and let the Suppression Chamber blow down to near atmospheric pressure. At that point (Thermocouple SP11 ~ 89 °C), the vent line was closed and the Suppression Chamber re-isolated from the outside atmosphere; pressure once again began to rise through the final end of the test.

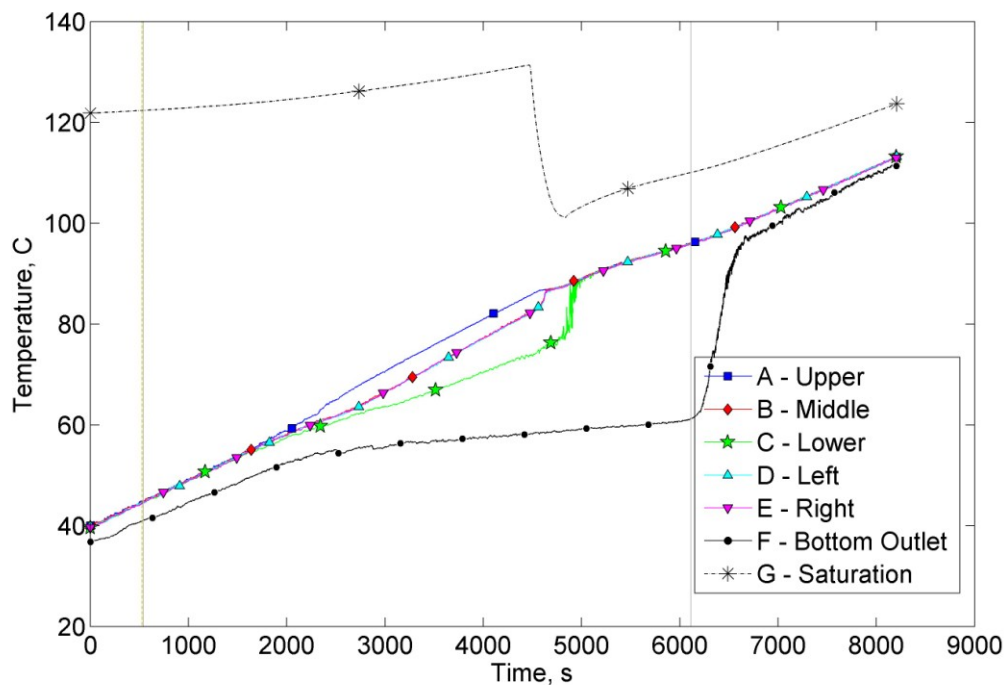


Figure 64: Test #24 Thermal Progression

The steam flow was maintained at 44.8 ± 1.3 g/s, and feedwater was 44.0 ± 1.8 g/s. The initial stratification profile developed as it had in the pre-pressurization case of Test #9. The peak top-mid level stratification was found to be 5.1 °C, the same as in Test #9. It was not impacted by the venting, as venting did not occur until about 21

minutes after the peak had passed. However, there was still significant stratification at that level when the venting occurred, and during venting (the sudden drop in saturation temperature in Figure 64) the difference suddenly and rapidly disappeared.

Similarly, the mid-low thermal stratification appears to have been strongly impacted by the venting procedure. Shortly after the end of the operation, the lower level temperatures jumped up to those of the upper levels. The peak stratification was then 14.6 °C, falling between the fully vented case (Test #6, 5.9 °C) and the standard alignment (Test #4, 20.9 °C). This was reflected in the low-outlet profiles as well, which produced a maximum difference of 36.6 °C, closer to Test #4's 43.3 °C than to Test #6's 21.0 °C.

4.4.25 Test #25

Test #25 was a low-power (57 kW) standard pressurization SRV test. It was also the last SRV test performed, and ran for more than 282 minutes.

The test had a steam flowrate of 23.9 ± 0.9 g/s, and feedwater was at 23.7 ± 1.1 g/s. The thermal profile in the Suppression Chamber was, as with the other SRV tests, largely well-mixed as depicted in Figure 65. The top-mid levels showed a peak separation of 1.9 °C, and the mid-low levels kept within 2.3 °C. The outlet temperatures did tend to lag behind the rest of the Suppression Chamber; the maximum difference was 4.4 °C, but the profile itself triggered the stratification detection algorithm.

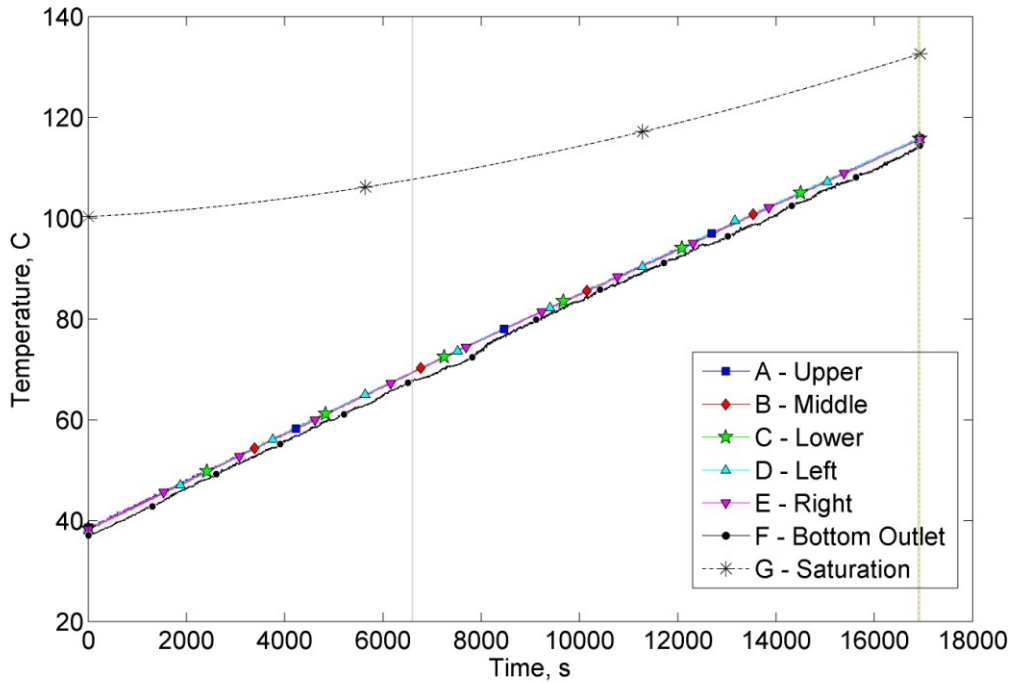


Figure 65: Test #25 Thermal Progression

4.4.26 Test #26

Test #26 was, in a manner not completely unlike Test #24, a venting procedure RCIC test. However, in this test the vent was initially open, and then closed partway through the test. As a result, the early portion of the test was essentially identical to the fully-vented mid-power case (Test #6). When the temperature from SP 11 registered 82 °C, however, the vent was closed and the Suppression Chamber subsequently began to pressurize (note the change in behavior for the saturation temperature in Figure 66); this was maintained through the end of the test. This test ran at mid-power (107 kW) for more than 143 minutes, and had no water injection into the steam line.

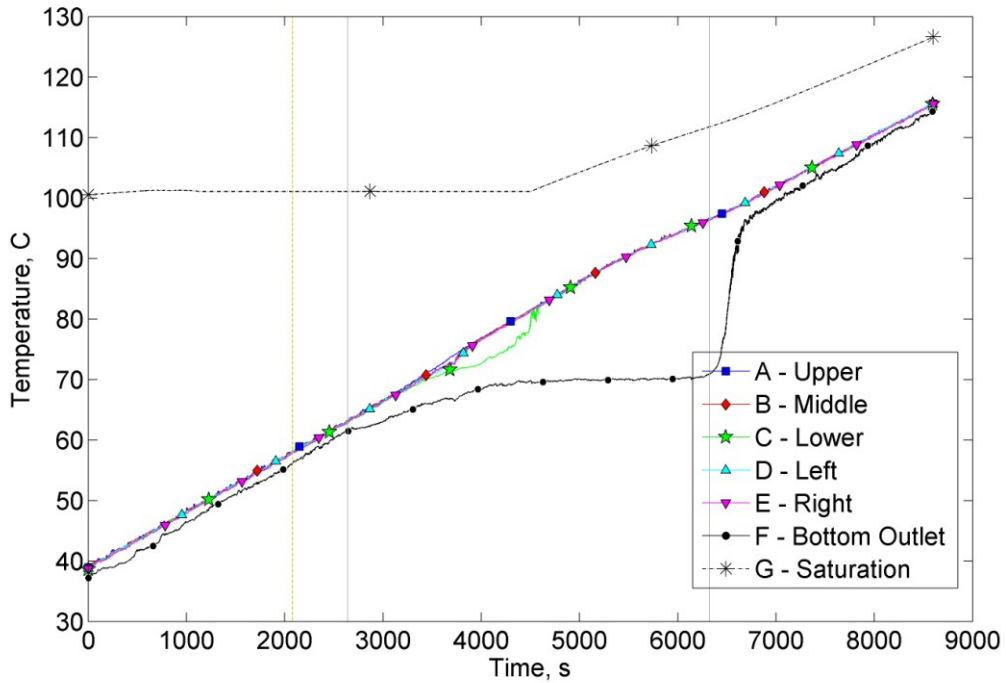


Figure 66: Test #26 Thermal Progression

The steam flowrate was 45.6 ± 1.3 g/s, and the feedwater flowed at 44.7 ± 1.6 g/s. Up to the vent closure, this test produced results in line with those of Test #6, and the timings were within a few short minutes for the major features. Here, both the top-mid and mid-low peak thermal stratification occurred before vent closure, producing separations of 2.2 °C and 5.8 °C, respectively. The values, in order, from Test # 6 were 2.4 °C and 5.9 °C.

The low-outlet stratification limit, however, occurred in Test #6 after more than 87 minutes; the vent closure in this test occurred near the 75-minute mark, and all subsequent data should reflect the influence of the vent closure. The low-outlet

stratification reached a greater limit at 27.7 °C here vs. the 21.0 °C seen in Test #6, and occurred at the 105 minute mark.

4.4.27 Test #27

Test #27 was a mid-power (107 kW) standard pressurization RCIC test with extra water injection to the steam line (0.8 GPM). It was similar to Test #8, except with a greater water injection to steam flowrate (0.8 vs 0.4 GPM). It was also the final test performed in the NRC testing program.

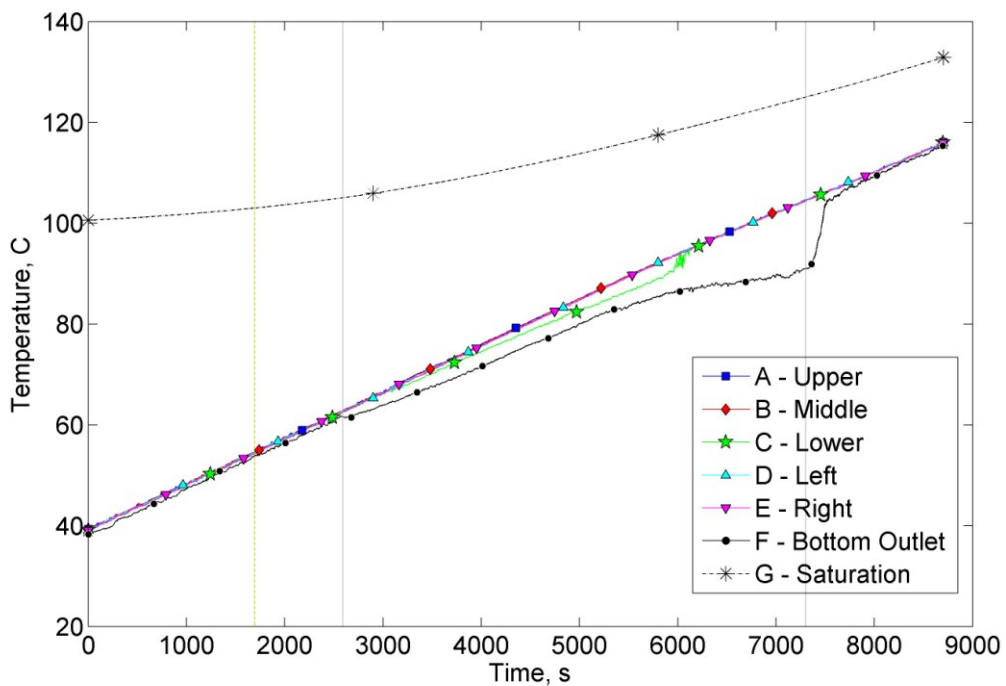


Figure 67: Test #27 Thermal Progression

Steam was kept to a flowrate of 44.8 ± 1.5 g/s, and feedwater flowed at 44.4 ± 1.6 g/s. With water injected to the steam line at 49.9 ± 1.6 g/s, the steam quality was lower than most other tests at 0.40 ± 0.03 (0.44 ± 0.02 past the orifice).

As was the case with other water-injected tests, the resulting thermal stratification profiles (Figure 67) did not flatten out as much as in the non-injected cases. In this test, the thermal stratification was more limited than the less-injected case (Test #8), and much more so than in the non-injected case (Test #4). The top-mid separation peaked at 1.7 °C here, reduced from the 2.3 °C in Test #8 and the 3.1 °C from Test #4. Similarly, the mid-low difference was 3.7 °C vs. the 11.7 °C and 20.9 °C of Tests #8 and #4, respectively. The diminished peak separation for the low-outlet temperatures was similarly significant, dropping to 15.7 °C from 36.8 °C in Test #8 and 43.3 °C in Test #4.

4.4.28 Test #28

Test #28 was the first of two constant 2-atm pre-pressurized RCIC tests performed. For this test, the vent line on the Suppression Chamber normally connected from the block valve to the blowdown drum was instead reconnected from the block valve to a backpressure regulator; after charging the Suppression Chamber with 15 psig of air, the regulator was carefully adjusted as necessary to maintain as constant as achievable the pressure in the Suppression Chamber.

This test was notable for starting at a much lower temperature than the earlier tests, and the test period began at 30 °C rather than the normal 40 °C (significant extra cooldown time permitted a cooler start temperature); this permitted the mid-power (107

kW) test to run for more than 170 minutes until temperatures approached saturation (demonstrated in Figure 68). There was no water injection into the steam line.

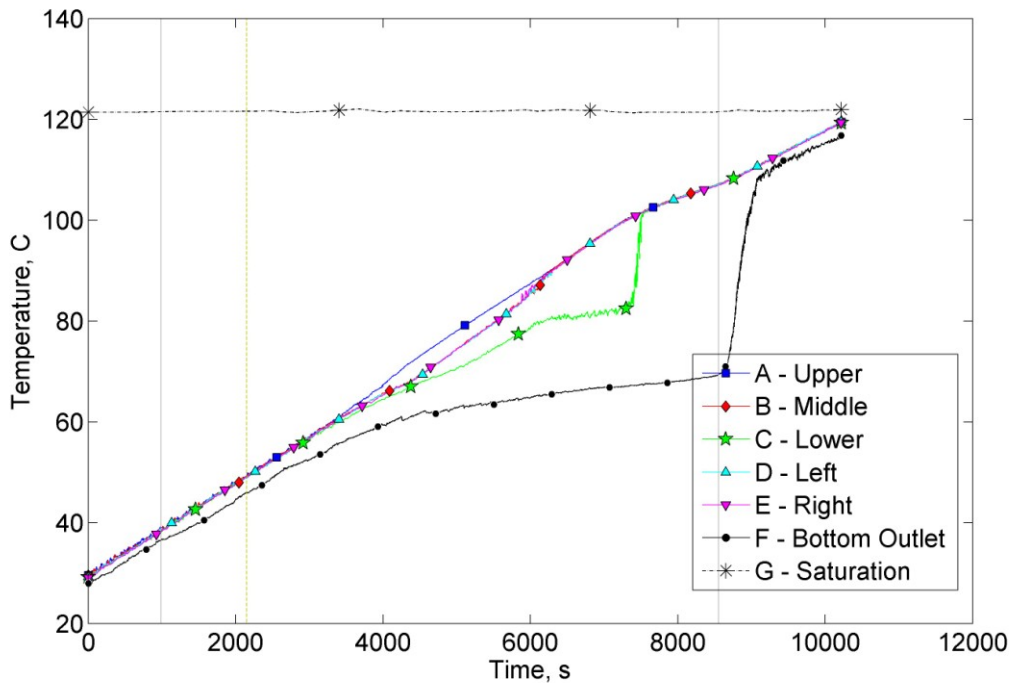


Figure 68: Test #28 Thermal Progression

The steam flow was maintained at 44.6 ± 1.5 g/s, and feedwater was sent to the steam generator at 43.9 ± 1.6 g/s. This produced a peak top-mid stratification of 4.5 °C, and a mid-low separation of 21.0 °C. The peak low-outlet difference was 39.6 °C.

4.4.29 Test #29

Test #29 was the second of two constant-pressure (2 atm) pre-pressurized RCIC tests. The vent line was arranged as in Test #28. The primary difference between this test and Test #28 was that this test used 0.4 GPM of water injection into the steam line.

In addition, early stages of work on another experimental facility at the lab (where the steam generator is a common component) may have slightly increased heat losses from the steam generator's steam piping. The start point was also lower than that of the standard tests, being 35 °C (40 °C in a standard test, 30 °C in Test #28).

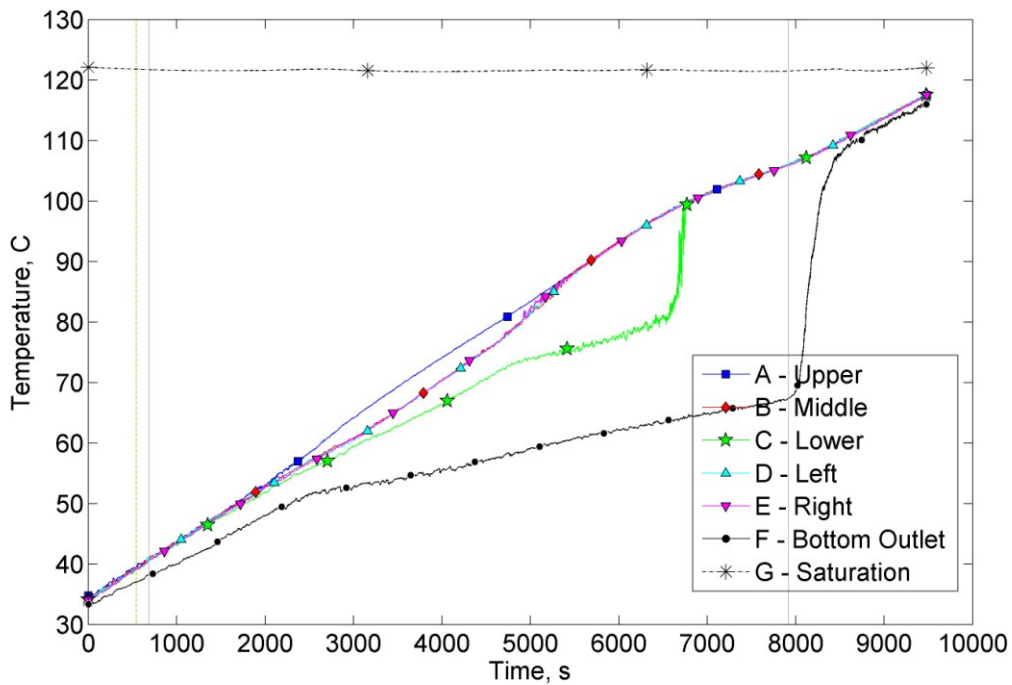


Figure 69: Test #29 Thermal Progression

This test was conducted at mid-power (107 kW), which produced a steam flow of 44.4 ± 1.3 g/s. Feedwater to the steam generator ran at 43.8 ± 1.4 g/s, and water injection to the steam line flowed at 25.0 ± 1.0 g/s. This produced a steam quality of 0.58 ± 0.02 , which rose to 0.61 ± 0.03 downstream of the orifice.

Thermal stratification (see Figure 69) was largely comparable to that of Test #28, but measured to be very slightly larger. The top-mid limit was essentially identical at 4.5 °C. The mid-low and low-outlet differences, however, were greater at 22.9 °C and 40.5 °C, compared to Test #28's 21.0 °C and 39.6 °C, respectively.

4.4.30 Test #30

Test #30 was another test that started at below-standard temperatures; it ran for almost 300 minutes with a nominal beginning temperature of 30 °C. It was the test with the most severe two-phase conditions sent to the RCIC turbine analog and sparger. It was a low-power (57 kW) RCIC test with standard pressurization conditions and 0.8 GPM of water injection into the steam line.

Steam flowed at 23.3 ± 0.8 g/s, and feedwater was sent to the steam generator at 23.0 ± 0.8 g/s. The water injection to the steam line, at 49.8 ± 0.9 g/s, produced the lowest steam quality in these tests at 0.24 ± 0.03 , which rose to 0.26 ± 0.03 downstream of the orifice.

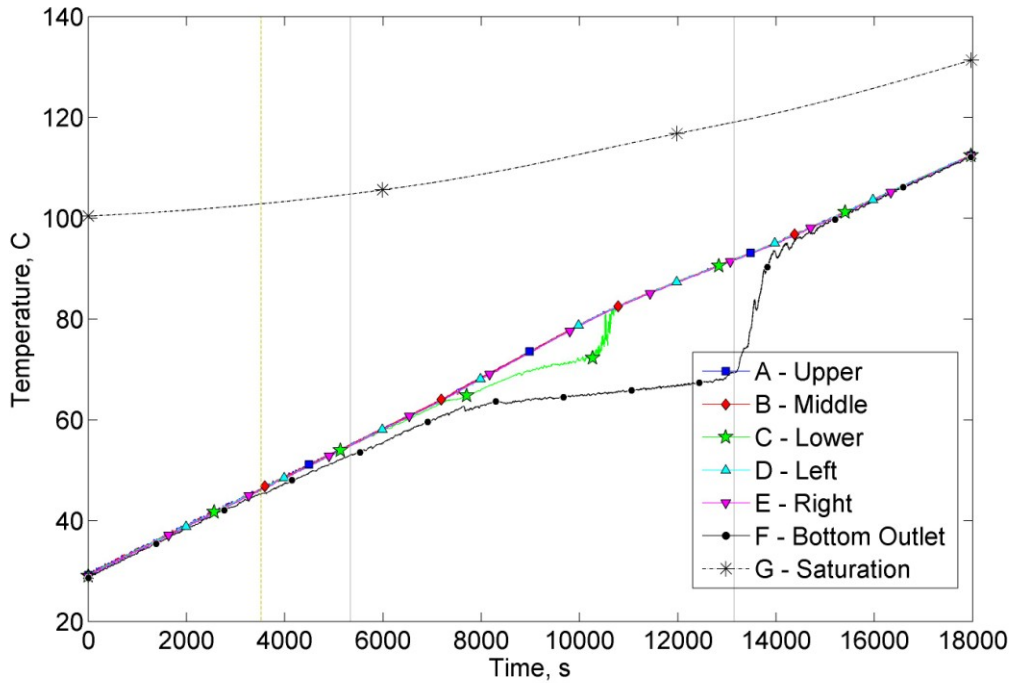


Figure 70: Test #30 Thermal Progression

Stratification (seen in Figure 70) was similar to both Test #2 and Test #21. The peak top-mid separation was only 1.3 °C (vs. 1.4 °C and 1.5 °C in Test #2 and Test #21, respectively). There was a limit of 10.1 °C difference for the mid-low region, between the 9.3 °C of Test #2 and the 10.6 °C of Test #21. The 24.2 °C maximum separation for the low-outlet region was greater than that of either of Test #2 or Test #21 (22.6 °C and 23.9 °C, respectively). One note of interest is that the thermal profile showed a flattening off not seen in higher-power water injection tests, and more closely resembled the non-injected cases.

4.4.31 Test #31

Test #31 was the lowest-power test conducted (32 kW). It ran for more than 523 minutes, the longest test on record by far, and started nominally at 35 °C (lower than the 40 °C in standard tests). Unfortunately, late in the test, the vortex flowmeter displayed symptoms of excessive acoustic noise in the steam flow. With low vapor velocities, the signal generated by the sensor in the vortex flowmeter can be relatively weak and may be susceptible to noise (especially valve hiss or water droplets flashing in the valve). The silencer installed after the shakedown tests proved adequate at higher velocities, but the threshold appears to have been reached late in this test.

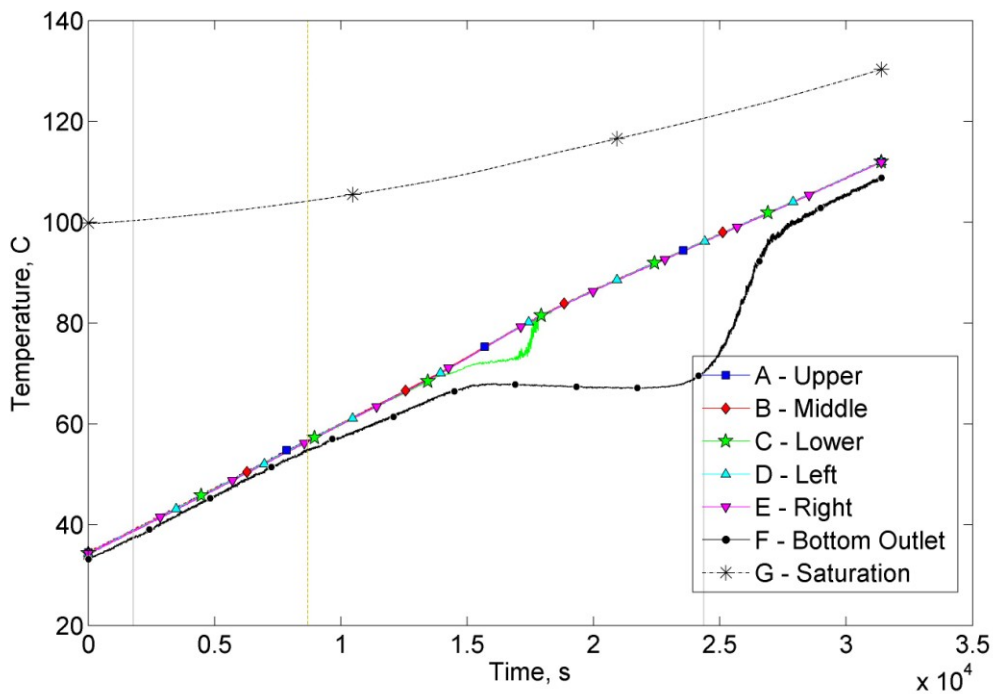


Figure 71: Test #31 Thermal Progression

Sometime after 400 minutes, the recorded flow rate showed spikes and trending increases in the flowrate that were unrealistic, and for this period can not be considered fully accurate. It should be noted that as the test progressed, pressure in the steam line rose in line with the Suppression Chamber's pressure, and was low compared to the steam generator. With a constant heater power and only lightly changing feedwater and pressure conditions in the steam generator, the actual flow through the main choke point (the main steam control valve, which should have experienced critical flow for most if not all of the test) should have remained fairly consistent during the excursions and inaccurate readings. However, with the greater pressures, the density of the steam would have been increasing; therefore, for the same massflow, the velocity through the vortex flowmeter would be lower. With the low velocities at the end of the test, it is estimated that the flowmeter would have been operating in the vicinity of 5% of its full scale range, relatively close to its lower limits.

This test was a standard alignment RCIC test at very low power. In the period up to the 400 minute mark, the steam and feedwater flowrates were 12.7 ± 0.4 g/s and 12.5 ± 0.6 g/s, respectively. For the entire test duration, including the period of inaccuracy for the vortex flowmeter, feedwater flowed at 12.9 ± 1.1 g/s. The measured value of the steam flowrate for the whole test was 13.0 ± 1.7 g/s; however, a more realistic value is estimated to be 12.8 ± 0.4 g/s.

Thermal stratification (profiled in Figure 71) in the topmost levels of the pool was more limited than in most of the other tests, and peaked at 1.0 °C. The mid-low separation, however, was not as remarkably low at 8.4 °C. Both are below the 1.4 °C

and 9.3 °C, respectively, recorded in Test #2, the closest comparison. The low-outlet difference reached a maximum of 27.9 °C, a value greater than the 22.6 °C of Test #2.

4.4.32 Test #32

Test #32 was a repeatability test for Test #4. It was a standard alignment RCIC test at mid-power (107 kW). It was intended to be the first of two repeatability tests, but a magnetic flowmeter failed during the first attempt to run this test. Diagnosis and replacement with a similar model took enough time to limit the repeatability series to this test. As a result, this was the final test performed.

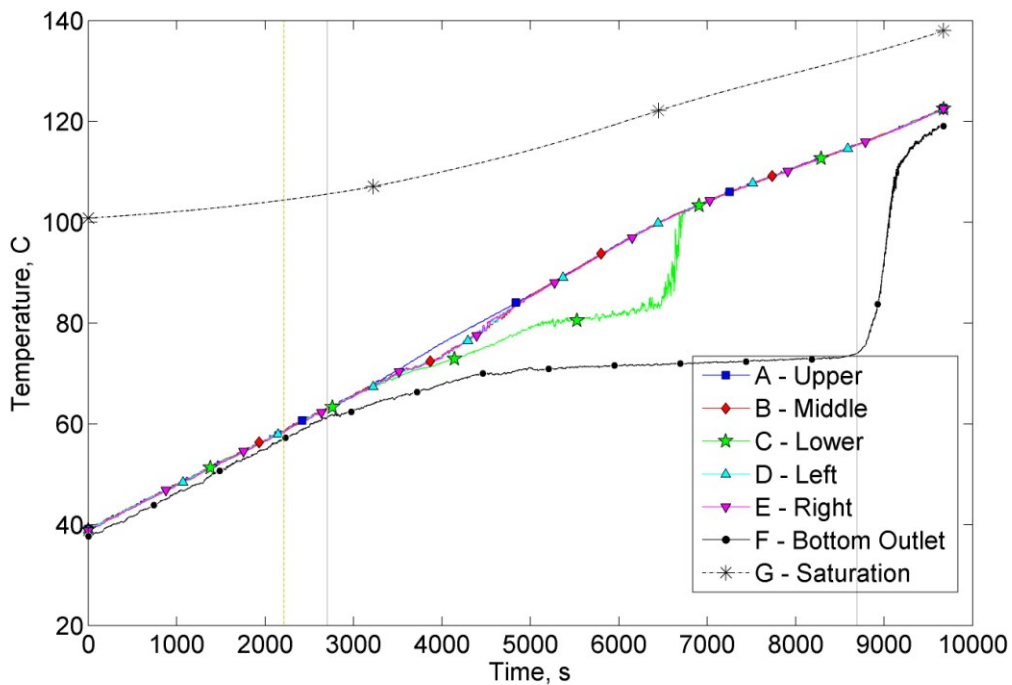


Figure 72: Test #32 Thermal Progression

Steam flowed at 44.7 ± 1.0 g/s. Feedwater to the steam generator had a flowrate of 44.3 ± 1.4 g/s.

The limits of thermal stratification and temperature profiles (shown in Figure 72) were very close to those of Test #4, and were all within one half of one degree of the Test #4 values. The top-mid peak difference was 2.8 °C (3.1 °C in Test #4). The mid-low and low-outlet separations were 20.7 °C and 43.5 °C, respectively; the comparable values for Test #4 were 20.9 °C and 43.3 °C, respectively.

4.5 OBSERVATIONS

Of the 32 tests performed, a minority (5) used the SRV-analog sparger. Even in the most severe case (Test #16), the thermal stratification was almost non-existent; these tests demonstrate the ability of the pool to be well-mixed by steam-condensing action. In the case where the pool would be much larger in comparison to the sparger and the mixing rate slower than the heatup rate, the development of a significant hot spot might still be possible with such a sparger design; however, these tests have provided little evidence to support it. The pool was essentially uniform.

The 27 RCIC-sparger tests, on the other hand, produced results demonstrating significant thermal stratification. While some tests produced limited and short-lived stratification, **EVERY RCIC-ALIGNMENT TEST PRODUCED THERMAL STRATIFICATION** in the Suppression Pool. Some tests produced very large gradients; Test #11, for example, had a peak thermal separation of 65.1 °C. The stratification, it should be noted, was entirely vertical; a characteristic horizontal profile (end-to-end and side-to-side within the Suppression Chamber) did not develop. That does not mean there

were no differences whatsoever; in fact, it would appear that the vessel-front thermocouple group (SP19-SP23) tended to reveal destratification somewhat earlier than the middle and rear sets. This could be the result of imprecision in placement of the thermocouples; the sensitive end has several (sometimes more than 6) inches of lead to its nearest anchor point, allowing for a fair degree of movement if any force is applied. As the vessel was not opened after testing, the current positions of the thermocouples are unclear. In addition, the vessel-front group is relatively close to the vessel outlet; it is not beyond the realm of possibility that the pump suction produces a local distortion in the thermal profile.

A second deviation from lateral uniformity comes from Thermocouple SP8, the thermocouple in the immediate vicinity of the RCIC Sparger outlet. It is unsurprising that a very local and chaotic hot spot develops there; it may in the condensing region once steam bubbles can grow beyond the sparger outlet, and likely represents a thermal plume. It is unclear if the rapid swings in temperature it sees result from very chaotic hot-cold water turbulence, or if it comes into contact with two-phase steam/water mixtures. The installation of additional instrumentation would clarify this and enable comparison to point-source plumes modeled in [52] or later adaptations of plume theory [53]. Before that point, the thermocouple's readings are in line with the other thermocouples at that level. The appearance of the hot spot at that location is a key feature of these tests, and is taken to represent a significant weakening of the mixing currents in the pool along with the weakening of the condensation.

While there are significant variations between the RCIC tests, a characteristic thermal profile can be defined. Test #4 produced a relatively prototypic profile, which has a number of features common to the tests. It is a convenient test to use in comparisons, and has therefore been labeled the 'baseline' test. Early on, the pool is almost uniform; operators in this period observed loud metallic 'pops' and 'bangs' not unlike the popping sounds of popcorn coming from the Suppression Chamber. Coincident with them were spikes in the differential pressure reading across the sparger as well as in Thermocouple SP1 (inserted into the sparger line near the outlet). These sounds and spikes revealed the presence of violent steam condensation events; the thermocouple readings even dipped (for very short periods) into well-subcooled values, indicating the presences of subcooled water being drawn into the steam line. These sounds and spikes are clear evidence for chugging oscillations, whose presence is expected with sufficient subcooling in the pool. The largest spikes in standard alignment tests occurred roughly once every 1 to 7 seconds; smaller pulsations seemed to be at greater frequencies. However, it should be noted that due to the data logging frequency of 10 points/second, events with frequencies greater than about 1 Hz would not be preserved well, and those greater than 5 Hz cannot be resolved at all. Although similar sounds come from SRV-alignment testing, that alignment lacks the differential pressure and sparger temperature instruments that can clearly resolve the events in the data.

As the pool warms up, the violence of the condensation events weakens. The spikes in the sparger temperature and differential pressure trend toward decreasing severity, suggesting that the chugging oscillations are of decreasing intensity.

Eventually, the spikes disappear altogether and the chugging transitions through less violent condensation regimes. Meanwhile, as the oscillations weaken, the thermal plume around the sparger begins to establish itself. Subsequently, the pool begins to thermally stratify; it would appear that the chugging oscillations are the primary driver of pool circulation in the early parts of the tests. There are chaotic, transient flows in and near the sparger in the chugging regime, and they are effective at distributing energy and maintaining bulk pool uniformity. With the diminished chugging oscillations, the pool stratifies with some residual mixing; the temperatures all continue to rise, but at different rates at different vertical positions. The lower levels of the pool have thermal profiles that begin to flatten out, and may stop rising entirely.

The pool upper and middle readings continue to rise, and typically display some slight divergence in their trends. Such divergence is limited; the greatest separation (seen in Test #11) was 5.6 °C, while the other tests tended to be well below that. At that peak, the active pool mixing from concurrent condensation is thought to be at its lowest point, although total mixing from residual earlier action may continue to decay away. Afterward, the upper and middle temperature readings reconverge to common values while continuing to rise. The sounds coming from the sparger tend to be, at this point, notably calmer than at the beginning of the test; the chugging oscillations have given way to less violent condensation, and bubbling from the sparger outlet begins. At first, this seems to agitate only the portion of the pool above the sparger outlet; the buoyancy drives flows in the upper parts of the pool, but only limited momentum seems to penetrate into the lower regions.

As the upper parts of the pool continue to absorb energy and heat up, the penetration depth from the bubbling-based agitation increases. As the test continues, the lower parts of the pool intermix with the above areas, and eventually the whole pool from top to bottom joins the agitated part; the entirety of the pool once again becomes well-mixed and essentially uniform. This destratification front can show steep thermal profiles; as the front creeps past a thermocouple, even several dozen degrees of thermal separation can be seen to vanish in just a few minutes.

After full destratification, effectively no re-stratification of the pool has been observed. The degree of stratification, as well as distortions to the prototypical profile, depend on the major independent variables in these tests: the steam flowrate/steam generator heater power, the pressurization condition, and the steam quality.

In addition to the characteristic thermal profile these tests generated, operators noticed one important piece of information (more accurately, the lack thereof): *during none of the tests was the pump observed to cavitate*. While this cannot be guaranteed to be the case for a full-scale system with a much different impellor design, it is important to note here. To ensure that operators were not missing it, during a cooldown period the pump was deliberately driven into a cavitating state; such a state was obvious to the operators.

With the number of different independent variables explored, it is useful to divide them into groups. For example, “Power Series” groups standard RCIC-alignment tests for comparison. Likewise, a “Pressurization Series” exists for constant power levels, and a “Two-Phase Series” similarly considers the effects of injecting water into

the steam line. Combinations of parameters can then more conveniently be compared to determine the greatest effects, and a special set of venting actions can be explored.

4.5.1 Steam Generator Power / Steam Flowrate

Part of the “Power Series” has been previously presented [50]. Tests #1, #2, #3, #4, #31, and #32 can be considered its primary constituents with some repetition for repeatability. The greatest stratification was seen at moderate power levels, while high and low power tests had much of their thermal profiles in common. While the upper-middle level separation for the high and low powers were closer to each other than to the moderate power cases (1.4 – 2.1 vs. 2.8 – 3.1 °C), even when the extra-low power test is added to the mix the spread, in actual numbers, is not great (between 1.0 and 3.1 °C). The middle-lower differences, greater in numerical value, again showed a clear difference between the moderate-power tests and the others (20.7 – 20.9 °C at mid-power vs. 5.5 – 10.8 °C). The peak separation was (in sheer numbers) very clear in the lower-outlet profile, ranging from 20.7 – 43.5 °C.

The moderate-power tests, which appear to be repeatable, seem to have found a sort of “sweet spot” for enhanced thermal stratification. Interestingly, the extra-low power test showed a greater separation in the lower-outlet profile than the low power tests (27.9 vs 20.7 – 22.6 °C). The mid and high power tests were nearly identical, ranging from 43.1 to 43.5 °C. This suggests a complicated set of phenomena contribute to the overall stratification relating to the steam flowrate; this would include the size/shape of any jet forming at the outlet (likely to be larger/deeper and more stable at greater flow rates), the ability to resist water ingress during chugging (greater steam

flowrates would better resist ingress), and the scale of buoyant flows (greater steam flows likely produce larger buoyant flows to distribute the thermal energy).

4.5.2 Pressurization Conditions

Some of the standard “Pressurization Series” has been presented previously [51]. The pressurization condition of the Suppression Chamber turned out to be the most important of the variables considered, and had a clear effect: greater pre-pressurization leads to greater bulk thermal stratification in the pool. If the pool is fully vented (atmospheric), the resulting stratification will be reduced below that of the standard alignment; it is enough to severely distort the prototypic thermal profile; at high power (Test #14), the distortion is so severe that the prototypic profile is unrecognizable. With increased pre-pressurization, the stratification is not only more pronounced, but even the characteristic thermal profile becomes clearer. The stratification is also longer-lived.

The primary tests in this series are mid-power Tests #4, #6, #9, #12, #28, and #32. Test #6 and Test #28 were at constant pressure (1 and 2 atm, respectively), while the rest isolated the Suppression Chamber from the atmosphere and accumulated pressure beginning with their starting points (1, 2, 4/3, and 1 atm, respectively). A smaller low-power pressurization series can be assembled from Tests #1 (standard), #2 (standard), #20 (atmospheric), and #22 (building up from 5 psig); a similar set of high power tests consists of Tests #3 (standard), #10 (building up from 5 psig), and #14 (atmospheric).

The low-power tests showed significantly more stratified lower regions with increasing pressure; the standard alignment temperature differences were on the order of 40% greater than those of the atmospheric test, and the 5 psig pre-pressurization was

more than double that of the atmospheric test. At mid-power, similar effects are seen: the constant 2-atm test has maximum temperature differences on the order of twice those of the atmospheric test (more than triple for the mid-low level separation). Test #12 (4/3 atm start point) had stratification that was almost 1/3 greater than the standard alignment, and Test #9 (starting from 2 atm) was roughly 1/2 greater than the standard alignment (and was still increasing for the lowest levels when equipment limitations forced cessation of the test).

Full power testing showed equally pronounced pressure effects. The atmospheric test was almost uniform from the top to lower thermocouple, and only saw 9.1 °C separation from the lower region to the outlet. While the pool upper levels were just as mixed as in the standard alignment, the lower and outlet stratification in the standard alignment were quadruple the values of the atmospheric test. Comparing the standard-alignment high power test to its pre-pressurized variant revealed an enormous fractional increase in the mid-low stratification: the peak separation increased by more than a factor of five. The low-outlet region did not see nearly as much of an effect (increasing less than 30%), but that in part could be due to the test ending (due to equipment limitations) long before its destratification point was reached.

Intuitively, the pressure effect can be connected to the differences in steam density. As the water in the pool is essentially incompressible, and the steam is introduced to the pool at similar pressures, the largest difference would relate to the fact that, without a phase change, the steam density at twice the absolute pressure would be approximately double that of the lower pressure. Similar-volume bubbles at greater

pressure would have more mass, and would then tend to take longer to condense as the latent heat from the bubble is distributed to greater liquid volumes, decreasing the violence of the condensation. For a given mass flowrate, the volumetric flowrate at higher pressures would be reduced; in latter stages of tests, the reduced bubble flow at the sparger outlet would result in less overall agitation

4.5.3 Two-Phase Steam/Water Testing

Injection of a two-phase steam/water mixture through the RCIC Sparger rather than single-phase steam appears to have a complicated set of effects. The mid-power “Two-Phase Series” consists of Tests #4 (standard), #8 (0.4 GPM injection), #27 (0.8 GPM injection), and #32 (standard). The high-power series consists of Tests #3 (standard) and #13 (0.6 GPM); at low power, the series contains Tests #1 (standard), #2 (standard), #21 (0.2 GPM), and #30 (0.8 GPM). In many, but not all, cases two-phase injection reduced the amount of stratification that developed. It tended to distort the characteristic thermal profile, and added some slight mixing to the lower pool levels throughout the test period. Instead of heat being deposited solely in the upper parts of the pool, the two-phase tests indicate some energy being deposited at lower levels in the pool; the “flattening out” part of the thermal profiles does not get as flat as in single-phase testing. Some of this is likely the result of condensed water in the steam penetrating further down into the lower regions of the pool than the injected vapor phase, well below the condensation interface.

High-power testing saw reductions on the order of 2/3 for the peak temperature differences in both the mid-low and low-outlet regions when water was injected,

reducing the sparger outlet quality to ~63%. A similar quality at mid-power resulted in smaller but still significant reductions in stratification severity; the peak mid-low stratification dropped by more than 40% and the low-outlet numbers decreased by 15%. Decreasing the steam quality further, to ~44%, resulted in decreases (compared to the standard alignment) revealing a much more mixed pool; the peak mid-low region temperature difference dropped by more than 80%, while the low-outlet region saw nearly 2/3 of the difference vanish.

At low power, an interesting trend reversal appears. Two-phase testing revealed an INCREASE in thermal stratification at the 63% steam quality level (only a small one; the low-outlet region saw an increase in the peak temperature difference of less than 6%). Further increase in water injection (decreasing the test-average steam quality to about 32%) further increased the ultimate degree of stratification (still by small amounts, on the order of 10% from the standard alignment). It would appear that the water injection interferes with the chugging oscillations, which seem to be suppressed at correspondingly lower pool temperatures with decreased steam quality. At the same time, in the low-power tests, the slower flow rates would give the condensed water in the steam line less penetrative power and a resultantly lower ability to agitate the pool.

It should be noted that the dry steam supply is consistent with the standard alignment case; in these two-phase tests, additional (liquid) flow is sent through the sparger, increasing the mass flux for essentially the same heat addition rate to the pool. The necessary changes in mass flux or heat addition makes separating the effects (mass flux and steam quality) more challenging.

4.5.4 Combined Parameters

When combinations of parameters were applied (i.e., pressurization with two-phase injection), the pressurization condition was the dominant factor in the overall stratification profile. The power levels and steam quality did play their roles, but they were of less significance than the pressure. Combined parameter testing was performed in Tests #7, #11, #18, #19, #23, and #29.

4.5.5 Active Venting Operations

Two tests were performed in which operators actively changed the venting condition mid-test: Test #24, in which a pre-pressurized Suppression Chamber was decompressed mid-test, and Test #26, which was maintained at atmospheric until a mid-test isolation. Test #26 performed as the atmospheric single-phase mid-power test (Test #6) until it was isolated as the pool bulk temperature crossed 82 °C; after that, it behaved as something of a cross between the atmospheric and standard alignment tests

The pre-pressurized depressurization test (Test #24) provides additional insight into the mixing behavior of the pool. Upon depressurization, the mid-low elevation stratification disappeared almost immediately. This effectively reveals that the mixing state of the pool is largely determined by current conditions rather than the heatup history in a test. While the temperatures of the unmixed portions are a function of the pool history, the active mixing state is not.

4.5.6 Comparison with Results from Other Facilities

The characteristic thermal profile found in these tests shows similar trends to those from both the University of Tokyo as well as the SIET tests. Remarkably, this

applies not only to the open-ended pipe sparger design but the multiple-side-hole design as well as depicted in Figure 73 [40] (notably, the pool was open to the atmosphere in the SIET tests).

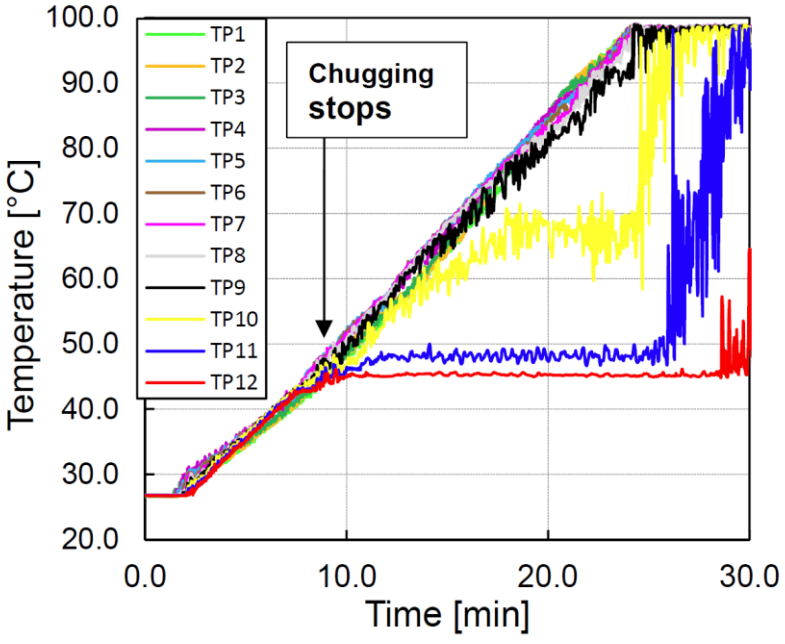


Figure 73: SIET Multi-Hole Sparger Pool Thermal Progression [40]

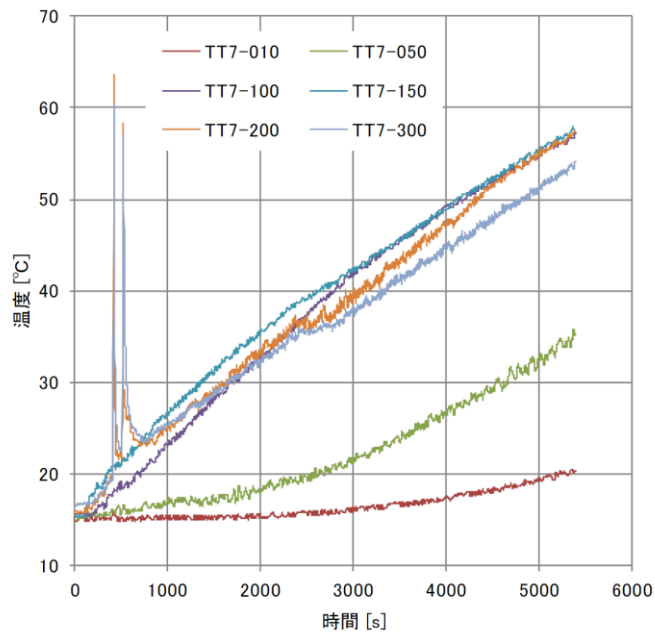


Figure 74: Atmospheric Thermal Progression, Reprinted with Permission from [54]

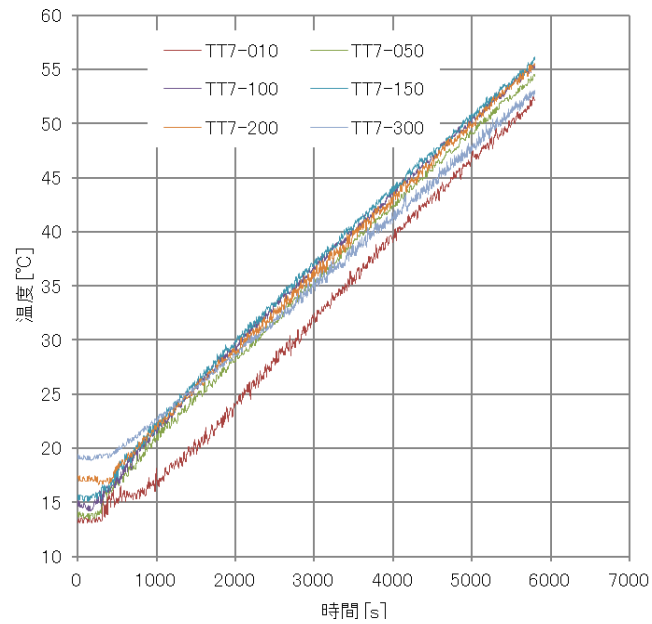


Figure 75: Vacuum Thermal Progression, Reprinted with Permission from [54]

Of particular relevance here, the effects of the pressurization conditions can be seen in the University of Tokyo tests. An interesting characteristic of them was that instead of above atmospheric pressures, testing was performed under atmospheric as well as vacuum conditions. In a manner not unlike the profiles seen for the NHTS tests, lower pressure in the test facility resulted in decreased thermal stratification. Vertical thermal profiles are shown for the atmospheric case in Figure 74 and for a vacuum (starting at -84 kPa gauge) case in Figure 75 [54].

A degree of similarity to the thermal progression in these NHTS tests was seen in POOLEX testing. As seen in Figure 76 [35], during the stratified period, the lower levels of the pool stayed at a relatively uniform, constant temperature. There was some separation in the upper portions of the pool, but the temperatures appear to move in concert with each other. It is important to note that steam injection was not constant, and the flowrate was dramatically increased at 4200 s to effect additional pool mixing; it was reduced over the succeeding hour until only small adjustments were needed to maintain the condensation position [35]. Even with the very different facility design and operation in the POOLEX tests, there remains a striking resemblance to the stratification data seen in the NHTS tests.

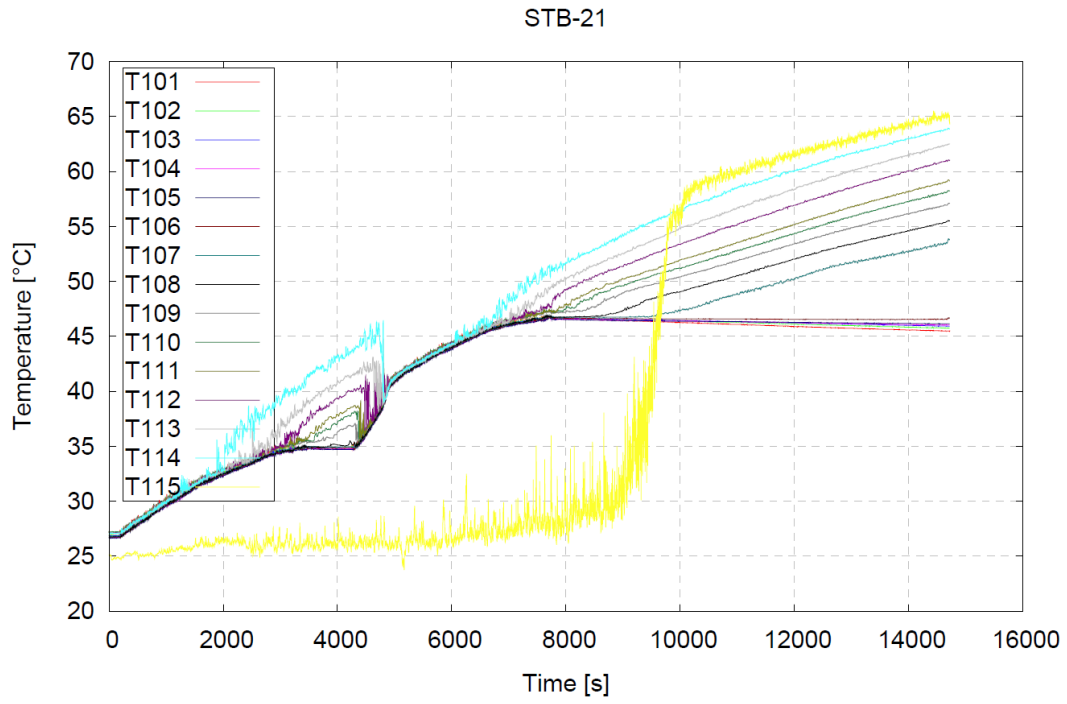


Figure 76: POOLEX STB-21 Test Thermal Progression [35]

5. ANALYSIS

The meaning and consequences of the data collected in this experimental program are presented here. The analysis attempts to produce a correlation that describes the aggregate mixing state of the Suppression Pool.

5.1 GOALS OF THE ANALYSIS

The characteristic thermal profiles seen developing through the test suite in this experimental program are the product of multiple phenomena occurring throughout each test. As direct contact condensation is a fundamental part of the experiment, relevant condensing regimes can be expected to play roles in the progression of each test. The notable, qualitatively observable, decrease in chugging intensity in the course of the RCIC tests in particular seems to be an important transition, as it appears to correspond well with the onset of bulk thermal stratification in the pool. While chugging appears to dominate the circulation patterns early in the tests, it is not the sole driver of pool circulation. Buoyancy-driven flows near the sparger outlet, especially late in the tests where steam bubbles may be able to reverse their initial direction and flow upward before condensing, become increasingly influential.

The transitions observed in the tests may be abrupt (as noted by operator observation in some tests, like Test #3, where the loud pops associated with strong chugging rapidly ceased) and easily noted by observant operators, or they may be smooth as one phenomenon gradually gives way to another (as in Test #21). The destratification profiles seen in the tests, in particular, would be near-impossible to

identify without the direct temperature measurements. The multiplicity of phenomena involved in this experiment, especially when two-phase injection is considered, can make the use of existing correlations problematic as the phenomena may interfere with each other or interact in unexpected ways. Furthermore, the bulk effects measured may not be due largely to one phenomenon at a time.

For the purposes of this endeavor, the phenomena that may appear in the tests shall be considered in aggregate rather than separately; the goal is a single expression at any given time to describe the system state rather than the effective summation of several independent relationships. As chugging features so prominently in these tests, the result is expected to appear in the form of a chugging-like formula. Instead of strictly establishing the chugging conditions, however, it will reveal an aggregate bulk mixing state in the pool; i.e., whether the heat from the injected steam is distributed into just a small portion of the pool or is dispersed into the entire pool at large.

The bulk thermal mixing state of the Suppression Pool is an important part of whether or not the Suppression Pool RCIC System will be able to perform their safety functions in extended operations. When the RCIC Pump draws suction at sufficiently low elevations in the pool, thermal stratification will tend to provide it protection; the cooler inlet water would be less of a cavitation risk and would provide better cooling for the system's lubrication oil. However, limiting the heat injection to just the upper portion of the pool would tend to increase containment pressurization as that is the driving interface between the pool and containment airspace. The model developed herein should provide a framework to address these concerns.

5.2 DEFINITION OF THERMAL STRATIFICATION KEY POINTS

The broadly similar thermal profiles found in the RCIC-alignment tests, and the distinctive features of those profiles, allow for the identification of specific “key points” in the data. Aside from certain operational points (e.g., the beginning and ending points of a test), these key points identify features of the tests that should share common phenomenologies. These include the beginning and ending of identified bulk pool thermal stratification, the first formation of an identifiable thermal plume near the RCIC sparger outlet, the peak thermal separation between vertical levels, and the subsequent disappearance/reconvergence of said thermal separation. Presumably, the similar features in the thermal profiles of the tests that identify specific key points relate to phenomenological similarity across the suite of RCIC tests at those points. The key points identified are as follows:

1. Beginning of test
2. First appearance of identifiable thermal plume at the RCIC sparger outlet
3. Onset of detectable bulk thermal stratification
4. Peak thermal separation between the upper and middle vertical levels of the pool
5. Disappearance of the thermal separation between the upper and middle pool levels
6. Peak thermal separation between the middle and lower vertical levels of the pool

7. Disappearance of the thermal separation between the middle and lower pool levels
8. Peak thermal separation between the lower vertical level of the pool and the outlet at the bottom
9. Beginning of reconvergence for the lower vertical pool level and the outlet at the bottom
10. Disappearance of the thermal separation between the lower vertical level of the pool and the outlet at the bottom
11. End of test
12. Minimum recorded value for the proposed correlation (as defined for KP2-4)
13. Maximum recorded value for the proposed correlation (as defined for KP2-4)
14. Peak thermal difference between the condensing/lower plume region and the bulk pool middle regions (unclear phenomena)

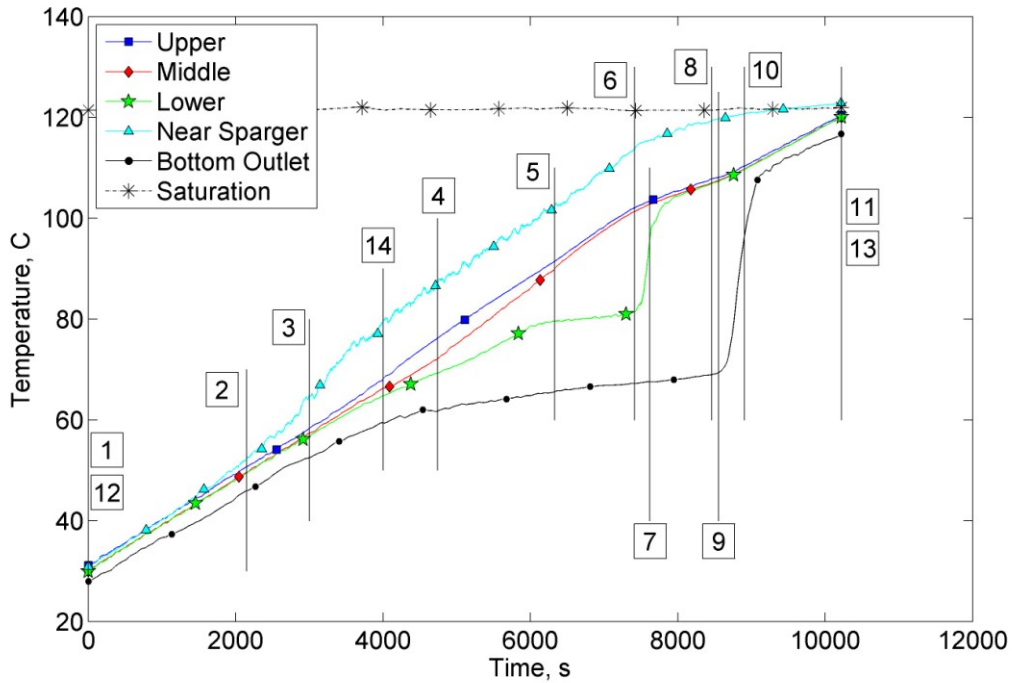


Figure 77: Key Point Progression in a Test

The descriptions of several of the above key points would benefit from further discussion, and are placed in their test progression in Figure 77. The thermal plume, central to Key Points 2 and 14, is only defined for RCIC tests (SRV runs are insufficiently instrumented). It is identified by comparison of the values for Thermocouples SP8 and SP9; SP8 is adjacent to the outlet of the RCIC sparger at the middle-level of the pool (approximately one inch away along the vessel axis) and SP9 is at the same vertical level, 12 inches further away axially from the sparger outlet. Due to the wild fluctuations in temperatures resulting from the nearby chaotic condensation, a smoothing algorithm is applied to these specific readings to determine the average local conditions. After the pool warms up sufficiently (this varies on test conditions), the

average SP8 readings rise significantly above the SP9 readings (which maintain bulk middle-level readings). Once the average difference between SP8 and SP9 rises above 2 °C and remains so for the following 60 seconds, a thermal plume is considered to have formed; this indicates the test has progressed through Key Point #2. Key Point #14 is where the average difference is at its maximum. However, due to the poor spatial resolution of the thermal profile and indeterminate flow patterns, the phenomena relating to this are largely unclear and unresolved.

The bulk thermal stratification, defined primarily through Key Points 3 and 9, uses more smoothing than was used for the plume detection. Bulk pool temperatures are taken as averages of thermocouples SP11, SP12, and SP13, and compared to the temperatures read at the bottom outlet of the pool. To trigger the detection of the onset of bulk thermal stratification (Key Point #3), three main conditions must be met. First, the difference between smoothed bulk and outlet temperatures must be greater than 2 °C at the onset and for a full minute after. Second, the rate of temperature increase for the smoothed bulk and outlet temperatures must be different; at the onset and for a full minute afterward, the outlet temperature can be increasing at a rate no more than 75% of that of the bulk. Third, for the subsequent three minutes (to four minutes after the onset), the smoothed outlet temperature can be increasing at no more than 95% of the rate of increase for the bulk temperatures.

Detection of the onset of full destratification (Key Point #9) has fewer requirements: the rate of increase of the smoothed temperature at the pool outlet must be at least twice that of the smoothed bulk temperatures at the detection point and for the

subsequent 60 seconds. Typically, the detection of Key Point #3 is well after that of Key Point #2. However, slowly-evolving temperature fluctuations can overcome the smoothing algorithms and lead to premature or inaccurate detection of the actual divergent trends; this appears to be the case, for example, in Test #21 as well as SRV Tests #16 and #25.

For Key Points 4, 6, and 8, the peak temperature differences are instantaneous (unsmoothed) values. The temperature differences are those within a vertical set (SP3-SP4-SP5-Outlet, SP11-SP12-SP13-Outlet, and SP19-SP20-SP21-Outlet), and the vertical set displaying the greatest difference is selected. However, due to the increasingly erratic behavior of Thermocouple SP4, Thermocouple SP4 was declared defective; this effectively limits that entire vertical set to consideration of lower to outlet region temperature differences (SP5-Outlet). The disappearances of the differences, as defined in Key Points 5, 7, and 10, use the same vertical thermocouple set as was found to have the maximum respective difference. This reconvergence is defined to be between the time of the maximum difference and the end of the test, and to be the point where the difference (with a smoothing algorithm applied) first drops below 1/3 of its peak value and stays below it for the subsequent 60 seconds. If the peak difference is less than 3 °C, the difference only needs to drop and stay below 1 °C. It should be noted that some tests did not proceed all the way through full destratification. For those tests, the relevant Key Points (generally Key Points 8, 9, and 10) are placed at the very end of the test.

5.3 CORRELATION DEVELOPMENT

Correlation development was based on the Key Points extracted from the RCIC-alignment tests. While five SRV runs were performed, their consistent full mixing in the Suppression Pool provides little impetus for more detailed mathematical modeling. Of the 27 RCIC-alignment tests, only those with clear and well defined Key Points in the early stages (Key Point #3 in particular, which should follow Key Point #2) were used in the development of the relationship; several tests had their bulk thermal stratification onset detection by the detection algorithm apparently go awry. To simplify things, only tests with steam qualities greater than 50% and steam mass flowrates greater than 20 g/s were considered in the development. This excludes Tests #27, #30, and #31. The primary Key Points used for development are Key Points 2, 3, 4, 5, 7, and 10; these cover the plume formation and initial stratification through the full destratification of the pool. Some skew is expected to result in the Key Point #10 results, as full destratification had not been achieved in some cases (Tests #1, #9, #10, #11, and #19); in such cases, Key Point #10 is placed at the very end of the test in the assumption that full destratification would have been forthcoming had the test proceeded.

For the correlation to be useful, it was essential to have a set of features. The values at the differing Key Points needed to be clear, consistent, and well-separated from those of other Key Points; there needed to be a 1:1 correspondence between the correlation value and the associated Key Point. As the tests progressed in time, the correlation needed to change monotonically (increasing was selected in this analysis).

The correlation development proceeds from a chugging-type relationship. As certain Key Points are thought to reflect transitions in the DCC regime, a correlation for the chugging regime boundary such as Aya and Nariai's (Eq. (1) [28]) or Liang and Griffith's (Eq. (2) [29]) was considered a good starting point. Due to the difficulties in directly applying Eq. (1) to the current system, Liang and Griffith's correlation (Eqs. (2)/(3)) was selected as the starting point. While bubbling does appear to play a significant role late in the tests, no consistent feature is present in the thermal profiles and therefore no Key Point is defined at temperatures specifically very close to saturation; condensation is expected to be a major part of every phenomenological Key Point. As a result, while one would expect that, near saturation, the primary relationship would be of a bubbling-type, the transformation from a chugging-type to bubbling-type relationship is far from complete for the current data set. Without the necessary data near or at saturation, the development of a bubbling-type relationship for the end-state data cannot be performed and the transition from the chugging-type to the bubbling-type relationship from the data gathered in this endeavor is at best incomplete and left for future researchers to explore. With adjustments for the latter Key Points, the form of the chugging-type relationship is believed to be valid for the current data.

In every test performed where the Suppression Chamber was isolated from atmospheric conditions, the pressure in the vapor space built up significantly as the pool temperature increased. This comes as no surprise; the air inventory was constant and heating up. In addition, the partial pressure of water vapor increased along with the pool surface and airspace temperatures. It is simple enough to estimate such conditions, and

is an important phenomenon in thermal hydraulics. As exemplified by Equation 7-23 in the classic text by Todreas and Kazimi, the containment pressure has contributions from water vapor and from the volume's heated air as shown in Eq. (8) [55].

$$p_2 = p_{w_2}(T_2) + p_{a_1} \frac{T_2}{T_1} \quad (8)$$

Not only was the pressure increase predictable in the tests, it was significant. The only tests that achieved pool temperatures close to saturation were those with some sort of vent mechanism. Indeed, Eq. (8) [55] reveals that such systems under reasonable isolation conditions can never fully saturate; in order for the water vapor pressure to equal the airspace pressure, all the noncondensibles would need to be vented away. While a local hot spot could produce localized boiling, such would be suppressed over the pool as a whole by the presence of noncondensibles.

With the qualitative observations of the operators noting that the chugging noises would be relatively quiet at the point that thermal stratification was accelerating, with a fair degree of support by the recorded data, it is considered here that Key Point #4 (peak temperature difference between the upper and middle vertical regions of the pool) represents the overall minimum of active mixing in the pool, and effectively represents a termination of the chugging regime. This is not to suggest that a chugging-type correlation would immediately lose meaningfulness after progression through the general end of major chugging events, or even that the chugging regime has such a sharp boundary. However, the relationship would be expected to begin transformation at that point into another form, if it is to continue to relate to the phenomena present in the

system after the cessation of major chugging. Key Points 2 and 3, then, represent the weakening of the chugging oscillations that the resultant decrease in overall pool mixing that allow their respective phenomena to appear. Key Points 5, 7, and 10 would then indicate increasing pool circulation from buoyancy-driven flows and an increasing role of bubbles surviving past the sparger outlet as the condensation rate slows.

Direct application of the chugging correlation from Liang and Griffith [29], as Eq. (3), to Key Point #4 reveals strong residual dependencies/unaccounted-for trends and that, on its own, it is insufficient to adequately describe the Key Point. The other Key Points have similar dependencies when examined with the correlation. This should come as little surprise, given the differing situations as well as the inclusion of two-phase injection and pressurization in these tests. In addition, gravitational effects are not addressed; these may be significant given the downward vertical orientation of the steam injection as buoyancy would tend to act in opposition to the direction of flow and cause an ultimate reversal of the injected fluid, especially later in the tests. Of lesser relevance to a strict chugging correlation, but of note here, is the depth of the outlet beneath the water surface; as a thermal plume forms around the sparger, the depth of the plume and its flows would conceivably affect the bulk vessel circulation.

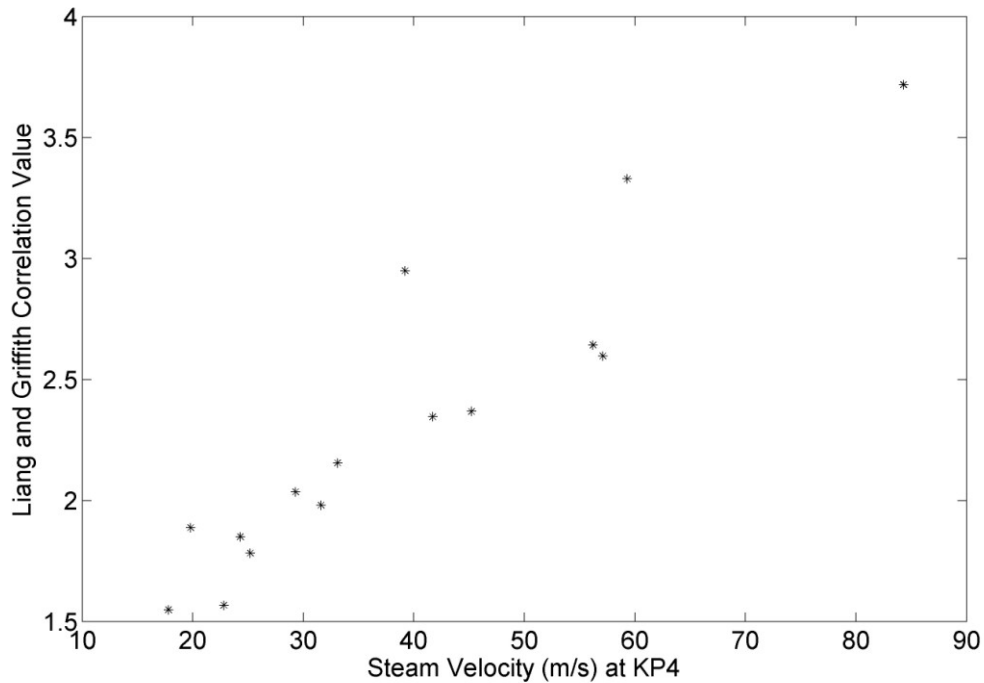


Figure 78: Liang and Griffith Correlation at Key Point #4

It can be seen in Figure 78 that the steam velocity has a strong residual dependency in Key Point #4. The sparger depth shows some dependency as well. If gravity is included, these can be grouped together in the form of a steam injection Froude number (Eq. (9) [57]) as in Eq. (10), where v_s is the velocity of the steam in the sparger and $d_{depth,outlet}$ is the depth of the outlet of the tube beneath the surface of the water; this again shows a trend at Key Point #4 when compared against the Liang and Griffith correlation as demonstrated in Figure 79. While this adaptation might be considered a stretched definition of the Froude number, it is useful in this analysis. The depth term provides a characteristic scale for natural convection in conjunction with the gravitational term; such was not part of the original correlation.

$$Fr = \frac{v}{\sqrt{g \cdot L}} \quad (9)$$

$$Fr_s \equiv \frac{v_s}{\sqrt{g \cdot d_{depth,outlet}}} \quad (10)$$

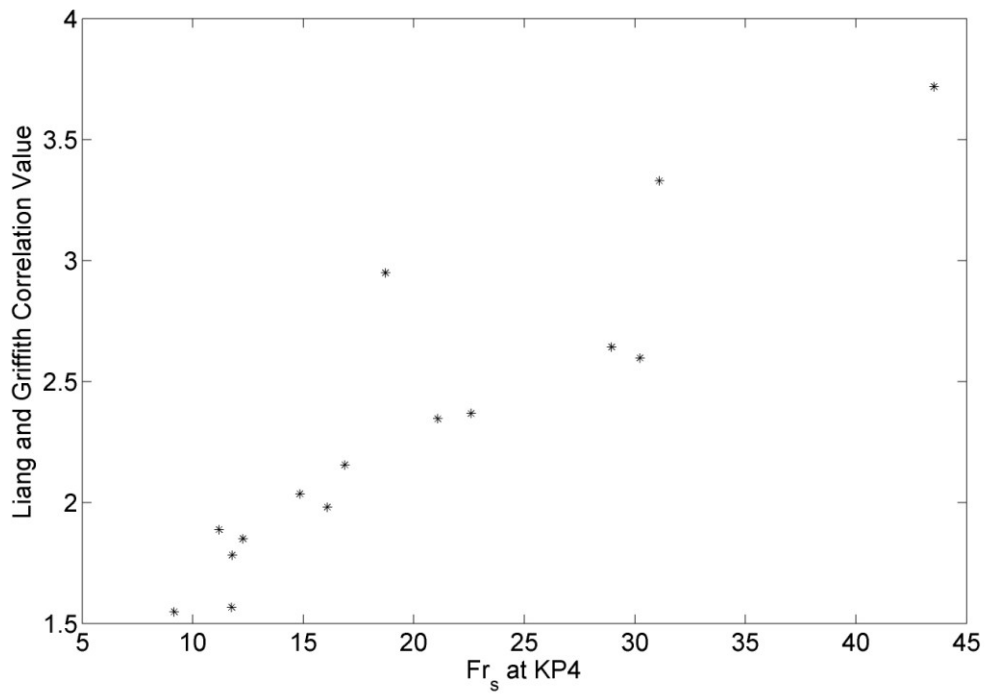


Figure 79: Liang and Griffith Correlation at Key Point #4, nondimensional

Multiplying the original correlation from Liang and Griffith, Eq. (3), by the Froude number expressed in Eq. (10) to a power of -0.5 will eliminate the trend, but another dependency remains (Figure 80, dropping the leading coefficient of 0.06): the steam and water density ratio. Upon inspection, the cleanest profile shows dependency

on the ratio of steam and water at saturation, where the saturation pressure is taken to be that of the steam line just upstream of the sparger. Clearly this in some form, or a surrogate for it, needs to be accounted for in the relationship. To account, the correlation can be casted to be that of Eq. (11):

$$\text{Pr}_w^{\frac{1}{2}} \left(\frac{\mu_s}{\mu_w} \right)^{\frac{1}{2}} \left(\frac{\rho_s}{\rho_w} \right)^{\frac{1}{2}} \text{Ja}_w^{-1} \text{Re}_s^{\frac{1}{2}} \text{Fr}_s^{-\frac{5}{8}} \left(\frac{\rho_{w,sat}}{\rho_{s,sat}} \right)^{\frac{5}{16}} \quad (11)$$

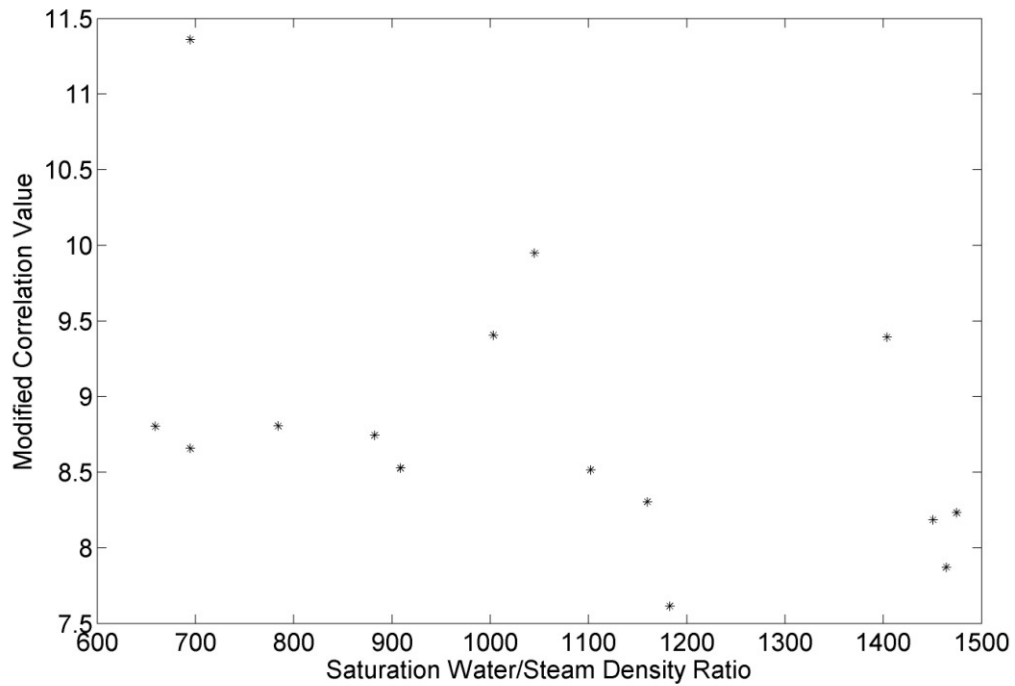


Figure 80: Saturation Water/Steam Density Ratio Dependency

Inclusion of the density ratio, to account for the dependencies, required adjustment of the exponent of the Froude number. It should be noted at this point that

inclusion of a form of the Froude number with this density ratio can be rearranged to reveal a form of the Richardson number (used in various forms in meteorology and in mixed convection problems; Eq. (12) [56] is occasionally used as a definition). With the Grashof number (Eq. (13) [58]) and considering a simplification not unlike the Boussinesq approximation in Eq. (14) [58], it follows that (when density differences are enormous) a simple density ratio shown in Eq. (15) leads to Eq. (16).

$$Ri = \frac{Gr}{Re^2} \quad (12)$$

$$Gr = \frac{g\beta(T_s - T_\infty)L^3}{\nu^2} \quad (13)$$

$$\beta \approx -\frac{1}{\rho} \frac{\Delta\rho}{\Delta T} = -\frac{1}{\rho} \frac{\rho_\infty - \rho}{T_\infty - T} \quad (14)$$

$$\beta(T_{hot} - T_{ref}) \approx \frac{\rho_{ref}}{\rho_{hot}} \quad (15)$$

$$Ri = \frac{Gr}{Re^2} = \frac{\left(\frac{g\beta(T_h - T_{ref})L^3}{\nu^2} \right)}{\left(\frac{\nu L}{\nu} \right)^2} = \frac{g\beta(T_h - T_{ref})L}{\nu^2} \quad (16)$$

$$\approx \frac{g \frac{\rho_{ref}}{\rho_{hot}} L}{\nu^2} = \frac{g \cdot L}{\nu^2} \cdot \frac{\rho_{ref}}{\rho_{hot}} = \frac{1}{Fr^2} \cdot \frac{\rho_{ref}}{\rho_{hot}}$$

While Eq. (11) – the Liang and Griffith correlation with corrections – resolves the dependencies that were shown to exist in the uncorrected version at Key Point #4, when applied to other Key Points, dependencies re-enter the picture. However, they are dependencies on terms already in the corrected relationship; resolving the dependencies

means adjusting the exponents rather than the addition of terms at the end of the formula. As the dependencies seemed to increase the further away in time/Key Points the period of interest is, a method to smoothly correct the growing dependencies was sought. One of the more promising enhancements came from defining a pressure ratio β_p in Eq. (17) to assist in defining the progression within a test. It compares the vapor pressure of the bulk liquid at the level of the sparger outlet (a function of its temperature) to the overall pressure at that level.

$$\beta_p \equiv \sqrt{\frac{P_{vap}}{P}} \quad (17)$$

Instead of attaching the parameter to the end of the relationship as with the other correction factors, Eq. (17) was inserted into the changing exponents. This was not limited to those of the correction factors, but to the Jakob number as well, producing a corrected correlation of Eq. (18):

$$\text{Pr}_w^{\frac{1}{2}} \left(\frac{\mu_s}{\mu_w} \right)^{\frac{1}{2}} \left(\frac{\rho_s}{\rho_w} \right)^{\frac{1}{2}} \text{Ja}_w^{-1 + \frac{1}{16}\beta_p} \text{Re}_s^{\frac{1}{2}} \text{Fr}_s^{-\frac{3}{8} - \frac{1}{2}\beta_p} \left(\frac{\rho_{w,sat}}{\rho_{s,sat}} \right)^{\frac{1}{4} + \frac{3}{16}\beta_p} \quad (18)$$

While Eq. (18) was sufficient for relating to Key Points 2-4 for single-phase tests, two-phase injection required additional accounting. Careful inspection revealed a correction that was surprisingly simple: division of the Jakob number by the steam quality. If the quality term is “unbounded” – that is, allowed to be greater than 1 for superheated steam following Eq. (19), then the Jakob number can be re-expressed as a “Two-Phase Jakob Number” shown in Eq. (20), which expresses a ratio of the thermal energy needed to bring the pool's water to saturation to that needed to fully condense the

two-phase steam. While not explored here, the “unbounded” quality may enable the extension of the correlation into the superheated steam region.

$$x_u = \frac{h_s - h_{w,sat}}{h_{s,sat} - h_{w,sat}} \quad (19)$$

$$Ja_{TP} = \frac{Ja_w}{x_u} = \frac{h_{w,sat} - h_w}{h_s - h_{w,sat}} \quad (20)$$

$$\text{Pr}_w^{\frac{1}{2}} \left(\frac{\mu_s}{\mu_w} \right)^{\frac{1}{2}} \left(\frac{\rho_s}{\rho_w} \right)^{\frac{1}{2}} \left(\frac{Ja_w}{x_u} \right)^{-1 + \frac{1}{16}\beta_p} \text{Re}_s^{\frac{1}{2}} \text{Fr}_s^{-\frac{3}{8} - \frac{1}{2}\beta_p} \left(\frac{\rho_{w,sat}}{\rho_{s,sat}} \right)^{\frac{1}{4} + \frac{3}{16}\beta_p} \quad (21)$$

In addition to the steam quality, a definition for the two-phase viscosity in the Reynolds number was needed if the viscosity terms would remain. Here, a volumetric mean (with no slip between water and steam phases; a presumed equality of their velocities) was considered, along with other homogenization methods such as quality-weighted reciprocals [59]. However, it was recognized that the viscosity terms cancel out of the correlation as currently expressed (including those from the Prandtl number, viscosity ratio, and Reynolds number).

With the above corrections, the chugging-type relationship of Eq. (21) was found to work well for Key Points 2-4. However, at Key Point #5, the saturation steam/water density ratio again shows a major dependency; correcting it greatly altered its exponent. The same is true of all later phenomenological Key Points. Worse, the exponent for the saturation steam/water density ratio is not the only one that may need adjusting. With adjustments made to it, by the final phenomenological Key Point (Key Point #10), a new dependency on the Jakob number can be seen to be developing (compare Figure 81 and

Figure 82). This is evidence to suggest that, at that point, the chugging-style relationship is finally breaking down and likely giving way to another type, probably bubbling-type, or one unencumbered by a zero/infinite value resulting from applying the Jakob number approaching saturation. However, even with the new dependency beginning to emerge at Key Point 10, the experiment's state can still be described with the final corrected form of the chugging-type relationship (henceforth called the “Mixing Number” or M_x) given in Eq. (22); it simplifies to Eq. (23). The F_1 term is expressed as part of Eq. (23). Unfortunately, Key Point 5 and later were unable to be smoothly transitioned through by use of β_p in the density ratio exponent; individual expressions for the exponent became the cleanest way to resolve the destratification Key Points.

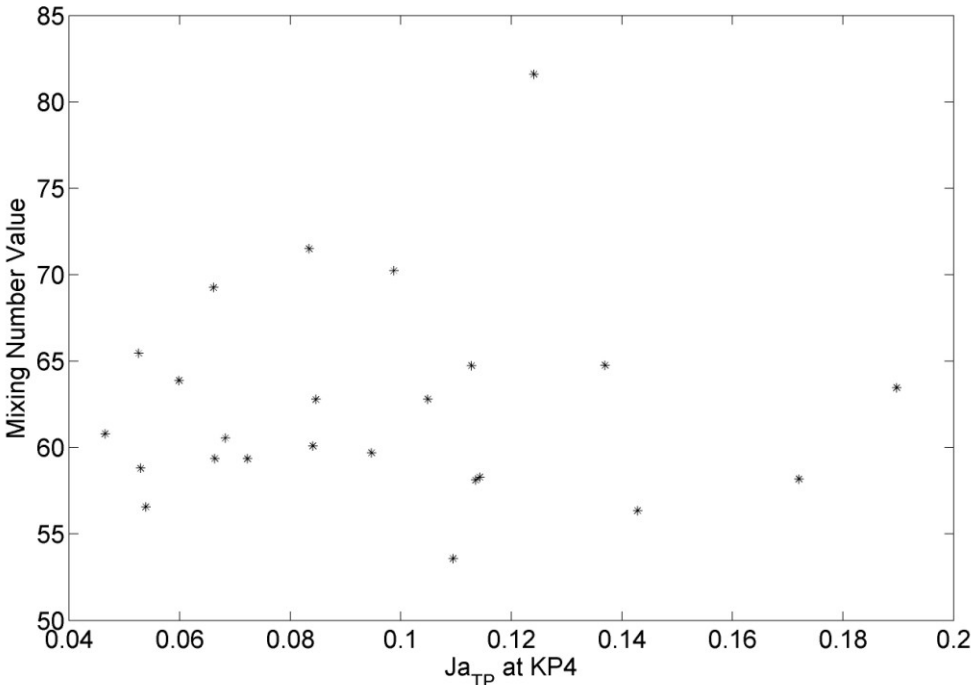


Figure 81: Mixing Number at Key Point #4

$$Mx = \text{Pr}_w^{\frac{1}{2}} \left(\frac{\mu_s}{\mu_w} \right)^{\frac{1}{2}} \left(\frac{\rho_s}{\rho_w} \right)^{\frac{1}{2}} \left(\frac{Ja_w}{x_u} \right)^{-1 + \frac{1}{16}\beta_p} \text{Re}_{TP}^{\frac{1}{2}} Fr_s^{\frac{3}{8} - \frac{1}{2}\beta_p} \left(\frac{\rho_{w,sat}}{\rho_{s,sat}} \right)^{F_1} \quad (22)$$

$$Mx = \left(\frac{c_{p,w} \cdot G_s \cdot d_{outlet}}{k_w} \right)^{\frac{1}{2}} \left(\frac{\rho_s}{\rho_w} \right)^{\frac{1}{2}} Ja_{TP}^{-1 + \frac{1}{16}\beta_p} Fr_s^{\frac{3}{8} - \frac{1}{2}\beta_p} \left(\frac{\rho_{w,sat}}{\rho_{s,sat}} \right)^{F_1}$$

where

$$F_1 = \begin{cases} \frac{1}{4} + \frac{3}{16}\beta_p, & 2-4 \\ \frac{13}{16}, & 5 \\ \frac{15}{16}, & 6-7 \\ 1, & 8-10 \end{cases} \quad (23)$$

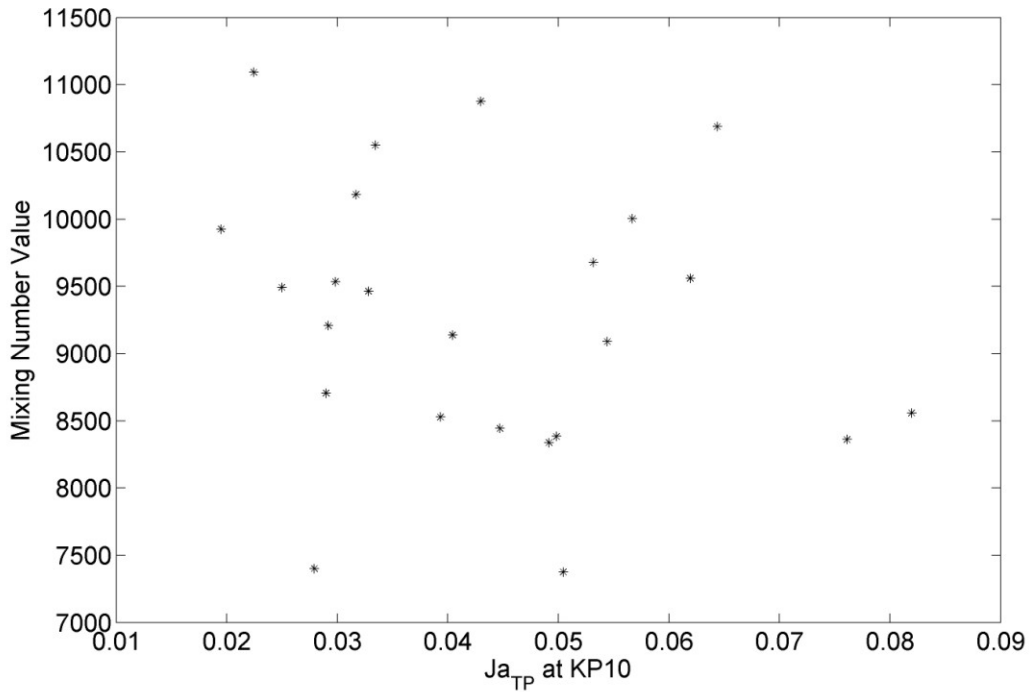


Figure 82: Mixing Number at Key Point #10

A summary of the results of the new correlation can be found in Table 11. For the decreasing-circulation period (Key Points 2-4), the relationship shows good agreement between the tests as well as clear separation between the Key Points. The increased spread for Key Point #3 (onset of bulk thermal stratification) is likely due to the difficulty of detection in the data processing; the other Key Points tend to be better defined and easier to detect in the data. Even with the expression beginning to break down by Key Point #10, the results were still within 11%.

Table 11: Spread in As-Measured Correlation Values

	Correlation Mean	Min	Max	σ	σ/mean
KP2	42.95	38.50	46.33	1.99	4.64%
KP3	47.11	29.23	73.24	7.67	16.3%
KP4	62.51	53.58	81.60	6.03	9.64%
KP5	1796	1614	1923	94.7	5.27%
KP7	5064	3894	5701	377	7.45%
KP10	9274	7376	11093	1009	10.9%

5.4 ERROR ANALYSIS

Due to the lack of a large number of tests with the same testing parameters, full statistical development of repeatability is not possible with the data gathered in this testing program. While Test Nos. 1&2 and 4&32 demonstrated a capacity for repeatability, they are insufficient for full quantitative analysis and reflect more qualitative measures. However, that does not preclude an analysis of the uncertainty in the collected data; it simply adds a limitation on its scope. Furthermore, if the correlation developed is assumed to be valid, then the comparison of data at

phenomenological Key Points can provide some insight into the overall spread, especially when combined with individual major contributions to error (i.e., instrument error) that would tend to shift the position/correlation value of the individual Key Point.

The approach used here to determine the error in the Mixing Number presents two outcomes: a probable conservative evaluation, and what should be a bounding evaluation that produced almost twice the value. Covariances were ignored/assumed to be zero (the use of the same instruments to compute multiple terms in the correlation will result in covariance terms), and in a number of cases “worst-case” evaluations were used. The relative standard deviations were calculated for each major term of the simplified expression for the Mixing Number; as a result, due to their dropping out of the final form, viscosities produced no impact on the error determination. The oft-used error propagation formula given by Eq. (24) [60] was used to propagate instrument error through to the total instrument error contribution.

$$\sigma_u^2 = \left(\frac{\partial u}{\partial x}\right)^2 \sigma_x^2 + \left(\frac{\partial u}{\partial y}\right)^2 \sigma_y^2 + \left(\frac{\partial u}{\partial z}\right)^2 \sigma_z^2 + \dots \quad (24)$$

where

$$u = u(x, y, z, \dots)$$

The single largest contributor in the baseline evaluation was the error propagated through the two-phase Jakob number ($\sigma = 2.2\%$). This has contributions not only from the vortex flowmeter instrument cluster and pool conditions, but also includes significant uncertainty due to an approximately 13% value in the heat loss coefficient in the main steam line (the effects of this are limited by the low heat loss values). The Froude number comes in a distant second in its contribution ($\sigma = 1.2\%$).

In what should be a bounding determination, the uncertainty in β_p becomes the dominant factor, enlarging every term that utilizes it. This is no surprise, as it exists in the exponents and constitutes a significant part of their overall values. In that evaluation, the Froude number becomes the largest single contributor ($\sigma = 3.2\%$) and the two-phase Jakob number drops to second place ($\sigma = 2.2\%$).

As the Mixing Number has multiple expressions for different points in the experiment's progression, multiple error terms have been developed. In the early stages (Key Points 2-4), the likely conservative estimate is that the Mixing Number can be determined by the experiment's instruments to a standard deviation of 2.7%; a bounding estimate puts it at 4.4%. Later (when $F_1 = 1$, which is applied to Key Points 5-10 as an overestimate), the measurements should produce a standard deviation of 2.8% in the Mixing Number. The respective bounding value is 4.0%.

With the bounding estimate, the measurement error in the Mx correlation is comparable to the spread in measured values for Key Points 2 and 5. As the measurement error applies to every datum, it contributes additional error to the measured values for each Key Point. Inclusion of the measurement error (using the bounding value of 4.4%) as well as the spread in measured correlation values at the various Key Points produce the estimated total uncertainty values show in Table 12. This assumes correct placement of the Key Point by the data processing script. Further development of the measurement error analysis can be found in Appendix B.

Table 12: Total Error in Correlation

	Correlation Mean	Total Error, σ/mean
KP2	42.95	4.72%
KP3	47.11	16.31%
KP4	62.51	9.69%
KP5	1796	5.35%
KP7	5064	7.50%
KP10	9274	10.92%

5.5 FULL SYSTEM MODEL CONSIDERATIONS

With the developed expression for the Key Points, one may begin to model the progression from state to state, given certain modeling assumptions. A number are made for the sake of simplicity, and significant room is left for future efforts to enhance the model.

The water in the pool is assumed to be representable by two separate volumes vertically stacked, and each is assumed to be homogenous. In the early parts of a test, Key Points 2-4, the upper volume consists of all the water at a vertical level above that of the RCIC sparger outlet. The lower level has the remainder of the water (below the sparger outlet). The upper volume is assumed to be in thermal equilibrium with the vapor space above it (including a relative humidity of 100%), and as a result it drives the pressurization of the chamber. Steam is injected and condensed in the upper volume. The lower volume provides water for the pump suction, and defines the pump inlet conditions.

From the beginning of steam injection up through Key Point #3, both water volumes are intermixed; the entire pool is uniform. In the data, stratification begins at

Key Point 3, but residual mixing tends to remain through Key Point #4 as different levels have their temperatures branch off from the upper level at different times, and tend to flatten out around Key Point #4. This is seen not only in the data gathered here but also in a number of profiles from the University of Tokyo [54], POOLEX [35], and SIET [40] tests, which have a greater vertical thermal resolution; the separation resembles a retreating front between the well-mixed upper and poorly-mixed lower regions. In this model, after Key Point #3, mixing between the upper and lower volumes ceases; the lower volume maintains its state, while heat is dumped solely to the upper volume.

The greatest thermal stratification in the upper pool regions in the data define Key Point #4, which is taken to represent the minima of pool mixing. Due to the modeling simplification of a uniform upper volume, no thermal separation is defined here in the upper regions. As the peak is relatively low, this simplification is thought to be less significant than others present in this model. Once Key Point #5 is reached, the upper region is considered to be well mixed.

After Key Point #5, there appears a vertical (downward) progression of a mixing front; the bottom of the upper water volume progresses down from the level of the sparger outlet. The upper volume, therefore, grows while remaining thoroughly mixed; the lower volume, maintaining the thermal state it had in Key Point #3, shrinks.

At Key Point #7, the vertical progression of the mixing front has reached the lower levels in the pool (8 inches above bottom), shifting considerable inventory from the lower volume to the upper. The peak mid-lower thermal separation in this model can

be taken to be just prior to this point. In the data, the peak separation is defined by Key Point #6, which typically occurs shortly before the temperature reading at the lower vertical level quickly rises to that of the middle and upper pool regions.

At Key Point #10, the advancing mixing front has reached the very bottom of the vessel; peak lower-outlet temperature differences are shortly prior to this (Key Point #8 in the data). After this point, the lower volume ceases to exist, and the upper water volume defined in this model encompasses the entirety of the pool. It continues to be well-mixed through the end of the test.

This model has several limitations. The instantaneous flattening of the lower-volume temperatures after Key Point #3 is a gross simplification of the data, and misses the continued temperature rise seen especially in the lower-level (not bottom/outlet) readings; this rise can continue PAST Key Point #5 before flattening out (as it appears to do even in Test #4). Whether this is residual circulation from prior steam injection or active mixing from concurrent steam injection is unclear. Additional water volumes, or thermal profiles within the volumes, may be useful. Furthermore, some profiles never flatten out; many of the two-phase injection tests show some intermixing between the upper and lower volumes for the entirety of the test. As a result, the peak temperature differences between the lower and outlet reading will be overstated by this model; those of the middle to lower level readings will be overstated even more. Due to the overstatements, this model should be considered to provide bounding values for the thermal stratification of the lower levels of the pool.

With regard to the upper levels, this model overstates the heat dumped into the upper volume. However, as it assumes complete mixture of the upper volume, there is no considered potential for the development of a thermal profile. The thermal separation between the top and the middle of the pool is ignored completely. The pressurization condition of the chamber, then, is not guaranteed to be overstated as a possible hot spot on the top of the volume is not considered.

5.6 SCALING DISCUSSION

While scaling from this experiment to full size in operating BWR systems cannot be completely established solely from the data gathered in testing, there is some basis for scalability. It was determined during the design phase that the full range of applicable Reynolds numbers in the sparger would be irreproducible with the equipment in the NHTS Laboratory. Even approaching them with the current steam supply would require sonic flows; this would drastically affect the condensation and steam jet profile at the sparger outlet. Instead, the Mach number was chosen as a scaling parameter for preservation. The facility can produce a peak sparger Mach number near 0.18; the full scale system was estimated to produce Mach numbers in the range of 0.1, which is easily attainable with less than full power operation of the steam generator. Preserving the Mach number has the added benefit of, in many of these tests, preserving the flow velocity and mass flux (Suppression Chamber conditions are comparable).

If a Fukushima-scale RCIC system consumes approximately 2.1 kg/s of steam, it would produce a mass flux at the sparger of 33 kg/m²s. At 2.51 kg/s [40], the mass flux is 39.7 kg/m²s. With enough subcooling in the Suppression Pool, this would land

squarely in the chugging regime for DCC according to the traditional maps. The mid-power (107 kW) tests produce similar mass fluxes ($\sim 34 \text{ kg/m}^2\text{s}$), and were originally thought to provide phenomenological similarity. However, given the multitude of regime maps (as well as the correlation developed here), the similarity becomes less clear.

An additional distortion affecting the utility of the correlation developed here is the aspect ratio between the Suppression Chamber and the sparger outlet. While the vessel used in these tests has a volume that scales from roughly 1:750 for a small BWR pool of 70,000 cubic feet to 1:1300 for a larger one of 125,000 cubic feet, the non-toroidal shape results in a much different diameter scale than expected – 1:5.9 in the case of Fukushima Daiichi Unit 2 [61]. The sparger diameter, however, scales to 1:6.9 – at least for Unit 2 [6], and the effect of position (closer to wall vs. near pool center) is unclear. Further testing with additional varied parameters can provide insight into some of these unknowns.

Beyond the previous distortions, the depth of the sparger outlet in the pool is not matched; here, it is roughly at half depth, while in Unit 2, it appears to be much closer to the pool's surface [6]. Furthermore, full-scale systems tend to operate with Suppression Pool levels below the center of the Torus (this will be affected by injection from the Condensate Storage Tank before RCIC System realignment to draw suction from the Suppression Pool). The depth term in the Fr_s component of the new correlation should account for this, but more tests at more varied pool depths are needed for confirmation.

The end result is that scaling to full-size systems is best thought of as a work-in-progress that would greatly benefit from experimental data with additional varied parameters.

6. CONCLUSIONS

In this work, an experiment has been performed to investigate the conditions a RCIC System may be exposed to in long-term operations, especially in a prolonged SBO scenario. Of major interest was the thermal behavior of the Suppression Pool, which in the long term serves as both the heat sink for steam from the reactor (through SRV as well as RCIC System operations) as well as the source of makeup water for the reactor. This work has shown a demonstrable capacity for thermal stratification in the Suppression Pool resulting from RCIC System operations.

Thermal stratification can contribute to extended RCIC Pump operability by limiting the pump's exposure to elevated temperatures. This has the trade-off of exposing the Suppression Chamber to increased pressure loading driven by warmer water at the surface of the pool. However, in these tests, the extra pressure was limited, as the warmer upper regions of the pool tended to have larger volumes of water than the cooler lower regions by virtue of pool and sparger geometry. The pressurization concern would be greater in cases where the cooler water volume is larger than the warmer water volume. Therefore, in a full-scale BWR Suppression Pool with similarity in design to the system here (which differs on a plant-by-plant basis), thermal stratification in the Suppression Pool is likely to act in an overall beneficial manner; the RCIC Pump would be protected (so long as its thermal limit is above the temperatures at which stratification forms), while the extra burden placed on the containment would be limited. Depending

on the scenario, the pool may fully destratify before containment pressure limits are reached.

The thermal conditions for pump suction (when the RCIC System is aligned to the Suppression Pool) are key determinants of the operating envelope for the pump, but are not the only important conditions. Net positive suction head requirements and temperature/pressure/speed/flow curves for the RCIC Turbine and Pump are also very important. While no cavitation in the pump in these tests during data operations, this cannot be guaranteed to be the case in full-scale systems without better piping details, loss terms, and TDP response curves.

The thermal behavior of the Suppression Pool can be modeled in manners developed in this work. A notable inadequacy of the traditional DCC regime maps was seen in these tests, and corrections to the chugging correlations were necessary to describe the data. While this was not a strict DCC study, parameters explored here have not been addressed in previous DCC experiments; the effects of pressure conditions are limited in the literature, while the effect of steam quality (saturated two-phase through the superheated region) appear to be completely absent from previous experiments. Characteristic thermal profiles were observed, and it was seen that sparger design and location are key in the thermal profile development.

In these tests, steam injection through an SRV analog was very effective at circulating and mixing the water in the Suppression Chamber. Injection through the RCIC Sparger analog, however, produced a characteristic thermal stratification profile. While variation of the test parameters resulted in sometimes significant distortions to the

characteristic profile, every RCIC-Alignment test produced thermal stratification. In most tests, the stratified profile eventually disappeared as mixing increased with decreasing pool subcooling. However, not every test (largely due to equipment limitations) proceeded all the way through to full destratification. The peak thermal stratification found in these tests ranged from weak to severe; one test saw a difference of 65.1 °C between the mixed and unmixed regions.

The characteristic thermal profiles from the RCIC-Alignment tests had a number of common features that were expressed in the tests. Identification and examination of those features, expressed as “Key Points” here, allowed the development of an empirical correlation that expresses the aggregate pool mixing state developed in this testing program. As chugging at the steam-water interface in the RCIC Sparger played a very prominent role in pool mixing conditions, the correlation development began with Liang and Griffith’s [29] expression for the boundary of the chugging; corrections were then applied to adapt it to the data gathered here.

Further testing would allow full scalability to be established. Specifically, further work remains for determining the effects of the aspect ratio between the sparger outlet size and pool dimensions as well as the effect of pool and sparger depth (the variations here are very limited in range); these are key for defining the scalability of these tests and the correlation developed from them. Without such work, the model developed here cannot be guaranteed to reflect full-scale conditions in a BWR.

In addition, a more complete exploration of the two-phase steam/water injection conditions should be performed. Although two-phase steam/water exploration has been

performed here, the limited number of tests that could be performed in a timely manner prevented a complete, thorough exploration of the two-phase steam-water regime as motivated by scenarios depicting reactor overfill from an uncontrolled RCIC System.

6.1 KEY FINDINGS

Of the results presented, there are several findings of broad substance:

- Thermal stratification can form in large pools where heat is injected through DCC of very pure steam; BWR Suppression Pools are not immune
- Thermal stratification can limit the high-temperature exposure to pumps drawing suction from the bottom of thermally stratified pools
- Chugging (at high pool subcooling) and bubbling (at low pool subcooling) can cause significant bulk mixing currents, but at intermediate levels of subcooling mixing currents are limited, permitting thermal stratification
- Vent tube/sparger design and placement are significant factors in the ability of stratification to form
- While steam injection rate, quality, and Suppression Chamber pressure conditions all affect the development of thermal profiles, pressure conditions are the most significant
- With the correlation developed in this effort, key events and phenomena in the development of thermal profiles in similar pools can be predicted

6.2 RELEVANCE TO THE EVENTS AT FUKUSHIMA DAIICHI

In the progression of events in the accidents at Fukushima Daiichi, the RCIC Systems continued operation into essentially uncharted territory. The data gathered here may be able to provide insight into the operational details for the Fukushima RCIC Systems.

The thermal stratification developed here would tend to limit exposure of the RCIC Pump to hot water, and could act to protect it. However, for the thermal stratification to develop, SRV operations would need to be limited, as injection through an SRV analog in these tests tended to mix the entire pool. It would also be affected by the specific design of the vent line – which was different between Unit 2 and Unit 3. Check valves and vacuum breakers are used in plant systems, but were not installed in this experimental facility. They would tend to limit the backpropagation of some phenomena to the RCIC Turbine, weaken chugging, and prevent the damaging mechanical loading of structures. This dampening of chugging oscillations could encourage thermal stratification to begin earlier, but the degree to which this is the case is uncertain.

At Fukushima, SRV actuation was contemporaneous with RCIC System operation. While this places the Suppression Pool in the role of primary heat sink, the large masses of other material in containment can act as additional thermal reservoirs. Further, flooding in the Torus room can seriously affect thermal distributions, and act to remove heat from containment. None of these conditions were explored in this work.

As a result, while these tests have demonstrated the potential for thermal stratification, they are not proof of its occurrence at Fukushima. More phenomena and specific operational details need to be considered to draw such conclusions. In addition, to apply the correlation developed herein, scalability to such systems needs to be established.

6.3 FUTURE WORK

Even the most exhaustive studies leave room for future development, and this is no different. Three categories of future efforts are identified here based on the necessary level of anticipated effort to perform the work.

Can be done quickly with limited system modification:

- Further analysis of existing data
- Two-phase regime fill-in
- Additional power levels
- Additional pressurization/venting conditions
- More/less water in the pool (varied depth)
- Closer adherence to plant operating procedures

Can be done with system overhaul:

- Other sparger sizes and designs
- Better vertical thermal resolution and additional plume details
- More instruments in/on/around sparger

- Ability to run pool/pump much hotter and explore bubbling
- Exploration of the effects of RCIC Pump suction aligned to the Condensate Storage Tank (no water extraction from the Suppression Pool)

Can be done only with major changes:

- Video recording of important locations
- Alternate Suppression Chambers
- Strict DCC investigation to produce new regime maps with additional variables (pressure, steam quality, vent tube design)
- Installation and investigation of Terry turbine-driven pump
- Effect of external cooling of the Suppression Chamber vessel (i.e., flooding of the Torus room in a BWR with the Mk. I containment)

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APPENDIX A
SYSTEM P&ID COLLECTION

This Appendix contains the P&IDs for the complete system and in more detail than those given in the main text. The analog to the RCIC Turbine is given in Figure 83 and the system overview is in Figure 84. The four subsequent P&IDs contain the more detailed drawings of the system, starting with the water deionization system and hot water tank in Figure 85. The bulk of the experiment in operating mode is then split into two parts along the physical separation imposed by the loading bay; the Steam Generator and connected equipment is given in Figure 86, and the Suppression Chamber side is diagrammed in Figure 87. After a test is finished, the system is realigned to Cooldown Mode; this is given in Figure 88.

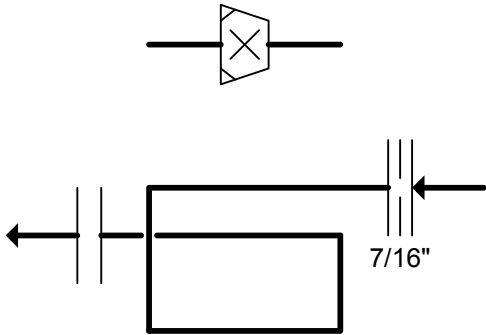


Figure 83: Turbine Analog Design

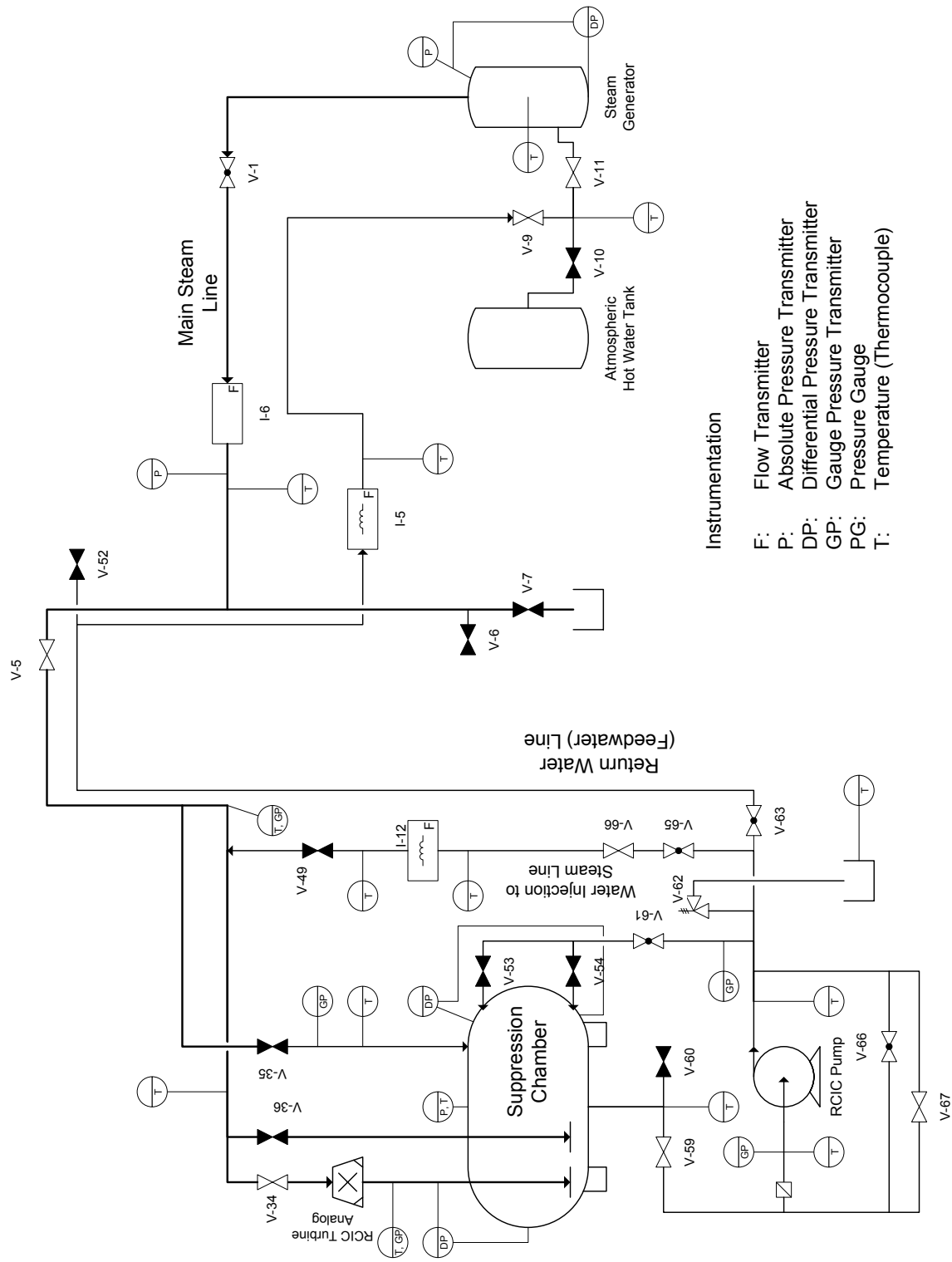


Figure 84: Enhanced System P&ID Overview

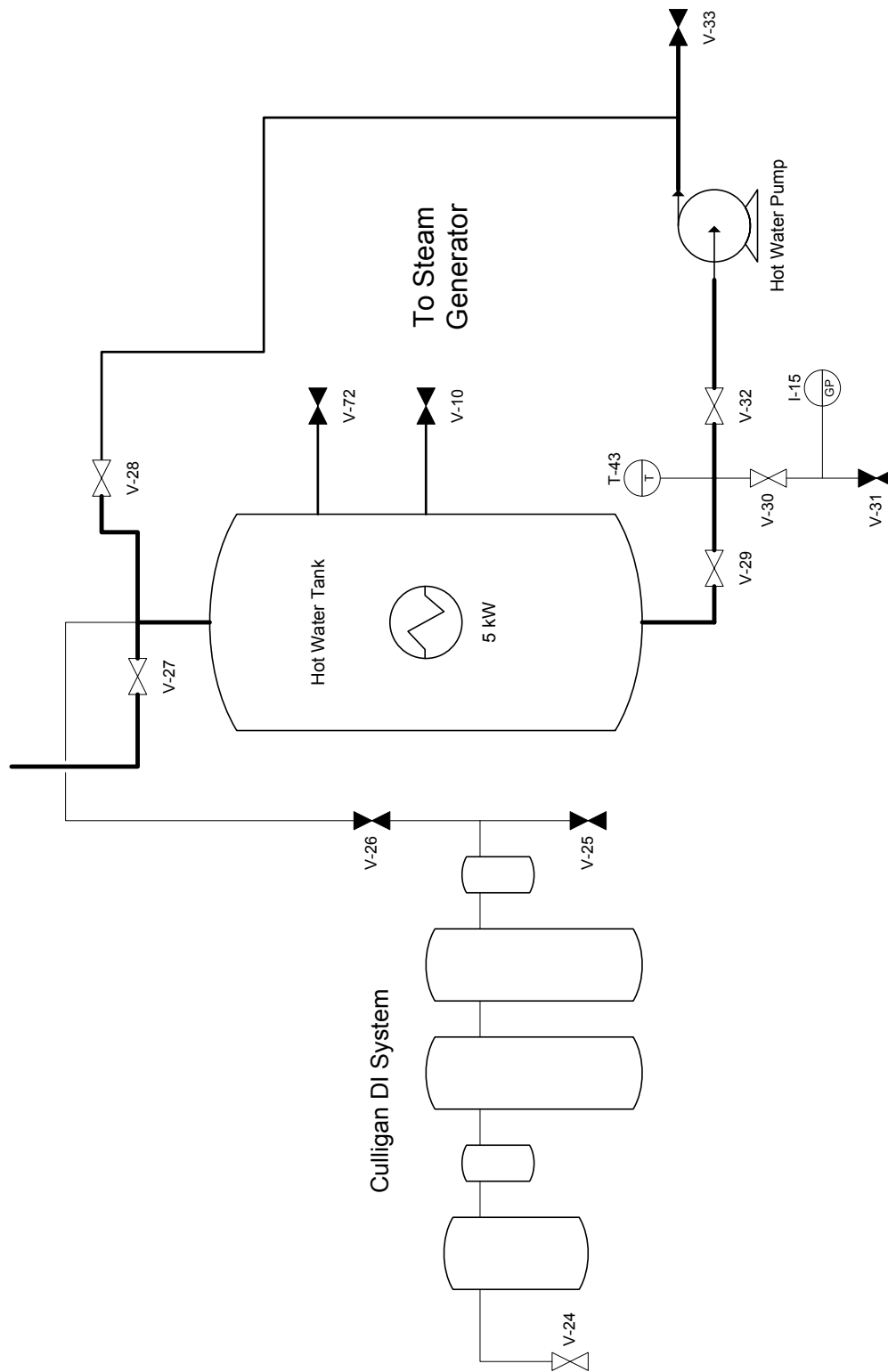


Figure 85: DI System and Hot Water Tank

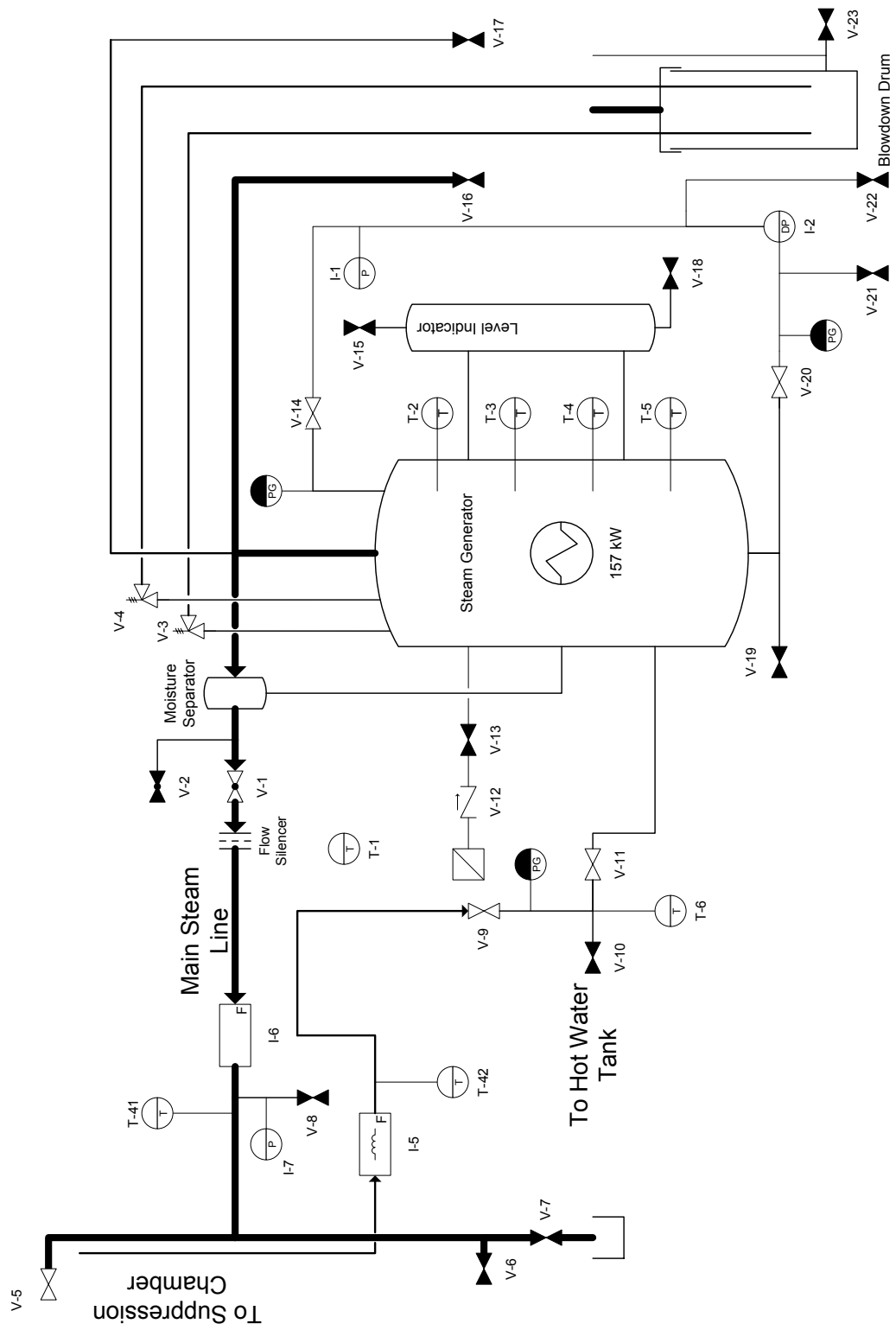


Figure 86: Steam Generator System P&ID

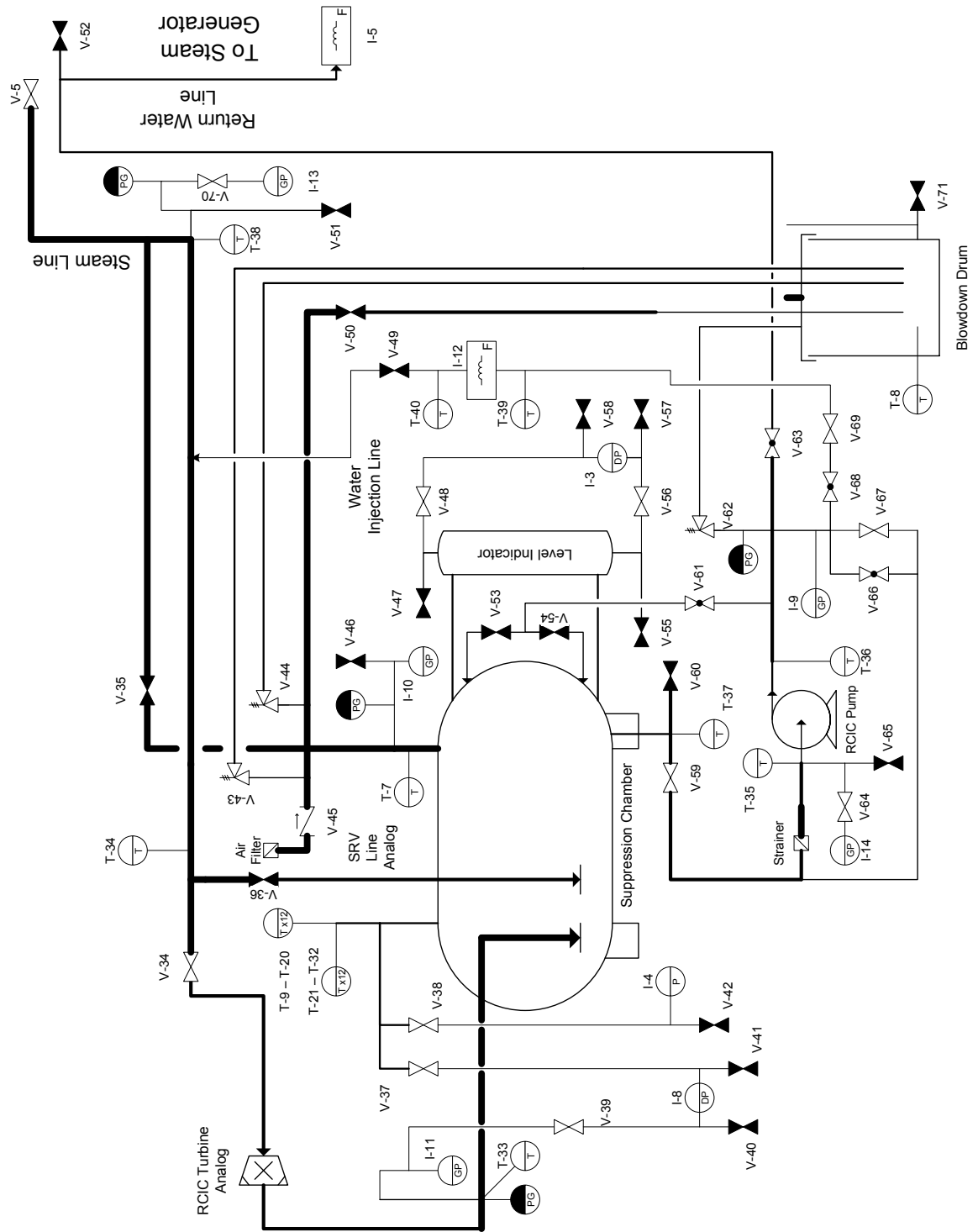


Figure 87: Suppression Chamber System

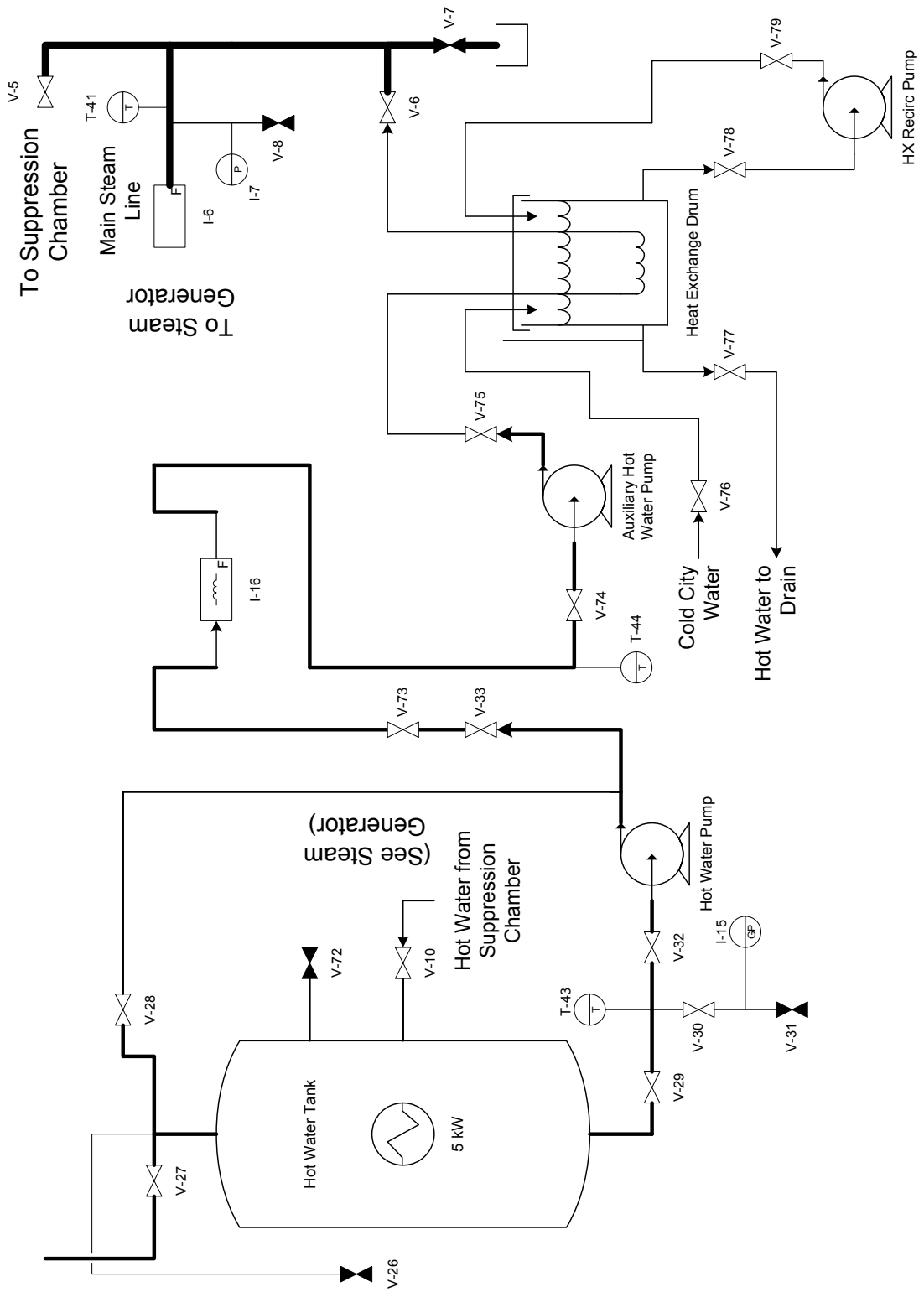


Figure 88: Cooldown Setup

APPENDIX B
MEASUREMENT ERROR ANALYSIS

This Appendix contains the details on the error analysis performed to propagate instrument error through to its resulting measurement error in the Mixing Number.

B.1 MAIN STEAM LINE MASSFLOW

To determine mass flows in the main steam line prior to water injection, the vortex flowmeter (I-6) is collocated with the main steam line pressure transmitter (I-7) and a main steam line temperature reading (T-41). The vortex flowmeter, when flow is in its accurate range, has an associated error of 1%. The pressure transmitter has an error of 0.1% of its Upper Range Value (130 psia, resulting in an error of 0.13 psi), and the Type T thermocouple with Special Limits of Error has an error of 0.5 °C. An ideal gas treatment for steam around 1 atm and 100 °C will lead to the greatest fractional error in computed density for the range of interest; the contribution of the pressure transmitter (proportional to P) translates to 0.884%, and the temperature error contribution (proportional to 1/T) is 0.134%. Application of the temperature error to the K-factor correction term (translates to a 0.0026% error) becomes vanishingly small when propagated through.

$$\left(\frac{\sigma_u}{u}\right)^2 = \left(\frac{\sigma_x}{x}\right)^2 + \left(\frac{\sigma_y}{y}\right)^2 \quad (25)$$

$$\sigma_u^2 = \sigma_x^2 + \sigma_y^2 \quad (26)$$

Application of Eq. (24) to multiplication or division ($u = xy$ or x/y) results in Eq. (25), while addition and subtraction ($u = x \pm y$) results in Eq. (26) [60]. Utilizing these formulae, respecting the vortex flowmeter's outputs defined by Eqs. (4) - (7), yields an error in the mass flowrate measurement of 1.342% (contributions of 1% from the meter

itself, 0.884% from the pressure measurement, and 0.134% from the temperature measurement).

In two-phase injection tests, the Badger M2000 magnetic flowmeter (I-12) monitors a secondary flow of material into the main steam line. The density difference of water across the 0.5 °C error of the thermocouples is not great, especially when the two measurement points are taken in conjunction. As a result, the 0.25% volumetric flow error of the flowmeter translates to 0.252% error in the mass flowrate. This includes the contribution of thermal expansion error from temperature measurement error, where the thermal expansion of water near 100 °C was estimated from steam table data to be $\sim 0.0007 \text{ 1/}^\circ\text{C}$. In two-phase tests, the flowrates and therefore the variances are additive by Eq. (26). The relative error, therefore, will improve under addition. To account for single-phase testing, the vortex flowmeter's mass flowrate relative error of 1.34% will be taken as a bounding value for the relative error of total massflow in single and two-phase tests.

B.2 POOL PRESSURE AND LEVEL

As with the Main Steam Line pressure transmitter, the Suppression Chamber's absolute pressure transmitter (I-4) has an error of 0.1% of its Upper Range Value (100 psia); this results in an error of 0.1 psi. The relative error, most limiting under atmospheric conditions, would be 0.68%. The pressure in the RCIC Sparger analog's outlet was assumed to be that of the steam line as it enters the vessel en route to the outlet; this is determined by summing the Suppression Chamber's airspace pressure with the differential pressure between it and the steam line (using I-8). The DP transmitter

has an error of 0.075% URV, which at 400 inH₂O translates to 0.011 psi. Combined with the AP transmitter's error under atmospheric conditions, the relative error of the steam injection pressure is 0.684%. It should be noted that in the processing script, smoothing was used to limit the influence of pressure spikes appearing from chugging oscillations.

The level of the pool is measured with another DP transmitter (I-3), comparing the airspace pressure with the hydraulic head at the pool bottom. Its common-mode pressure issue was assumed to be resolved in data processing with a compensation curve (see Section 3.3.6), and density-based adjustments for hot levels are provided as well. Its URV of 80 inH₂O translates to an error of 0.06 inH₂O (0.166 cmH₂O). The density-correction for a hot pool is expected to be worst as the pool approaches its hot limits (before relief valve actuation); near 150 °C, use of the X-Steam steam tables revealed a partial derivative of density with respect to temperature of -0.934 kg/m³-K (with a density of 917 kg/m³). With 4 vertical temperature measurements in the pool to account for local density, a simplification of the processing algorithm for hot pool levels resembles Eq. (27).

$$z = \frac{\Delta P_{level}}{\frac{1}{4}g(\rho_{outlet} + \rho_{low} + \rho_{middle} + \rho_{upper})} \quad (27)$$

The 0.467 kg/m³ error in density at each measurement point propagates through, with the 0.166 cmH₂O error of the DP transmitter, to a final level error of 0.167 cm. With a pool level near 82 cm hot (lower when cold), this is a 0.205% relative error.

B.3 ENTHALPIES

The enthalpies of both injected two-phase steam and nearby pool water are involved in the correlation as well as their saturation conditions. This analysis takes into account heat loss when determining the enthalpy of steam in the RCIC sparger analog.

B.3.1 Heat Loss

Data recorded during Test #4 was used to estimate a heat loss coefficient for the Main Steam Line. With a room temperature of 24.9 °C and a pressure of 51.6 psia in the MSL, the steam temperature dropped from 147.3 °C at the flowmeter to 141.9 °C near the turbine analog inlet. Massflow was 46.3 g/s, and there was assumed to be no significant pressure drop between the temperature measurements. Under these conditions, the heat loss was approximately 560 W. Using a simple heat loss formulation ($\dot{Q} = H\Delta T$) with the difference between only the room temperature and steam temperature at the vortex flowmeter, H is approximately 4.58 W/K. The error in H, owing to the limited temperature difference between the upstream and downstream temperatures as well as inclusion of the mass flowrate error, is 12.969%. A $c_p = 2.21$ kJ/kg around 144.5 °C was applied to the temperature errors in the calculation. With this error in the coefficient, its use with uncertain temperatures (room temperature of 25 °C, steam of 100 °C) will result in an estimated heat loss error of 13.003%. While the relative error is large, the heat loss itself is not (560 W is less than 1% of the low-power tests' steam generator power of 57 kW).

B.3.2 Pool Subcooling

The pool subcooling enthalpy ($h_{w,sat} - h_w$) depends on local pressure and temperature. The saturation enthalpy of water increases at a rate of 1.179×10^{-3} kJ/kg-Pa around 1 bar, and c_p for water is around 4.18 kJ/kg-K. Temperature error is, as with every other thermocouple used here, 0.5 °C. Combining the temperature and pressure error (0.1 psi), the error in the subcooling enthalpy is 2.244 kJ/kg. When the pool is on the order of 25 °C subcooled, this yields a relative error of 2.148%.

B.3.3 Steam Enthalpy

At the vortex flowmeter, when steam is around 1 bar at 100 °C, the partial derivative of enthalpy with respect to pressure is -12.7 kJ/kg-bar (and closer to -7.6 kJ/kg-bar near 8 bar). With the error in the pressure measurement (0.13 psi), this results in an error in enthalpy of 0.114 kJ/kg. The c_p value for saturated steam, in the range of interest here, goes from 2.08 kJ/kg-K at 1 bar to 2.60 kJ/kg-K at 8 bar. Application of the temperature error (0.5 °C) at 8 bar yields an error of 1.30 kJ/kg. When combined (unrealistically) with the pressure contribution (value from 1 bar), the overall error in enthalpy at the vortex flowmeter is 1.305 kJ/kg.

$$h_{mix} = \frac{\dot{m}_{st} h_{st} + \dot{m}_w h_w - \dot{Q}_{loss}}{\dot{m}_{st} + \dot{m}_w} \quad (28)$$

Downstream of the vortex flowmeter, at the inlet to the turbine analog, the enthalpy of the two-phase mixture is estimated by Eq. (28). Application of Eq. (24) to Eq. (28) produces Eq. (29). For this determination, certain reference conditions are helpful. Steam will be initially be referenced to 150 °C with an enthalpy of 2758 kJ/kg,

a room temperature of 25 °C, and the flowrate will be 24 g/s steam in a single-phase test for analytical simplicity. This reduces Eq. (28) to Eq. (30):

$$\sigma_{mix}^2 = \frac{1}{(\dot{m}_s + \dot{m}_w)^2} \sigma_{\dot{Q}}^2 + \left(\frac{\dot{m}_s}{\dot{m}_s + \dot{m}_w} \right)^2 \sigma_{h_s}^2 + \left(\frac{\dot{m}_w}{\dot{m}_s + \dot{m}_w} \right)^2 \sigma_{h_w}^2 + \left[\frac{\dot{m}_w(h_s - h_w) + \dot{Q}}{(\dot{m}_s + \dot{m}_w)^2} \right]^2 \sigma_{\dot{m}_s}^2 + \left[\frac{\dot{m}_s(h_w - h_s) + \dot{Q}}{(\dot{m}_s + \dot{m}_w)^2} \right]^2 \sigma_{\dot{m}_w}^2 \quad (29)$$

$$h = h_{st} - \frac{\dot{Q}_{loss}}{\dot{m}_{st}} \quad (30)$$

At the vortex flowmeter, the steam enthalpy's error was 1.305 kJ/kg. The Badger flowmeter's two thermocouples enables registration of water enthalpy to ± 1.478 kJ/kg. To bound two-phase tests as the main steam line goes near water-solid, the 1.478 kJ/kg value will be the value applied. Here, heat loss is estimated at 572 W; this produces a loss of 23.846 ± 3.117 kJ/kg. Propagation of the initial enthalpy error brings the total error in enthalpy to 3.450 kJ/kg for Eq. (30). The full treatment from Eq. (29) for a two-phase test (the same steam conditions with 12 g/s water at 65 °C) results in $h_{mix} = 1913.559 \pm 10.769$ kJ/kg, a value greater than either saturated steam or saturated water conditions.

Pressure in the Suppression Chamber was always less than 8 bar, which has a latent heat of vaporization of 2047.67 kJ/kg; it is greater at lower pressures and will therefore be used as a minimum bounding value. Used as such, the steam quality can be determined to ± 0.00526 in the described two-phase case.

The determination of the error in the "Two-Phase Jakob Number" from Eq. (20), Ja/x_u , proceeds with additional error due to the uncertain saturation enthalpy of water.

Previously in B.3.2, the subcooling enthalpy error was found to be 2.244 kJ/kg. Inclusion of the saturation enthalpy error (0.818 kJ/kg due to pressure measurement error) brings the full condensation enthalpy (the enthalpy the two-phase saturated steam-water mixture would need to lose to bring it to fully saturate water at the same pressure) error from 10.769 to 10.800 kJ/kg. Combining this all for the two-phase case above, with an atmospheric pool, Ja_{TP} is 0.09818 ± 0.00166 (a 1.692% relative error). Warming the pool to 25 °C subcooling brings it to 0.07030 ± 0.00159 (a 2.255% relative error). This will be considered the representative relative error in Ja_{TP} moving forward.

B.4 PRESSURE BETA PARAMETER

An estimate for the error in β_p defined in Eq. (17) can be estimated for pressures around 1 bar and water temperatures near 40 °C by applying a value of dP_{sat}/dT , which ranges from 0.128 bar/°C at 150 °C, through 0.036 bar/°C at 100 °C, down to 0.00394 bar/°C at 40 °C. With a vapor pressure of 0.0738 bar, temperature error (0.5 °C) brings the relative error in computed vapor pressure to 2.666%. Bringing in the error in the measured pressure (0.684%) brings the relative error to 2.752% for everything under the radical. Including the effects of the radical follows Eq. (31), as it proceeds from Eq. (24).

$$u = x^a$$

$$\sigma_u^2 = \left(\frac{\partial u}{\partial x} \right)^2 \sigma_x^2 = (ax^{a-1})^2 \sigma_x^2 = \left(\frac{au}{x} \right)^2 \sigma_x^2 = a^2 \left(\frac{\sigma_x}{x} \right)^2 \quad (31)$$

The effect of the radical is to halve the relative error. Therefore, the relative error for β_p is 1.376%

B.5 DENSITY

Densities appear in the final form of the correlation as two density ratios. One includes two-phase steam and subcooled water, while the other density ratio is between saturated water and saturated steam.

B.5.1 Saturation Density Ratio

The density ratio of saturated water to saturated steam is a function of saturation pressure, and has its steepest changes at low pressure. Upon steam table inspection at 1 bar, the ratio is decreasing at a rate of 1553/bar from 1624. Applying the pressure measurement error, the error in the density ratio becomes 0.663%.

B.5.2 Subcooled Water Density

The density of subcooled water in the range of applicable pressures is primarily a function of temperature. At the upper range of temperatures in this experiment (150 °C), water density is 917 kg/m³ and dropping at a rate of 0.934 kg/m³-K. Use of the temperature error gives a relative error in subcooled water density of 0.0509%.

B.5.3 Two-Phase Steam Density

Steam here is treated homogeneously. Therefore, in the two-phase region, the two-phase steam density can be expressed as a function of liquid and vapor saturation densities along with the quality as shown in Eq. (32):

$$\rho_{TP} = \frac{\rho_{l,sat}\rho_{v,sat}}{x\rho_{l,sat} + (1-x)\rho_{v,sat}} \quad (32)$$

Application of Eq. (24) to Eq. (32) yields Eq. (33), which simplifies to Eq. (34):

$$\begin{aligned}
\sigma_{\rho_{TP}}^2 = & \left\{ \frac{-\rho_{l,sat}\rho_{v,sat}(\rho_{l,sat} - \rho_{v,sat})}{(x\rho_{l,sat} + (1-x)\rho_{v,sat})^2} \right\}^2 \sigma_x^2 \\
& + \left\{ \frac{\rho_{v,sat}(x\rho_{l,sat} + [1-x]\rho_{v,sat}) + x\rho_{l,sat}\rho_{v,sat}}{(x\rho_{l,sat} + [1-x]\rho_{v,sat})^2} \right\}^2 \sigma_{\rho_{l,sat}}^2 \\
& + \left\{ \frac{\rho_{l,sat}(x\rho_{l,sat} + [1-x]\rho_{v,sat}) + [1-x]\rho_{l,sat}\rho_{v,sat}}{(x\rho_{l,sat} + [1-x]\rho_{v,sat})^2} \right\}^2 \sigma_{\rho_{v,sat}}^2
\end{aligned} \tag{33}$$

$$\begin{aligned}
\left(\frac{\sigma_{\rho_{TP}}}{\rho_{TP}} \right)^2 = & \left\{ \frac{\rho_{l,sat}\rho_{v,sat}}{x\rho_{l,sat} + [1-x]\rho_{v,sat}} \right\}^2 \sigma_x^2 \\
& + \left\{ \frac{1}{\rho_{l,sat}} + \frac{x}{x\rho_{l,sat} + [1-x]\rho_{v,sat}} \right\}^2 \sigma_{\rho_{l,sat}}^2 \\
& + \left\{ \frac{1}{\rho_{v,sat}} + \frac{1-x}{x\rho_{l,sat} + [1-x]\rho_{v,sat}} \right\}^2 \sigma_{\rho_{v,sat}}^2
\end{aligned} \tag{34}$$

When the steam is superheated (no water injection), ideal gas treatments near 100 °C and 1 bar produce a relative error from pressure and temperature of 0.706%. Near 1 bar saturation pressure, the saturation density of water changes at approximately -19.9 kg/m³-bar. For steam, the rate is 0.552 kg/m³-bar. These produce water and steam saturation density relative errors of 0.0144% and 0.642%, respectively. Upon insertion into Eq. (34), at 1 bar, the relative error in wet steam density ranges from 0.526% near saturated water (x = 0) to nearly 1.22% at dry saturated steam (x = 1).

B.6 OTHER PROPERTIES

Two of the three properties which constitute the subcooled water's Prandtl number remain in the final correlation; the viscosity term drops out. The remaining ratio, c_p/k , depends largely on the water's temperature. The largest swings in the temperatures of interest happen at low temperatures. At 40 °C, the ratio has a value of 6647.286 1/Pa-

s (as estimated from application of steam tables) and is changing at a rate of -13.473 1/Pa-s-K. Applying the temperature measurement error produces a relative error of 0.101%.

B.7 CORRELATION TERMS

The final form of the correlation is expressed in 5 nondimensional groups; two of these, Ja_{TP} and the saturation density ratio, have already had their instrumentation-related relative errors derived.

B.7.1 Steam Froude Number

The Froude number from Eq. (10) can be re-expressed as Eq. (35) to utilize terms with previously defined error.

$$Fr_s = \frac{\dot{m}_{TP}}{\rho_{TP} A \sqrt{g \cdot d_{outlet}}} \quad (35)$$

The depth term is the depth of the sparger's outlet, not that of the entire pool. It takes the pool depth and subtracts 39.4 cm (the height of the outlet above the pool bottom). With a pool depth of 75 cm, the outlet would be at a depth of 35.6 cm. This readily increases the relative error to 0.469% in the depth term (the level error from B.2 is 0.167 cm). Propagation of the errors from the depth, mass flowrate (1.342%), and density (1.22%) results in a relative error of 1.828% in this Froude number.

B.7.2 Two-Phase Density Ratio

Recalling the subcooled water density relative error of 0.0509% and the wet steam density relative error of 1.219% enables quick propagation through to the relative

error of the density ratio. For the wet steam / subcooled water density ratio, this is 1.220%

B.7.3 Radical Group

The group $c_p * G * d / k$, which is the leading group in Eq. (23) and can be placed under a radical (it is raised to the power of $1/2$), is ready for its terms to have their errors propagate to the group as a whole. The result is a relative error of 1.345%, recalling the error in c_p / k (0.101%) and G (1.342%).

B.8 INCLUSION OF EXPONENTS

Each of the nondimensional groups is raised to a power that is nonunity, with the exception of the saturation density group at KP10. Some of the exponents are constant, while others vary with β_p .

B.8.1 Constant Powers

The radical group, two-phase density ratio, and saturation density ratio at KP10 all have constant exponents. Following from Eq.(31), computing their relative error is straightforward. For the radical group, the relative error becomes 0.673% (from 1.345%). The two-phase density ratio has its relative error drop to 0.610% from 1.220%. Finally, at KP10, the saturation density ratio, with a power of 1, remains at 0.663%. The KP10 value was chosen rather than KP5 or KP7 to provide an estimate that would be applicable to all the constant-power Key Points, and would not be an underestimate.

B.8.2 Variable Powers

The use of exponents with error requires another formulation for error propagation in addition to those defined previously. This formulation is shown in Eq. (32).

$$\begin{aligned}u &= x^y; \\ \sigma_u^2 &= (yx^{y-1})\sigma_x^2 + [\ln(x)]^2 \sigma_y^2; \\ \left(\frac{\sigma_u}{u}\right)^2 &= \left(y\frac{\sigma_x}{x}\right)^2 + (\ln(x)\sigma_y)^2\end{aligned}\tag{36}$$

For the parameters that have exponents with β_p , two values will be considered for β_p . One, a bounding value where $\beta_p=1$, and a more realistic value applicable to the Key Points. The realistic, nonbounding value of β_p is that of a pressure of 1 bar with a pool temperature of 40 °C; β_p is then 0.272 and the relative error computed for the parameter in B.4 is 1.376%.

The value for the Two-Phase Jakob number (which has a relative error of 2.255% as computed in B.3.3 before consideration of the exponent) is slightly unrealistic for a 1-bar pool at 40 °C, being based on a subcooling of 25 °C. Nevertheless, it shall be used as a reference point. A quirk of the value for the exponent (Ja_{TP} is raised to a power of $1 + \beta_p/16$) results in the greater β_p value slightly reducing the relative error (2.127%) when compared to the lesser value for β_p (producing 2.218% error), as it brings the exponent closer to zero than it otherwise would be. Therefore, the bounding estimate will be set to 2.218%.

The steam Froude number is estimated from a mass flowrate of 75 g/s, a pool depth of 75 cm, and a pressure of 1 bar with saturated steam. The resultant value for Fr_s

is then 51.758. Propagation of the error (1.828% in B.7.1) through with the exponents (a power of $-3/8 - \beta_p/2$) brings its final relative error to 1.190%, which increases to 3.151% in the bounding estimate.

The final term, the saturated density ratio, uses the previous reference value of 1624 from B.5.1 with a relative error of 0.663%. Its expression for the exponent changes; Key Points 2-4 use $1/4 + 3\beta_p/16$, while Key Point #10 uses a value of 1. The realistic relative error was computed to be 0.555%, while the bounding estimate increased to 1.929%.

B.9 OVERALL ESTIMATES

With the completed estimates, bounding and realistic, for each of the terms in the Mixing Number correlation (including exponents), four cases will be considered: a bounding case and a realistic case for early stages (KP2-4) and the same consideration for late stages, using KP10 as the reference formulation.

Due to constant exponents or limiting assumptions, three of the terms in the Mixing Number correlation have relative errors that do not change with stage or case. These are the radical group (0.673%), the steamflow/pool water density ratio (0.610%), and the two-phase Jakob Number (2.218%). The steam injection Froude Number has a realistic error estimate of 1.190% and a bounding value of 3.151% for early and late stages. Finally, the saturation density ratio, in late stages, has a 0.663% error in both realistic and bounding cases; early stages have a realistic estimate of 0.555% error and a bounding estimate of 1.929% relative error.

Propagation to the overall measurement error for the Mixing Number in the early stages produces a realistic estimate of 2.733%; the bounding estimate increases it to 4.359%. Late-stage error similarly ranges from a base case of 2.757% to a bounding estimate of 4.014%. Considering these four cases, in all cases the measurement error for the Mixing number should be better than 5%.

APPENDIX C
DATA PROCESSING SCRIPT

This Appendix lists the Matlab script used for processing the collected data.

C.1 GUIDELINES

In order to run, the saved data file must be loaded into memory in Matlab and stored in the 'data' array; the command

```
data = load('outputfile.dat');
```

will perform the task where outputfile.dat is the filename of the saved data file. From there, a number of parameters need to be specified. These include a name for the run, test beginning detection options (using a smoothed or instantaneous temperature), starting temperature, whether or not to save the generated figures, whether or not to put titles on the figures, whether it was an SRV or RCIC run, and a base output directory.

The run's name is set by

```
testname = 'NAME_OF_TEST';
```

where NAME_OF_TEST is the string expressing the name. The start detection conditions are set by

```
smooth_sp12 = 1;  
startingtemp = 40;
```

where the 1 tells the script to use a smoothing algorithm to detect the threshold temperature for the test beginning detection (use a value of 0 to use instantaneous temperature readings for this purpose). The value of 40 sets the threshold temperature to 40 °C; this can be set lower as in the cool-start tests. The commands to set the options for the figures are

```
savefigs = 'y';
```

```
showtitles = 0;
```

where 'y' tells the script to save the figures ('n' will instruct it to save nothing), and the 0 instructs the script to NOT place titles on the figures (useful for reports; setting it to 1 will insert titles). The remaining options, set by

```
use_turbine = 1;  
outpath = 'C:\OUTPUTDIR';
```

tell the script to process the data as a RCIC test (setting use_turbine to 0 instructs the script to process the data as an SRV run) and to save the output in the C:\OUTPUTDIR directory.

The script was written to be able to take advantage of parallel processing capabilities when available. In older versions of Matlab, the command

```
matlabpool open
```

opens up a parallel computing pool for use by the script; it can be closed after processing is complete. Before running the script, it is important to have the XSteam.m steam table function available to Matlab. Originally written by Magnus Holmgren, it returns water properties according to the IAPWS IF-97 standard, and is available for download from the MathWorks community site. With everything ready, the processing script can be invoked at the Matlab prompt with the command

```
rcic_processor
```

which can then take significant time to complete. Progress indication is given by occasional notices printed to screen as processing steps complete; the charts will appear

once processing has completed. At the termination of the script, the savefigs variable will be reset to 'n'.

Besides the figures, there is a text file generated by the script as output containing the processed results in a somewhat human-readable form. If one wishes to dump the processed numeric data into a spreadsheet, a subsequent script can be called after setting the savefigs variable to 'y'. It is invoked at the Matlab prompt with

```
spreadshout
```

and will save a more spreadsheet-friendly set of results in a separate text file elsewhere in the output directory; the savefigs option will again be reset to 'n'. Opening the file, copying, and pasting into MS-Excel will put the numbers extracted from the processed output into individual cells.

The data processing script depends on the saved data file having the correct structure. This file is a text file, containing n rows and 136 columns of numbers. Each row is for a specific point in time (set in LabVIEW to be 0.1 s apart for the current data set), and each column contains data from a specific computation. These include mean voltages over the 0.1-s period, temperatures, derived data, etc. Not every column is used by the data processing script.

The meanings of the columns in the data file recorded by LabVIEW are given in Table 13, Table 14, Table 15, Table 16, and Table 17. Cooldown mode records additional data, which is stored in subsequent additional columns in the output files. These additional columns have data as given by Table 18.

Table 13: Output File Columns 1-28

<u>Column</u>	<u>Datum</u>
1	Time, s
2	Room Temperature, C (T-1)
3	RT σ
4	Steam Generator Top Temperature, C (T-2)
5	SG T σ
6	Steam Generator Upper Temperature, C (T-3)
7	SG U σ
8	Steam Generator Middle Temperature, C (T-4)
9	SG M σ
10	Steam Generator Lower Temperature, C (T-5)
11	SG L σ
12	Steam Generator Water Injection Temperature, C (T-6)
13	SG WI σ
14	Suppression Chamber Top Flange Temperature, C (T-7)
15	SP TF σ
16	Suppression Chamber Blowdown Drum Temperature, C (T-8)
17	SP BD σ
18	SP 24 (T-9)
19	SP 24 σ
20	SP 23 (T-10)
21	SP 23 σ
22	SP 22 (T-11)
23	SP 22 σ
24	SP 21 (T-12)
25	SP 21 σ
26	SP 20 (T-13)
27	SP 20 σ
28	SP 19 (T-14)

Table 14: Output File Columns 29-56

<u>Column</u>	<u>Datum</u>
29	SP 19 σ
30	SP 18 (T-15)
31	SP 18 σ
32	SP 17 (T-16)
33	SP 17 σ
34	SP 16 (T-17)
35	SP 16 σ
36	SP 15 (T-18)
37	SP 15 σ
38	SP 14 (T-19)
39	SP 14 σ
40	SP 13 (T-20)
41	SP 13 σ
42	SP 12 (T-21)
43	SP 12 σ
44	SP 11 (T-22)
45	SP 11 σ
46	SP 10 (T-23)
47	SP 10 σ
48	SP 9 (T-24)
49	SP 9 σ
50	SP 8 (T-25)
51	SP 8 σ
52	SP 7 (T-26)
53	SP 7 σ
54	SP 6 (T-27)
55	SP 6 σ
56	SP 5 (T-28)

Table 15: Output File Columns 57-84

Column	Datum
57	SP 5 σ
58	SP 4 (T-29)
59	SP 4 σ
60	SP 3 (T-30)
61	SP 3 σ
62	SP 2 (T-31)
63	SP 2 σ
64	SP 1 (T-32)
65	SP 1 σ
66	Turbine Analog Downstream Temperature (T-33)
67	Turbine DS σ
68	Steam Line Downstream of Water Injection Temperature (T-34)
69	MSL WI DS σ
70	Pump Inlet Temperature (T-35)
71	Pump In σ
72	Pump Outlet Temperature (T-36)
73	Pump Out σ
74	Suppression Pool Outlet Temperature (T-37)
75	SP Out σ
76	Steam Line Upstream of Water Injection Temperature (T-38)
77	MSL US WI σ
78	Water Injection Line to MSL Upstream Temperature (T-39)
79	WIMSL US σ
80	Water Injection Line to MSL Downstream Temperature (T-40)
81	WIMSL DS σ
82	Main Steam Line Temperature (T-41)
83	MSL σ
84	Feedwater Temperature at Flowmeter (T-42)

Table 16: Output File Columns 85-112

<u>Column</u>	<u>Datum</u>
85	FWM σ
86	SG Pressure V (I-1)
87	SG P σ
88	SG Pressure psia
89	SG DP V (I-2)
90	SG DP σ
91	SG Level, inH2O
92	SP DP V (I-3)
93	SP DP σ
94	Suppression Pool Level cmH2O
95	SC Pressure V (I-4)
96	SC P σ
97	Suppression Chamber Pressure psia
98	Feedwater to SG V (I-5)
99	FW SG σ
100	Water Return to SG GPM
101	Water Return to SG Density kg/m ³
102	Water Return to SG Mass Flow kg/s
103	Main Steam Line Vortex Flowmeter V (I-6)
104	MSL VF σ
105	Steam Density, kg/m ³
106	Corrected K Factor
107	Steam Flow Rate, kg/s
108	Main Steam Line Pressure V (I-7)
109	MSL P σ
110	MSL Pressure psia
111	RCIC Turbine Outlet-SP DP V (I-8)
112	RCIC TO-SP DP σ

Table 17: Output File Columns 113-136

Column	Datum
113	Turbine Outlet-SP DP inH2O
114	Pump Discharge GP V (I-9)
115	Pump Out GP σ
116	RCIC Pump Outlet Pressure psig
117	SC GP V (I-10)
118	SC GP σ
119	Suppression Chamber Gauge Pressure psig
120	Turbine Outlet GP V (I-11)
121	TO GP σ
122	Turbine Outlet Gauge Pressure psig
123	Water Injection to Steam Line V (I-12)
124	WISL σ
125	WISL GPM
126	WISL Water Density kg/m ³
127	Water Injection to Steam Line Mass Flowrate kg/s
128	Main Steam Line GP V (I-13)
129	MSL GP σ
130	Main Steam Line Gauge Pressure, psig
131	Pump Cavitation Sensor V (not present)
132	Pump CS σ
133	Pump Cavitation Sensor Placeholder (unused)
134	Pump Inlet GP V (I-14)
135	Pump Inlet GP σ
136	Pump Inlet Gauge Pressure, psi

Table 18: Additional Cooldown Output File Columns

<u>Additional Column</u>	<u>Datum</u>
1	Hot Water Tank Outlet Temperature, C (T-43)
2	HWTO σ
3	Between Hot Water Pumps Temperature, C (T-44)
4	BHWP σ
5	Hot Water Tank Magnetic Flowmeter (I-16)
6	HWTMF σ
7	Hot Water Tank Outlet Flowrate, GPM
8	Hot Water Tank Level GP (I-15)
9	HWTL σ
10	Hot Water Tank Flow-Corrected Level, inches

C.2 SOURCE – RCIC_PROCESSOR.M

```
% Matlab script rcic_plots_rcicland.m
% Makes plots for a pre-loaded output data file from the RCIC LabVIEW
% program. The array to load is 'data', which is n x 136. n is
% expected to be huge, having recorded a full output set of 136 values 10
% times per second for hours.
% Here, a full set of analysis is performed and plots are generated that
% should be comprehensible in B&W with the markers applied to the lines

%
% =====
% DATA PREPARATION SECTION
% =====
%

outstring=[];
filehandle=[];
crlf = sprintf('\r\n');
spargeroffset = -4.0956; % offset, inH2O, for Sparger DP transmitter
% reading as gathered from mean(mar13(1:9000,113))
disp(' ')
disp('Welcome to RCIC - LAND !')

% Determine export condition
if (strcmp(testname, '') == 0) && strcmp(savefigs, 'y') && (strcmp(outpath, '') == 0)
    % save the figures to disk
    outdir = [outpath '\Export\' testname '\'];
    disp(['Saving Text and JPEG Files to ' outdir])
    mkdir(outdir);
    disp(' ')
    save_em=1;
    filehandle=fopen([outdir testname ' results_rcicland.txt'], 'w+');
    fprintf(filehandle, '%s\r\n', ['Output Saved to ' outdir]);
    mfigoutdir = [outpath '\Mfigs\' testname '\'];
    disp(['Saving MATLAB Figure Files to ' mfigoutdir])
    mkdir(mfigoutdir);
```

```

else
    save_em=0;
    disp('Not Saving Figures to Disk')
end

% Determine the beginning and end times

% Test Begins when SP12 first hits 40 degrees C
% Test Ends one minute before the steam flowrate drops below 10 g/s
foundbeg=0;
foundend=0;
indices=[1201, size(data, 1)-1200];

% Some, esp. SRV, tests make initial noises on SP 12 that can trigger a
% premature test beginning
% If so, a 20-second mean value can be used instead of the instantaneous
% value for SP 12
begintemps=data(:, 42);
if smooth_sp12 == 1
    % use smoothing
    outstring = 'Using 20-second SP 12 averages for beginning detection';
    disp(outstring)
    if save_em == 1
        fprintf(filehandle, '%s\r\n', outstring);
    end
    for index = 101:(size(data,1)-100)
        begintemps(index)=mean(data(index-100:index+100, 42));
    end
else
    % do not use smoothing
    outstring = 'Using instantaneous 0-s SP 12 values for beginning detection';
    disp(outstring)
    if save_em == 1
        fprintf(filehandle, '%s\r\n', outstring);
    end
    begintemps=data(:,42);
end

for index=1201:size(data, 1)-1200
    if begintemps(index) >= startingtemp
        if foundbeg == 0
            % found beginning
            foundbeg=1;
            indices(1)=index;
        end
    end
    if (foundbeg == 1) && (foundend == 0)
        % check to see if end has been found
        if data(index, 107) <= 0.01
            % found end
            foundend=1;
            indices(2)=index;
        end
    end
end
end
trunind = indices(1);
if foundend == 1
    % found end signal
    % step back to end limit one minute before signal
    for index=indices(2): -1: 1
        if data(index,1) <= (data(indices(2),1) - 60)
            % found the correct end
            break
        end
    end
end
else

```

```

    index = size(data,1)-1200;
end

trunind = [trunind index indices(2)];
% set up trimmed data array

trmdat=data(indices(1):index,:);
trmdat(:,1) = trmdat(:,1) - data(indices(1),1);

% set up expanded trimmed array for regression through both ends
trmreg = data( (indices(1)-1200) : (index+1200), :);
trmreg(:,1) = trmreg(:,1) - data(indices(1),1);

% Time data is in Column 1.

t=trmdat(:,1);

if foundbeg == 0
    outstring='Beginning NOT detected, using t_first';
    disp(outstring)
    if save_em == 1
        fprintf(filehandle, '%s\r\n', outstring);
    end
end

if foundend == 0
    outstring='End NOT detected, using t_final';
    disp(outstring)
    if save_em == 1
        fprintf(filehandle, '%s\r\n', outstring);
    end
end

outstring=['Beginning (KEY POINT #1) detected at t plus ' num2str(data(indices(1),1)) ' s,
    and ending (KEY POINT #11) at t plus ' num2str(data(index,1)) ' s, for a time
    period of ' num2str(t(end)) ' s.'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

outstring=['Original Data Record Time: ' num2str(data(end,1)) ' s'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

%
% =====
% DATA PROCESSING SECTION
% =====
%

% initialize the Key Points Vector
ind_end = length(t);
keypoints_ind = [1, ind_end, ind_end, ind_end, ind_end, ind_end, ind_end, ind_end,
    ind_end, ind_end, ind_end, ind_end, ind_end, ind_end];
% Beginning Key Point
keypoints_ind(1) = 1;
% Ending Key Point
keypoints_ind(11) = ind_end;

% Test Start, Plume Detection, Stratification Onset, Peak Top-Mid, Top-Mid
% Reconverge, Peak Mid-Low, Mid-Low reconverge, Peak Low-Out,
% Stratification End, Test End, Min Mixing Number, Max Mixing Number

```



```

% Initialize the Pool Level Offset Correction Routine
% data gathered in 2015_05_19_test2_pressures.dat
% The following was used to generate the coefficients
% linear extrapolation was used on both the high-pressure and low-pressure
% ends in order to extend the approximate valid range
%
% The approximate valid range is from ~13 to ~103 psia (gas space pressure)
% in the Suppression Chamber
%
%
% pressurelevelcurve = load('..\Data\2015_05_19_test2_pressures.dat');
% [n,ind] = min( pressurelevelcurve(1:23670,97));
% unsorteddx = [n; pressurelevelcurve(1240:23670,97)];
% unsortedy = [(pressurelevelcurve(ind,94) - pressurelevelcurve(ind,94));
% (pressurelevelcurve(1240:23670,94) - pressurelevelcurve(ind,94))];
% c3 = polyfit(unsorteddx(1:500), unsortedy(1:500), 1);
% c2 = polyfit(unsorteddx(5761:11760), unsortedy(5761:11760), 1);
% low_y = polyval(c3, [10; 10.5; 11; 11.5; 12; 12.5; 13; 13.5; 14]);
% high_y = polyval(c2, [101; 101.5; 102; 102.5; 103; 103.5; 104; 104.5; 105]);
% coeffs = polyfit([10; 10.5; 11; 11.5; 12; 12.5; 13; 13.5; 14; unsorteddx; 101; 101.5;
% 102; 102.5; 103; 103.5; 104; 104.5; 105], [low_y; unsortedy; high_y], 21);
%
% The instrument repots 0 cm when the fill is at or below 7.62 cm (to the
% very bottom) -- its bottom pickup is at z = 7.62 cm (the offsets will be
% subtracted from the indication/reading)
pool_levelgauge_offset = -7.62;

pool_level_offset_coeffs = zeros(1,22);

pool_level_offset_coeffs(01) = -4.704607582712959e-33;
pool_level_offset_coeffs(02) = 2.276830460057674e-30;
pool_level_offset_coeffs(03) = 7.536374883715246e-28;
pool_level_offset_coeffs(04) = -1.026160591394114e-24;
pool_level_offset_coeffs(05) = 4.494410880292239e-22;
pool_level_offset_coeffs(06) = -1.196603784791618e-19;
pool_level_offset_coeffs(07) = 2.229530134698593e-17;
pool_level_offset_coeffs(08) = -3.091202409527790e-15;
pool_level_offset_coeffs(09) = 3.296650614743879e-13;
pool_level_offset_coeffs(10) = -2.756730928255758e-11;
pool_level_offset_coeffs(11) = 1.827364042074039e-09;
pool_level_offset_coeffs(12) = -9.651355766825126e-08;
pool_level_offset_coeffs(13) = 4.063655352840353e-06;
pool_level_offset_coeffs(14) = -1.359106037748376e-04;
pool_level_offset_coeffs(15) = 0.003582795870262;
pool_level_offset_coeffs(16) = -0.073514262386104;
pool_level_offset_coeffs(17) = 1.152395400243147;
pool_level_offset_coeffs(18) = -13.428940832825903;
pool_level_offset_coeffs(19) = 1.116385190403100e+02;
pool_level_offset_coeffs(20) = -6.195804714026652e+02;
pool_level_offset_coeffs(21) = 2.032312773917644e+03;
pool_level_offset_coeffs(22) = -2.931852420874044e+03;

% Determine Pool Saturation Temperatures
poolsat=t;
for index=1:size(poolsat,1)
    poolsat(index)=XSteam('Tsat_p', trmdat(index, 97)*0.0689475728);
end

% Then smooth the rear temperatures
stratsmooth_0 = zeros(size(trmreg,1)-2400, 1); % time
stratsmooth_1 = stratsmooth_0; % Upper

```

```

stratsmooth_2 = stratsmooth_0; % Lower
stratsmooth_3 = stratsmooth_0; % Condensing SP8
stratsmooth_4 = stratsmooth_0; % Mid SP9
stratsmooth_5 = stratsmooth_0; % Out
midsmooth_up = stratsmooth_0; % SP 11
midsmooth_mid = stratsmooth_0; % SP 12
midsmooth_low = stratsmooth_0; % SP 13
smoothwater = stratsmooth_0; % water injection to steam line
smoothedP = stratsmooth_0;
smoothedDP = smoothedP;
smoothedMSLP = stratsmooth_0;
smoothedMSLT = stratsmooth_0;
smoothedMSLmdot = stratsmooth_0;
smoothedwaterT = stratsmooth_0;
smoothedRoomT = stratsmooth_0;
steamenthreg = stratsmooth_0;
smoothedMSLEnth = stratsmooth_0;
MTMDeltaT = stratsmooth_0;
MMLDeltaT = stratsmooth_0;
MLODeltaT = stratsmooth_0;
% Regression analysis
disp('Smoothing 1, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % time
    stratsmooth_0(relind) = trmreg(index, 1);
    % compute and store smoothed temps
    % rear upper SP 3
    p1 = polyfit(x, trmreg( (index-300) : (index+300), 60), 1);
    stratsmooth_1(relind) = p1(2);
end
disp('Smoothing 2, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % rear lower SP 5
    p2 = polyfit(x, trmreg( (index-300) : (index+300), 56), 1);
    stratsmooth_2(relind) = p2(2);
end
disp('Smoothing 3, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % near exhaust/middle SP 8
    p3 = polyfit(x, trmreg( (index-300) : (index+300), 50), 1);
    stratsmooth_3(relind) = p3(2);
end
disp('Smoothing 4, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % further from exhaust/middle SP 9
    p4 = polyfit(x, trmreg( (index-300) : (index+300), 48), 1);
    stratsmooth_4(relind) = p4(2);
end
disp('Smoothing 5, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % pool outlet
    p5 = polyfit(x, trmreg( (index-300) : (index+300), 74), 1);

```

```

        stratsmooth_5(relind) = p5(2);
end
disp('Smoothing 6, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % water injection to steamline kg/s
    p5 = polyfit(x, trmreg( (index-300) : (index+300), 127), 1);
    smoothwater(relind) = p5(2);
end
disp('Smoothing 7, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % Suppression Pool P, psia
    p5 = polyfit(x, trmreg( (index-300) : (index+300), 97), 1);
    smoothedP(relind) = p5(2);
end
disp('Smoothing 8, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % Instead of 1-minute values, 2-minute values are used here to really
    % smooth out the effects of the chugging spikes (+/- 1 minute,
    % shouldn't go further out than that due to the stopping criterion)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-600) : (index+600), 1) - trmreg(index,1);
    % Sparger DP, inH2O (should eliminate chugging oscillations)
    p5 = polyfit(x, trmreg( (index-600) : (index+600), 113) - spargeroffset, 1);
    smoothedDP(relind) = p5(2);
end
% P in the line upstream of the sparger, bar absolute
spargerP = (0.0689475728 * smoothedP) + (0.0024884 * smoothedDP);
disp('Smoothing 9, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % Steam Line P, psia
    p5 = polyfit(x, trmreg( (index-300) : (index+300), 110), 1);
    smoothedMSLP(relind) = p5(2);
end
disp('Smoothing 10, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % Steam Line T, degrees C
    p5 = polyfit(x, trmreg( (index-300) : (index+300), 82), 1);
    smoothedMSLT(relind) = p5(2);
end
disp('Smoothing 11, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % Steam Flowrate, kg/s
    p5 = polyfit(x, trmreg( (index-300) : (index+300), 107), 1);
    smoothedMSLmdot(relind) = p5(2);
end
disp('Smoothing 12, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % Water Injection to Steam Line Temperature, C

```

```

    p5 = polyfit(x, 0.5 * (trmreg( (index-300) : (index+300), 78) + trmreg( (index-
        300) : (index+300), 80)), 1);
    smoothedwaterT(relind) = p5(2);
end
disp('Smoothing 13, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % Lab Temperature, C
    p5 = polyfit(x, (trmreg( (index-300) : (index+300), 2)), 1);
    smoothedRoomT(relind) = p5(2);
end
disp('Smoothing 14, ...')
parfor relind = 1: (size(trmreg,1))
    % get source data and compute immediate MSL enthalpy at the flowmeter
    s_enth=XSteam('h_pT', trmreg(relind, 110)*0.0689475728, trmreg(relind, 82));
    steamenthreg(relind) = s_enth;
end
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % Steam Flowrate, kg/s
    p5 = polyfit(x, (steamenthreg( (index-300) : (index+300) )), 1);
    smoothedMSLEnth(relind) = p5(2);
end
disp('Smoothing 15, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % Pool Mid-Axis Top-Mid Smoothed Delta T
    p5 = polyfit(x, (trmreg( (index-300) : (index+300), 44) - trmreg( (index-300) :
        (index+300), 42)), 1);
    MTMDeltaT(relind) = p5(2);
end
disp('Smoothing 16, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % Pool Mid-Axis Mid-Low Smoothed Delta T
    p5 = polyfit(x, (trmreg( (index-300) : (index+300), 42) - trmreg( (index-300) :
        (index+300), 40)), 1);
    MMLDeltaT(relind) = p5(2);
end
disp('Smoothing 17, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % Pool Mid-Axis Mid-Low Smoothed Delta T
    p5 = polyfit(x, (trmreg( (index-300) : (index+300), 40) - trmreg( (index-300) :
        (index+300), 74)), 1);
    MLODeltaT(relind) = p5(2);
end
disp('Smoothing 18, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % SP 11 Temperatures
    p5 = polyfit(x, (trmreg( (index-300) : (index+300), 44)), 1);
    midsmooth_up(relind) = p5(2);
end
disp('Smoothing 19, ...')

```

```

parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % SP 12 Temperatures
    p5 = polyfit(x, (trmreg( (index-300) : (index+300), 42)), 1);
    midsmooth_mid(relind) = p5(2);
end
disp('Smoothing 20, ...')
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index,1);
    % SP 13 Temperatures
    p5 = polyfit(x, (trmreg( (index-300) : (index+300), 40)), 1);
    midsmooth_low(relind) = p5(2);
end

disp('Correcting Pool Levels...')
% compute the commone-mode pressure reading offset:
leveloffsets = polyval(pool_level_offset_coeffs, trmreg(:, 97));
% remove the offsets from the reading
reglevels = trmreg(:, 94) - leveloffsets - pool_levelgauge_offset;
% smooth it to get cold levels
coldlevels = stratsmooth_0;
hotdepth = stratsmooth_0;
parfor relind = 1: (size(trmreg,1)-2400)
    % get source data
    index = relind + 1200;
    x = trmreg( (index-300) : (index+300), 1) - trmreg(index, 1);
    % Pool Water Level, cm
    p5 = polyfit(x, (reglevels( (index-300) : (index+300) ) ), 1);
    % find the cold-water level
    coldlevels(relind) = p5(2);
    currentlevel = p5(2);
    % translate to hot (around measured T) levels
    sgref = 999.9720; % peak density at 1 atm, 4 degrees C
    sgref_out = XSteam('rho_pT', (smoothedP(relind)*0.0689475728 + 0.100),
        stratsmooth_5(relind)) / sgref;
    sgref_low = XSteam('rho_pT', (smoothedP(relind)*0.0689475728 + 0.055),
        midsmooth_low(relind)) / sgref;
    sgref_mid = XSteam('rho_pT', (smoothedP(relind)*0.0689475728 + 0.037),
        midsmooth_mid(relind)) / sgref;
    sgref_top = XSteam('rho_pT', (smoothedP(relind)*0.0689475728 + 0.020),
        midsmooth_up(relind)) / sgref;
    sgtopmid = 0.5 * (sgref_top + sgref_mid);
    sgmidlow = 0.5 * (sgref_mid + sgref_low);
    sglowout = 0.5 * (sgref_low + sgref_out);

    % determine the heated level (cm) of the pool
    if 8*2.54*sglowout + 7*2.54*sgmidlow + 7*2.54*sgtopmid <= currentlevel
        % level is above the top thermocouple
        hotdepth(relind) = ((currentlevel - ( (8*2.54*sglowout) + (7*2.54*sgmidlow) +
            (7*2.54*sgtopmid) ) ) / sgref_top) + ( (8*2.54*sglowout) + (7*2.54*sgmidlow) +
            (7*2.54*sgtopmid) );
    elseif 8*2.54*sglowout + 7*2.54*sgmidlow <= currentlevel
        % level is between the top and mid thermocouple
        hotdepth(relind) = ((currentlevel - ( (8*2.54*sglowout) + (7*2.54*sgmidlow) ) ) /
            sgref_mid) + ( (8*2.54*sglowout) + (7*2.54*sgmidlow) );
    elseif 8*2.54*sglowout <= currentlevel
        % level is between the mid and low thermocouple
        hotdepth(relind) = ((currentlevel - (8*2.54*sglowout)) / sgref_low) +
            (8*2.54*sglowout);
    else
        % level is between the low thermocouple and outlet
        hotdepth(relind) = currentlevel / sgref_out;
    end
end

```

```

end

% do one more iteration for pre-start readings, unsmoothed readings

% find the cold-water level
coldlevelprestart = data(1, 94) - pool_levelgauge_offset -
    polyval(pool_level_offset_coeffs, data(1, 97));
currentlevel = coldlevelprestart;
hotlevelprestart = coldlevelprestart;
% translate to hot (around measured T) levels
sgref = 999.9720; % peak density at 1 atm, 4 degrees C
sgref_out = XSteam('rho_pT', (data(1,97)*0.0689475728 + 0.100), data(1,74)) / sgref;
sgref_low = XSteam('rho_pT', (data(1,97)*0.0689475728 + 0.055), data(1,40)) / sgref;
sgref_mid = XSteam('rho_pT', (data(1,97)*0.0689475728 + 0.037), data(1,42)) / sgref;
sgref_top = XSteam('rho_pT', (data(1,97)*0.0689475728 + 0.020), data(1,44)) / sgref;
sgtopmid = 0.5 * (sgref_top + sgref_mid);
sgmidlow = 0.5 * (sgref_mid + sgref_low);
sglowout = 0.5 * (sgref_low + sgref_out);

% determine the heated level (cm) of the pool
if 8*2.54*sglowout + 7*2.54*sgmidlow + 7*2.54*sgtopmid <= currentlevel
    % level is above the top thermocouple
    hotlevelprestart = ((currentlevel - ( 8*2.54*sglowout) + (7*2.54*sgmidlow) +
        (7*2.54*sgtopmid) ) ) / sgref_top) + ( (8*2.54*sglowout) + (7*2.54*sgmidlow) +
        (7*2.54*sgtopmid) );
elseif 8*2.54*sglowout + 7*2.54*sgmidlow <= currentlevel
    % level is between the top and mid thermocouple
    hotlevelprestart = ((currentlevel - ( 8*2.54*sglowout) + (7*2.54*sgmidlow) ) ) /
        sgref_mid) + ( (8*2.54*sglowout) + (7*2.54*sgmidlow) );
elseif 8*2.54*sglowout <= currentlevel
    % level is between the mid and low thermocouple
    hotlevelprestart = ((currentlevel - (8*2.54*sglowout)) / sgref_low) +
        (8*2.54*sglowout);
else
    % level is between the low thermocouple and outlet
    hotlevelprestart = currentlevel / sgref_out;
end

% Determine Stratification Period
disp('Examining Pool Stratification...')
stratstart=[-1 -1];
stratend= [-1 -1];

comptemps = [trmreg(:,1), (trmreg(:,44) + trmreg(:,42) + trmreg(:,40))/3, trmreg(:,74)];
pooldt = zeros(size(comptemps,1),1);
poolt=pooldt;
outletdt = poolt;
outlett=outletdt;
% Regression analysis
disp('Processing, 1...')
parfor index = 601: (size(comptemps,1)-600)
    % get source data
    x = comptemps( (index-600) : (index+600), 1) - trmreg(index,1);
    y = comptemps( (index-600) : (index+600), 2:3);
    % compute and store smoothed temps
    p1 = polyfit(x,y(:,1),1);
    p2 = polyfit(x,y(:,2),1);
    % pooldt(index)=p1(1);
    poolt(index)=p1(2);
    % outletdt(index) = p2(1);

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```

        outlett(index)=p2(2);
    end
    disp('Processing, 2...')
    parfor index = 901: (size(comptemps,1)-900)
        % get source data
        x = comptemps( (index-900) : (index+900), 1) - trmreg(index,1);
        y = [poolt( (index-900) : (index+900) ), outlett( (index-900) : (index+900) )];
        % compute and store dT/dt
        p1 = polyfit(x,y(:,1),1);
        p2 = polyfit(x,y(:,2),1);
        pooltdt(index)=p1(1);
        % poolt(index)=p1(2);
        outletdt(index) = p2(1);
        % outlett(index)=p2(2);
    end

    %average the slopes
    m1 = zeros(size(comptemps,1),1);
    m2 = zeros(size(comptemps,1),1);
    disp('Analyzing...')
    parfor index = 901: (size(comptemps,1)-900)
        m1(index)=mean(pooltdt((index-300): (index+300)));
        m2(index)=mean(outletdt((index-300): (index+300)));
    end
    onsets=zeros(size(comptemps,1),1);
    endsets=onsets;
    unsets=endsets;
    checkunsets=0;
    unsetind=0;
    % determine onset of stratification
    for index = 1201: (size(comptemps,1)-1200)
        if (poolt(index) - outlett(index) >= 2) && ( m2(index) <= 0.75 * m1(index) )
            % could be stratifying
            onsets(index)=1;
        end
        % check for high rate of change
        if ( m2(index) >= 0.95 * m1(index) )
            % might not be stratifying
            unsets(index)=1;
        end
    end
    beg_ind=0;
    stratified=0;
    destratified=0;
    end_ind=0;
    for index = 1: size(onsets,1)
        if stratified == 0
            % find the defined onset
            if (onsets(index) == 0)
                % nope
                beg_ind=0;
            elseif beg_ind == 0
                % start counting
                beg_ind = index;
            else
                % check if duration long enough
                if (comptemps(index,1) - comptemps(beg_ind,1) >= 60)
                    %maybe stratified, check unsets
                    % stratified
                    stratified=1;
                    unsetind=index;
                end
            end
        end
        elseif checkunsets == 0
            if unsets(index) == 0
                if (comptemps(index,1) - comptemps(unsetind,1) >= 180)
                    % stratified

```

```

        checkunsets=1;
    end
else
    % rose too high, not stratified
    stratified = 0;
end
elseif destratified == 0
    % find end of stratification
    if (outletdt(index) >= 2 * pooldt(index))
        % maybe destratifying
        endsets(index) = 1;
        if end_ind == 0
            %start counting
            end_ind = index;
        else
            %check counter
            if (comptemps(index,1) - comptemps(end_ind,1) >= 60)
                % destratifying
                destratified=1;
            end
        end
    else
        % not destratifying
        end_ind = 0;
        endsets(index) = 0;
    end
else
    if (outletdt(index) >= 2 * pooldt(index))
        % maybe destratifying
        endsets(index) = 1;
    else
        % not destratifying
        endsets(index) = 0;
    end
end
end

if stratified == 1
    % translate to the trimmed data
    stratstartind = beg_ind - 1200;
    if destratified == 1
        stratendind = end_ind - 1200;
    else
        % sort of a dummy value
        stratendind = size(trmdat, 1);
    end
else
    % dummy value
    stratstartind = size(trmdat, 1);
    stratendind = stratstartind;
end

% store indices in the Key Points
keypoints_ind(3) = stratstartind;
keypoints_ind(9) = stratendind;

if stratified == 1
    outstring=['Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT
    #3) at t plus ' num2str(comptemps(beg_ind, 1)) ' s, T_bulk = '
    num2str(comptemps(beg_ind, 2)) ' C and T_out = ' num2str(comptemps(beg_ind, 3)) '
    C'];
    outstring = [outstring crlf 'Stratification Beginning SP12 Temperature = '
    num2str(trmdat(beg_ind - 1200, 42)) ' C'];
    outstring = [outstring crlf 'Stratification Beginning Pressure = '
    num2str(trmdat(beg_ind - 1200, 97)) ' psia'];
else

```



```

        outstring = 'No Bulk Pool to Outlet Thermal Stratification Detected (KEY POINT #3), 0
            0 0 0 0 0. ';
    end
    disp(outstring)
    if save_em == 1
        fprintf(filehandle, '%s\r\n', outstring);
    end

    if destratified == 1
        outstring = ['Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY
            POINT #9) at t plus ' num2str(comptemps(end_ind, 1)) ' s, T_bulk = '
            num2str(comptemps(end_ind, 2)) ' C and T_out = ' num2str(comptemps(end_ind, 3)) '
            C'];
        outstring = [outstring crlf 'Stratification Ending SP12 Temperature = '
            num2str(trmdat(end_ind - 1200, 42)) ' C'];
        outstring = [outstring crlf 'Stratification Ending Pressure = '
            num2str(trmdat(end_ind - 1200, 97)) ' psia'];
    else
        outstring = 'No Bulk Pool to Outlet Destratification Detected (KEY POINT #9), 0 0 0 0
            0 0. ';
    end
    disp(outstring)
    if save_em == 1
        fprintf(filehandle, '%s\r\n', outstring);
    end

    outstring='Detecting Plume Appearance...';
    disp(outstring)
    plume_ind = length(t);
    outstring = ['No Plume detected, setting t_plume (KEY POINT #2) to the end at '
        num2str(t(plume_ind)) ' s. '];

    for ind = 1:length(t) - 600
        % using smoothed temps, for each of the current and subsequent 600
        % points, if the hotspot temperature is greater than the upper level
        % temperature by more than one degree AND MORE THAN 2 DEGREES greater
        % than the mid-level temperature, a plume is assumed to be present
        if (sum( (stratsmooth_3(ind:ind+600) - stratsmooth_4(ind:ind+600)) > 2) == 601) &&
            (sum( (stratsmooth_3(ind:ind+600) - stratsmooth_1(ind:ind+600)) > 1) == 601)
            % detected plume formation!
            plume_ind = ind;
            outstring = ['Plume detected! Setting t_plume (KEY POINT #2) to '
                num2str(t(plume_ind)) ' s. '];
            break
        end
    end
    end

    keypoints_ind(2) = plume_ind;

    avppcrdt = mean(stratsmooth_3(plume_ind:stratendind) -
        stratsmooth_4(plume_ind:stratendind));
    avppcrdtsd = std(stratsmooth_3(plume_ind:stratendind) -
        stratsmooth_4(plume_ind:stratendind));
    avpptrdt = mean(stratsmooth_3(plume_ind:stratendind) -
        stratsmooth_1(plume_ind:stratendind));
    avpptrdtsd = std(stratsmooth_3(plume_ind:stratendind) -
        stratsmooth_1(plume_ind:stratendind));
    if isinf(avppcrdt) || isnan(avppcrdt)
        avppcrdt = 0;
    end
    if isinf(avppcrdtsd) || isnan(avppcrdtsd)
        avppcrdtsd = 0;
    end
    if isinf(avpptrdt) || isnan(avpptrdt)
        avpptrdt = 0;
    end

```

```

end
if isinf(avpptrdtsd) || isnan(avpptrdtsd)
    avpptrdtsd = 0;
end
outstring = [outstring crlf 'At t = ' num2str(t(plume_ind)) ' s, the pool pressure is '
    num2str(trmdat(plume_ind, 97)) ' psia while the Smoothed Upper, Mid, SP8, Lower,
    and Outlet Temperatures are ' num2str(stratsmooth_1(plume_ind)) ', '
    num2str(stratsmooth_4(plume_ind)) ', ' num2str(stratsmooth_3(plume_ind)) ', '
    num2str(stratsmooth_2(plume_ind)) ', and ' num2str(stratsmooth_5(plume_ind)) ' C,
    respectively. ' ];
outstring = [outstring crlf 'Over the Plume Period (Plume Detected to Destratification),
    the mean Smothed SP8-SP9 temperatures were ' num2str(avppcrdt) ' +/- '
    num2str(avppcrdtsd) ' C.'];
outstring = [outstring crlf 'Over the Plume Period (Plume Detected to Destratification),
    the mean Smoothed SP8-Upper temperatures were ' num2str(avpptrdt) ' +/- '
    num2str(avpptrdtsd) ' C.'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

outstring='Processing Enthalpies and Steam Quality...';
disp(outstring)

% time, steam_enth, steam_sat_enth, water_enth, water_sat_enth,
% mixture_enth, quality, turbine_hg, turbine_hl, turbine_quality
steamarray=[t t t t t t t t];
smoothedenth = [t t];
velocities = 0*[t t t];
smoothedenthtemp = smoothedenth;
steamarraytemp = steamarray;
hsteam = t;
htop = hsteam;
hmid = hsteam;
hcondensing = hsteam;
hlow = hsteam;
hout = hsteam;
hmidsat = hsteam;
rhomid = hsteam;
rhocond = hsteam;
mdcond = hsteam;
mdcondcool = hsteam;
mdcondvol = mdcond;
mdcondcoolvol = mdcondcool;
mdcondinj = hsteam;
mdcondinjcool = hsteam;
mdcondinjvol = mdcond;
mdcondcoolinjvol = mdcondcool;
smoothwaterh = smoothwater;
hsatL = [t t];
hsatG = [t t];
if mean(smoothwater) > 0.001
    % water-injected test
    twophasetest = 1;
else
    % steam only
    twophasetest = 0;
end
hlcoeff=4.57841; % W/K (MSL T to Room T, from V Flowmeter to DS of W Inj.)
% do the calculations
parfor index=1:size(steamarray,1)
    % enthalpy at water injection
    s_enth=smoothedMSLEnth(index);
    steamarray(index,2) = s_enth - (hlcoeff * (smoothedMSLT(index)-smoothedRoomT(index))
        / (1000*smoothedMSLmdot(index)) );
end

```

```

htop(index) = XSteam('h_pT', (smoothedP(index)*0.0689475728 + 0.020),
    stratsmooth_1(index));
hmid(index) = XSteam('h_pT', (smoothedP(index)*0.0689475728 + 0.037),
    stratsmooth_4(index));
hlow(index) = XSteam('h_pT', (smoothedP(index)*0.0689475728 + 0.055),
    stratsmooth_2(index));
hout(index) = XSteam('h_pT', (smoothedP(index)*0.0689475728 + 0.100),
    stratsmooth_5(index));
hcondensing(index) = XSteam('h_pT', (smoothedP(index)*0.0689475728 + 0.037),
    stratsmooth_3(index));
hmidsat(index) = XSteam('hL_p', (smoothedP(index)*0.0689475728 + 0.037));
rhomid(index) = XSteam('rho_pT', (smoothedP(index)*0.0689475728 + 0.037),
    stratsmooth_4(index));
rhocond(index) = XSteam('rho_pT', (smoothedP(index)*0.0689475728 + 0.037),
    stratsmooth_3(index));
% steam pre-injection velocities
steamrho = XSteam('rho_ph', smoothedMSLP(index)*0.0689475728, s_enth);
velocities(index, 1) = (smoothedMSLmdot(index) / steamrho) / (pi() * (0.020447^2));
% saturation enthalpies, DS of orifice
hsatL(index, 2) = XSteam('hL_p', spargerP(index));
hsatG(index, 2) = XSteam('hV_p', spargerP(index));
end
parfor index=1:size(steamarray,1)
    % saturated steam enthalpy (MSL pressure)
    steamarray(index,3) = XSteam('hV_p', smoothedMSLP(index)*0.0689475728);
    hsatG(index, 1) = steamarray(index,3);
end
parfor index=1:size(steamarray,1)
    % estimated liquid enthalpy (DS measurement)
    steamarray(index,4) = XSteam('h_pT', smoothedMSLP(index)*0.0689475728,
        trmdat(index,80));
    smoothwaterh(index) = XSteam('h_pT', smoothedMSLP(index)*0.0689475728,
        smoothedwaterT(index));
    % water pre-injection velocities
    waterrho = XSteam('rho_ph', smoothedMSLP(index)*0.0689475728, smoothwaterh(index));
    velocities(index, 2) = (smoothwater(index) / waterrho) / (pi() * (0.004625^2));
end
parfor index=1:size(steamarray,1)
    % saturated liquid enthalpy (MSL pressure)
    steamarray(index,5) = XSteam('hL_p', smoothedMSLP(index)*0.0689475728);
    hsatL(index, 1) = steamarray(index,5);
end
parfor index=1:size(steamarray,1)
    % MSL flow enthalpy post-injection
    steamarraytemp(index,6) = (steamarray(index,2)*trmdat(index,107) +
        steamarray(index,4)*trmdat(index,127)) / (trmdat(index,107) + trmdat(index,127));
    smoothedenth(index, 1) = (steamarray(index,2)*smoothedMSLmdot(index) +
        twophasetest*smoothwaterh(index)*smoothwater(index)) / (smoothedMSLmdot(index) +
        twophasetest*smoothwater(index));
end
steamarray(:,6) = steamarraytemp(:,6);

%total flow energy, including velocities
if twophasetest == 1
    % include water E
    TotalEnth = smoothedenth(:, 1) + (0.001*(((velocities(:,1).^2) .* smoothedMSLmdot) +
        ((velocities(:,1).^2) .* smoothwater)) ./ (smoothedMSLmdot + smoothwater));
else
    % steam only
    TotalEnth = smoothedenth(:, 1) + 0.001*(velocities(:,1).^2);
end

% Determine new (including flow energy) enthalpies US&DS of turbine analog
%
sparger_area = (pi() * (0.020447^2));
AdjustedEnth_US = 0 * TotalEnth;
AdjustedEnth_DS = 0 * TotalEnth;

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```

tempvels1 = t;
tempvels2 = t;
disp('Accounting for Density Changes and Acceleration Energetics ... ');
parfor index = 1:length(TotalEnth)
    % get conditions
    h_tot = TotalEnth(index);
    p_curr = smoothedMSLP(index)*0.0689475728;
    mdot_tot = smoothedMSLmdot(index) + smoothwater(index);
    % set up loop
    h_new = h_tot;
    looplum = 1000;
    numloops = 0;
    executeloop = 1;
    % find the new flow (subtracting velocity energy) enthalpy for the
    % conditions just upstream of the orifice
    while executeloop == 1
        % loop counter
        numloops = numloops + 1;
        % get new density, velocity, enthalpy
        temprho = XSteam('rho_ph', p_curr, h_new);
        tempvel = mdot_tot / (temprho * sparger_area);
        temp_h = h_tot - ((tempvel^2)/1000);
        h_old = h_new;
        h_new = (0.382*h_old) + (0.618*temp_h);
        % end the loop?
        if (numloops > looplum) || abs(h_old - h_new) < 1e-9
            % end the loop
            executeloop = 0;
        end
    end
    % store it
    AdjustedEnth_US(index) = h_new;
    tempvels1(index) = tempvel;

    % set up the next loop
    p_curr = spargerP(index);
    h_new = h_tot;
    looplum = 1000;
    numloops = 0;
    executeloop = 1;
    % find the new flow (subtracting velocity energy) enthalpy for the
    % conditions just downstream of the orifice
    while executeloop == 1
        % loop counter
        numloops = numloops + 1;
        % get new density, velocity, enthalpy
        temprho = XSteam('rho_ph', p_curr, h_new);
        tempvel = mdot_tot / (temprho * sparger_area);
        temp_h = h_tot - ((tempvel^2)/1000);
        h_old = h_new;
        h_new = (0.382*h_old) + (0.618*temp_h);
        % end the loop?
        if (numloops > looplum) || abs(h_old - h_new) < 1e-9
            % end the loop
            executeloop = 0;
        end
    end
    % store it
    AdjustedEnth_DS(index) = h_new;
    tempvels2(index) = tempvel;
end
disp(' ... Done! Continuing with the Qualities ... ');
velocities(:, 3:4) = [tempvels1, tempvels2];
AdjustedQuality = [t, t];

parfor index=1:size(steamarray,1)
    % quality in MSL

```

```

steamarraytemp(index,7) = (steamarray(index,6) - steamarray(index,5)) /
    (steamarray(index,3) - steamarray(index,5));
smoothedenthtemp(index, 2) = (smoothedenth(index, 1) - steamarray(index,5)) /
    (steamarray(index,3) - steamarray(index,5));
AdjustedQuality(index, 1) = (AdjustedEnth_US(index) - hsatL(index, 1)) / (hsatG(index,
    1) - hsatL(index, 1));
end
steamarray(:,7) = steamarraytemp(:,7);
smoothedenth(:, 2) = smoothedenthtemp(:, 2);
parfor index=1:size(steamarray,1)
    % saturated vapor enthalpy, estimated from post-turbine GP
    steamarray(index,8) = XSteam('hV_p', (trmdat(index, 97) + (0.0361272918274*(4.1 +
        trmdat(index,113))))*0.0689475728);
end
parfor index=1:size(steamarray,1)
    % saturated liquid enthalpy, estimated from post-turbine GP
    steamarray(index,9) = XSteam('hL_p', (trmdat(index, 97) + (0.0361272918274*(4.1 +
        trmdat(index,113))))*0.0689475728);
end
parfor index=1:size(steamarray,1)
    % estimated post-turbine quality
    steamarraytemp(index,10) = (steamarray(index,6) - steamarray(index,9)) /
        (steamarray(index,8) - steamarray(index,9));
    smoothedenthtemp(index, 3) = (smoothedenth(index, 1) - steamarray(index,9)) /
        (steamarray(index,8) - steamarray(index,9));
    AdjustedQuality(index, 2) = (AdjustedEnth_DS(index) - hsatL(index, 2)) / (hsatG(index,
        2) - hsatL(index, 2));
end
steamarray(:,10) = steamarraytemp(:,10);
smoothedenth(:, 3) = smoothedenthtemp(:, 3);
hsteam = AdjustedEnth_DS;
% condensation flowrates

parfor index=1:size(steamarray,1)
    % all flowrates are strictly the condensing/cooling side -- they do not
    % include the injected steam flow quantities
    mdcond(index) = ((hsteam(index) - hmidsat(index)) / (hmidsat(index) - hmid(index))) *
        smoothedMSLmdot(index);
    mdcondvol(index) = mdcond(index) / rhomid(index);
    mdcondcool(index) = ((hsteam(index) - hcondensing(index)) / (hcondensing(index) -
        hmid(index))) * smoothedMSLmdot(index);
    mdcondcoolvol(index) = mdcondcool(index) / rhocond(index);
    % water-injection adjusted values
    mdcondinj(index) = mdcond(index);
    mdcondinjvol(index) = mdcondvol(index);
    mdcondinjcool(index) = mdcondcool(index);
    mdcondcoolinjvol(index) = mdcondcoolvol(index);
    if twophasetest == 1
        % water-injection
        mdcondinj(index) = ((smoothedenth(index,1) - hmidsat(index)) / (hmidsat(index) -
            hmid(index))) * (smoothedMSLmdot(index) + smoothwater(index));
        mdcondinjvol(index) = mdcondinj(index) / rhomid(index);
        mdcondinjcool(index) = ((smoothedenth(index,1) - hcondensing(index)) /
            (hcondensing(index) - hmid(index))) * (smoothedMSLmdot(index) +
            smoothwater(index));
        mdcondcoolinjvol(index) = mdcondinjcool(index) / rhocond(index);
    end
end
end

outstring='    ...done!';
disp(outstring)

qualinfo = [NaN NaN NaN NaN NaN NaN NaN NaN NaN NaN NaN];
[qualinfo(1) qualinfo(2)] = min(steamarray(:,7));
[qualinfo(3) qualinfo(4)] = max(steamarray(:,7));
qualinfo(5) = mean(steamarray(:,7));

```

```

qualinfo(6) = std(steamarray(:,7));
[qualinfo(7) qualinfo(8)] = min(steamarray(:,10));
[qualinfo(9) qualinfo(10)] = max(steamarray(:,10));
qualinfo(11) = mean(steamarray(:,10));
qualinfo(12) = std(steamarray(:,10));

outstring=['Minimum Steam Quality: ' num2str(qualinfo(1)) ' at t plus '
           num2str(t(qualinfo(2))) ' s'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

outstring=['Maximum Steam Quality: ' num2str(qualinfo(3)) ' at t plus '
           num2str(t(qualinfo(4))) ' s'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

outstring=['Time-Averaged Steam Quality: ' num2str(qualinfo(5)) ' +/- '
           num2str(qualinfo(6)) ];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

if use_turbine == 1
    outstring=['Minimum Turbine Outlet Steam Quality: ' num2str(qualinfo(7)) ' at t plus '
              ' num2str(t(qualinfo(8))) ' s'];
    disp(outstring)
    if save_em == 1
        fprintf(filehandle, '%s\r\n', outstring);
    end

    outstring=['Maximum Turbine Outlet Steam Quality: ' num2str(qualinfo(9)) ' at t plus '
              ' num2str(t(qualinfo(10))) ' s'];
    disp(outstring)
    if save_em == 1
        fprintf(filehandle, '%s\r\n', outstring);
    end

    outstring=['Time-Averaged Turbine Outlet Steam Quality: ' num2str(qualinfo(11)) '
              +/- ' num2str(qualinfo(12)) ];
    disp(outstring)
    if save_em == 1
        fprintf(filehandle, '%s\r\n', outstring);
    end
else
    outstring='SRV Alignment, no RCIC Turbine 0 0 0 0 0 0 ';
    disp(outstring)
    if save_em == 1
        fprintf(filehandle, '%s\r\n', outstring);
    end
end

% Finding min and max T-changerates
inclusionlen = 1500;
sindex = trunind;
if sindex(1) < inclusionlen+1
    sindex(1) = inclusionlen+1;
end
if sindex(3) + inclusionlen > size(data,1)
    sindex(3) = size(data,1) - inclusionlen;
elseif sindex(3) - inclusionlen > sindex(2)
    sindex(3) = sindex(2);
end

```

```

end
disp('Processing slopes of rear stratification set ...')
vsmooth_top = zeros(size(data,1), 2);
vsmooth_mid = vsmooth_top;
vsmooth_low = vsmooth_top;
vsmooth_out = vsmooth_top;
vsmooth_hot = vsmooth_top;

parfor ind=sindex(1):sindex(3)
    xvals = data(ind - inclusionlen : ind + inclusionlen, 1) - data(ind, 1);
    yvals_top = data(ind - inclusionlen : ind + inclusionlen, 60);
    yvals_mid = data(ind - inclusionlen : ind + inclusionlen, 48);
    yvals_low = data(ind - inclusionlen : ind + inclusionlen, 56);
    yvals_out = data(ind - inclusionlen : ind + inclusionlen, 74);
    yvals_hot = data(ind - inclusionlen : ind + inclusionlen, 50);
    p1 = polyfit(xvals, yvals_top, 1);
    vsmooth_top(ind, :) = p1;
    p2 = polyfit(xvals, yvals_mid, 1);
    vsmooth_mid(ind, :) = p2;
    p3 = polyfit(xvals, yvals_low, 1);
    vsmooth_low(ind, :) = p3;
    p4 = polyfit(xvals, yvals_out, 1);
    vsmooth_out(ind, :) = p4;
    p5 = polyfit(xvals, yvals_hot, 1);
    vsmooth_hot(ind, :) = p5;
end
disp('Searching...')
% find max and min slopes
topdt = [0, 0, 0, 0];
[topdt(1) topdt(2)] = max(vsmooth_top(sindex(1):sindex(3)-inclusionlen,1));
[topdt(3) topdt(4)] = min(vsmooth_top(sindex(1):sindex(3)-inclusionlen,1));
middt = [0, 0, 0, 0];
[middt(1) middt(2)] = max(vsmooth_mid(sindex(1):sindex(3)-inclusionlen,1));
[middt(3) middt(4)] = min(vsmooth_mid(sindex(1):sindex(3)-inclusionlen,1));
lowdt = [0, 0, 0, 0];
[lowdt(1) lowdt(2)] = max(vsmooth_low(sindex(1):sindex(3)-inclusionlen,1));
[lowdt(3) lowdt(4)] = min(vsmooth_low(sindex(1):sindex(3)-inclusionlen,1));
outdt = [0, 0, 0, 0];
[outdt(1) outdt(2)] = max(vsmooth_out(sindex(1):sindex(3)-inclusionlen,1));
[outdt(3) outdt(4)] = min(vsmooth_out(sindex(1):sindex(3)-inclusionlen,1));
hotdt = [0, 0, 0, 0];
[hotdt(1) hotdt(2)] = max(vsmooth_hot(sindex(1):sindex(3)-inclusionlen,1));
[hotdt(3) hotdt(4)] = min(vsmooth_hot(sindex(1):sindex(3)-inclusionlen,1));

% find max and min slope differences
stopmid = vsmooth_top((sindex(1):sindex(3) - inclusionlen), 1) -
    vsmooth_mid((sindex(1):sindex(3) - inclusionlen), 1);
smidlow = vsmooth_mid((sindex(1):sindex(3) - inclusionlen), 1) -
    vsmooth_low((sindex(1):sindex(3) - inclusionlen), 1);
slowout = vsmooth_low((sindex(1):sindex(3) - inclusionlen), 1) -
    vsmooth_out((sindex(1):sindex(3) - inclusionlen), 1);
shotmid = vsmooth_hot((sindex(1):sindex(3) - inclusionlen), 1) -
    vsmooth_mid((sindex(1):sindex(3) - inclusionlen), 1);

stopmiddt = [0 0 0 0];
smidlowdt = [0 0 0 0];
slowoutdt = [0 0 0 0];
shotmiddt = [0 0 0 0];

[stopmiddt(1) stopmiddt(2)] = max(stopmid);
[stopmiddt(3) stopmiddt(4)] = min(stopmid);
[smidlowdt(1) smidlowdt(2)] = max(smidlow);
[smidlowdt(3) smidlowdt(4)] = min(smidlow);
[slowoutdt(1) slowoutdt(2)] = max(slowout);
[slowoutdt(3) slowoutdt(4)] = min(slowout);
[shotmiddt(1) shotmiddt(2)] = max(shotmid);

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[shotmiddt(3) shotmiddt(4)] = min(shotmid);

outstring = ['Smoothed Changerates may not fully include test beginning and end periods,
analysis ending at t plus ' num2str(data((sindex(3)-inclusionlen),1) -
data(sindex(1),1)) ' s; using ' num2str(inclusionlen * 2/10) ' s smoothing'];
outstring=[outstring crlf 'Max and min smoothed upper level changerates: '
num2str(60*topdt(1)) ' degrees/min at t plus ' num2str(t(topdt(2))) ' s and '
num2str(60*topdt(3)) ' degrees/min at t plus ' num2str(t(topdt(4))) ' s,
respectively'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
outstring=['Max and min smoothed mid (SP9) level changerates: ' num2str(60*middt(1)) '
degrees/min at t plus ' num2str(t(middt(2))) ' s and ' num2str(60*middt(3)) '
degrees/min at t plus ' num2str(t(middt(4))) ' s, respectively'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
outstring=['Max and min smoothed upper-mid level changerate differences: '
num2str(60*stopmiddt(1)) ' degrees/min at t plus ' num2str(t(stopmiddt(2))) ' s
and ' num2str(60*stopmiddt(3)) ' degrees/min at t plus ' num2str(t(stopmiddt(4)))
' s, respectively'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
outstring=['Max and min smoothed lower level changerates: ' num2str(60*lowdt(1)) '
degrees/min at t plus ' num2str(t(lowdt(2))) ' s and ' num2str(60*lowdt(3)) '
degrees/min at t plus ' num2str(t(lowdt(4))) ' s, respectively'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
outstring=['Max and min smoothed mid-lower level changerate differences: '
num2str(60*smidlowdt(1)) ' degrees/min at t plus ' num2str(t(smidlowdt(2))) ' s
and ' num2str(60*smidlowdt(3)) ' degrees/min at t plus ' num2str(t(smidlowdt(4)))
' s, respectively'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
outstring=['Max and min smoothed outlet level changerates: ' num2str(60*outdt(1)) '
degrees/min at t plus ' num2str(t(outdt(2))) ' s and ' num2str(60*outdt(3)) '
degrees/min at t plus ' num2str(t(outdt(4))) ' s, respectively'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
outstring=['Max and min smoothed lower-outlet level changerate differences: '
num2str(60*slowoutdt(1)) ' degrees/min at t plus ' num2str(t(slowoutdt(2))) ' s
and ' num2str(60*slowoutdt(3)) ' degrees/min at t plus ' num2str(t(slowoutdt(4)))
' s, respectively'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
outstring=['Max and min smoothed hot (SP8) level changerates: ' num2str(60*hotdt(1)) '
degrees/min at t plus ' num2str(t(hotdt(2))) ' s and ' num2str(60*hotdt(3)) '
degrees/min at t plus ' num2str(t(hotdt(4))) ' s, respectively'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
outstring=['Max and min smoothed hot-mid (SP8-SP9) level changerate differences: '
num2str(60*shotmiddt(1)) ' degrees/min at t plus ' num2str(t(shotmiddt(2))) ' s

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        and ' num2str(60*shotmidt(3)) ' degrees/min at t plus ' num2str(t(shotmidt(4)))
        ' s, respectively'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% Property Collection
steamprops = zeros(length(t), 60 );
testrelationship = 0*t;
testrelationship2 = testrelationship;
testrelationship3 = testrelationship;
testrelationship4 = testrelationship;

disp('Determining and Collecting Fluid Properties ... ');

parfor index=1:length(t)
    % put the sparger & pool middle steam/water properties together in a
    % table, where the source P/T/h used smoothing algorithms
    e1 = TotalEnth(index); % sparger steam enthalpy + velocity
    e2 = AdjustedEnth_DS(index); % sparger enthalpy
    e3 = hmid(index); % pool mid enthalpy (bulk)
    e4 = hsatL(index, 2); % sparger water saturation enthalpy
    e5 = hsatG(index, 2); % sparger steam saturation enthalpy
    e6 = e4 - e3; % pool mid subcooling enthalpy
    e7 = e1 - e4; % sparger steam full condensation enthalpy
    e8 = XSteam('h_pT', (smoothedP(index)*0.0689475728 + 0.037), stratsmooth_3(index)); %
        smoothed plume hot spot enthalpy
    e9 = htop(index); % pool rear upper smoothed enthalpy
    e10 = hlow(index); % pool rear lower smoothed enthalpy
    e11 = hout(index); % pool outlet smoothed enthalpy
    rho1 = XSteam('rho_ph', spargerP(index), e3); % pool mid (bulk) density
    rho2 = XSteam('rhoL_p', spargerP(index)); % sparger saturated water density
    rho3 = XSteam('rhoV_p', spargerP(index)); % sparger saturated steam density
    rho4 = XSteam('rho_ph', spargerP(index), e2); % sparger steam flow density
    x1 = AdjustedQuality(index, 2); % sparger steam quality - unbounded
    x2 = x1; % sparger steam quality -- within bounds
    if x2 > 1
        % keep x2 within [0,1]
        x2 = 1;
    elseif x2 < 0
        x2 = 0;
    end
    vf1 = x2 / (x2 + ((1 - x2)*rho3/rho2)); % sparger void fraction
    v1 = velocities(index, 4); % sparger velocity
    md1 = smoothedMSLmdot(index); % mdot steam
    md2 = smoothwater(index); % mdot water into steam line
    if twophasetest == 1
        md3 = smoothedMSLmdot(index) + smoothwater(index); % mdot sparger steam total
    else
        md3 = smoothedMSLmdot(index);
    end
    mu1 = XSteam('my_ph', spargerP(index), e3); % sparger subcooled water viscosity
    mu2 = XSteam('my_ph', spargerP(index), e4); % sparger saturated water viscosity
    mu3 = XSteam('my_ph', spargerP(index), e5); % sparger saturated steam viscosity
    mu4 = XSteam('my_ph', spargerP(index), e2); % sparger steam viscosity
    if isnan(mu4)
        % homogeneous two-phase sparger steam viscosity
        mu4 = (x2 * mu3 * rho4 / rho3) + ( (1-x2) * mu2 * rho4 / rho2);
    end
    sig1 = XSteam('st_T', stratsmooth_4(index)); % s/w surface tension for Tsat = Tmid
    sig2 = XSteam('st_p', spargerP(index)); % s/w surface tension for Psat = sparger P
    p1 = spargerP(index); % sparger pressure (bar)
    p2 = smoothedP(index)*0.0689475728; % pool airspace pressure, bar
    p3 = p2 + 0.037; % approx mid-level P, bar
    p4 = XSteam('psat_T', stratsmooth_4(index)); % saturation (vapor) pressure at Tmid
    p5 = XSteam('psat_T', stratsmooth_3(index)); % saturation (vapor) pressure at Tplume

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t1 = stratsmooth_4(index); % mid-level bulk temperature
t2 = XSteam('T_ph', spargerP(index), e2); % sparger steam temperature
t3 = XSteam('Tsat_p', spargerP(index)); % sparger steam saturation temperature
t4 = stratsmooth_3(index); % smoothed plume T
t5 = stratsmooth_1(index); % Upper-Level Pool Rear Smoothed Temperature
t6 = stratsmooth_2(index); % Lower-Level Pool Rear Smoothed Temperature
t7 = stratsmooth_5(index); % Pool Outlet Smoothed Temperature
cp1 = XSteam('Cp_ph', p3, e3); % pool mid bulk heat capacity
cp2 = XSteam('CpL_p', p1); % sparger saturated water heat capacity
cp3 = XSteam('CpV_p', p1); % sparger saturated steam heat capacity
k1 = XSteam('tc_ph', p3, e3); % pool bulk mid thermal conductivity
k2 = XSteam('tcL_p', p1); % sparger saturated water thermal conductivity
k3 = XSteam('tcL_p', p1); % sparger saturated steam thermal conductivity
g1 = md3 / sparger_area;
d1 = 2*0.020447; % sparger diameter (m)
d2 = 2*0.004625; % water injection line diameter
d3 = 15.5*0.0254; % sparger outlet elevation
d4 = coldlevels(index)/100; % pool cold level
d5 = hotdepth(index)/100; % pool hot level
re_tp = g1 * d1 / mu4; % two-phase Reynolds number (sparger steam)
pr1 = 1000 * mu1 * cp1 / k1; % pool mid (bulk) water Prandtl number
pr2 = 1000 * mu2 * cp2 / k2; % sparger saturated water Prandtl number
pr3 = 1000 * mu3 * cp3 / k3; % sparger saturated steam Prandtl number
cs1 = XSteam('w_ph', p3, e3); % pool mid bulk sonic velocity
cs2 = XSteam('wL_p', p1); % sparger saturated water sonic velocity
cs3 = XSteam('wV_p', p1); % sparger saturated steam sonic velocity
cs4 = XSteam('w_ph', p1, e2); % sparger steam sonic velocity
if isnan(cs4)
    % determine a homogeneous 2-phase sonic velocity
    % DOUBLE-CHECK THIS RELATIONSHIP!!!!
    cs4 = 1 / ( ((1-vf1)*sqrt( ((1-vf1)/(cs2^2)) + ((vf1*rho2/rho3)/(cs3^2)) )) +
                ((vf1)*sqrt( ((vf1)/(cs3^2)) + (((1-vf1)*rho3/rho2)/(cs2^2)) ));
end

% additional derived quantities for use in the computation
bp = sqrt(p4./p1);
ja_tp = e6 ./ e7;
ja_w = (e4-e3)./(e5-e4);
gr_s = 9.81 * ((rho2 - rho4)./rho4) .* (d5 - d3).^3 ./ (mu4./rho4).^2;
gr_ss = 9.81 * ((rho1 - rho3)./rho3) .* (d5 - d3).^3 ./ (mu3./rho3).^2;
gr_w = 9.81 * ((rho1 - rho2)./rho2) .* (d5 - d3).^3 ./ (mu2./rho2).^2;
ri_s = 9.81 * ((rho1 - rho4)./rho4) .* (d5 - d3).^1 ./ (v1.^2);
fr_s = v1 ./ sqrt(9.81 * (d5-d3));
we = rho4 .* v1.^2 .* d1 ./ sig2;

% store it all
steamprops(index, :) = [g1, d1, d2, d3, d4, d5, x1, x2, vf1, v1, re_tp, sig1, sig2,
    md1, md2, md3, t1, t2, t3, t4, t5, t6, t7, cp1, cp2, cp3, k1, k2, k3, pr1, pr2,
    pr3, rho1, rho2, rho3, rho4, mu1, mu2, mu3, mu4, cs1, cs2, cs3, cs4, p1, p2, p3,
    p4, p5, e1, e2, e3, e4, e5, e6, e7, e8, e9, e10, e11];

% calculate the Mixing Number
% testrelationship_older(index) = ((e6 ./ e7) .^(9/8)) .* (e3 ./ e6) .^(1/4) .*
    (e4 ./ e5) .* (e2 ./ e7) .^(1/6) .* (re_tp .^(-1/8)) .*
    ( ( (0.5 .* rho4 .* v1 .* v1 / 100000) + p4) ./(p1) ) .* ((p1 ./ p4) ) .* (rho3 ./
    rho4) .* (rho2 ./ rho3) .^0.5 .* (rho2 ./ rho1) .* (sig1 ./ sig2) .*
    (pr1 .^(1/4)) .* (p1 .* d1 ./ sig2) .^(-3/8) .* x2 .^(1/8) .* (p4 .* d1 ./
    sig1) .^(1/8);

% there's still a weird v1 dependence
% (ja_w.^(-1/8) .* x1.^(-5/8) .* re_tp .^(1/2) .* pr1 .^(1/4) .* ( (p4 + (0.5 .*
    rho4 .* v1 .^2 ./ 100000) ) ./ p1 ) .^(1/2) .* (gr_w ./ (re_tp.^2)) .^(1/2) .*
    (rho3 ./ rho2) .^(1/4) .* (v1 ./ cs2) .^(3/8) .* (cs3 ./ cs2) .^(1/2) .* (sig2 ./ sig1) .^(
    -1/4) .* ((t3+273.15) ./ (t1+273.15)) .^(-1/4) .* ((d5-d3) ./ 1.5) .^(-1/2) .*
    gr_w .^(1/16) .* ( (1 - (p4 ./ p1) .^4) + (p4 ./ p1) .^4 .* gr_s ./ gr_w .*
    pr1 .^(1) ) .^(8/16) .* (pr1 .* pr2 ./ (pr1 + pr2)) .^(1/4) );

```

```

% testrelationship_old(index) = (re_tp).^ (10/16) .* pr1.^ (1/8) .* ja_w.^ (-1/2) .*
  (rho2./rho3).^ (8/64) .* (gr_w./re_tp.^2) .^(+21/64) .* ((d5-d3)/1.5).^ (-
  3/4) .* x1.^ (-2/16) .* ((1-(p4./p1).^4) + (p4./p1).^4 .*gr_s./gr_w.*1) .^( 21/64);

% derived from Key Point #2 and #4, but probably won't work for x < 0.5
% or for mdot < 20 g/s

% set for KP 2, 4, 5, 7, 10
% there is a common core, and a multiplier
% the multiplier is common through KP 4, but is unique for KP 5, 7, and
% 10 (correlation numbers 2, 3, and 4, respectively)
partcrazy = pr1.^ (8/16) .* (mu4./mu1) .^( (+8/16) ) .* (rho4./rho1) .^( (8/16) ) .*
  (ja_w./x1) .^( -16/16 + ((1/16).*bp) ) .* re_tp .^( 8/16) .* fr_s .^( (-6/16) +
  ((-8/16).*bp) );
testrelationship(index) = partcrazy .* (rho2./rho3).^( (4/16) + ((3/16).*bp) );
testrelationship2(index) = partcrazy .* (rho2./rho3).^( (13/16) ) ;
testrelationship3(index) = partcrazy .* (rho2./rho3).^( (15/16) ) ;
testrelationship4(index) = partcrazy .* (rho2./rho3).^( (16/16) ) ;
% testrelationship(index) = pr1 .^( 1/2) .* (mu4./mu1) .^( 1/4) .* (rho4./rho1) .^(
  1/2) .* (rho4 .* 1000.*e7 ./ (100000.*p1) ) .^( 1/2) .* ja_w .^( -6/8 +
  ((8/16).*bp) ) .* x1 .^( 12/16 - ((1/2).*bp) ) .* re_tp .^( 1/2) .* ri_s .^( (1/4)
  + ((1/2).*bp) ) .* fr_s .^( ((3/16) + ((3/8).*bp) );
% testrelationship(index) = x2 .^(12/16) .* ((re_tp.^0.5)./ja_w) .^( 16/16) .*
  pr1.^(+16/32).* ( ri_s) .^(16/16) .*x2 .^( -8/16) .^( 0.25 +
  0.5*(p4./p1).^ (32/64) ) .* (mu4./mu1).^ (2/8) .*
  ((0.5*v1.^2)/(1000*e6)).^(5/32) .* ja_w.^ (+8/16) .*
  ((1000*e7)/(100000*p1./rho4)).^(+1/2) .* (rho4./rho1).^ (1/2) ;
% testrelationship(index) = x2 .^(12/16) .* ((re_tp.^0.5)./ja_w) .^( 16/16) .*
  pr1.^(+16/32).* pr2.^(1/2).* ( ri_s) .^(16/16) .*x2 .^( -
  8/16) .^( (p4./p1).^ (32/64) ) .* ((t1+273.15)/(t2+273.15)).^( -16/8) .*
  (mu4./mu1).^ (2/8) .* ((0.5*v1.^2)/(1000*e6)).^(4/32) .* ja_w.^ (+8/16) .*
  ((1000*e7)/(100000*p1./rho4)).^(1/1) .* (rho4./rho1).^ (1/2) .* (sig1./sig2);
% testrelationship(index) = x1 .^(1/16) .* ((re_tp.^0.5)./ja_w) .^( 12/16) .*
  pr1.^( -0/32) .* pr2.^(1/2) .* (pr1.^( -8/16) .* (pr2./pr1) .^( -32/16) .*
  ri_s .^0.5 .*x1.^( -4/16) ) .^( (p4./p1).^ (32/64) ) .* ((d5-d3)/1.5) .^(+2/4) .*
  exp(-1*(16/16) .* (p4./p1).^ (2/4) ) .* ((t1+273.15)/(t3+273.15)).^( -16/8) .*
  (rho2./rho3).^( -4/16) .* (mu3./mu2).^(1/2) .* ja_w .^( -4/16) .*
  ((1000*e7)/(100000*p1./rho4)).^(1/1) .* (rho3./rho4).^0.25 .*
  ((rho1./rho2).^ (2);
% testrelationship(index) = x1 .^(32/32) .* ja_w .^( -8/16) .* re_tp .^( 28/16) .*
  pr1.^(4/32) .* pr2.^(6/4) .* ri_s .^( (t1+273.15)/(t3+273.15) ) .* ((d5-
  d3)/1.5) .^( -3/4) .* exp(-(p4./p1).^ (2/4) ) .*
  ((t1+273.15)/(t3+273.15)).^(4/8) .* (rho2./rho3).^ (1/16);
% testrelationship2(index) = (re_tp).^ (8/16) .* pr1 .^(2/16) .* pr2 .^( 1/16) .*
  ja_w .^( -8/16) .* ri_s .^(+4/16) .* ((d5-d3)/1.5) .^( -1/4) .* x1.^(+4/16) .*
  exp(-(p4./p1).^0.5) .* (p4./p1).^ (1/16);

```

end

```

steampropsdesc = 'Sparger Massflux (kg/m2-s) g1, Sparger Diameter (m) d1, Water Injection
  Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level
  d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction v1,
  Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface
  Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot
  (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1,
  Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4,
  Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool
  Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water
  Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal
  Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat
  Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2,
  Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m3) rho1, Sparger Sat Water
  Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger
  Subcooled T mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger
  Sat Steam Viscosity mu3, Sparger Sat Steam Viscosity mu4, Pool Mid Sonic Velocity
  (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity

```

```

cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx
Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total
Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water
Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam
Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed
Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy
e11';

```

```

disp(' ... Done! ');

```

```

% To decompose the steam properties table:

```

```

%
% g1 = steamprops(:, 01 );
% d1 = steamprops(:, 02 );
% d2 = steamprops(:, 03 );
% d3 = steamprops(:, 04 );
% d4 = steamprops(:, 05 );
% d5 = steamprops(:, 06 );
% x1 = steamprops(:, 07 );
% x2 = steamprops(:, 08 );
% vf1 = steamprops(:, 09 );
% v1 = steamprops(:, 10 );
% re_tp = steamprops(:, 11 );
% sig1 = steamprops(:, 12 );
% sig2 = steamprops(:, 13 );
% md1 = steamprops(:, 14 );
% md2 = steamprops(:, 15 );
% md3 = steamprops(:, 16 );
% t1 = steamprops(:, 17 );
% t2 = steamprops(:, 18 );
% t3 = steamprops(:, 19 );
% t4 = steamprops(:, 20 );
% t5 = steamprops(:, 21 );
% t6 = steamprops(:, 22 );
% t7 = steamprops(:, 23 );
% cp1 = steamprops(:, 24 );
% cp2 = steamprops(:, 25 );
% cp3 = steamprops(:, 26 );
% k1 = steamprops(:, 27 );
% k2 = steamprops(:, 28 );
% k3 = steamprops(:, 29 );
% pr1 = steamprops(:, 30 );
% pr2 = steamprops(:, 31 );
% pr3 = steamprops(:, 32 );
% rho1 = steamprops(:, 33 );
% rho2 = steamprops(:, 34 );
% rho3 = steamprops(:, 35 );
% rho4 = steamprops(:, 36 );
% mu1 = steamprops(:, 37 );
% mu2 = steamprops(:, 38 );
% mu3 = steamprops(:, 39 );
% mu4 = steamprops(:, 40 );
% cs1 = steamprops(:, 41 );
% cs2 = steamprops(:, 42 );
% cs3 = steamprops(:, 43 );
% cs4 = steamprops(:, 44 );
% p1 = steamprops(:, 45 );
% p2 = steamprops(:, 46 );
% p3 = steamprops(:, 47 );
% p4 = steamprops(:, 48 );
% p5 = steamprops(:, 49 );
% e1 = steamprops(:, 50 );
% e2 = steamprops(:, 51 );
% e3 = steamprops(:, 52 );
% e4 = steamprops(:, 53 );
% e5 = steamprops(:, 54 );

```

```

% e6 = steamprops(:, 55 );
% e7 = steamprops(:, 56 );
% e8 = steamprops(:, 57 );
% e9 = steamprops(:, 58 );
% e10 = steamprops(:, 59 );
% e11 = steamprops(:, 60 );

%
% =====
% DATA ANALYSIS SECTION
% =====
%

% present some run details
meansteam = mean(1000*trmdat(:,107));
sigsteam = std(1000*trmdat(:,107));
meanfeedwater = mean(1000*trmdat(:,102));
sigfeed = std(1000*trmdat(:,102));
meaninject = mean(1000*trmdat(:,127));
siginject = std(1000*trmdat(:,127));

outstring=['The mean steam flow rate was ' num2str(meansteam) ' +/- ' num2str(sigsteam) '
          g/s'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

outstring=['The mean feedwater flow rate was ' num2str(meanfeedwater) ' +/- '
          num2str(sigfeed) ' g/s'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

outstring=['The mean water injection to steam flow rate was ' num2str(meaninject) ' +/- '
          num2str(siginject) ' g/s'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% condensing region data

if stratified == 1
    % condensing SP8-SP9 average DT
    avcrdt = mean(stratsmooth_3(stratstartind:stratendind) -
                  stratsmooth_4(stratstartind:stratendind));
    avcrdtsd = std(stratsmooth_3(stratstartind:stratendind) -
                  stratsmooth_4(stratstartind:stratendind));

    % upper-SP8 average DT
    avtcdt = mean(stratsmooth_3(stratstartind:stratendind) -
                  stratsmooth_1(stratstartind:stratendind));
    avtcdtsd = std(stratsmooth_3(stratstartind:stratendind) -
                  stratsmooth_1(stratstartind:stratendind));

    outstring=['Mean Smoothed Condensing Region SP8-SP9 delta T is ' num2str(avcrdt) '
              +/- ' num2str(avcrdtsd) ' C over the Stratification Period, beginning at '
              num2str(stratsmooth_3(stratstartind)-stratsmooth_4(stratstartind)) ' C and ending
              at ' num2str(stratsmooth_3(stratendind)-stratsmooth_4(stratendind)) ' C'];

```

```

    outstring=[outstring crlf 'Mean Smoothed SP8-Upper Pool delta T is ' num2str(avtcdt)
        ' +/- ' num2str(avtcdtsd) ' C over the Stratification Period, beginning at '
        num2str(stratsmooth_3(stratstartind)-stratsmooth_1(stratstartind)) ' C and ending
        at ' num2str(stratsmooth_3(stratendind)-stratsmooth_1(stratendind)) ' C'];
    outstring = [outstring crlf 'The stratification period begins and ends with Smoothed
        SP8 readings of ' num2str(stratsmooth_3(stratstartind)) ' and '
        num2str(stratsmooth_3(stratendind)) ' C, respectively' ];
    outstring = [outstring crlf 'The stratification period begins and ends with
        condensing flows of ' num2str(mdcondinj(stratstartind)) ' and '
        num2str(mdcondinj(stratendind)) ' kg/s, respectively.'];
    outstring = [outstring crlf 'The stratification period begins and ends with
        condensing+cooling flows of ' num2str(mdcondinjcool(stratstartind)) ' and '
        num2str(mdcondinjcool(stratendind)) ' kg/s, respectively.'];
    outstring = [outstring crlf 'The stratification period had a mean sparger steam
        enthalpy of ' num2str(mean(AdjustedEnth_DS(stratstartind:stratendind))) ' +/- '
        num2str(std(AdjustedEnth_DS(stratstartind:stratendind))) ' kJ/kg.'];
    disp(outstring)
    if save_em == 1
        fprintf(filehandle, '%s\r\n', outstring);
    end
else
    outstring = 'No stratification; 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0. ';
    disp(outstring)
    if save_em == 1
        fprintf(filehandle, '%s\r\n', outstring);
    end
end

outstring = ['At plume detection, the condensing and condensing+cooling flows are '
    num2str(mdcondinj(plume_ind)) ' and ' num2str(mdcondinjcool(plume_ind)) ' kg/s,
    respectively'];
plumepse = [NaN, NaN];
plumepse(1) = mean(smoothedenth(plume_ind:stratendind));
plumepse(2) = std(smoothedenth(plume_ind:stratendind));
if isnan(plumepse(1)) || isinf(plumepse(1))
    plumepse(1) = 0;
end
if isnan(plumepse(2)) || isinf(plumepse(2))
    plumepse(2) = 0;
end
outstring = [outstring crlf 'The plume period had a mean steam enthalpy of '
    num2str(plumepse(1)) ' +/- ' num2str(plumepse(2)) ' kJ/kg.'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% stratification data

% Top-Mid temps
topmidsm = stratsmooth_1 - stratsmooth_4;

% Top-Lower temps
toplowsm = stratsmooth_1 - stratsmooth_2;

% Mid-Lower temps
midlowsm = stratsmooth_4 - stratsmooth_2;

% Upper-Outlet temps
upoutsm = stratsmooth_1 - stratsmooth_5;

% Mid-outlet temps
midoutsm = stratsmooth_4 - stratsmooth_5;

```

```

% Lower-outlet temps
lowoutsm = stratsmooth_2 - stratsmooth_5;

% Find Max Smoothed Top-Mid stratification
[y, ind] = max(topmidsm);
outstring=['Maximum Smoothed Top-Mid delta T is ' num2str(y) ' degrees C at t plus '
          num2str(t(ind)) ' s with T_upper = ' num2str(stratsmooth_1(ind)) ' C and T_mid = '
          num2str(stratsmooth_4(ind)) ' C'];
outstring = [outstring crlf 'At t plus ' num2str(t(ind)) ' s, Smoothed SP8-SP9 is '
            num2str(stratsmooth_3(ind) - stratsmooth_4(ind)) ' C and Smoothed SP8-Top is '
            num2str(stratsmooth_3(ind) - stratsmooth_1(ind)) ' C, where Smoothed SP8 is '
            num2str(stratsmooth_3(ind)) ' C and Pool P = ' num2str(trmdat(ind, 97)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% Find Max Smoothed Top-Lower stratification
[y, ind] = max(toplowsm);
outstring=['Maximum Smoothed Top-Lower delta T is ' num2str(y) ' degrees C at t plus '
          num2str(t(ind)) ' s with T_upper = ' num2str(stratsmooth_1(ind)) ' C and T_low = '
          num2str(stratsmooth_2(ind)) ' C'];
outstring = [outstring crlf 'At t plus ' num2str(t(ind)) ' s, Smoothed SP8-SP9 is '
            num2str(stratsmooth_3(ind) - stratsmooth_4(ind)) ' C and Smoothed SP8-Top is '
            num2str(stratsmooth_3(ind) - stratsmooth_1(ind)) ' C, where Smoothed SP8 is '
            num2str(stratsmooth_3(ind)) ' C and Pool P = ' num2str(trmdat(ind, 97)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% Find Max Smoothed Mid-lower stratification
[y, ind] = max(midlowsm);
outstring=['Maximum Smoothed Mid-Lower delta T is ' num2str(y) ' degrees C at t plus '
          num2str(t(ind)) ' s with T_mid = ' num2str(stratsmooth_4(ind)) ' C and T_low = '
          num2str(stratsmooth_2(ind)) ' C'];
outstring = [outstring crlf 'At t plus ' num2str(t(ind)) ' s, Smoothed SP8-SP9 is '
            num2str(stratsmooth_3(ind) - stratsmooth_4(ind)) ' C and Smoothed SP8-Top is '
            num2str(stratsmooth_3(ind) - stratsmooth_1(ind)) ' C, where Smoothed SP8 is '
            num2str(stratsmooth_3(ind)) ' C and Pool P = ' num2str(trmdat(ind, 97)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% Find Max Smoothed Top-Outlet stratification
[y, ind] = max(upoutsm);
outstring=['Maximum Smoothed Top-Outlet delta T is ' num2str(y) ' degrees C at t plus '
          num2str(t(ind)) ' s with T_upper = ' num2str(stratsmooth_1(ind)) ' C and T_out = '
          num2str(stratsmooth_5(ind)) ' C'];
outstring = [outstring crlf 'At t plus ' num2str(t(ind)) ' s, Smoothed SP8-SP9 is '
            num2str(stratsmooth_3(ind) - stratsmooth_4(ind)) ' C and Smoothed SP8-Top is '
            num2str(stratsmooth_3(ind) - stratsmooth_1(ind)) ' C, where Smoothed SP8 is '
            num2str(stratsmooth_3(ind)) ' C and Pool P = ' num2str(trmdat(ind, 97)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% Find Max Smoothed Mid-Outlet stratification
[y, ind] = max(midoutsm);
outstring=['Maximum Smoothed Mid-Outlet delta T is ' num2str(y) ' degrees C at t plus '
          num2str(t(ind)) ' s with T_mid = ' num2str(stratsmooth_4(ind)) ' C and T_out = '
          num2str(stratsmooth_5(ind)) ' C'];

```

```

outstring = [outstring crlf 'At t plus ' num2str(t(ind)) ' s, Smoothed SP8-SP9 is '
            num2str(stratsmooth_3(ind) - stratsmooth_4(ind)) ' C and Smoothed SP8-Top is '
            num2str(stratsmooth_3(ind) - stratsmooth_1(ind)) ' C, where Smoothed SP8 is '
            num2str(stratsmooth_3(ind)) ' C and Pool P = ' num2str(trmdat(ind, 97)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% Find Max Smoothed Lower-Outlet stratification
[y, ind] = max(lowoutsm);
outstring=['Maximum Smoothed Lower-Outlet delta T is ' num2str(y) ' degrees C at t plus '
            num2str(t(ind)) ' s with T_low = ' num2str(stratsmooth_2(ind)) ' C and T_out = '
            num2str(stratsmooth_5(ind)) ' C'];
outstring = [outstring crlf 'At t plus ' num2str(t(ind)) ' s, Smoothed SP8-SP9 is '
            num2str(stratsmooth_3(ind) - stratsmooth_4(ind)) ' C and Smoothed SP8-Top is '
            num2str(stratsmooth_3(ind) - stratsmooth_1(ind)) ' C, where Smoothed SP8 is '
            num2str(stratsmooth_3(ind)) ' C and Pool P = ' num2str(trmdat(ind, 97)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% Find Max Sparger Local Relative Temperature
[y, ind] = max(stratsmooth_3 - stratsmooth_4);
% Store the Key Point
keypoints_ind(14) = ind;
outstring=['Maximum Smoothed Condensing Region SP8-SP9 delta T is ' num2str(y) ' degrees
            C at (KEY POINT #14) t plus ' num2str(t(ind)) ' s with T_SP8 = '
            num2str(stratsmooth_3(ind)) ' C and T_SP9 = ' num2str(stratsmooth_4(ind)) ' C and
            Pool P = ' num2str(trmdat(ind, 97)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% Find Max Sparger Local Relative Temperature (top)
[y, ind] = max(stratsmooth_3 - stratsmooth_1);
outstring=['Maximum Smoothed Condensing Region SP8-Upper delta T is ' num2str(y) '
            degrees C at t plus ' num2str(t(ind)) ' s with T_SP8 = '
            num2str(stratsmooth_3(ind)) ' C and T_upper = ' num2str(stratsmooth_1(ind)) ' C
            and Pool P = ' num2str(trmdat(ind, 97)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% unsmoothed basic stratification data

% Top-Mid temps
topmid = [ (trmdat(:,60)-trmdat(:,58)), (trmdat(:,44)-trmdat(:,42)), (trmdat(:,28)-
            trmdat(:,26))];
topmidno4 = [ t*0, (trmdat(:,44)-trmdat(:,42)), (trmdat(:,28)-trmdat(:,26))];

% Top-Lower temps
toplow = [ (trmdat(:,60)-trmdat(:,56)), (trmdat(:,44)-trmdat(:,40)), (trmdat(:,28)-
            trmdat(:,24))];

% Mid-Lower temps
midlow = [ (trmdat(:,58)-trmdat(:,56)), (trmdat(:,42)-trmdat(:,40)), (trmdat(:,26)-
            trmdat(:,24))];
midlowno4 = [ t*0, (trmdat(:,42)-trmdat(:,40)), (trmdat(:,26)-trmdat(:,24))];

```



```

% Upper-Outlet temps
upout = [ (trmdat(:,60)-trmdat(:,74)), (trmdat(:,44)-trmdat(:,74)), (trmdat(:,28)-
trmdat(:,74))];

% Mid-outlet temps
midout = [ (trmdat(:,58)-trmdat(:,74)), (trmdat(:,42)-trmdat(:,74)), (trmdat(:,26)-
trmdat(:,74))];
midoutno4 = [ t*0, (trmdat(:,42)-trmdat(:,74)), (trmdat(:,26)-trmdat(:,74))];

% Lower-outlet temps
lowout = [ (trmdat(:,56)-trmdat(:,74)), (trmdat(:,40)-trmdat(:,74)), (trmdat(:,24)-
trmdat(:,74))];

% Find Max Top-Mid stratification
[temps, inds] = max(topmidno4);
[y, ind] = max(temps);
% get T values
if ind == 1
    % rear set
    tempsc = [trmdat(inds(ind), 60), trmdat(inds(ind), 58)];
elseif ind == 2
    % middle set
    tempsc = [trmdat(inds(ind), 44), trmdat(inds(ind), 42)];
elseif ind == 3
    % front set
    tempsc = [trmdat(inds(ind), 28), trmdat(inds(ind), 26)];
else
    % oops
    tempsc = [0, 0];
end
% Store the Key Point
keypoints_ind(4) = inds(ind);
outstring=['Maximum Top-Mid delta T is ' num2str(temps(ind)) ' degrees C at (KEY POINT #4)
t plus ' num2str(t(inds(ind))) ' s ignoring SP 4, with temperatures of '
num2str(tempsc(1)) ' and ' num2str(tempsc(2)) ' C, respectively, at Set # '
num2str(ind) ', where Pool P = ' num2str(trmdat(inds(ind), 97)) ' psia and
T_outlet = ' num2str(trmdat(inds(ind), 74)) ' C'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% Find the Top-Mid Reconvergence Point
RP = length(t);
PV = temps(ind);
foundreconverge = 0;
for n = inds(ind):(RP-600)
    dtvals = MTMDeltaT(n:n+600);
    % look at t through t plus 1 minute, and check for reconvergence for the
    % entire minute in the smoothed mid-axis data
    % reconvergence is delta T less than 1 degree OR less than 1/3 of the
    % Peak Difference
    if (sum(dtvals > (PV/3)) == 0) || (sum(dtvals > (1)) == 0)
        % found it!
        foundreconverge = 1;
        break
    end
end
if foundreconverge == 0
    % if the standard method did not find reconvergence, check the tail end
    for n = RP-600 : RP
        dtvals = MTMDeltaT(n:RP);
        % look at t through the end, and check for reconvergence for the
        % entire period (< 1 min) in the smoothed mid-axis data
        % reconvergence is delta T less than 1 degree OR less than 1/3 of the
        % Peak Difference
        if (sum(dtvals > (PV/3)) == 0) || (sum(dtvals > (1)) == 0)

```

```

                % found it!
                foundreconverge = 1;
                break
            end
        end
    end
end
if foundreconverge == 1
    outstring = ['Top-Mid Reconvergence Detected at (KEY POINT #5) t plus ' num2str(t(n))
        ' s with a Smoothed Mid-Axis Top-Mid Delta T of ' num2str(MTMDeltaT(n)) ' C and a
        raw SP12 Reading of ' num2str(trmdat(n,42)) ' C. '];
else
    n = RP;
    outstring = ['Top-Mid Reconvergence NOT Detected, setting t to (KEY POINT #5) t plus
        ' num2str(t(n)) ' s with a Smoothed Mid-Axis Top-Mid Delta T of '
        num2str(MTMDeltaT(n)) ' C and a raw SP12 Reading of ' num2str(trmdat(n,42)) ' C.
        '];
end
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
keypoints_ind(5) = n;

% Find Max Top-Lower stratification
[temps, inds] = max(toplow);
[y, ind] = max(temps);
% get T values
if ind == 1
    % rear set
    tempsc = [trmdat(inds(ind), 60), trmdat(inds(ind), 56)];
elseif ind == 2
    % middle set
    tempsc = [trmdat(inds(ind), 44), trmdat(inds(ind), 40)];
elseif ind == 3
    % front set
    tempsc = [trmdat(inds(ind), 28), trmdat(inds(ind), 24)];
else
    % oops
    tempsc = [0, 0];
end
outstring=['Maximum Top-Lower delta T is ' num2str(temps(ind)) ' degrees C at t plus '
    num2str(t(inds(ind))) ' s, with temperatures of ' num2str(tempsc(1)) ' and '
    num2str(tempsc(2)) ' C, respectively, at Set # ' num2str(ind) ' , where Pool P =
    ' num2str(trmdat(inds(ind), 97)) ' psia and T_outlet = ' num2str(trmdat(inds(ind),
    74)) ' C'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% Find Max Mid-Lower stratification
[temps, inds] = max(midlowno4);
[y, ind] = max(temps);
% get T values
if ind == 1
    % rear set
    tempsc = [trmdat(inds(ind), 58), trmdat(inds(ind), 56)];
elseif ind == 2
    % middle set
    tempsc = [trmdat(inds(ind), 42), trmdat(inds(ind), 40)];
elseif ind == 3
    % front set
    tempsc = [trmdat(inds(ind), 26), trmdat(inds(ind), 24)];
else
    % oops
    tempsc = [0, 0];
end
end

```

```

% Store the Key Point
keypoints_ind(6) = inds(ind);
outstring=['Maximum Mid-Low delta T is ' num2str(temps(ind)) ' degrees C at (KEY POINT #6)
          t plus ' num2str(t(inds(ind))) ' s ignoring SP 4, with temperatures of '
          num2str(tempsc(1)) ' and ' num2str(tempsc(2)) ' C, respectively, at Set # '
          num2str(inds) ' , where Pool P = ' num2str(trmdat(inds(ind), 97)) ' psia and
          T_outlet = ' num2str(trmdat(inds(ind), 74)) ' C'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% Find the Mid-Low Reconvergence Point
RP = length(t);
PV = temps(ind);
foundreconverge = 0;
for n = inds(ind):(RP-600)
    dtvals = MMLDeltaT(n:n+600);
    % look at t through t plus 1 minute, and check for reconvergence for the
    % entire minute in the smoothed mid-axis data
    % reconvergence is delta T less than 1 degree OR less than 1/3 of the
    % Peak Difference
    if (sum(dtvals > (PV/3)) == 0) || (sum(dtvals > (1)) == 0)
        % found it!
        foundreconverge = 1;
        break
    end
end
if foundreconverge == 0
    % if the standard method did not find reconvergence, check the tail end
    for n = RP-600 : RP
        dtvals = MMLDeltaT(n:RP);
        % look at t through the end, and check for reconvergence for the
        % entire period (< 1 min) in the smoothed mid-axis data
        % reconvergence is delta T less than 1 degree OR less than 1/3 of the
        % Peak Difference
        if (sum(dtvals > (PV/3)) == 0) || (sum(dtvals > (1)) == 0)
            % found it!
            foundreconverge = 1;
            break
        end
    end
end
if foundreconverge == 1
    outstring = ['Mid-Low Reconvergence Detected at (KEY POINT #7) t plus ' num2str(t(n))
                ' s with a Smoothed Mid-Axis Mid-Low Delta T of ' num2str(MMLDeltaT(n)) ' C and a
                raw SP12 Reading of ' num2str(trmdat(n,42)) ' C. '];
else
    n = RP;
    outstring = ['Mid-Low Reconvergence NOT Detected, setting t to (KEY POINT #7) t plus
                ' num2str(t(n)) ' s with a Smoothed Mid-Axis Mid-Low Delta T of '
                num2str(MMLDeltaT(n)) ' C and a raw SP12 Reading of ' num2str(trmdat(n,42)) ' C.
                '];
end
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
keypoints_ind(7) = n;

% Find Max Top-Outlet stratification
[temps, inds] = max(upout);
[y, ind] = max(temps);
% get T values
if ind == 1
    % rear set
    tempsc = [trmdat(inds(ind), 60), trmdat(inds(ind), 74)];

```

```

elseif ind == 2
    % middle set
    tempsc = [trmdat(inds(ind), 44), trmdat(inds(ind), 74)];
elseif ind == 3
    % front set
    tempsc = [trmdat(inds(ind), 28), trmdat(inds(ind), 74)];
else
    % oops
    tempsc = [0, 0];
end
outstring=['Maximum Top-Outlet delta T is ' num2str(temps(ind)) ' degrees C at t plus '
          num2str(t(inds(ind))) ' s, with temperatures of ' num2str(tempsc(1)) ' and '
          num2str(tempsc(2)) ' C, respectively, at Set # ' num2str(ind) ' , where Pool P =
          ' num2str(trmdat(inds(ind), 97)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% Find Max Mid-Outlet stratification
[temps, inds] = max(midoutno4);
[y, ind] = max(temps);
% get T values
if ind == 1
    % rear set
    tempsc = [trmdat(inds(ind), 58), trmdat(inds(ind), 74)];
elseif ind == 2
    % middle set
    tempsc = [trmdat(inds(ind), 42), trmdat(inds(ind), 74)];
elseif ind == 3
    % front set
    tempsc = [trmdat(inds(ind), 26), trmdat(inds(ind), 74)];
else
    % oops
    tempsc = [0, 0];
end
outstring=['Maximum Mid-Outlet delta T is ' num2str(temps(ind)) ' degrees C at t plus '
          num2str(t(inds(ind))) ' s ignoring SP 4, with temperatures of ' num2str(tempsc(1))
          ' and ' num2str(tempsc(2)) ' C, respectively, at Set # ' num2str(ind) ' , where
          Pool P = ' num2str(trmdat(inds(ind), 97)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% Find Max Lower-Outlet stratification
[temps, inds] = max(lowout);
[y, ind] = max(temps);
% get T values
if ind == 1
    % rear set
    tempsc = [trmdat(inds(ind), 56), trmdat(inds(ind), 74)];
elseif ind == 2
    % middle set
    tempsc = [trmdat(inds(ind), 40), trmdat(inds(ind), 74)];
elseif ind == 3
    % front set
    tempsc = [trmdat(inds(ind), 24), trmdat(inds(ind), 74)];
else
    % oops
    tempsc = [0 0];
end
% Store the Key Point
keypoints_ind(8) = inds(ind);
outstring=['Maximum Lower-Outlet delta T is ' num2str(temps(ind)) ' degrees C at (KEY
          POINT #8) t plus ' num2str(t(inds(ind))) ' s, with temperatures of '

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        num2str(tempsc(1)) ' and ' num2str(tempsc(2)) ' C, respectively, at Set # '
        num2str(ind) ' , where Pool P = ' num2str(trmdat(inds(ind), 97)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% Find the Lower-Outlet Reconvergence Point
RP = length(t);
PV = temps(ind);
foundreconverge = 0;
for n = inds(ind):(RP-600)
    dtvals = MLODeltaT(n:n+600);
    % look at t through t plus 1 minute, and check for reconvergence for the
    % entire minute in the smoothed mid-axis data
    % reconvergence is delta T less than 1 degree OR less than 1/3 of the
    % Peak Difference
    if (sum(dtvals > (PV/3)) == 0) || (sum(dtvals > (1)) == 0)
        % found it!
        foundreconverge = 1;
        break
    end
end
if foundreconverge == 0
    % if the standard method did not find reconvergence, check the tail end
    for n = RP-600 : RP
        dtvals = MLODeltaT(n:RP);
        % look at t through the end, and check for reconvergence for the
        % entire period (< 1 min) in the smoothed mid-axis data
        % reconvergence is delta T less than 1 degree OR less than 1/3 of the
        % Peak Difference
        if (sum(dtvals > (PV/3)) == 0) || (sum(dtvals > (1)) == 0)
            % found it!
            foundreconverge = 1;
            break
        end
    end
end
if foundreconverge == 1
    outstring = ['Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus '
        num2str(t(n)) ' s with a Smoothed Mid-Axis Low-Outlet Delta T of '
        num2str(MLODeltaT(n)) ' C and a raw SP12 Reading of ' num2str(trmdat(n,42)) ' C.
        '];
else
    n = RP;
    outstring = ['Low-Outlet Reconvergence NOT Detected, setting t to (KEY POINT #10) t
        plus ' num2str(t(n)) ' s with a Smoothed Mid-Axis Low-Outlet Delta T of '
        num2str(MLODeltaT(n)) ' C and a raw SP12 Reading of ' num2str(trmdat(n,42)) ' C.
        '];
end
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
keypoints_ind(10) = n;

% SP Pressures
% Min
[y, ind] = min(trmdat(:,97));
outstring=['Minimum SP Pressure is ' num2str(y) ' psia at t plus ' num2str(t(ind)) ' s'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
% Max
[y, ind] = max(trmdat(:,97));
outstring=['Maximum SP Pressure is ' num2str(y) ' psia at t plus ' num2str(t(ind)) ' s'];

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```

disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
% Beginning
outstring=['Beginning SP Pressure is ' num2str(trmdat(1,97)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
% End
outstring=['Ending SP Pressure is ' num2str(trmdat(end,97)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
% Mean
y = mean(trmdat(:,97));
ind = std(trmdat(:,97));
outstring=['Time-Average SP Pressure is ' num2str(y) ' +/- ' num2str(ind) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% SP Levels
outstring='SP Levels are fully corrected and compensated';
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
% Initial, Pre-start
outstring=['Pre-Start SP Level is ' num2str(coldlevelprestart) ' cm (cold) / '
    num2str(hotlevelprestart) ' cm (hot) at ' num2str(data(1,97)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
% Beginning
outstring=['Beginning Smoothed SP Level is ' num2str(coldlevels(1)) ' cm (cold) / '
    num2str(hotdepth(1)) ' cm (hot) at ' num2str(smoothedP(1)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
% Ending
outstring=['Ending Smoothed SP Level is ' num2str(coldlevels(end)) ' cm (cold) / '
    num2str(hotdepth(end)) ' cm (hot) at ' num2str(smoothedP(end)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
% Min
[y, ind] = min(coldlevels);
outstring=['Minimum Smoothed Cold SP Level is ' num2str(y) ' cm at t plus '
    num2str(t(ind)) ' s and ' num2str(smoothedP(ind)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
[y, ind] = min(hotdepth);
outstring=['Minimum Smoothed Hot SP Level is ' num2str(y) ' cm at t plus ' num2str(t(ind))
    ' s and ' num2str(smoothedP(ind)) ' psia'];
disp(outstring)

```

```

if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
% Max
[y, ind] = max(coldlevels);
outstring=['Maximum Smoothed Cold SP Level is ' num2str(y) ' cm at t plus '
    num2str(t(ind)) ' s and ' num2str(smoothedP(ind)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
[y, ind] = max(hotdepth);
outstring=['Maximum Smoothed Hot SP Level is ' num2str(y) ' cm at t plus ' num2str(t(ind))
    ' s and ' num2str(smoothedP(ind)) ' psia'];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% Temperatures
outstring=['SP 12 Temperature at the beginning is ' num2str(trmdat(1,42)) ' C, and at the
    end is ' num2str(trmdat(end,42)) ' C '];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

% Mixing Number
outstring=['At plume detection, the Mixing Number is '
    num2str(testrelationship(plume_ind)) ' '];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end

[y1, ind1] = min(testrelationship);
[y2, ind2] = max(testrelationship);
outstring = ['The Mixing Number ranges from a minimum of ' num2str(y1) ' at (KEY POINT
    #12) t plus ' num2str(t(ind1)) ' s to a maximum of ' num2str(y2) ' at (KEY POINT
    #13) t plus ' num2str(t(ind2)) ' s; it had a mean value of '
    num2str(mean(testrelationship)) ' +/- ' num2str(std(testrelationship)) ' over the
    test period. '];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
keypoints_ind(12) = ind1;
keypoints_ind(13) = ind2;

% Key Point Data Dumps
outstring=['Key Points have Data Dumps of the following for each Key Point: '
    steampropsdesc];
disp(outstring)
if save_em == 1
    fprintf(filehandle, '%s\r\n', outstring);
end
for n=1:length(keypoints_ind)
    outstring=['KEY POINT #' num2str(n) ' (t plus ' num2str(t(keypoints_ind(n))) ' s with
        a Mixing Number of ' num2str(testrelationship(keypoints_ind(n))) ' ): '
        num2str(steamprops(keypoints_ind(n), :)) ' '];
    disp(outstring)
    if save_em == 1
        fprintf(filehandle, '%s\r\n', outstring);
    end
end
end

```

```

%
% =====
% PLOT GENERATION SECTION
% =====
%

disp(' ')
disp('Generating Plots for the Loaded & Computed Data')

% Smoothed Pool Temperatures
% Create a new figure
fighandle=figure;
text=['Figure', ' ', num2str(fighandle), ' has the smoothed rear pool temperatures.'];
disp(text)

% set up plot
x1 = stratsmooth_0;
y1 = stratsmooth_1;
x2 = stratsmooth_0;
y2 = stratsmooth_3;
x3 = stratsmooth_0;
y3 = stratsmooth_4;
x4 = stratsmooth_0;
y4 = stratsmooth_2;
x5 = stratsmooth_0;
y5 = stratsmooth_5;
x6 = t;
y6 = poolsat;
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x5pdist = floor(x5(end)/11);
x6pdist = floor(x6(end)/3);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);

```



```

for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
x5p = x5(1);
y5p = y5(1);
for ind = 2:length(x5)
    if x5p(end) + x5pdist <= x5(ind)
        % append the point to the array
        x5p = [x5p x5(ind)];
        y5p = [y5p y5(ind)];
    end
end
x6p = x6(1);
y6p = y6(1);
for ind = 2:length(x6)
    if x6p(end) + x6pdist <= x6(ind)
        % append the point to the array
        x6p = [x6p x6(ind)];
        y6p = [y6p y6(ind)];
    end
end
end
ploth1 = plot(x1(1), y1(1), 'b-s', x2(1), y2(1), 'c-^', x3(1), y3(1), 'r-d', x4(1), y4(1),
    'g-p', x5(1), y5(1), 'k-o', x6(1), y6(1), 'k-.*');
% add data lines
hold on
ploth2 = plot(x1, y1, 'b-', x2, y2, 'c-', x3, y3, 'r-', x4, y4, 'g-', x5, y5, 'k-', x6,
    y6, 'k-.');
ploth3 = plot(x1p, y1p, 'bs', x2p, y2p, 'c^', x3p, y3p, 'rd', x4p, y4p, 'gp', x5p, y5p,
    'ko', x6p, y6p, 'k*');
set(ploth1(1), 'MarkerFaceColor', 'b');
set(ploth1(1), 'MarkerEdgeColor', 'k');
set(ploth3(1), 'MarkerFaceColor', 'b');
set(ploth3(1), 'MarkerEdgeColor', 'k');
set(ploth1(2), 'MarkerFaceColor', 'c');
set(ploth1(2), 'MarkerEdgeColor', 'k');
set(ploth3(2), 'MarkerFaceColor', 'c');
set(ploth3(2), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerFaceColor', 'r');
set(ploth1(3), 'MarkerEdgeColor', 'k');
set(ploth3(3), 'MarkerFaceColor', 'r');
set(ploth3(3), 'MarkerEdgeColor', 'k');
set(ploth1(4), 'MarkerFaceColor', 'g');
set(ploth1(4), 'MarkerEdgeColor', 'k');
set(ploth1(4), 'MarkerSize', 10);
set(ploth3(4), 'MarkerFaceColor', 'g');
set(ploth3(4), 'MarkerEdgeColor', 'k');
set(ploth3(4), 'MarkerSize', 10);
set(ploth1(5), 'MarkerFaceColor', 'k');
set(ploth1(5), 'MarkerEdgeColor', 'k');
set(ploth1(5), 'MarkerSize', 5);
set(ploth3(5), 'MarkerFaceColor', 'k');
set(ploth3(5), 'MarkerEdgeColor', 'w');
set(ploth3(5), 'MarkerSize', 5);
set(ploth1(6), 'MarkerSize', 10);
set(ploth3(6), 'MarkerSize', 10);
xlabel('Time, s');
ylabel('Temperature, C');
if showtitles == 1
    title('Smoothed Near-Sparger-End Pool Temperatures');
end
end
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
    0.7]);

```

```

line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold off
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
set(fighandle, 'Position', [48 48 960 624]);
set(fighandle, 'PaperOrientation', 'portrait');
set(fighandle, 'PaperSize', [10 6.5]);
set(fighandle, 'PaperPosition', [0 0 10 6.5]);
figname = [testname '_pool_back_smoothed_temps'];
set(fighandle, 'Name', figname);
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
legendhandle = legend('A - Upper', 'B - Near Sparger (Middle)', 'C - Further from Sparger
(Middle)', 'D - Lower', 'E - Outlet', 'F - Saturation', 'Location', 'NorthWest');
set(legendhandle, 'Color', 'none');
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(fighandle, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(fighandle, [mfigoutdir figname], 'fig')
end

```

```

% Enthalpies

```

```

% Create a new figure
fighandle=figure;
text=['Figure', ' ', num2str(fighandle), ' has the smoothed rear pool enthalpies.'];
disp(text)

```

```

% set up plot
x1 = t;
y1 = htop;
x2 = t;
y2 = hcondensing;
x3 = t;
y3 = hmid;
x4 = t;
y4 = hlow;
x5 = t;
y5 = hout;
x6 = t;
y6 = AdjustedEnth_DS;
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x5pdist = floor(x5(end)/11);
x6pdist = floor(x6(end)/3);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end

```

```

    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
x5p = x5(1);
y5p = y5(1);
for ind = 2:length(x5)
    if x5p(end) + x5pdist <= x5(ind)
        % append the point to the array
        x5p = [x5p x5(ind)];
        y5p = [y5p y5(ind)];
    end
end
x6p = x6(1);
y6p = y6(1);
for ind = 2:length(x6)
    if x6p(end) + x6pdist <= x6(ind)
        % append the point to the array
        x6p = [x6p x6(ind)];
        y6p = [y6p y6(ind)];
    end
end
ploth1 = plot(x1(1), y1(1), 'b-s', x2(1), y2(1), 'c-^', x3(1), y3(1), 'r-d', x4(1), y4(1),
    'g-p', x5(1), y5(1), 'k-o', x6(1), y6(1), 'k:*');
hold on
ploth2 = plot(x1, y1, 'b-', x2, y2, 'c-', x3, y3, 'r-', x4, y4, 'g-', x5, y5, 'k-', x6,
    y6, 'k:');
ploth3 = plot(x1p, y1p, 'bs', x2p, y2p, 'c^', x3p, y3p, 'rd', x4p, y4p, 'gp', x5p, y5p,
    'ko', x6p, y6p, 'k*');
set(ploth1(1), 'MarkerFaceColor', 'b');
set(ploth1(1), 'MarkerEdgeColor', 'k');
set(ploth3(1), 'MarkerFaceColor', 'b');
set(ploth3(1), 'MarkerEdgeColor', 'k');
set(ploth1(2), 'MarkerFaceColor', 'c');
set(ploth1(2), 'MarkerEdgeColor', 'k');
set(ploth3(2), 'MarkerFaceColor', 'c');
set(ploth3(2), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerFaceColor', 'r');
set(ploth1(3), 'MarkerEdgeColor', 'k');
set(ploth3(3), 'MarkerFaceColor', 'r');
set(ploth3(3), 'MarkerEdgeColor', 'k');
set(ploth1(4), 'MarkerFaceColor', 'g');
set(ploth1(4), 'MarkerEdgeColor', 'k');
set(ploth1(4), 'MarkerSize', 10);
set(ploth3(4), 'MarkerFaceColor', 'g');
set(ploth3(4), 'MarkerEdgeColor', 'k');
set(ploth3(4), 'MarkerSize', 10);
set(ploth1(5), 'MarkerFaceColor', 'k');
set(ploth1(5), 'MarkerEdgeColor', 'k');
set(ploth1(5), 'MarkerSize', 5);
set(ploth3(5), 'MarkerFaceColor', 'k');

```

```

set(plots3(5), 'MarkerEdgeColor', 'w');
set(plots3(5), 'MarkerSize', 5);
set(plots1(6), 'MarkerSize', 10);
set(plots3(6), 'MarkerSize', 10);
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold off
if showtitles == 1
    title('Smoothed Near-Sparger End Pool Enthalpies');
end
xlabel('Time, s');
ylabel('Enthalpy, kJ/kg');
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
set(fighandle, 'Position', [48 48 960 624]);
set(fighandle, 'PaperOrientation', 'portrait');
set(fighandle, 'PaperSize', [10 6.5]);
set(fighandle, 'PaperPosition', [0 0 10 6.5]);
figname = [testname '_pool_back_smoothed_enthalpies'];
set(fighandle, 'Name', figname);
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
legendhandle = legend('A - Upper', 'B - Near Sparger (Middle)', 'C - Further from Sparger
(Middle)', 'D - Lower', 'E - Outlet', 'F - Steam In', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(fighandle, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(fighandle, [mfigoutdir figname], 'fig')
end

% Delta T

% Create a new figure
fighandle=figure;
text=['Figure', ' ', num2str(fighandle), ' is the Local Delta T'];
disp(text)

% set up plot
x1 = t;
y1 = stratsmooth_3-stratsmooth_4;
x2 = t;
y2 = stratsmooth_3-stratsmooth_1;
x3 = t;
y3 = poolsat-stratsmooth_3;
x1pdist = floor(x1(end)/5);
x2pdist = floor(x2(end)/6);
x3pdist = floor(x3(end)/7);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
    end
end

```

```

        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
end

[ax,h1,h2] = plotyy(x1, [y1, y2], x3, y3);
hold(ax(1), 'on');
hold(ax(2), 'on');
ploth2a = plot(ax(1), x1(1), y1(1), 'b-s', x2(1), y2(1), 'g-p');
ploth2b = plot(ax(1), x1p, y1p, 'bs', x2p, y2p, 'gp');
ploth3a = plot(ax(2), x3(1), y3(1), 'r-d');
ploth3b = plot(ax(2), x3p, y3p, 'rd');
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold(ax(1), 'off');
hold(ax(2), 'off');
set(ax(2), 'YColor', 'r')
set(h1(1), 'Color', 'b');
set(h1(2), 'Color', 'g');
set(h2, 'Color', 'r');
set(ploth2a(1), 'MarkerEdgeColor', 'k');
set(ploth2a(2), 'MarkerEdgeColor', 'k');
set(ploth2b(1), 'MarkerEdgeColor', 'k');
set(ploth2b(2), 'MarkerEdgeColor', 'k');
set(ploth3a, 'MarkerEdgeColor', 'k');
set(ploth3b, 'MarkerEdgeColor', 'k');
set(ploth2a(1), 'MarkerFaceColor', 'b');
set(ploth2a(2), 'MarkerFaceColor', 'g');
set(ploth2a(2), 'MarkerSize', 10);
set(ploth2b(1), 'MarkerFaceColor', 'b');
set(ploth2b(2), 'MarkerFaceColor', 'g');
set(ploth2b(2), 'MarkerSize', 10);
set(ploth3a, 'MarkerFaceColor', 'r');
set(ploth3b, 'MarkerFaceColor', 'r');
xlabel('Time, s');
if showtitles == 1
    title('Condensing Region Delta T');
end
set(get(ax(1), 'Ylabel'), 'String', 'Delta T, C');
set(get(ax(2), 'Ylabel'), 'String', 'Saturation - Pool Condensing Delta T, C');
set(findall(fighandle, 'type', 'axes'), 'fontSize', 16)
set(findall(fighandle, 'type', 'text'), 'fontSize', 16)
set(fighandle, 'Position', [48 48 960 624]);
set(fighandle, 'PaperOrientation', 'portrait');
set(fighandle, 'PaperSize', [10 6.5]);
set(fighandle, 'PaperPosition', [0 0 10 6.5]);
set(ax(1), 'YTickMode', 'auto');
set(ax(2), 'YTickMode', 'auto');
set(ax(1), 'YLimMode', 'auto');
set(ax(2), 'YLimMode', 'auto');
figname = [testname '_delta_T'];
set(fighandle, 'Name', figname);
set(findall(fighandle, 'type', 'axes'), 'fontSize', 16)
set(findall(fighandle, 'type', 'text'), 'fontSize', 16)
legendhandle = legend([ploth2a, ploth3a], 'A - Condensing - SP9', 'B - Condensing -
Upper', 'C - Saturation - Condensing', 'Location', 'Best');
set(legendhandle, 'Color', 'none');

```

```

% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(fighandle, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(fighandle, [mfigoutdir figname], 'fig')
end

% Delta h, cooling

% Create a new figure
fighandle=figure;
text=['Figure', ' ', num2str(fighandle), ' is the Local Condensing Enthalpy'];
disp(text)

% set up plot
x1 = t;
y1 = AdjustedEnth_DS - hsatL(:,2);
x2 = t;
y2 = AdjustedEnth_DS - hcondensing;
x3 = t;
y3 = mdcondinj;
x4 = t;
if use_turbine == 1
    y4 = mdcondinjcool;
else
    y4 = 0*mdcondinjcool;
end
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end

```

```

end
end
[ax, h1, h2] = plotyy(x1, [y1, y2], x3, [y3, y4]);
hold(ax(1), 'on');
hold(ax(2), 'on');
ploth2a = plot(ax(1), x1(1), y1(1), 'b-s', x2(1), y2(1), 'g-p');
ploth2b = plot(ax(1), x1p, y1p, 'bs', x2p, y2p, 'gp');
ploth3a = plot(ax(2), x3(1), y3(1), 'r-d', x4(1), y4(1), 'm-v');
ploth3b = plot(ax(2), x3p, y3p, 'rd', x4p, y4p, 'mv');
set(h1(1), 'Color', 'b');
set(h1(2), 'Color', 'g');
set(h2(1), 'Color', 'r');
set(h2(2), 'Color', 'm');
set(ploth2a(1), 'MarkerEdgeColor', 'k');
set(ploth2a(2), 'MarkerEdgeColor', 'k');
set(ploth2b(1), 'MarkerEdgeColor', 'k');
set(ploth2b(2), 'MarkerEdgeColor', 'k');
set(ploth3a(1), 'MarkerEdgeColor', 'k');
set(ploth3a(2), 'MarkerEdgeColor', 'k');
set(ploth3b(1), 'MarkerEdgeColor', 'k');
set(ploth3b(2), 'MarkerEdgeColor', 'k');
set(ploth2a(1), 'MarkerFaceColor', 'b');
set(ploth2a(2), 'MarkerFaceColor', 'g');
set(ploth2a(2), 'MarkerSize', 10);
set(ploth2b(1), 'MarkerFaceColor', 'b');
set(ploth2b(2), 'MarkerFaceColor', 'g');
set(ploth2b(2), 'MarkerSize', 10);
set(ploth3a(1), 'MarkerFaceColor', 'r');
set(ploth3a(2), 'MarkerFaceColor', 'm');
set(ploth3b(1), 'MarkerFaceColor', 'r');
set(ploth3b(2), 'MarkerFaceColor', 'm');
xlabel('Time, s');
set(get(ax(1), 'YLabel'), 'String', 'Steam Delta h, kJ/kg');
set(get(ax(2), 'YLabel'), 'String', 'Water mdot, kg/s');
if showtitles == 1
    title('Condensing Region Enthalpy and Massflows');
end
set(findall(fighandle, 'type', 'axes'), 'fontSize', 16)
set(findall(fighandle, 'type', 'text'), 'fontSize', 16)
set(fighandle, 'Position', [48 48 960 624]);
set(fighandle, 'PaperOrientation', 'portrait');
set(fighandle, 'PaperSize', [10 6.5]);
set(fighandle, 'PaperPosition', [0 0 10 6.5]);
set(ax(1), 'YTickMode', 'auto');
set(ax(2), 'YTickMode', 'auto');
set(ax(1), 'YLimMode', 'auto');
set(ax(2), 'YLimMode', 'auto');
rtlims = get(ax(2), 'YLim');
if rtlims(1) < 0
    rtlims(1) = 0;
    % keep chart above zero
end
if use_turbine == 1
    if rtlims(2) > 1.25 * max(mdcondinjcool(stratstartind:stratendind))
        % too high
        rtlims(2) = ceil(1.25 * max(mdcondinjcool(stratstartind:stratendind)));
    end
    if rtlims(2) > 10 * max(mdcondinj)
        rtlims(2) = 10 * max(mdcondinj);
    end
else
    if rtlims(2) > 1.25 * max(mdcondinj)
        % too high
        rtlims(2) = ceil(1.25 * max(mdcondinj));
    end
end
set(ax(2), 'YLim', rtlims);

```

```

line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold(ax(1), 'off');
hold(ax(2), 'off');
figname = [testname '_delta_h'];
set(figure, 'Name', figname);
set(findall(figure, 'type', 'axes'), 'fontSize', 16)
set(findall(figure, 'type', 'text'), 'fontSize', 16)
legendhandle = legend([ploth2a', ploth3a'], 'A - Condensing', 'B - Condensing & Cooling',
'C - mdot - Condensing', 'D - mdot - Condensing & Cooling', 'Location',
'NorthWest');
set(legendhandle, 'Color', 'none');
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(figure, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(figure, [mfigoutdir figname], 'fig')
end
end

```

```

% Pool Temperatures - Outlet End

```

```

% Create a new figure
figure=figure;
text(['Figure', ' ', num2str(figure), ' is the Outlet End Pool Temperature.']);
disp(text)

```

```

% SP 18 is in Column 30
% SP 19 is in Column 28
% SP 20 is in Column 26
% SP 21 is in Column 24
% SP 22 is in Column 22
% SP 23 is in Column 20
% SP Top Flange is in Column 14
% SP Outlet is in Column 74

```

```

% set up plot
x1 = t;
y1 = trmdat(:,28);
x2 = t;
y2 = trmdat(:,26);
x3 = t;
y3 = trmdat(:,24);
x4 = t;
y4 = trmdat(:,22);
x5 = t;
y5 = trmdat(:,20);
x6 = t;
y6 = trmdat(:,74);
x7 = t;
y7 = poolsat;
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x5pdist = floor(x5(end)/11);
x6pdist = floor(x6(end)/13);
x7pdist = floor(x6(end)/3);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
    end
end

```



```

        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
x5p = x5(1);
y5p = y5(1);
for ind = 2:length(x5)
    if x5p(end) + x5pdist <= x5(ind)
        % append the point to the array
        x5p = [x5p x5(ind)];
        y5p = [y5p y5(ind)];
    end
end
x6p = x6(1);
y6p = y6(1);
for ind = 2:length(x6)
    if x6p(end) + x6pdist <= x6(ind)
        % append the point to the array
        x6p = [x6p x6(ind)];
        y6p = [y6p y6(ind)];
    end
end
x7p = x7(1);
y7p = y7(1);
for ind = 2:length(x7)
    if x7p(end) + x7pdist <= x7(ind)
        % append the point to the array
        x7p = [x7p x7(ind)];
        y7p = [y7p y7(ind)];
    end
end
ploth1 = plot(x1(1), y1(1), 'b-s', x2(1), y2(1), 'r-d', x3(1), y3(1), 'g-p', x4(1), y4(1),
    'c-^', x5(1), y5(1), 'm-v', x6(1), y6(1), 'k-o', x7(1), y7(1), 'k-.*');
% add data lines
hold on
ploth2 = plot(x1, y1, 'b-', x2, y2, 'r-', x3, y3, 'g-', x4, y4, 'c-', x5, y5, 'm-', x6,
    y6, 'k-', x7, y7, 'k-.');
ploth3 = plot(x1p, y1p, 'bs', x2p, y2p, 'rd', x3p, y3p, 'gp', x4p, y4p, 'c^', x5p, y5p,
    'mv', x6p, y6p, 'ko', x7p, y7p, 'k*');
set(ploth1(1), 'MarkerFaceColor', 'b');

```

```

set(ploth1(1), 'MarkerEdgeColor', 'k');
set(ploth3(1), 'MarkerFaceColor', 'b');
set(ploth3(1), 'MarkerEdgeColor', 'k');
set(ploth1(2), 'MarkerFaceColor', 'r');
set(ploth1(2), 'MarkerEdgeColor', 'k');
set(ploth3(2), 'MarkerFaceColor', 'r');
set(ploth3(2), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerFaceColor', 'g');
set(ploth1(3), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerSize', 10);
set(ploth3(3), 'MarkerFaceColor', 'g');
set(ploth3(3), 'MarkerEdgeColor', 'k');
set(ploth3(3), 'MarkerSize', 10);
set(ploth1(4), 'MarkerFaceColor', 'c');
set(ploth1(4), 'MarkerEdgeColor', 'k');
set(ploth3(4), 'MarkerFaceColor', 'c');
set(ploth3(4), 'MarkerEdgeColor', 'k');
set(ploth1(5), 'MarkerFaceColor', 'm');
set(ploth1(5), 'MarkerEdgeColor', 'k');
set(ploth3(5), 'MarkerFaceColor', 'm');
set(ploth3(5), 'MarkerEdgeColor', 'k');
set(ploth1(6), 'MarkerFaceColor', 'k');
set(ploth1(6), 'MarkerEdgeColor', 'k');
set(ploth1(6), 'MarkerSize', 5);
set(ploth3(6), 'MarkerFaceColor', 'k');
set(ploth3(6), 'MarkerEdgeColor', 'w');
set(ploth3(6), 'MarkerSize', 5);
set(ploth1(7), 'MarkerSize', 10);
set(ploth3(7), 'MarkerSize', 10);
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold off
if showtitles == 1
    title('Outlet End Pool Temperatures, Facing Away from the Sparger End');
end
xlabel('Time, s');
ylabel('Temperature, C');
legendhandle = legend('A - Upper', 'B - Middle', 'C - Lower', 'D - Left', 'E - Right', 'F
- Bottom Outlet', 'G - Saturation', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_pool_front_temps'];
set(findall(fighandle, 'type', 'axes'), 'fontSize', 16)
set(findall(fighandle, 'type', 'text'), 'fontSize', 16)
set(fighandle, 'Position', [48 48 960 624]);
set(fighandle, 'PaperOrientation', 'portrait');
set(fighandle, 'PaperSize', [10 6.5]);
set(fighandle, 'PaperPosition', [0 0 10 6.5]);
set(fighandle, 'Name', figname);
set(findall(fighandle, 'type', 'axes'), 'fontSize', 16)
set(findall(fighandle, 'type', 'text'), 'fontSize', 16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(fighandle, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(fighandle, [mfigoutdir figname], 'fig')
end

% T & x

% create a new figure
fighandle=figure;
text=['Figure', ' ', num2str(fighandle), ' is the steam temperature and quality.'];
disp(text)

```

```

% set up plot
x1 = t;
y1 = AdjustedQuality(:,1);
x2 = t;
if use_turbine == 1
    y2 = AdjustedQuality(:,2);
else
    y2 = 0*AdjustedQuality(:,2);
end
x3 = t;
y3 = trmdat(:,76);
x4 = t;
y4 = trmdat(:,68);
x5 = t;
y5 = trmdat(:, 66);
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x5pdist = floor(x5(end)/11);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
x5p = x5(1);
y5p = y5(1);
for ind = 2:length(x5)
    if x5p(end) + x5pdist <= x5(ind)
        % append the point to the array
        x5p = [x5p x5(ind)];
        y5p = [y5p y5(ind)];
    end
end
[ax, h1, h2] = plotyy(x1, [y1, y2], x3, [y3, y4, y5]);

```

```

hold(ax(1), 'on');
hold(ax(2), 'on');
ploth2a = plot(ax(1), x1(1), y1(1), 'b-s', x2(1), y2(1), 'g-p');
ploth2b = plot(ax(1), x1p, y1p, 'bs', x2p, y2p, 'gp');
ploth3a = plot(ax(2), x3(1), y3(1), 'r-d', x4(1), y4(1), 'm-v', x5(1), y5(1), 'c-^');
ploth3b = plot(ax(2), x3p, y3p, 'rd', x4p, y4p, 'mv', x5p, y5p, 'c^');
set(ax(1), 'YLimMode', 'auto');
set(ax(2), 'YLimMode', 'auto');
ylvals = get(ax(1), 'YLim');
ylvals(2) = 0.1 * ceil(10*ylvals(2));
if ylvals(1) > 0
    ylvals(1) = 0;
end
set(ax(1), 'YLim', ylvals);
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold(ax(1), 'off');
hold(ax(2), 'off');
set(h1(1), 'Color', 'b');
set(h1(2), 'Color', 'g');
set(h2(1), 'Color', 'r');
set(h2(2), 'Color', 'm');
set(h2(3), 'Color', 'c');
set(ploth2a(1), 'MarkerEdgeColor', 'k');
set(ploth2a(2), 'MarkerEdgeColor', 'k');
set(ploth2b(1), 'MarkerEdgeColor', 'k');
set(ploth2b(2), 'MarkerEdgeColor', 'k');
set(ploth3a(1), 'MarkerEdgeColor', 'k');
set(ploth3a(2), 'MarkerEdgeColor', 'k');
set(ploth3a(3), 'MarkerEdgeColor', 'k');
set(ploth3b(1), 'MarkerEdgeColor', 'k');
set(ploth3b(2), 'MarkerEdgeColor', 'k');
set(ploth3b(3), 'MarkerEdgeColor', 'k');
set(ploth2a(1), 'MarkerFaceColor', 'b');
set(ploth2a(2), 'MarkerFaceColor', 'g');
set(ploth2a(2), 'MarkerSize', 10);
set(ploth2b(1), 'MarkerFaceColor', 'b');
set(ploth2b(2), 'MarkerFaceColor', 'g');
set(ploth2b(2), 'MarkerSize', 10);
set(ploth3a(1), 'MarkerFaceColor', 'r');
set(ploth3a(2), 'MarkerFaceColor', 'm');
set(ploth3a(3), 'MarkerFaceColor', 'c');
set(ploth3b(1), 'MarkerFaceColor', 'r');
set(ploth3b(2), 'MarkerFaceColor', 'm');
set(ploth3b(3), 'MarkerFaceColor', 'c');
xlabel('Time, s');
set(findall(fighandle, 'type', 'axes'), 'fontSize', 16)
set(findall(fighandle, 'type', 'text'), 'fontSize', 16)
set(fighandle, 'Position', [48 48 960 624]);
set(fighandle, 'PaperOrientation', 'portrait');
set(fighandle, 'PaperSize', [10 6.5]);
set(fighandle, 'PaperPosition', [0 0 10 6.5]);
set(get(ax(1), 'Ylabel'), 'String', 'Quality');
set(get(ax(2), 'Ylabel'), 'String', 'Temperature, C');
set(ax(1), 'YTickMode', 'auto');
set(ax(2), 'YTickMode', 'auto');
xlabel('Time, s');
if showtitles == 1
    title('Steam Quality');
end
legendhandle = legend([ploth2a', ploth3a'], 'Estimated Smoothed Steam Quality', 'Turbine
Outlet Smoothed Quality', 'Pre-Injection T', 'Post-Injection T', 'Turbine Outlet
T', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_steam_quality'];

```

```

set(fighandle, 'Name', figname);
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(fighandle, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(fighandle, [mfigoutdir figname], 'fig')
end

% create a new figure
fighandle=figure;
text=['Figure', ' ', num2str(fighandle), ' is the steam flowpath temperature.'];
disp(text)

% Steam Path Temperature Plot

% Steam Generator void temperature is in Column 4
% Vortex Flowmeter Steam Temperature is in Column 82
% Steam Line upstream of Water Injection Temperature is in Column 76
% Steam Line Downstream of Water Injection Temperature in in Column 68
% RCIC Turbine Outlet Temperature is in Column 66
% SP 1 Temperature is in Column 64

% set up plot
x1 = t;
y1 = trmdat(:, 4);
x2 = t;
y2 = trmdat(:, 82);
x3 = t;
y3 = trmdat(:, 76);
x4 = t;
y4 = trmdat(:, 68);
x5 = t;
y5 = trmdat(:, 66);
x6 = t;
y6 = trmdat(:, 64);
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x5pdist = floor(x5(end)/11);
x6pdist = floor(x6(end)/13);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)

```

```

        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
x5p = x5(1);
y5p = y5(1);
for ind = 2:length(x5)
    if x5p(end) + x5pdist <= x5(ind)
        % append the point to the array
        x5p = [x5p x5(ind)];
        y5p = [y5p y5(ind)];
    end
end
x6p = x6(1);
y6p = y6(1);
for ind = 2:length(x6)
    if x6p(end) + x6pdist <= x6(ind)
        % append the point to the array
        x6p = [x6p x6(ind)];
        y6p = [y6p y6(ind)];
    end
end
end

ploth1 = plot(x1(1), y1(1), 'b-s', x2(1), y2(1), 'r-d', x3(1), y3(1), 'g-p', x4(1), y4(1),
    'c-^', x5(1), y5(1), 'm-v', x6(1), y6(1), 'k-o');
% add data lines
hold on
ploth2 = plot(x1, y1, 'b-', x2, y2, 'r-', x3, y3, 'g-', x4, y4, 'c-', x5, y5, 'm-', x6,
    y6, 'k-');
ploth3 = plot(x1p, y1p, 'bs', x2p, y2p, 'rd', x3p, y3p, 'gp', x4p, y4p, 'c^', x5p, y5p,
    'mv', x6p, y6p, 'ko');
set(ploth1(1), 'MarkerFaceColor', 'b');
set(ploth1(1), 'MarkerEdgeColor', 'k');
set(ploth3(1), 'MarkerFaceColor', 'b');
set(ploth3(1), 'MarkerEdgeColor', 'k');
set(ploth1(2), 'MarkerFaceColor', 'r');
set(ploth1(2), 'MarkerEdgeColor', 'k');
set(ploth3(2), 'MarkerFaceColor', 'r');
set(ploth3(2), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerFaceColor', 'g');
set(ploth1(3), 'MarkerEdgeColor', 'k');
set(ploth3(3), 'MarkerFaceColor', 'g');
set(ploth3(3), 'MarkerEdgeColor', 'k');
set(ploth1(4), 'MarkerFaceColor', 'c');
set(ploth1(4), 'MarkerEdgeColor', 'k');
set(ploth3(4), 'MarkerFaceColor', 'c');
set(ploth3(4), 'MarkerEdgeColor', 'k');
set(ploth1(5), 'MarkerFaceColor', 'm');
set(ploth1(5), 'MarkerEdgeColor', 'k');
set(ploth3(5), 'MarkerFaceColor', 'm');
set(ploth3(5), 'MarkerEdgeColor', 'k');
set(ploth1(6), 'MarkerFaceColor', 'k');
set(ploth1(6), 'MarkerEdgeColor', 'k');
set(ploth1(6), 'MarkerSize', 5);
set(ploth3(6), 'MarkerFaceColor', 'k');

```

```

set(plots(6), 'MarkerEdgeColor', 'w');
set(plots(6), 'MarkerSize', 5);
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold off
set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
set(figure, 'Position', [48 48 960 624]);
set(figure, 'PaperOrientation', 'portrait');
set(figure, 'PaperSize', [10 6.5]);
set(figure, 'PaperPosition', [0 0 10 6.5]);
if showtitles == 1
    title('Steam Path Temperatures');
end
xlabel('Time, s');
ylabel('Temperature, C');
legendhandle = legend('Steam Generator Outlet', 'Main Steam Line at Flowmeter', 'Main
    Steam Line Upstream of Water Injection', 'Main Steam Line Downstream of Water
    Injection', 'Turbine Outlet', 'SP1 - RCIC Sparger Outlet', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_steam_temps'];
set(figure, 'Name', figname);
set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(figure, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(figure, [mfigoutdir figname], 'fig')
end
end

```

```

% Water Flowpath Temperature Plot

```

```

% Create a new figure
figure=figure;
text(['Figure', ' ', num2str(figure), ' is the water flowpath temperature.']);
disp(text)

```

```

% SP Outlet Temperature is in Column 74
% RCIC Pump Inlet Temperature is in Column 70
% RCIC Pump Outlet Temperature in in Column 72
% Return Water Flowmeter Temperature is in Column 84
% Steam Generator Water Injection Temperature is in Column 12
% Water Injection to Steam Line is the average of two temperatures
%     Upstream is in Column 78
%     Downstream is in Column 80

```

```

% set up plot
x1 = t;
y1 = trmdat(:, 74);
x2 = t;
y2 = trmdat(:, 70);
x3 = t;
y3 = trmdat(:, 72);
x4 = t;
y4 = trmdat(:, 84);
x5 = t;
y5 = trmdat(:, 12);
x6 = t;
y6 = (0.5*(trmdat(:,78)+trmdat(:,80)));
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);

```

```

x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x5pdist = floor(x5(end)/11);
x6pdist = floor(x6(end)/13);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
x5p = x5(1);
y5p = y5(1);
for ind = 2:length(x5)
    if x5p(end) + x5pdist <= x5(ind)
        % append the point to the array
        x5p = [x5p x5(ind)];
        y5p = [y5p y5(ind)];
    end
end
x6p = x6(1);
y6p = y6(1);
for ind = 2:length(x6)
    if x6p(end) + x6pdist <= x6(ind)
        % append the point to the array
        x6p = [x6p x6(ind)];
        y6p = [y6p y6(ind)];
    end
end
end

ploth1 = plot(x1(1), y1(1), 'b-s', x2(1), y2(1), 'r-d', x3(1), y3(1), 'g-p', x4(1), y4(1),
             'c-^', x5(1), y5(1), 'm-v', x6(1), y6(1), 'k-o');
% add data lines
hold on
ploth2 = plot(x1, y1, 'b-', x2, y2, 'r-', x3, y3, 'g-', x4, y4, 'c-', x5, y5, 'm-', x6,
             y6, 'k-');
ploth3 = plot(x1p, y1p, 'bs', x2p, y2p, 'rd', x3p, y3p, 'gp', x4p, y4p, 'c^', x5p, y5p,
             'mv', x6p, y6p, 'ko');

```



```

set(ploth1(1), 'MarkerFaceColor', 'b');
set(ploth1(1), 'MarkerEdgeColor', 'k');
set(ploth3(1), 'MarkerFaceColor', 'b');
set(ploth3(1), 'MarkerEdgeColor', 'k');
set(ploth1(2), 'MarkerFaceColor', 'r');
set(ploth1(2), 'MarkerEdgeColor', 'k');
set(ploth3(2), 'MarkerFaceColor', 'r');
set(ploth3(2), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerFaceColor', 'g');
set(ploth1(3), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerSize', 10);
set(ploth3(3), 'MarkerFaceColor', 'g');
set(ploth3(3), 'MarkerEdgeColor', 'k');
set(ploth3(3), 'MarkerSize', 10);
set(ploth1(4), 'MarkerFaceColor', 'c');
set(ploth1(4), 'MarkerEdgeColor', 'k');
set(ploth3(4), 'MarkerFaceColor', 'c');
set(ploth3(4), 'MarkerEdgeColor', 'k');
set(ploth1(5), 'MarkerFaceColor', 'm');
set(ploth1(5), 'MarkerEdgeColor', 'k');
set(ploth3(5), 'MarkerFaceColor', 'm');
set(ploth3(5), 'MarkerEdgeColor', 'k');
set(ploth1(6), 'MarkerFaceColor', 'k');
set(ploth1(6), 'MarkerEdgeColor', 'k');
set(ploth1(6), 'MarkerSize', 5);
set(ploth3(6), 'MarkerFaceColor', 'k');
set(ploth3(6), 'MarkerEdgeColor', 'w');
set(ploth3(6), 'MarkerSize', 5);
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold off
set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
set(figure, 'Position', [48 48 960 624]);
set(figure, 'PaperOrientation', 'portrait');
set(figure, 'PaperSize', [10 6.5]);
set(figure, 'PaperPosition', [0 0 10 6.5]);
if showtitles == 1
    title('Water Flowath Temperatures');
end
xlabel('Time, s');
ylabel('Temperature, C');
legendhandle = legend('Suppression Pool Outlet', 'RCIC Pump Inlet', 'RCIC Pump Outlet',
    'Water to Steam Generator Flowmeter', 'Steam Generator Injection Point', 'Avg.
    Water Injection to Steam Line (US & DS)', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_water_flow_temps'];
set(figure, 'Name', figname);
set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(figure, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(figure, [mfigoutdir figname], 'fig')
end

% Pool Temperatures - Upper Horizontal

% Create a new figure
figure=figure;
text=['Figure', ' ', num2str(figure), ' is the axial upper-level pool temperature.'];
disp(text)

```

```

% SP 19 is in Column 28
% SP 11 is in Column 44
% SP 3 is in Column 60

% set up plot
x1 = t;
y1 = trmdat(:,28);
x2 = t;
y2 = trmdat(:,44);
x3 = t;
y3 = trmdat(:,60);
x4 = t;
y4 = poolsat;
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
ploth1 = plot(x1(1), y1(1), 'b-s', x2(1), y2(1), 'r-d', x3(1), y3(1), 'g-p', x4(1), y4(1),
    'k-.*');
% add data lines
hold on
ploth2 = plot(x1, y1, 'b-', x2, y2, 'r-', x3, y3, 'g-', x4, y4, 'k-.');
ploth3 = plot(x1p, y1p, 'bs', x2p, y2p, 'rd', x3p, y3p, 'gp', x4p, y4p, 'k*');
set(ploth1(1), 'MarkerFaceColor', 'b');
set(ploth1(1), 'MarkerEdgeColor', 'k');
set(ploth3(1), 'MarkerFaceColor', 'b');
set(ploth3(1), 'MarkerEdgeColor', 'k');
set(ploth1(2), 'MarkerFaceColor', 'r');
set(ploth1(2), 'MarkerEdgeColor', 'k');
set(ploth3(2), 'MarkerFaceColor', 'r');

```

```

set(plots3(2), 'MarkerEdgeColor', 'k');
set(plots1(3), 'MarkerFaceColor', 'g');
set(plots1(3), 'MarkerEdgeColor', 'k');
set(plots1(3), 'MarkerSize', 10);
set(plots3(3), 'MarkerFaceColor', 'g');
set(plots3(3), 'MarkerEdgeColor', 'k');
set(plots3(3), 'MarkerSize', 10);
set(plots1(4), 'MarkerSize', 10);
set(plots3(4), 'MarkerSize', 10);
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold off
set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
set(figure, 'Position', [48 48 960 624]);
set(figure, 'PaperOrientation', 'portrait');
set(figure, 'PaperSize', [10 6.5]);
set(figure, 'PaperPosition', [0 0 10 6.5]);
if showtitles == 1
    title('Suppression Pool Upper-Level Axial Temperatures');
end
xlabel('Time, s');
ylabel('Temperature, C');
legendhandle = legend('Upper Front', 'Upper Middle', 'Upper Rear', 'Saturation',
    'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_pool_upper_horiz_temps'];
set(figure, 'Name', figname);
set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(figure, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(figure, [mfigoutdir figname], 'fig')
end

% Pool Temperatures - Middle Horizontal

% Create a new figure
figure=figure;
text=['Figure', ' ', num2str(figure), ' is the axial mid-level pool temperature.'];
disp(text)

% SP 4 is in Column 58
% SP 8 is in Column 50
% SP 9 is in Column 48
% SP 10 is in Column 46
% SP 12 is in Column 42
% SP 16 is in Column 34
% SP 17 is in Column 32
% SP 20 is in Column 26
% SP 24 is in Column 18

% set up plot
x1 = t;
y1 = trmdat(:,50);
x2 = t;
y2 = trmdat(:,48);
x3 = t;
y3 = trmdat(:,46);
x4 = t;

```

```

y4 = trmdat(:,42);
x5 = t;
y5 = trmdat(:,34);
x6 = t;
y6 = trmdat(:,32);
x7 = t;
y7 = trmdat(:,26);
x8 = t;
y8 = trmdat(:,18);
x9 = t;
y9 = poolsat;
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x5pdist = floor(x5(end)/11);
x6pdist = floor(x6(end)/13);
x7pdist = floor(x7(end)/(17/2));
x8pdist = floor(x8(end)/(19/2));
x9pdist = floor(x9(end)/3);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
x5p = x5(1);
y5p = y5(1);
for ind = 2:length(x5)
    if x5p(end) + x5pdist <= x5(ind)
        % append the point to the array
        x5p = [x5p x5(ind)];
        y5p = [y5p y5(ind)];
    end
end
x6p = x6(1);
y6p = y6(1);

```

```

for ind = 2:length(x6)
    if x6p(end) + x6pdist <= x6(ind)
        % append the point to the array
        x6p = [x6p x6(ind)];
        y6p = [y6p y6(ind)];
    end
end
x7p = x7(1);
y7p = y7(1);
for ind = 2:length(x7)
    if x7p(end) + x7pdist <= x7(ind)
        % append the point to the array
        x7p = [x7p x7(ind)];
        y7p = [y7p y7(ind)];
    end
end
x8p = x8(1);
y8p = y8(1);
for ind = 2:length(x8)
    if x8p(end) + x8pdist <= x8(ind)
        % append the point to the array
        x8p = [x8p x8(ind)];
        y8p = [y8p y8(ind)];
    end
end
x9p = x9(1);
y9p = y9(1);
for ind = 2:length(x9)
    if x9p(end) + x9pdist <= x9(ind)
        % append the point to the array
        x9p = [x9p x9(ind)];
        y9p = [y9p y9(ind)];
    end
end
ploth1 = plot(x1(1), y1(1), 'b-s', x2(1), y2(1), 'r-d', x3(1), y3(1), 'g-p', x4(1), y4(1),
    'c-^', x5(1), y5(1), 'm-v', x6(1), y6(1), 'k-o', x7(1), y7(1), 'y->', x8(1),
    y8(1), 'y-<', x9(1), y9(1), 'k-.*');
% add data lines
hold on
ploth2 = plot(x1, y1, 'b-', x2, y2, 'r-', x3, y3, 'g-', x4, y4, 'c-', x5, y5, 'm-', x6,
    y6, 'k-', x7, y7, 'y-', x8, y8, 'y-', x9, y9, 'k-.');
ploth3 = plot(x1p, y1p, 'bs', x2p, y2p, 'rd', x3p, y3p, 'gp', x4p, y4p, 'c^', x5p, y5p,
    'mv', x6p, y6p, 'ko', x7p, y7p, 'y>', x8p, y8p, 'y<', x9p, y9p, 'k*');
set(ploth1(7), 'Color', [1, 155/255, 0]);
set(ploth2(7), 'Color', [1, 155/255, 0]);
set(ploth3(7), 'Color', [1, 155/255, 0]);
set(ploth1(8), 'Color', [139/255, 115/255, 85/255]);
set(ploth2(8), 'Color', [139/255, 115/255, 85/255]);
set(ploth3(8), 'Color', [139/255, 115/255, 85/255]);
set(ploth1(1), 'MarkerFaceColor', 'b');
set(ploth1(1), 'MarkerEdgeColor', 'w');
set(ploth3(1), 'MarkerFaceColor', 'b');
set(ploth3(1), 'MarkerEdgeColor', 'w');
set(ploth1(2), 'MarkerFaceColor', 'r');
set(ploth1(2), 'MarkerEdgeColor', 'k');
set(ploth3(2), 'MarkerFaceColor', 'r');
set(ploth3(2), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerFaceColor', 'g');
set(ploth1(3), 'MarkerEdgeColor', 'k');
set(ploth3(3), 'MarkerFaceColor', 'g');
set(ploth3(3), 'MarkerEdgeColor', 'k');
set(ploth3(3), 'MarkerSize', 10);
set(ploth1(4), 'MarkerFaceColor', 'c');
set(ploth1(4), 'MarkerEdgeColor', 'k');
set(ploth3(4), 'MarkerFaceColor', 'c');
set(ploth3(4), 'MarkerEdgeColor', 'k');

```

```

set(plots1(5), 'MarkerFaceColor', 'm');
set(plots1(5), 'MarkerEdgeColor', 'k');
set(plots3(5), 'MarkerFaceColor', 'm');
set(plots3(5), 'MarkerEdgeColor', 'k');
set(plots1(6), 'MarkerFaceColor', 'k');
set(plots1(6), 'MarkerEdgeColor', 'k');
set(plots1(6), 'MarkerSize', 5);
set(plots3(6), 'MarkerFaceColor', 'k');
set(plots3(6), 'MarkerEdgeColor', 'w');
set(plots3(6), 'MarkerSize', 5);
set(plots1(7), 'MarkerFaceColor', [1, 155/255, 0]);
set(plots1(7), 'MarkerEdgeColor', 'k');
set(plots3(7), 'MarkerFaceColor', [1, 155/255, 0]);
set(plots3(7), 'MarkerEdgeColor', 'k');
set(plots1(8), 'MarkerFaceColor', [139/255, 115/255, 85/255]);
set(plots1(8), 'MarkerEdgeColor', 'k');
set(plots3(8), 'MarkerFaceColor', [139/255, 115/255, 85/255]);
set(plots3(8), 'MarkerEdgeColor', 'k');
set(plots1(9), 'MarkerSize', 10);
set(plots3(9), 'MarkerSize', 10);
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold off
set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
set(figure, 'Position', [48 48 960 624]);
set(figure, 'PaperOrientation', 'portrait');
set(figure, 'PaperSize', [10 6.5]);
set(figure, 'PaperPosition', [0 0 10 6.5]);
if showtitles == 1
    title('Suppression Pool Mid-Level Axial Temperatures');
end
xlabel('Time, s');
ylabel('Temperature, C');
legendhandle = legend('A - Near-Sparger (0.63 m)', 'B - 0.94 m', 'C - 1.24 m', 'D - 1.55
m', 'E - 1.85 m', 'F - 2.16 m', 'G - 2.46 m', 'H - Front (2.77 m)', 'J -
Saturation', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_pool_mid_horiz_temps'];
set(figure, 'Name', figname);
set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(figure, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(figure, [mfigoutdir figname], 'fig')
end

% Pool Temperatures - Lower Horizontal

% Create a new figure
figure=figure;
text=['Figure', ' ', num2str(figure), ' is the axial lower-level pool temperature.'];
disp(text)

% SP 21 is in Column 24
% SP 13 is in Column 40
% SP 5 is in Column 56

% set up plot
x1 = t;

```

```

y1 = trmdat(:,24);
x2 = t;
y2 = trmdat(:,40);
x3 = t;
y3 = trmdat(:,56);
x4 = t;
y4 = poolsat;
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
ploth1 = plot(x1(1), y1(1), 'b-s', x2(1), y2(1), 'r-d', x3(1), y3(1), 'g-p', x4(1), y4(1),
    'k-.*');
% add data lines
hold on
ploth2 = plot(x1, y1, 'b-', x2, y2, 'r-', x3, y3, 'g-', x4, y4, 'k-.');
ploth3 = plot(x1p, y1p, 'bs', x2p, y2p, 'rd', x3p, y3p, 'gp', x4p, y4p, 'k*');
set(ploth1(1), 'MarkerFaceColor', 'b');
set(ploth1(1), 'MarkerEdgeColor', 'k');
set(ploth3(1), 'MarkerFaceColor', 'b');
set(ploth3(1), 'MarkerEdgeColor', 'k');
set(ploth1(2), 'MarkerFaceColor', 'r');
set(ploth1(2), 'MarkerEdgeColor', 'k');
set(ploth3(2), 'MarkerFaceColor', 'r');
set(ploth3(2), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerFaceColor', 'g');
set(ploth1(3), 'MarkerEdgeColor', 'k');
set(ploth3(3), 'MarkerFaceColor', 'g');
set(ploth3(3), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerSize', 10);
set(ploth3(3), 'MarkerFaceColor', 'g');
set(ploth3(3), 'MarkerEdgeColor', 'k');
set(ploth3(3), 'MarkerSize', 10);

```

```

set(plots(4), 'MarkerSize', 10);
set(plots(3), 'MarkerSize', 10);
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold off
set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
set(figure, 'Position', [48 48 960 624]);
set(figure, 'PaperOrientation', 'portrait');
set(figure, 'PaperSize', [10 6.5]);
set(figure, 'PaperPosition', [0 0 10 6.5]);
if showtitles == 1
    title('Suppression Pool Lower-Level Axial Temperatures');
end
xlabel('Time, s');
ylabel('Temperature, C');
legendhandle = legend('Lower Front', 'Lower Middle', 'Lower Rear', 'Saturation',
    'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_pool_lower_horiz_temps'];
set(figure, 'Name', figname);
set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(figure, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(figure, [mfigoutdir figname], 'fig')
end

% Pool Temperatures - Sparger End

% Create a new figure
figure=figure;
text=['Figure', ' ', num2str(figure), ' is the Sparger End Pool Temperature.'];
disp(text)

% SP 2 is in Column 62
% SP 3 is in Column 60
% SP 4 is in Column 58
% SP 5 is in Column 56
% SP 6 is in Column 54
% SP 7 is in Column 52

% set up plot
x1 = t;
y1 = trmdat(:, 60);
x2 = t;
y2 = trmdat(:, 58);
x3 = t;
y3 = trmdat(:, 56);
x4 = t;
y4 = trmdat(:, 54);
x5 = t;
y5 = trmdat(:, 52);
x6 = t;
y6 = poolsat;
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x5pdist = floor(x5(end)/11);

```



```

x6pdist = floor(x6(end)/3);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
x5p = x5(1);
y5p = y5(1);
for ind = 2:length(x5)
    if x5p(end) + x5pdist <= x5(ind)
        % append the point to the array
        x5p = [x5p x5(ind)];
        y5p = [y5p y5(ind)];
    end
end
x6p = x6(1);
y6p = y6(1);
for ind = 2:length(x6)
    if x6p(end) + x6pdist <= x6(ind)
        % append the point to the array
        x6p = [x6p x6(ind)];
        y6p = [y6p y6(ind)];
    end
end
ploth1 = plot(x1(1), y1(1), 'b-s', x2(1), y2(1), 'c-^', x3(1), y3(1), 'r-d', x4(1), y4(1),
    'g-p', x5(1), y5(1), 'k-o', x6(1), y6(1), 'k-.*');
% add data lines
hold on
ploth2 = plot(x1, y1, 'b-', x2, y2, 'c-', x3, y3, 'r-', x4, y4, 'g-', x5, y5, 'k-', x6,
    y6, 'k-.');
ploth3 = plot(x1p, y1p, 'bs', x2p, y2p, 'c^', x3p, y3p, 'rd', x4p, y4p, 'gp', x5p, y5p,
    'ko', x6p, y6p, 'k*');
set(ploth1(1), 'MarkerFaceColor', 'b');
set(ploth1(1), 'MarkerEdgeColor', 'k');
set(ploth3(1), 'MarkerFaceColor', 'b');
set(ploth3(1), 'MarkerEdgeColor', 'k');

```

```

set(ploth1(2), 'MarkerFaceColor', 'c');
set(ploth1(2), 'MarkerEdgeColor', 'k');
set(ploth3(2), 'MarkerFaceColor', 'c');
set(ploth3(2), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerFaceColor', 'r');
set(ploth1(3), 'MarkerEdgeColor', 'k');
set(ploth3(3), 'MarkerFaceColor', 'r');
set(ploth3(3), 'MarkerEdgeColor', 'k');
set(ploth1(4), 'MarkerFaceColor', 'g');
set(ploth1(4), 'MarkerEdgeColor', 'k');
set(ploth1(4), 'MarkerSize', 10);
set(ploth3(4), 'MarkerFaceColor', 'g');
set(ploth3(4), 'MarkerEdgeColor', 'k');
set(ploth3(4), 'MarkerSize', 10);
set(ploth1(5), 'MarkerFaceColor', 'k');
set(ploth1(5), 'MarkerEdgeColor', 'k');
set(ploth1(5), 'MarkerSize', 5);
set(ploth3(5), 'MarkerFaceColor', 'k');
set(ploth3(5), 'MarkerEdgeColor', 'w');
set(ploth3(5), 'MarkerSize', 5);
set(ploth1(6), 'MarkerSize', 10);
set(ploth3(6), 'MarkerSize', 10);
rtlims = get(get(fighandle, 'CurrentAxes'), 'YLim');
if rtlims(2) > 1.2 * max(poolsat)
    rtlims(2) = 10 * ceil(1.2*max(poolsat/10));
end
set(get(fighandle, 'CurrentAxes'), 'YLim', rtlims);
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
    0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold off
set(findall(fighandle, 'type', 'axes'), 'fontSize', 16)
set(findall(fighandle, 'type', 'text'), 'fontSize', 16)
set(fighandle, 'Position', [48 48 960 624]);
set(fighandle, 'PaperOrientation', 'portrait');
set(fighandle, 'PaperSize', [10 6.5]);
set(fighandle, 'PaperPosition', [0 0 10 6.5]);
if showtitles == 1
    title('Sparger End Pool Temperatures, Facing Outlet End');
end
xlabel('Time, s');
ylabel('Temperature, C');
legendhandle = legend('A - Upper', 'B - Middle (bad)', 'C - Lower', 'D - Left', 'E -
    Right', 'F - Saturation', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_pool_back_temps'];
set(fighandle, 'Name', figname);
set(findall(fighandle, 'type', 'axes'), 'fontSize', 16)
set(findall(fighandle, 'type', 'text'), 'fontSize', 16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(fighandle, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(fighandle, [mfigoutdir figname], 'fig')
end

% Pool Temperatures - Middle

% Create a new figure
fighandle=figure;
text(['Figure', ' ', num2str(fighandle), ' is the Mid-Axis Pool Temperature.'];
disp(text)

```

```

% SP 11 is in Column 44
% SP 12 is in Column 42
% SP 13 is in Column 40
% SP 14 is in Column 38
% SP 15 is in Column 36

% set up plot
x1 = t;
y1 = trmdat(:, 44);
x2 = t;
y2 = trmdat(:, 42);
x3 = t;
y3 = trmdat(:, 40);
x4 = t;
y4 = trmdat(:, 38);
x5 = t;
y5 = trmdat(:, 36);
x6 = t;
y6 = poolsat;
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x5pdist = floor(x5(end)/11);
x6pdist = floor(x6(end)/3);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
x5p = x5(1);
y5p = y5(1);
for ind = 2:length(x5)
    if x5p(end) + x5pdist <= x5(ind)
        % append the point to the array
        x5p = [x5p x5(ind)];
    end
end

```

```

        y5p = [y5p y5(ind)];
    end
end
x6p = x6(1);
y6p = y6(1);
for ind = 2:length(x6)
    if x6p(end) + x6pdist <= x6(ind)
        % append the point to the array
        x6p = [x6p x6(ind)];
        y6p = [y6p y6(ind)];
    end
end
end
ploth1 = plot(x1(1), y1(1), 'b-s', x2(1), y2(1), 'c-^', x3(1), y3(1), 'r-d', x4(1), y4(1),
    'g-p', x5(1), y5(1), 'k-o', x6(1), y6(1), 'k-.*');
% add data lines
hold on
ploth2 = plot(x1, y1, 'b-', x2, y2, 'c-', x3, y3, 'r-', x4, y4, 'g-', x5, y5, 'k-', x6,
    y6, 'k-.');
ploth3 = plot(x1p, y1p, 'bs', x2p, y2p, 'c^', x3p, y3p, 'rd', x4p, y4p, 'gp', x5p, y5p,
    'ko', x6p, y6p, 'k*');
set(ploth1(1), 'MarkerFaceColor', 'b');
set(ploth1(1), 'MarkerEdgeColor', 'k');
set(ploth3(1), 'MarkerFaceColor', 'b');
set(ploth3(1), 'MarkerEdgeColor', 'k');
set(ploth1(2), 'MarkerFaceColor', 'c');
set(ploth1(2), 'MarkerEdgeColor', 'k');
set(ploth3(2), 'MarkerFaceColor', 'c');
set(ploth3(2), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerFaceColor', 'r');
set(ploth1(3), 'MarkerEdgeColor', 'k');
set(ploth3(3), 'MarkerFaceColor', 'r');
set(ploth3(3), 'MarkerEdgeColor', 'k');
set(ploth1(4), 'MarkerFaceColor', 'g');
set(ploth1(4), 'MarkerEdgeColor', 'k');
set(ploth1(4), 'MarkerSize', 10);
set(ploth3(4), 'MarkerFaceColor', 'g');
set(ploth3(4), 'MarkerEdgeColor', 'k');
set(ploth3(4), 'MarkerSize', 10);
set(ploth1(5), 'MarkerFaceColor', 'k');
set(ploth1(5), 'MarkerEdgeColor', 'k');
set(ploth1(5), 'MarkerSize', 5);
set(ploth3(5), 'MarkerFaceColor', 'k');
set(ploth3(5), 'MarkerEdgeColor', 'w');
set(ploth3(5), 'MarkerSize', 5);
set(ploth1(6), 'MarkerSize', 10);
set(ploth3(6), 'MarkerSize', 10);
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
    0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold off
set(findall(figure, 'type', 'axes'), 'fontSize', 16)
set(findall(figure, 'type', 'text'), 'fontSize', 16)
set(figure, 'Position', [48 48 960 624]);
set(figure, 'PaperOrientation', 'portrait');
set(figure, 'PaperSize', [10 6.5]);
set(figure, 'PaperPosition', [0 0 10 6.5]);
if showtitles == 1
    title('Mid-Axis Pool Temperatures, Facing Outlet End');
end
end
xlabel('Time, s');
ylabel('Temperature, C');
legendhandle = legend('A - Upper', 'B - Middle', 'C - Lower', 'D - Left', 'E - Right', 'F
    - Saturation', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_pool_mid_temps'];
set(figure, 'Name', figname);

```

```

set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
% save to jpeg file
filename = [figname '.jpg'];
if save_em == 1
    print(figure, '-djpeg90', '-r300', [outdir filename]);
    saveas(figure, [mfigoutdir filename], 'fig')
end

% Flowrates

% Create a new figure
figure=figure;
text=['Figure', ' ', num2str(figure), ' is the Flowrate.'];
disp(text)

% Steam Flowrate (kg/s) is in Column 107
% Water Return Flowrate (kg/s) is in Column 102
% Water Injection to Steam Line (kg/s) is in Column 127

% set up plot
x1 = t;
y1 = 1000*trmdat(:,107);
x2 = t;
y2 = 1000*trmdat(:,102);
x3 = t;
y3 = 1000*trmdat(:,127);
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
plot(x1(1), y1(1), 'b-s', x2(1), y2(1), 'c^', x3(1), y3(1), 'r-d');
% add data lines
hold on
plot(x1, y1, 'b-', x2, y2, 'c-', x3, y3, 'r-');
plot(x1p, y1p, 'bs', x2p, y2p, 'c^', x3p, y3p, 'rd');
set(plot(1), 'MarkerFaceColor', 'b');
set(plot(1), 'MarkerEdgeColor', 'k');

```

```

set(plots3(1), 'MarkerFaceColor', 'b');
set(plots3(1), 'MarkerEdgeColor', 'k');
set(plots1(2), 'MarkerFaceColor', 'c');
set(plots1(2), 'MarkerEdgeColor', 'k');
set(plots3(2), 'MarkerFaceColor', 'c');
set(plots3(2), 'MarkerEdgeColor', 'k');
set(plots1(3), 'MarkerFaceColor', 'r');
set(plots1(3), 'MarkerEdgeColor', 'k');
set(plots3(3), 'MarkerFaceColor', 'r');
set(plots3(3), 'MarkerEdgeColor', 'k');
set(get(figure, 'CurrentAxes'), 'YLim', [0 25*ceil(mean(1000*trmdat(:,102))/18.75)]);
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold off
set(findall(figure, 'type', 'axes'), 'fontSize', 16)
set(findall(figure, 'type', 'text'), 'fontSize', 16)
set(figure, 'Position', [48 48 960 624]);
set(figure, 'PaperOrientation', 'portrait');
set(figure, 'PaperSize', [10 6.5]);
set(figure, 'PaperPosition', [0 0 10 6.5]);
if showtitles == 1
    title('Mass Flow Rates');
end
xlabel('Time, s');
ylabel('Flowrate, g/s');
legendhandle = legend('Steam Flowrate', 'Water Return to Steam Generator', 'Water
Injection to Steam Line', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_flowrates'];
set(figure, 'Name', figname);
set(findall(figure, 'type', 'axes'), 'fontSize', 16)
set(findall(figure, 'type', 'text'), 'fontSize', 16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(figure, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(figure, [mfigoutdir figname], 'fig')
end

% Pressures

% Create a new figure
figure=figure;
text(['Figure', ' ', num2str(figure), ' is the Gas Pressure.']);
disp(text)

% SG Pressure is in Column 88
% MSL Pressure is in Column 110
% SP Pressure is in Column 97

% set up plot
x1 = t;
y1 = trmdat(:,88);
x2 = t;
y2 = trmdat(:,110);
x3 = t;
y3 = trmdat(:,97);
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x1p = x1(1);
y1p = y1(1);

```

```

for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
ploth1 = plot(x1(1), y1(1), 'b-s', x2(1), y2(1), 'c-^', x3(1), y3(1), 'r-d');
% add data lines
hold on
ploth2 = plot(x1, y1, 'b-', x2, y2, 'c-', x3, y3, 'r-');
ploth3 = plot(x1p, y1p, 'bs', x2p, y2p, 'c^', x3p, y3p, 'rd');
set(ploth1(1), 'MarkerFaceColor', 'b');
set(ploth1(1), 'MarkerEdgeColor', 'k');
set(ploth3(1), 'MarkerFaceColor', 'b');
set(ploth3(1), 'MarkerEdgeColor', 'k');
set(ploth1(2), 'MarkerFaceColor', 'c');
set(ploth1(2), 'MarkerEdgeColor', 'k');
set(ploth3(2), 'MarkerFaceColor', 'c');
set(ploth3(2), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerFaceColor', 'r');
set(ploth1(3), 'MarkerEdgeColor', 'k');
set(ploth3(3), 'MarkerFaceColor', 'r');
set(ploth3(3), 'MarkerEdgeColor', 'k');
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold off
set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
set(figure, 'Position', [48 48 960 624]);
set(figure, 'PaperOrientation', 'portrait');
set(figure, 'PaperSize', [10 6.5]);
set(figure, 'PaperPosition', [0 0 10 6.5]);
if showtitles == 1
    title('System Vapor Space Pressures');
end
xlabel('Time, s');
ylabel('Pressure, psia');
legendhandle = legend('Steam Generator', 'Main Steam Line', 'Suppression Chamber',
    'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_pressures'];
set(figure, 'Name', figname);
set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
% save to jpeg file
fileoutname = [figname '.jpg'];

```

```

if save_em == 1
    print(fighandle, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(fighandle, [mfigoutdir figname], 'fig')
end

% Turbine

% Create a new figure
fighandle=figure;
text=['Figure', ' ', num2str(fighandle), ' is the Turbine/Sparger Performance.'];
disp(text)

% Turbine Inlet Temperature is in Column 68
% Turbine Outlet Temperature is in Column 66
% Sparger Outlet Temperature in Column 64
% Sparger Delta P is in Column 113

% set up plot
x1 = t;
y1 = trmdat(:,68);
x2 = t;
y2 = trmdat(:,66);
x3 = t;
y3 = trmdat(:,64);
x4 = t;
y4 = trmdat(:,113) - spargeroffset;
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end

```



```

end
end
[ax, h1, h2] = plotyy(x1, [y1, y2, y3], x4, [y4]);
hold(ax(1), 'on');
hold(ax(2), 'on');
ploth2a = plot(ax(1), x1(1), y1(1), 'b-s', x2(1), y2(1), 'g-p', x3(1), y3(1), 'r-d');
ploth2b = plot(ax(1), x1p, y1p, 'bs', x2p, y2p, 'gp', x3p, y3p, 'rd');
ploth3a = plot(ax(2), x4(1), y4(1), 'm-v');
ploth3b = plot(ax(2), x4p, y4p, 'mv');
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold(ax(1), 'off');
hold(ax(2), 'off');
set(ax(2), 'YColor', 'm')
set(h1(1), 'Color', 'b');
set(h1(2), 'Color', 'g');
set(h1(3), 'Color', 'r');
set(h2(1), 'Color', 'm');
set(ploth2a(1), 'MarkerEdgeColor', 'k');
set(ploth2a(2), 'MarkerEdgeColor', 'k');
set(ploth2a(3), 'MarkerEdgeColor', 'k');
set(ploth2b(1), 'MarkerEdgeColor', 'k');
set(ploth2b(2), 'MarkerEdgeColor', 'k');
set(ploth2b(3), 'MarkerEdgeColor', 'k');
set(ploth3a(1), 'MarkerEdgeColor', 'k');
set(ploth3b(1), 'MarkerEdgeColor', 'k');
set(ploth2a(1), 'MarkerFaceColor', 'b');
set(ploth2a(2), 'MarkerFaceColor', 'g');
set(ploth2a(2), 'MarkerSize', 10);
set(ploth2a(3), 'MarkerFaceColor', 'r');
set(ploth2b(1), 'MarkerFaceColor', 'b');
set(ploth2b(2), 'MarkerFaceColor', 'g');
set(ploth2b(2), 'MarkerSize', 10);
set(ploth2b(3), 'MarkerFaceColor', 'r');
set(ploth3a(1), 'MarkerFaceColor', 'm');
set(ploth3b(1), 'MarkerFaceColor', 'm');
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
set(fighandle, 'Position', [48 48 960 624]);
set(fighandle, 'PaperOrientation', 'portrait');
set(fighandle, 'PaperSize', [10 6.5]);
set(fighandle, 'PaperPosition', [0 0 10 6.5]);
set(get(ax(1),'Ylabel'),'String','Temperature, C');
set(get(ax(2),'Ylabel'),'String','Sparger DP, inH2O');
set(ax(1), 'YTickMode', 'auto');
set(ax(2), 'YTickMode', 'auto');
set(ax(1), 'YLimMode', 'auto');
set(ax(2), 'YLimMode', 'auto');
xlabel('Time, s');
if showtitles == 1
    title('RCIC Turbine Analog/Sparger Performance');
end
legendhandle = legend([ploth2a', ploth3a'], 'A - Turbine Analog Inlet T', 'B - Turbine
Analog Outlet T', 'C - Sparger Outlet T', 'D - Sparger DP', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_turbine'];
set(fighandle, 'Name', figname);
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(fighandle, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(fighandle, [mfigoutdir figname], 'fig')
end
end

```

```

% Vertical-Horizontal Pool Thermal Profile NO SP 4

% Create a new figure
fighandle=figure;
text=['Figure', ' ', num2str(fighandle), ' is the Vert-Horiz Center Thermal Profile.'];
disp(text)

% SP 3 is in Column 60
% SP 4 is in Column 58 -- bad, don't use
% SP 5 is in Column 56
% SP 11 is in Column 44
% SP 12 is in Column 42
% SP 13 is in Column 40
% SP 19 is in Column 28
% SP 20 is in Column 26
% SP 21 is in Column 24
% SP Outlet is in Column 74

% set up plot
x1 = t;
y1 = trmdat(:, 60);
x2 = t;
y2 = trmdat(:, 56);
x3 = t;
y3 = trmdat(:, 44);
x4 = t;
y4 = trmdat(:, 42);
x5 = t;
y5 = trmdat(:, 40);
x6 = t;
y6 = trmdat(:, 28);
x7 = t;
y7 = trmdat(:, 26);
x8 = t;
y8 = trmdat(:, 24);
x9 = t;
y9 = trmdat(:, 74);
x10 = t;
y10 = poolsat;
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x5pdist = floor(x5(end)/11);
x6pdist = floor(x6(end)/13);
x7pdist = floor(x7(end)/(17/2));
x8pdist = floor(x8(end)/(19/2));
x9pdist = floor(x9(end)/(23/2));
x10pdist = floor(x10(end)/3);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array

```

```

        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
x5p = x5(1);
y5p = y5(1);
for ind = 2:length(x5)
    if x5p(end) + x5pdist <= x5(ind)
        % append the point to the array
        x5p = [x5p x5(ind)];
        y5p = [y5p y5(ind)];
    end
end
x6p = x6(1);
y6p = y6(1);
for ind = 2:length(x6)
    if x6p(end) + x6pdist <= x6(ind)
        % append the point to the array
        x6p = [x6p x6(ind)];
        y6p = [y6p y6(ind)];
    end
end
x7p = x7(1);
y7p = y7(1);
for ind = 2:length(x7)
    if x7p(end) + x7pdist <= x7(ind)
        % append the point to the array
        x7p = [x7p x7(ind)];
        y7p = [y7p y7(ind)];
    end
end
x8p = x8(1);
y8p = y8(1);
for ind = 2:length(x8)
    if x8p(end) + x8pdist <= x8(ind)
        % append the point to the array
        x8p = [x8p x8(ind)];
        y8p = [y8p y8(ind)];
    end
end
x9p = x9(1);
y9p = y9(1);
for ind = 2:length(x9)
    if x9p(end) + x9pdist <= x9(ind)
        % append the point to the array
        x9p = [x9p x9(ind)];
        y9p = [y9p y9(ind)];
    end
end
end

```

```

x10p = x10(1);
y10p = y10(1);
for ind = 2:length(x10)
    if x10p(end) + x10pdist <= x10(ind)
        % append the point to the array
        x10p = [x10p x10(ind)];
        y10p = [y10p y10(ind)];
    end
end
end
ploth1 = plot(x1(1), y1(1), 'b-s', x2(1), y2(1), 'r-d', x3(1), y3(1), 'g-p', x4(1), y4(1),
    'c-^', x5(1), y5(1), 'm-v', x6(1), y6(1), 'k-o', x7(1), y7(1), 'y->', x8(1),
    y8(1), 'y-<', x9(1), y9(1), 'y-h', x10(1), y10(1), 'k-.*');
% add data lines
hold on
ploth2 = plot(x1, y1, 'b-', x2, y2, 'r-', x3, y3, 'g-', x4, y4, 'c-', x5, y5, 'm-', x6,
    y6, 'k-', x7, y7, 'y-', x8, y8, 'y-', x9, y9, 'y-', x10, y10, 'k-.');
ploth3 = plot(x1p, y1p, 'bs', x2p, y2p, 'rd', x3p, y3p, 'gp', x4p, y4p, 'c^', x5p, y5p,
    'mv', x6p, y6p, 'ko', x7p, y7p, 'y>', x8p, y8p, 'y<', x9p, y9p, 'yh', x10p, y10p,
    'k*');

set(ploth1(7), 'Color', [1, 155/255, 0]);
set(ploth2(7), 'Color', [1, 155/255, 0]);
set(ploth3(7), 'Color', [1, 155/255, 0]);
set(ploth1(8), 'Color', [139/255, 115/255, 85/255]);
set(ploth2(8), 'Color', [139/255, 115/255, 85/255]);
set(ploth3(8), 'Color', [139/255, 115/255, 85/255]);
set(ploth1(9), 'Color', [0/255, 0.4, 0/255]);
set(ploth2(9), 'Color', [0/255, 0.4, 0/255]);
set(ploth3(9), 'Color', [0/255, 0.4, 0/255]);

set(ploth1(1), 'MarkerFaceColor', 'b');
set(ploth1(1), 'MarkerEdgeColor', 'w');
set(ploth3(1), 'MarkerFaceColor', 'b');
set(ploth3(1), 'MarkerEdgeColor', 'w');
set(ploth1(2), 'MarkerFaceColor', 'r');
set(ploth1(2), 'MarkerEdgeColor', 'k');
set(ploth3(2), 'MarkerFaceColor', 'r');
set(ploth3(2), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerFaceColor', 'g');
set(ploth1(3), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerSize', 10);
set(ploth3(3), 'MarkerFaceColor', 'g');
set(ploth3(3), 'MarkerEdgeColor', 'k');
set(ploth3(3), 'MarkerSize', 10);
set(ploth1(4), 'MarkerFaceColor', 'c');
set(ploth1(4), 'MarkerEdgeColor', 'k');
set(ploth3(4), 'MarkerFaceColor', 'c');
set(ploth3(4), 'MarkerEdgeColor', 'k');
set(ploth1(5), 'MarkerFaceColor', 'm');
set(ploth1(5), 'MarkerEdgeColor', 'k');
set(ploth3(5), 'MarkerFaceColor', 'm');
set(ploth3(5), 'MarkerEdgeColor', 'k');
set(ploth1(6), 'MarkerFaceColor', 'k');
set(ploth1(6), 'MarkerEdgeColor', 'k');
set(ploth1(6), 'MarkerSize', 5);
set(ploth3(6), 'MarkerFaceColor', 'k');
set(ploth3(6), 'MarkerEdgeColor', 'w');
set(ploth3(6), 'MarkerSize', 5);
set(ploth1(7), 'MarkerFaceColor', [1, 155/255, 0]);
set(ploth1(7), 'MarkerEdgeColor', 'k');
set(ploth3(7), 'MarkerFaceColor', [1, 155/255, 0]);
set(ploth3(7), 'MarkerEdgeColor', 'k');
set(ploth1(8), 'MarkerFaceColor', [139/255, 115/255, 85/255]);
set(ploth1(8), 'MarkerEdgeColor', 'k');
set(ploth3(8), 'MarkerFaceColor', [139/255, 115/255, 85/255]);
set(ploth3(8), 'MarkerEdgeColor', 'k');
set(ploth1(9), 'MarkerFaceColor', [0/255, 0.4, 0/255]);
set(ploth1(9), 'MarkerEdgeColor', 'k');
set(ploth1(9), 'MarkerSize', 10);

```

```

set(plots3(9), 'MarkerFaceColor', [0/255, 0.4, 0/255]);
set(plots3(9), 'MarkerEdgeColor', 'k');
set(plots3(9), 'MarkerSize', 10);
set(plots1(10), 'MarkerSize', 10);
set(plots3(10), 'MarkerSize', 10);
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold off
set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
set(figure, 'Position', [48 48 960 624]);
set(figure, 'PaperOrientation', 'portrait');
set(figure, 'PaperSize', [10 6.5]);
set(figure, 'PaperPosition', [0 0 10 6.5]);
if showtitles == 1
    title('Horizontal & Vertical Pool Thermal Profile');
end
xlabel('Time, s');
ylabel('Temperature, C');
legendhandle = legend('Rear Upper', 'Rear Lower', 'Mid Upper', 'Mid Middle', 'Mid Lower',
    'Front Upper', 'Front Middle', 'Front Lower', 'Bottom Outlet', 'Saturation',
    'Location', 'NorthWest');
set(legendhandle, 'Color', 'none');
figname = [testname '_pool_vert_horiz_temps_noSP4'];
set(figure, 'Name', figname);
set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(figure, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(figure, [mfigoutdir figname], 'fig')
end

% Air-Vertical Middle Profile

% Create a new figure
figure=figure;
text=['Figure', ' ', num2str(figure), ' is the Air-Water VertHoriz Thermal Profile.'];
disp(text)

% SP 2 is in Column 62 (rear air)
% SP 3 is in Column 60 (rear top)
% SP 11 is in Column 44 (mid-top)
% SP 12 is in Column 42 (mid-mid)
% SP 13 is in Column 40 (mid-low)
% SP 18 is in Column 30 (front air)
% SP 19 is in Column 28 (front upper)
% SP Outlet is in Column 74

% set up plot
x1 = t;
y1 = trmdat(:, 60);
x2 = t;
y2 = trmdat(:, 44);
x3 = t;
y3 = trmdat(:, 28);
x4 = t;
y4 = trmdat(:, 42);
x5 = t;
y5 = trmdat(:, 40);
x6 = t;

```

```

y6 = trmdat(:, 74);
x7 = t;
y7 = trmdat(:, 62);
x8 = t;
y8 = trmdat(:, 30);
x9 = t;
y9 = poolsat;
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x5pdist = floor(x5(end)/11);
x6pdist = floor(x6(end)/13);
x7pdist = floor(x7(end)/(17/2));
x8pdist = floor(x8(end)/(19/2));
x9pdist = floor(x9(end)/3);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
x5p = x5(1);
y5p = y5(1);
for ind = 2:length(x5)
    if x5p(end) + x5pdist <= x5(ind)
        % append the point to the array
        x5p = [x5p x5(ind)];
        y5p = [y5p y5(ind)];
    end
end
x6p = x6(1);
y6p = y6(1);
for ind = 2:length(x6)
    if x6p(end) + x6pdist <= x6(ind)
        % append the point to the array
        x6p = [x6p x6(ind)];
    end
end

```

```

        y6p = [y6p y6(ind)];
    end
end
x7p = x7(1);
y7p = y7(1);
for ind = 2:length(x7)
    if x7p(end) + x7pdist <= x7(ind)
        % append the point to the array
        x7p = [x7p x7(ind)];
        y7p = [y7p y7(ind)];
    end
end
x8p = x8(1);
y8p = y8(1);
for ind = 2:length(x8)
    if x8p(end) + x8pdist <= x8(ind)
        % append the point to the array
        x8p = [x8p x8(ind)];
        y8p = [y8p y8(ind)];
    end
end
x9p = x9(1);
y9p = y9(1);
for ind = 2:length(x9)
    if x9p(end) + x9pdist <= x9(ind)
        % append the point to the array
        x9p = [x9p x9(ind)];
        y9p = [y9p y9(ind)];
    end
end
ploth1 = plot(x1(1), y1(1), 'b-s', x2(1), y2(1), 'r-d', x3(1), y3(1), 'g-p', x4(1), y4(1),
    'c-^', x5(1), y5(1), 'm-v', x6(1), y6(1), 'k-o', x7(1), y7(1), 'y->', x8(1),
    y8(1), 'y-<', x9(1), y9(1), 'k-.*');
% add data lines
hold on
ploth2 = plot(x1, y1, 'b-', x2, y2, 'r-', x3, y3, 'g-', x4, y4, 'c-', x5, y5, 'm-', x6,
    y6, 'k-', x7, y7, 'y-', x8, y8, 'y-', x9, y9, 'k-.');
ploth3 = plot(x1p, y1p, 'bs', x2p, y2p, 'rd', x3p, y3p, 'gp', x4p, y4p, 'c^', x5p, y5p,
    'mv', x6p, y6p, 'ko', x7p, y7p, 'y>', x8p, y8p, 'y<', x9p, y9p, 'k*');
set(ploth1(7), 'Color', [1, 155/255, 0]);
set(ploth2(7), 'Color', [1, 155/255, 0]);
set(ploth3(7), 'Color', [1, 155/255, 0]);
set(ploth1(8), 'Color', [139/255, 115/255, 85/255]);
set(ploth2(8), 'Color', [139/255, 115/255, 85/255]);
set(ploth3(8), 'Color', [139/255, 115/255, 85/255]);
set(ploth1(1), 'MarkerFaceColor', 'b');
set(ploth1(1), 'MarkerEdgeColor', 'w');
set(ploth3(1), 'MarkerFaceColor', 'b');
set(ploth3(1), 'MarkerEdgeColor', 'w');
set(ploth1(2), 'MarkerFaceColor', 'r');
set(ploth1(2), 'MarkerEdgeColor', 'k');
set(ploth3(2), 'MarkerFaceColor', 'r');
set(ploth3(2), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerFaceColor', 'g');
set(ploth1(3), 'MarkerEdgeColor', 'k');
set(ploth3(3), 'MarkerFaceColor', 'g');
set(ploth3(3), 'MarkerEdgeColor', 'k');
set(ploth3(3), 'MarkerSize', 10);
set(ploth1(4), 'MarkerFaceColor', 'c');
set(ploth1(4), 'MarkerEdgeColor', 'k');
set(ploth3(4), 'MarkerFaceColor', 'c');
set(ploth3(4), 'MarkerEdgeColor', 'k');
set(ploth1(5), 'MarkerFaceColor', 'm');
set(ploth1(5), 'MarkerEdgeColor', 'k');
set(ploth3(5), 'MarkerFaceColor', 'm');
set(ploth3(5), 'MarkerEdgeColor', 'k');

```

```

set(plots1(6), 'MarkerFaceColor', 'k');
set(plots1(6), 'MarkerEdgeColor', 'k');
set(plots1(6), 'MarkerSize', 5);
set(plots3(6), 'MarkerFaceColor', 'k');
set(plots3(6), 'MarkerEdgeColor', 'w');
set(plots3(6), 'MarkerSize', 5);
set(plots1(7), 'MarkerFaceColor', [1, 155/255, 0]);
set(plots1(7), 'MarkerEdgeColor', 'k');
set(plots3(7), 'MarkerFaceColor', [1, 155/255, 0]);
set(plots3(7), 'MarkerEdgeColor', 'k');
set(plots1(8), 'MarkerFaceColor', [139/255, 115/255, 85/255]);
set(plots1(8), 'MarkerEdgeColor', 'k');
set(plots3(8), 'MarkerFaceColor', [139/255, 115/255, 85/255]);
set(plots3(8), 'MarkerEdgeColor', 'k');
set(plots1(9), 'MarkerSize', 10);
set(plots3(9), 'MarkerSize', 10);
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold off
set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
set(figure, 'Position', [48 48 960 624]);
set(figure, 'PaperOrientation', 'portrait');
set(figure, 'PaperSize', [10 6.5]);
set(figure, 'PaperPosition', [0 0 10 6.5]);
if showtitles == 1
    title('Suppression Pool Axial Air & Water Temperatures');
end
xlabel('Time, s');
ylabel('Temperature, C');
legendhandle = legend('A - Rear Upper', 'B - Mid Upper', 'C - Front Upper', 'D - Mid
Middle', 'E - Mid Lower', 'F - Outlet', 'G - Rear Airspace', 'H - Front Airspace',
'J - Saturation', 'Location', 'NorthWest');
set(legendhandle, 'Color', 'none');
figname = [testname '_pool_axial_air_water_temps'];
set(figure, 'Name', figname);
set(findall(figure,'type','axes'),'fontSize',16)
set(findall(figure,'type','text'),'fontSize',16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(figure, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(figure, [mfigoutdir figname], 'fig')
end

% Slopes (Temperature changerates)

% Create a new figure
figure=figure;
text=['Figure', ' ', num2str(figure), ' has the 5-minute Rear Temperature
Changerates.'];
disp(text)

% set up plot
x1 = data(sindex(1):sindex(3)-inclusionlen, 1) - data(sindex(1), 1);
y1 = 60*vsmooth_top(sindex(1):sindex(3)-inclusionlen, 1);
x2 = data(sindex(1):sindex(3)-inclusionlen, 1) - data(sindex(1), 1);
y2 = 60*vsmooth_hot(sindex(1):sindex(3)-inclusionlen, 1);
x3 = data(sindex(1):sindex(3)-inclusionlen, 1) - data(sindex(1), 1);
y3 = 60*vsmooth_mid(sindex(1):sindex(3)-inclusionlen, 1);
x4 = data(sindex(1):sindex(3)-inclusionlen, 1) - data(sindex(1), 1);
y4 = 60*vsmooth_low(sindex(1):sindex(3)-inclusionlen, 1);

```



```

x5 = data(sindex(1):sindex(3)-inclusionlen, 1) - data(sindex(1), 1);
y5 = 60*vsmooth_out(sindex(1):sindex(3)-inclusionlen, 1);
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x5pdist = floor(x5(end)/11);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
x5p = x5(1);
y5p = y5(1);
for ind = 2:length(x5)
    if x5p(end) + x5pdist <= x5(ind)
        % append the point to the array
        x5p = [x5p x5(ind)];
        y5p = [y5p y5(ind)];
    end
end
ploth1 = plot(x1(1), y1(1), 'b-s', x3(1), y3(1), 'r-d', x4(1), y4(1), 'g-p', x5(1), y5(1),
    'k-o');
hold on
ploth2 = plot(x1, y1, 'b-', x3, y3, 'r-', x4, y4, 'g-', x5, y5, 'k-');
ploth3 = plot(x1p, y1p, 'bs', x3p, y3p, 'rd', x4p, y4p, 'gp', x5p, y5p, 'ko');
set(ploth1(1), 'MarkerFaceColor', 'b');
set(ploth1(1), 'MarkerEdgeColor', 'k');
set(ploth3(1), 'MarkerFaceColor', 'b');
set(ploth3(1), 'MarkerEdgeColor', 'k');
set(ploth1(2), 'MarkerFaceColor', 'r');
set(ploth1(2), 'MarkerEdgeColor', 'k');
set(ploth3(2), 'MarkerFaceColor', 'r');
set(ploth3(2), 'MarkerEdgeColor', 'k');
set(ploth1(3), 'MarkerFaceColor', 'g');
set(ploth1(3), 'MarkerEdgeColor', 'k');

```

```

set(plots1(3), 'MarkerSize', 10);
set(plots3(3), 'MarkerFaceColor', 'g');
set(plots3(3), 'MarkerEdgeColor', 'k');
set(plots3(3), 'MarkerSize', 10);
set(plots1(4), 'MarkerFaceColor', 'k');
set(plots1(4), 'MarkerEdgeColor', 'k');
set(plots1(4), 'MarkerSize', 5);
set(plots3(4), 'MarkerFaceColor', 'k');
set(plots3(4), 'MarkerEdgeColor', 'w');
set(plots3(4), 'MarkerSize', 5);
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold off
if showtitles == 1
    title('Smoothed Rear Temperature Changerates');
end
xlabel('Time, s');
ylabel('Smoothed Changerate, degrees/min');
set(findall(fighandle, 'type', 'axes'), 'fontSize', 16)
set(findall(fighandle, 'type', 'text'), 'fontSize', 16)
set(fighandle, 'Position', [48 48 960 624]);
set(fighandle, 'PaperOrientation', 'portrait');
set(fighandle, 'PaperSize', [10 6.5]);
set(fighandle, 'PaperPosition', [0 0 10 6.5]);
figname = [testname '_pool_back_smoothed_changerates'];
set(fighandle, 'Name', figname);
set(findall(fighandle, 'type', 'axes'), 'fontSize', 16)
set(findall(fighandle, 'type', 'text'), 'fontSize', 16)
legendhandle = legend('A - Upper', 'C - 12 in. from Sparger (Middle)', 'D - Lower', 'E -
Outlet', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(fighandle, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(fighandle, [mfigoutdir figname], 'fig')
end

```

```

% Slope Differences: Top-Middle (Temperature changerates)

```

```

% Create a new figure
fighandle=figure;
text=['Figure', ' ', num2str(fighandle), ' has the 5-minute Top-Mid Rear Temperature
Changerate Differences.'];
disp(text)

```

```

% set up plot
x1 = data(sindex(1):sindex(3)-inclusionlen, 1) - data(sindex(1), 1);
y1 = (vsmooth_top(sindex(1):sindex(3)-inclusionlen, 2) - vsmooth_mid(sindex(1):sindex(3)-
inclusionlen, 2));
x2 = data(sindex(1):sindex(3)-inclusionlen, 1) - data(sindex(1), 1);
y2 = 60*stopmid;
x1pdist = floor(x1(end)/9);
x2pdist = floor(x1(end)/11);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end

```

```

end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
[ax, h1, h2] = plotyy(x1, [y1], x2, [y2]);
hold(ax(1), 'on');
hold(ax(2), 'on');
ploth2a = plot(ax(1), x1(1), y1(1), 'b-s');
ploth2b = plot(ax(1), x1p, y1p, 'bs');
ploth3a = plot(ax(2), x2(1), y2(1), 'r-d');
ploth3b = plot(ax(2), x2p, y2p, 'rd');
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold(ax(1), 'off');
hold(ax(2), 'off');
set(ax(1), 'YColor', 'b');
set(ax(2), 'YColor', 'r');
set(h1(1), 'Color', 'b');
set(h2(1), 'Color', 'r');
set(ploth2a(1), 'MarkerEdgeColor', 'k');
set(ploth2b(1), 'MarkerEdgeColor', 'k');
set(ploth3a(1), 'MarkerEdgeColor', 'k');
set(ploth3b(1), 'MarkerEdgeColor', 'k');
set(ploth2a(1), 'MarkerFaceColor', 'b');
set(ploth2b(1), 'MarkerFaceColor', 'b');
set(ploth3a(1), 'MarkerFaceColor', 'r');
set(ploth3b(1), 'MarkerFaceColor', 'r');
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
set(fighandle, 'Position', [48 48 960 624]);
set(fighandle, 'PaperOrientation', 'portrait');
set(fighandle, 'PaperSize', [10 6.5]);
set(fighandle, 'PaperPosition', [0 0 10 6.5]);
set(get(ax(1), 'Ylabel'), 'String', 'Smoothed Temperature Difference, C');
set(get(ax(2), 'Ylabel'), 'String', 'Smoothed dT/dt Difference, Degrees/min');
set(ax(1), 'YTickMode', 'auto');
set(ax(2), 'YTickMode', 'auto');
set(ax(1), 'YLimMode', 'auto');
set(ax(2), 'YLimMode', 'auto');
xlabel('Time, s');
if showtitles == 1
    title('5-Minute Smoothed Rear Temperature & Changerate Differences');
end
legendhandle = legend([ploth2a', ploth3a'], 'A - Rear Top-Middle T(t) Difference', 'B -
Rear Top-Middle dT/dt Difference', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_pool_back_smoothed_changerate_difference_topmid'];
set(fighandle, 'Name', figname);
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(fighandle, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(fighandle, [mfigoutdir figname], 'fig')
end

```

```

% Slope Differences: Mid-Low (Temperature changerates)

% Create a new figure
fighandle=figure;
text=['Figure', ' ', num2str(fighandle), ' has the 5-minute Mid-Low Rear Temperature
      Changerate Differences.'];
disp(text)

% set up plot
x1 = data(sindex(1):sindex(3)-inclusionlen, 1) - data(sindex(1), 1);
y1 = (vsmooth_mid(sindex(1):sindex(3)-inclusionlen, 2) - vsmooth_low(sindex(1):sindex(3)-
      inclusionlen,2));
x2 = data(sindex(1):sindex(3)-inclusionlen, 1) - data(sindex(1), 1);
y2 = 60*smidlow;
x1pdist = floor(x1(end)/9);
x2pdist = floor(x1(end)/11);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
[ax, h1, h2] = plotyy(x1, [y1], x2, [y2]);
hold(ax(1), 'on');
hold(ax(2), 'on');
ploth2a = plot(ax(1), x1(1), y1(1), 'b-s');
ploth2b = plot(ax(1), x1p, y1p, 'bs');
ploth3a = plot(ax(2), x2(1), y2(1), 'r-d');
ploth3b = plot(ax(2), x2p, y2p, 'rd');
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold(ax(1), 'off');
hold(ax(2), 'off');
set(ax(1), 'YColor', 'b');
set(ax(2), 'YColor', 'r');
set(h1(1), 'Color', 'b');
set(h2(1), 'Color', 'r');
set(ploth2a(1), 'MarkerEdgeColor', 'k');
set(ploth2b(1), 'MarkerEdgeColor', 'k');
set(ploth3a(1), 'MarkerEdgeColor', 'k');
set(ploth3b(1), 'MarkerEdgeColor', 'k');
set(ploth2a(1), 'MarkerFaceColor', 'b');
set(ploth2b(1), 'MarkerFaceColor', 'b');
set(ploth3a(1), 'MarkerFaceColor', 'r');
set(ploth3b(1), 'MarkerFaceColor', 'r');
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
set(fighandle, 'Position', [48 48 960 624]);
set(fighandle, 'PaperOrientation', 'portrait');
set(fighandle, 'PaperSize', [10 6.5]);
set(fighandle, 'PaperPosition', [0 0 10 6.5]);
set(get(ax(1), 'Ylabel'), 'String', 'Smoothed Temperature Difference, C');

```

```

set(get(ax(2), 'Ylabel'), 'String', 'Smoothed dT/dt Difference, Degrees/min');
set(ax(1), 'YTickMode', 'auto');
set(ax(2), 'YTickMode', 'auto');
set(ax(1), 'YLimMode', 'auto');
set(ax(2), 'YLimMode', 'auto');
xlabel('Time, s');
if showtitles == 1
    title('5-Minute Smoothed Rear Temperature & Changerate Differences');
end
legendhandle = legend([ploth2a', ploth3a'], 'A - Rear Middle-Low T(t) Difference', 'B -
    Rear Middle-Low dT/dt Difference', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_pool_back_smoothed_changerate_difference_midlow'];
set(fighandle, 'Name', figname);
set(findall(fighandle, 'type', 'axes'), 'fontSize', 16)
set(findall(fighandle, 'type', 'text'), 'fontSize', 16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(fighandle, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(fighandle, [mfigoutdir figname], 'fig')
end

% Slope Differences: Low-Out (Temperature changerates)

% Create a new figure
fighandle=figure;
text=['Figure', ' ', num2str(fighandle), ' has the 5-minute Low-Out Rear Temperature
    Changerate Differences.'];
disp(text)

% set up plot
x1 = data(sindex(1):sindex(3)-inclusionlen, 1) - data(sindex(1), 1);
y1 = (vsmooth_low(sindex(1):sindex(3)-inclusionlen, 2) - vsmooth_out(sindex(1):sindex(3)-
    inclusionlen, 2));
x2 = data(sindex(1):sindex(3)-inclusionlen, 1) - data(sindex(1), 1);
y2 = 60*slowout;
x1pdist = floor(x1(end)/9);
x2pdist = floor(x1(end)/11);
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
[ax, h1, h2] = plotyy(x1, [y1], x2, [y2]);
hold(ax(1), 'on');
hold(ax(2), 'on');
ploth2a = plot(ax(1), x1(1), y1(1), 'b-s');
ploth2b = plot(ax(1), x1p, y1p, 'bs');
ploth3a = plot(ax(2), x2(1), y2(1), 'r-d');
ploth3b = plot(ax(2), x2p, y2p, 'rd');

```

```

line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold(ax(1), 'off');
hold(ax(2), 'off');
set(ax(1), 'YColor', 'b')
set(ax(2), 'YColor', 'r')
set(h1(1), 'Color', 'b');
set(h2(1), 'Color', 'r');
set(ploth2a(1), 'MarkerEdgeColor', 'k');
set(ploth2b(1), 'MarkerEdgeColor', 'k');
set(ploth3a(1), 'MarkerEdgeColor', 'k');
set(ploth3b(1), 'MarkerEdgeColor', 'k');
set(ploth2a(1), 'MarkerFaceColor', 'b');
set(ploth2b(1), 'MarkerFaceColor', 'b');
set(ploth3a(1), 'MarkerFaceColor', 'r');
set(ploth3b(1), 'MarkerFaceColor', 'r');
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
set(fighandle, 'Position', [48 48 960 624]);
set(fighandle, 'PaperOrientation', 'portrait');
set(fighandle, 'PaperSize', [10 6.5]);
set(fighandle, 'PaperPosition', [0 0 10 6.5]);
set(get(ax(1),'Ylabel'),'String','Smoothed Temperature Difference, C');
set(get(ax(2),'Ylabel'),'String','Smoothed dT/dt Difference, Degrees/min');
set(ax(1), 'YTickMode', 'auto');
set(ax(2), 'YTickMode', 'auto');
set(ax(1), 'YLimMode', 'auto');
set(ax(2), 'YLimMode', 'auto');
xlabel('Time, s');
if showtitles == 1
    title('5-Minute Smoothed Rear Temperature & Changerate Differences');
end
legendhandle = legend([ploth2a, ploth3a], 'A - Rear Lower-Outlet T(t) Difference', 'B -
Rear Lower-Outlet dT/dt Difference', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_pool_back_smoothed_changerate_difference_lowout'];
set(fighandle, 'Name', figname);
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(fighandle, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(fighandle, [mfigoutdir figname], 'fig')
end

% Mixing Number

% Smoothed Pool Temperatures
% Create a new figure
fighandle=figure;
text=['Figure', ' ', num2str(fighandle), ' has the smoothed rear pool temperatures and
the Mixing Number (Type 1).'];
disp(text)

% set up plot
x1 = stratsmooth_0;
y1 = stratsmooth_1;
x2 = stratsmooth_0;
y2 = stratsmooth_3;
x3 = stratsmooth_0;
y3 = stratsmooth_4;

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```

x4 = stratsmooth_0;
y4 = stratsmooth_2;
x5 = stratsmooth_0;
y5 = stratsmooth_5;
x6 = t;
y6 = poolsat;
x7 = t;
y7 = testrelationship;
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x5pdist = floor(x5(end)/11);
x6pdist = floor(x6(end)/3);
x7pdist = floor(x7(end)/(13));
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
x5p = x5(1);
y5p = y5(1);
for ind = 2:length(x5)
    if x5p(end) + x5pdist <= x5(ind)
        % append the point to the array
        x5p = [x5p x5(ind)];
        y5p = [y5p y5(ind)];
    end
end
x6p = x6(1);
y6p = y6(1);
for ind = 2:length(x6)
    if x6p(end) + x6pdist <= x6(ind)
        % append the point to the array
        x6p = [x6p x6(ind)];
        y6p = [y6p y6(ind)];
    end
end

```

```

end
end
x7p = x7(1);
y7p = y7(1);
for ind = 2:length(x7)
    if x7p(end) + x7pdist <= x7(ind)
        % append the point to the array
        x7p = [x7p x7(ind)];
        y7p = [y7p y7(ind)];
    end
end
end
[ax, h1, h2] = plotyy(x1, [y1, y2, y3, y4, y5, y6], x7, [y7]);
hold(ax(1), 'on');
hold(ax(2), 'on');
ploth2a = plot(ax(1), x1(1), y1(1), 'b-s', x2(1), y2(1), 'c-^', x3(1), y3(1), 'r-d',
    x4(1), y4(1), 'g-p', x5(1), y5(1), 'k-o', x6(1), y6(1), 'k-.*');
ploth2b = plot(ax(1), x1p, y1p, 'bs', x2p, y2p, 'c^', x3p, y3p, 'rd', x4p, y4p, 'gp', x5p,
    y5p, 'ko', x6p, y6p, 'k*');
ploth3a = plot(ax(2), x7(1), y7(1), 'm-v');
ploth3b = plot(ax(2), x7p, y7p, 'mv');
set(ax(1), 'YLimMode', 'auto');
set(ax(2), 'YLimMode', 'auto');
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
    0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold(ax(1), 'off');
hold(ax(2), 'off');
set(ax(2), 'YColor', 'm')
set(h1(1), 'Color', 'b');
set(h1(2), 'Color', 'c');
set(h1(3), 'Color', 'r');
set(h1(4), 'Color', 'g');
set(h1(5), 'Color', 'k');
set(h1(6), 'Color', 'k');
set(h1(6), 'LineStyle', '-.');
set(h2(1), 'Color', 'm');
set(ploth2a(1), 'MarkerEdgeColor', 'k');
set(ploth2a(2), 'MarkerEdgeColor', 'k');
set(ploth2a(3), 'MarkerEdgeColor', 'k');
set(ploth2a(4), 'MarkerEdgeColor', 'k');
set(ploth2a(5), 'MarkerEdgeColor', 'k');
set(ploth2a(6), 'MarkerEdgeColor', 'k');
set(ploth2b(1), 'MarkerEdgeColor', 'k');
set(ploth2b(2), 'MarkerEdgeColor', 'k');
set(ploth2b(3), 'MarkerEdgeColor', 'k');
set(ploth2b(4), 'MarkerEdgeColor', 'k');
set(ploth2b(5), 'MarkerEdgeColor', 'w');
set(ploth2b(6), 'MarkerEdgeColor', 'k');
set(ploth3a(1), 'MarkerEdgeColor', 'k');
set(ploth3b(1), 'MarkerEdgeColor', 'k');
set(ploth2a(1), 'MarkerFaceColor', 'b');
set(ploth2a(2), 'MarkerFaceColor', 'c');
set(ploth2a(3), 'MarkerFaceColor', 'r');
set(ploth2a(4), 'MarkerFaceColor', 'g');
set(ploth2a(4), 'MarkerSize', 10);
set(ploth2a(5), 'MarkerFaceColor', 'k');
set(ploth2a(5), 'MarkerSize', 5);
set(ploth2a(6), 'MarkerFaceColor', 'k');
set(ploth2b(1), 'MarkerFaceColor', 'b');
set(ploth2b(2), 'MarkerFaceColor', 'c');
set(ploth2b(3), 'MarkerFaceColor', 'r');
set(ploth2b(4), 'MarkerFaceColor', 'g');
set(ploth2b(4), 'MarkerSize', 10);
set(ploth2b(5), 'MarkerFaceColor', 'k');
set(ploth2b(5), 'MarkerSize', 5);
set(ploth2b(6), 'MarkerFaceColor', 'k');

```



```

set(ploth3a(1), 'MarkerFaceColor', 'm');
set(ploth3b(1), 'MarkerFaceColor', 'm');
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
set(fighandle, 'Position', [48 48 960 624]);
set(fighandle, 'PaperOrientation', 'portrait');
set(fighandle, 'PaperSize', [10 6.5]);
set(fighandle, 'PaperPosition', [0 0 10 6.5]);
set(get(ax(1), 'Ylabel'), 'String', 'Temperature, C');
set(get(ax(2), 'Ylabel'), 'String', 'Mixing Number (nondimensional)');
set(ax(1), 'YTickMode', 'auto');
set(ax(2), 'YTickMode', 'auto');
xlabel('Time, s');
if showtitles == 1
    title('Smoothed Rear Pool Temperatures and the Mixing Number (Type 1)');
end
legendhandle = legend([ploth2a', ploth3a'], 'A - Upper', 'B - Near Sparger (Middle)', 'C
    - Further from Sparger (Middle)', 'D - Lower', 'E - Outlet', 'F - Saturation', 'G
    - Mixing Number 1', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_crazynumber_t1'];
set(fighandle, 'Name', figname);
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(fighandle, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(fighandle, [mfigoutdir figname], 'fig')
end

% Smoothed Pool Temperatures
% Create a new figure
fighandle=figure;
text=['Figure', ' ', num2str(fighandle), ' has the smoothed rear pool temperatures and
    the Mixing Number (Type 2).'];
disp(text)

% set up plot
x1 = stratsmooth_0;
y1 = stratsmooth_1;
x2 = stratsmooth_0;
y2 = stratsmooth_3;
x3 = stratsmooth_0;
y3 = stratsmooth_4;
x4 = stratsmooth_0;
y4 = stratsmooth_2;
x5 = stratsmooth_0;
y5 = stratsmooth_5;
x6 = t;
y6 = poolsat;
x7 = t;
y7 = testrelationship2;
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x5pdist = floor(x5(end)/11);
x6pdist = floor(x6(end)/3);
x7pdist = floor(x7(end)/(13));
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
    end
end

```

```

        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
x5p = x5(1);
y5p = y5(1);
for ind = 2:length(x5)
    if x5p(end) + x5pdist <= x5(ind)
        % append the point to the array
        x5p = [x5p x5(ind)];
        y5p = [y5p y5(ind)];
    end
end
x6p = x6(1);
y6p = y6(1);
for ind = 2:length(x6)
    if x6p(end) + x6pdist <= x6(ind)
        % append the point to the array
        x6p = [x6p x6(ind)];
        y6p = [y6p y6(ind)];
    end
end
x7p = x7(1);
y7p = y7(1);
for ind = 2:length(x7)
    if x7p(end) + x7pdist <= x7(ind)
        % append the point to the array
        x7p = [x7p x7(ind)];
        y7p = [y7p y7(ind)];
    end
end
[ax, h1, h2] = plotyy(x1, [y1, y2, y3, y4, y5, y6], x7, [y7]);
hold(ax(1), 'on');
hold(ax(2), 'on');
ploth2a = plot(ax(1), x1(1), y1(1), 'b-s', x2(1), y2(1), 'c-^', x3(1), y3(1), 'r-d',
    x4(1), y4(1), 'g-p', x5(1), y5(1), 'k-o', x6(1), y6(1), 'k-.*');
ploth2b = plot(ax(1), x1p, y1p, 'bs', x2p, y2p, 'c^', x3p, y3p, 'rd', x4p, y4p, 'gp', x5p,
    y5p, 'ko', x6p, y6p, 'k*');
ploth3a = plot(ax(2), x7(1), y7(1), 'm-v');
ploth3b = plot(ax(2), x7p, y7p, 'mv');
set(ax(1), 'YLimMode', 'auto');

```

```

set(ax(2), 'YLimMode', 'auto');
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold(ax(1), 'off');
hold(ax(2), 'off');
set(ax(2), 'YColor', 'm')
set(h1(1), 'Color', 'b');
set(h1(2), 'Color', 'c');
set(h1(3), 'Color', 'r');
set(h1(4), 'Color', 'g');
set(h1(5), 'Color', 'k');
set(h1(6), 'Color', 'k');
set(h1(6), 'LineStyle', '-. ');
set(h2(1), 'Color', 'm');
set(plots2a(1), 'MarkerEdgeColor', 'k');
set(plots2a(2), 'MarkerEdgeColor', 'k');
set(plots2a(3), 'MarkerEdgeColor', 'k');
set(plots2a(4), 'MarkerEdgeColor', 'k');
set(plots2a(5), 'MarkerEdgeColor', 'k');
set(plots2a(6), 'MarkerEdgeColor', 'k');
set(plots2b(1), 'MarkerEdgeColor', 'k');
set(plots2b(2), 'MarkerEdgeColor', 'k');
set(plots2b(3), 'MarkerEdgeColor', 'k');
set(plots2b(4), 'MarkerEdgeColor', 'k');
set(plots2b(5), 'MarkerEdgeColor', 'w');
set(plots2b(6), 'MarkerEdgeColor', 'k');
set(plots3a(1), 'MarkerEdgeColor', 'k');
set(plots3b(1), 'MarkerEdgeColor', 'k');
set(plots2a(1), 'MarkerFaceColor', 'b');
set(plots2a(2), 'MarkerFaceColor', 'c');
set(plots2a(3), 'MarkerFaceColor', 'r');
set(plots2a(4), 'MarkerFaceColor', 'g');
set(plots2a(4), 'MarkerSize', 10);
set(plots2a(5), 'MarkerFaceColor', 'k');
set(plots2a(5), 'MarkerSize', 5);
set(plots2a(6), 'MarkerFaceColor', 'k');
set(plots2b(1), 'MarkerFaceColor', 'b');
set(plots2b(2), 'MarkerFaceColor', 'c');
set(plots2b(3), 'MarkerFaceColor', 'r');
set(plots2b(4), 'MarkerFaceColor', 'g');
set(plots2b(4), 'MarkerSize', 10);
set(plots2b(5), 'MarkerFaceColor', 'k');
set(plots2b(5), 'MarkerSize', 5);
set(plots2b(6), 'MarkerFaceColor', 'k');
set(plots3a(1), 'MarkerFaceColor', 'm');
set(plots3b(1), 'MarkerFaceColor', 'm');
set(findall(fighandle, 'type', 'axes'), 'fontSize', 16)
set(findall(fighandle, 'type', 'text'), 'fontSize', 16)
set(fighandle, 'Position', [48 48 960 624]);
set(fighandle, 'PaperOrientation', 'portrait');
set(fighandle, 'PaperSize', [10 6.5]);
set(fighandle, 'PaperPosition', [0 0 10 6.5]);
set(get(ax(1), 'Ylabel'), 'String', 'Temperature, C');
set(get(ax(2), 'Ylabel'), 'String', 'Mixing Number (nondimensional)');
set(ax(1), 'YTickMode', 'auto');
set(ax(2), 'YTickMode', 'auto');
xlabel('Time, s');
if showtitles == 1
    title('Smoothed Rear Pool Temperatures and the Mixing Number (Type 2)');
end
legendhandle = legend([plots2a', plots3a'], 'A - Upper', 'B - Near Sparger (Middle)', 'C
- Further from Sparger (Middle)', 'D - Lower', 'E - Outlet', 'F - Saturation', 'G
- Mixing Number 2', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_crazynumber_t2'];

```

```

set(fighandle, 'Name', figname);
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(fighandle, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(fighandle, [mfigoutdir figname], 'fig')
end

% Smoothed Pool Temperatures
% Create a new figure
fighandle=figure;
text=['Figure', ' ', num2str(fighandle), ' has the smoothed rear pool temperatures and
      the Mixing Number (Type 3).'];
disp(text)

% set up plot
x1 = stratsmooth_0;
y1 = stratsmooth_1;
x2 = stratsmooth_0;
y2 = stratsmooth_3;
x3 = stratsmooth_0;
y3 = stratsmooth_4;
x4 = stratsmooth_0;
y4 = stratsmooth_2;
x5 = stratsmooth_0;
y5 = stratsmooth_5;
x6 = t;
y6 = poolsat;
x7 = t;
y7 = testrelationship3;
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x5pdist = floor(x5(end)/11);
x6pdist = floor(x6(end)/3);
x7pdist = floor(x7(end)/(13));
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end

```

```

        end
    end
    x4p = x4(1);
    y4p = y4(1);
    for ind = 2:length(x4)
        if x4p(end) + x4pdist <= x4(ind)
            % append the point to the array
            x4p = [x4p x4(ind)];
            y4p = [y4p y4(ind)];
        end
    end
    x5p = x5(1);
    y5p = y5(1);
    for ind = 2:length(x5)
        if x5p(end) + x5pdist <= x5(ind)
            % append the point to the array
            x5p = [x5p x5(ind)];
            y5p = [y5p y5(ind)];
        end
    end
    x6p = x6(1);
    y6p = y6(1);
    for ind = 2:length(x6)
        if x6p(end) + x6pdist <= x6(ind)
            % append the point to the array
            x6p = [x6p x6(ind)];
            y6p = [y6p y6(ind)];
        end
    end
    x7p = x7(1);
    y7p = y7(1);
    for ind = 2:length(x7)
        if x7p(end) + x7pdist <= x7(ind)
            % append the point to the array
            x7p = [x7p x7(ind)];
            y7p = [y7p y7(ind)];
        end
    end
    [ax, h1, h2] = plotyy(x1, [y1, y2, y3, y4, y5, y6], x7, [y7]);
    hold(ax(1), 'on');
    hold(ax(2), 'on');
    ploth2a = plot(ax(1), x1(1), y1(1), 'b-s', x2(1), y2(1), 'c-^', x3(1), y3(1), 'r-d',
        x4(1), y4(1), 'g-p', x5(1), y5(1), 'k-o', x6(1), y6(1), 'k-.*');
    ploth2b = plot(ax(1), x1p, y1p, 'bs', x2p, y2p, 'c^', x3p, y3p, 'rd', x4p, y4p, 'gp', x5p,
        y5p, 'ko', x6p, y6p, 'k*');
    ploth3a = plot(ax(2), x7(1), y7(1), 'm-v');
    ploth3b = plot(ax(2), x7p, y7p, 'mv');
    set(ax(1), 'YLimMode', 'auto');
    set(ax(2), 'YLimMode', 'auto');
    line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
    line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
        0.7]);
    line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
    hold(ax(1), 'off');
    hold(ax(2), 'off');
    set(ax(2), 'YColor', 'm');
    set(h1(1), 'Color', 'b');
    set(h1(2), 'Color', 'c');
    set(h1(3), 'Color', 'r');
    set(h1(4), 'Color', 'g');
    set(h1(5), 'Color', 'k');
    set(h1(6), 'Color', 'k');
    set(h1(6), 'LineStyle', '-.');
    set(h2(1), 'Color', 'm');
    set(ploth2a(1), 'MarkerEdgeColor', 'k');
    set(ploth2a(2), 'MarkerEdgeColor', 'k');
    set(ploth2a(3), 'MarkerEdgeColor', 'k');

```

```

set(ploth2a(4), 'MarkerEdgeColor', 'k');
set(ploth2a(5), 'MarkerEdgeColor', 'k');
set(ploth2a(6), 'MarkerEdgeColor', 'k');
set(ploth2b(1), 'MarkerEdgeColor', 'k');
set(ploth2b(2), 'MarkerEdgeColor', 'k');
set(ploth2b(3), 'MarkerEdgeColor', 'k');
set(ploth2b(4), 'MarkerEdgeColor', 'k');
set(ploth2b(5), 'MarkerEdgeColor', 'w');
set(ploth2b(6), 'MarkerEdgeColor', 'k');
set(ploth3a(1), 'MarkerEdgeColor', 'k');
set(ploth3b(1), 'MarkerEdgeColor', 'k');
set(ploth2a(1), 'MarkerFaceColor', 'b');
set(ploth2a(2), 'MarkerFaceColor', 'c');
set(ploth2a(3), 'MarkerFaceColor', 'r');
set(ploth2a(4), 'MarkerFaceColor', 'g');
set(ploth2a(4), 'MarkerSize', 10);
set(ploth2a(5), 'MarkerFaceColor', 'k');
set(ploth2a(5), 'MarkerSize', 5);
set(ploth2a(6), 'MarkerFaceColor', 'k');
set(ploth2b(1), 'MarkerFaceColor', 'b');
set(ploth2b(2), 'MarkerFaceColor', 'c');
set(ploth2b(3), 'MarkerFaceColor', 'r');
set(ploth2b(4), 'MarkerFaceColor', 'g');
set(ploth2b(4), 'MarkerSize', 10);
set(ploth2b(5), 'MarkerFaceColor', 'k');
set(ploth2b(5), 'MarkerSize', 5);
set(ploth2b(6), 'MarkerFaceColor', 'k');
set(ploth3a(1), 'MarkerFaceColor', 'm');
set(ploth3b(1), 'MarkerFaceColor', 'm');
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
set(fighandle, 'Position', [48 48 960 624]);
set(fighandle, 'PaperOrientation', 'portrait');
set(fighandle, 'PaperSize', [10 6.5]);
set(fighandle, 'PaperPosition', [0 0 10 6.5]);
set(get(ax(1), 'Ylabel'), 'String', 'Temperature, C');
set(get(ax(2), 'Ylabel'), 'String', 'Mixing Number (nondimensional)');
set(ax(1), 'YTickMode', 'auto');
set(ax(2), 'YTickMode', 'auto');
xlabel('Time, s');
if showtitles == 1
    title('Smoothed Rear Pool Temperatures and the Mixing Number (Type 3)');
end
legendhandle = legend([ploth2a, ploth3a], 'A - Upper', 'B - Near Sparger (Middle)', 'C
- Further from Sparger (Middle)', 'D - Lower', 'E - Outlet', 'F - Saturation', 'G
- Mixing Number 3', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_crazynumber_t3'];
set(fighandle, 'Name', figname);
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(fighandle, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(fighandle, [mfigoutdir figname], 'fig')
end

% Smoothed Pool Temperatures
% Create a new figure
fighandle=figure;
text=['Figure', ' ', num2str(fighandle), ' has the smoothed rear pool temperatures and
the Mixing Number (Type 4).'];
disp(text)

```

```

% set up plot
x1 = stratsmooth_0;
y1 = stratsmooth_1;
x2 = stratsmooth_0;
y2 = stratsmooth_3;
x3 = stratsmooth_0;
y3 = stratsmooth_4;
x4 = stratsmooth_0;
y4 = stratsmooth_2;
x5 = stratsmooth_0;
y5 = stratsmooth_5;
x6 = t;
y6 = poolsat;
x7 = t;
y7 = testrelationship4;
x1pdist = floor(x1(end)/4);
x2pdist = floor(x2(end)/5);
x3pdist = floor(x3(end)/7);
x4pdist = floor(x4(end)/9);
x5pdist = floor(x5(end)/11);
x6pdist = floor(x6(end)/3);
x7pdist = floor(x7(end)/(13));
x1p = x1(1);
y1p = y1(1);
for ind = 2:length(x1)
    if x1p(end) + x1pdist <= x1(ind)
        % append the point to the array
        x1p = [x1p x1(ind)];
        y1p = [y1p y1(ind)];
    end
end
x2p = x2(1);
y2p = y2(1);
for ind = 2:length(x2)
    if x2p(end) + x2pdist <= x2(ind)
        % append the point to the array
        x2p = [x2p x2(ind)];
        y2p = [y2p y2(ind)];
    end
end
x3p = x3(1);
y3p = y3(1);
for ind = 2:length(x3)
    if x3p(end) + x3pdist <= x3(ind)
        % append the point to the array
        x3p = [x3p x3(ind)];
        y3p = [y3p y3(ind)];
    end
end
x4p = x4(1);
y4p = y4(1);
for ind = 2:length(x4)
    if x4p(end) + x4pdist <= x4(ind)
        % append the point to the array
        x4p = [x4p x4(ind)];
        y4p = [y4p y4(ind)];
    end
end
x5p = x5(1);
y5p = y5(1);
for ind = 2:length(x5)
    if x5p(end) + x5pdist <= x5(ind)
        % append the point to the array
        x5p = [x5p x5(ind)];
        y5p = [y5p y5(ind)];
    end
end

```

```

end
x6p = x6(1);
y6p = y6(1);
for ind = 2:length(x6)
    if x6p(end) + x6pdist <= x6(ind)
        % append the point to the array
        x6p = [x6p x6(ind)];
        y6p = [y6p y6(ind)];
    end
end
x7p = x7(1);
y7p = y7(1);
for ind = 2:length(x7)
    if x7p(end) + x7pdist <= x7(ind)
        % append the point to the array
        x7p = [x7p x7(ind)];
        y7p = [y7p y7(ind)];
    end
end
[ax, h1, h2] = plotyy(x1, [y1, y2, y3, y4, y5, y6], x7, [y7]);
hold(ax(1), 'on');
hold(ax(2), 'on');
plot2a = plot(ax(1), x1(1), y1(1), 'b-s', x2(1), y2(1), 'c-^', x3(1), y3(1), 'r-d',
    x4(1), y4(1), 'g-p', x5(1), y5(1), 'k-o', x6(1), y6(1), 'k-*');
plot2b = plot(ax(1), x1p, y1p, 'bs', x2p, y2p, 'c^', x3p, y3p, 'rd', x4p, y4p, 'gp', x5p,
    y5p, 'ko', x6p, y6p, 'k*');
plot3a = plot(ax(2), x7(1), y7(1), 'm-v');
plot3b = plot(ax(2), x7p, y7p, 'mv');
set(ax(1), 'YLimMode', 'auto');
set(ax(2), 'YLimMode', 'auto');
line([t(plume_ind), t(plume_ind)], ylim, 'LineStyle', '--', 'Color', [0.75, 0.75, 0.0]);
line([t(stratstartind), t(stratstartind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7,
    0.7]);
line([t(stratendind), t(stratendind)], ylim, 'LineStyle', '-', 'Color', [0.7, 0.7, 0.7]);
hold(ax(1), 'off');
hold(ax(2), 'off');
set(ax(2), 'YColor', 'm');
set(h1(1), 'Color', 'b');
set(h1(2), 'Color', 'c');
set(h1(3), 'Color', 'r');
set(h1(4), 'Color', 'g');
set(h1(5), 'Color', 'k');
set(h1(6), 'Color', 'k');
set(h1(6), 'LineStyle', '-.');
set(h2(1), 'Color', 'm');
set(plot2a(1), 'MarkerEdgeColor', 'k');
set(plot2a(2), 'MarkerEdgeColor', 'k');
set(plot2a(3), 'MarkerEdgeColor', 'k');
set(plot2a(4), 'MarkerEdgeColor', 'k');
set(plot2a(5), 'MarkerEdgeColor', 'k');
set(plot2a(6), 'MarkerEdgeColor', 'k');
set(plot2b(1), 'MarkerEdgeColor', 'k');
set(plot2b(2), 'MarkerEdgeColor', 'k');
set(plot2b(3), 'MarkerEdgeColor', 'k');
set(plot2b(4), 'MarkerEdgeColor', 'k');
set(plot2b(5), 'MarkerEdgeColor', 'w');
set(plot2b(6), 'MarkerEdgeColor', 'k');
set(plot3a(1), 'MarkerEdgeColor', 'k');
set(plot3b(1), 'MarkerEdgeColor', 'k');
set(plot2a(1), 'MarkerFaceColor', 'b');
set(plot2a(2), 'MarkerFaceColor', 'c');
set(plot2a(3), 'MarkerFaceColor', 'r');
set(plot2a(4), 'MarkerFaceColor', 'g');
set(plot2a(4), 'MarkerSize', 10);
set(plot2a(5), 'MarkerFaceColor', 'k');
set(plot2a(5), 'MarkerSize', 5);
set(plot2a(6), 'MarkerFaceColor', 'k');

```



```

set(ploth2b(1), 'MarkerFaceColor', 'b');
set(ploth2b(2), 'MarkerFaceColor', 'c');
set(ploth2b(3), 'MarkerFaceColor', 'r');
set(ploth2b(4), 'MarkerFaceColor', 'g');
set(ploth2b(4), 'MarkerSize', 10);
set(ploth2b(5), 'MarkerFaceColor', 'k');
set(ploth2b(5), 'MarkerSize', 5);
set(ploth2b(6), 'MarkerFaceColor', 'k');
set(ploth3a(1), 'MarkerFaceColor', 'm');
set(ploth3b(1), 'MarkerFaceColor', 'm');
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
set(fighandle, 'Position', [48 48 960 624]);
set(fighandle, 'PaperOrientation', 'portrait');
set(fighandle, 'PaperSize', [10 6.5]);
set(fighandle, 'PaperPosition', [0 0 10 6.5]);
set(get(ax(1), 'Ylabel'), 'String', 'Temperature, C');
set(get(ax(2), 'Ylabel'), 'String', 'Mixing Number (nondimensional)');
set(ax(1), 'YTickMode', 'auto');
set(ax(2), 'YTickMode', 'auto');
xlabel('Time, s');
if showtitles == 1
    title('Smoothed Rear Pool Temperatures and the Mixing Number (Type 4)');
end
legendhandle = legend([ploth2a', ploth3a'], 'A - Upper', 'B - Near Sparger (Middle)', 'C
    - Further from Sparger (Middle)', 'D - Lower', 'E - Outlet', 'F - Saturation', 'G
    - Mixing Number 4', 'Location', 'Best');
set(legendhandle, 'Color', 'none');
figname = [testname '_crazynumber_t4'];
set(fighandle, 'Name', figname);
set(findall(fighandle,'type','axes'),'fontSize',16)
set(findall(fighandle,'type','text'),'fontSize',16)
% save to jpeg file
fileoutname = [figname '.jpg'];
if save_em == 1
    print(fighandle, '-djpeg90', '-r300', [outdir fileoutname]);
    saveas(fighandle, [mfigoutdir figname], 'fig')
end

% Close the log file
if save_em == 1
    fprintf(filehandle, '%s\r\n', 'End');
    fclose(filehandle);
    disp('Closing Output Text File')
end

save_em = 0;
clear startingtemp;
savefigs='n';

```

C.3 SOURCE – SPREADSHOUT.M

```

%spreadshout.m

tabchar = sprintf('\t');
tabchar = [' ' tabchar];
filehandle = [];
fileh2 = [];
crlf = sprintf('\r\n');
outdir = [outpath '\Export\' testname '\'];
disp(['Loading ' outdir testname '_results_rcicland.txt' ' ...']);

```

```

filehandle = fopen([outdir testname '_results_rcicland.txt'], 'r');
filetext = fscanf(filehandle,'%c',inf);
fclose(filehandle);
textdat = filetext;
disp('Removing non-numeric data ...');
for ind = 1:length(textdat)
    if isempty(str2num(textdat(ind)))
        % either decimal, -, +, e, or non-numeric, check for decimal
        if ind < length(textdat)
            if textdat(ind) == '.'
                % decimal or period, check for decimal (numbers right and
                % left)
                if ind == 1
                    % period?
                    textdat(ind) = ' ';
                elseif isempty(str2num(textdat(ind-1)))
                    % period
                    textdat(ind) = ' ';
                elseif isempty(str2num(textdat(ind+1)))
                    % period
                    textdat(ind) = ' ';
                end
            elseif textdat(ind) == '-'
                if isempty(str2num(textdat(ind+1))) && (textdat(ind+1) ~= '.')
                    % not a negative number leader
                    textdat(ind) = ' ';
                end
            elseif textdat(ind) == '+'
                if isempty(str2num(textdat(ind+1))) && (textdat(ind+1) ~= '.')
                    % not a number leader
                    textdat(ind) = ' ';
                end
            elseif (textdat(ind) == 'e') || (textdat(ind) == 'E')
                % Power indicator?
                if ind > 1
                    if isempty(str2num(textdat(ind-1)))
                        % no preceding numeric
                        textdat(ind) = ' ';
                    elseif (~isempty(str2num(textdat(ind+1)))) && (textdat(ind+1) ~= '+')
                        && (textdat(ind+1) ~= '-')
                            % no succeeding numeric/+/-
                            textdat(ind) = ' ';
                    end
                else
                    % too early
                    textdat(ind) = ' ';
                end
            else
                % non-numeric
                textdat(ind) = ' ';
            end
        else
            % last character, not a decimal or -
            textdat(ind) = ' ';
        end
    elseif str2num(textdat(ind)) == 1i
        % no imaginaries
        textdat(ind) = ' ';
    end
end
disp('Converting ...');
numericdata = str2num(textdat);
outstring = '';
for ind=1:length(numericdata)
    outstring = [outstring num2str(numericdata(ind)) tabchar];
end
disp('Data: ');

```

```

disp(outstring);

if savefigs == 'y'
    mkdir([outpath '\extracted_numerics\'] );
    fileh2 = fopen([outpath '\extracted_numerics\extracted.txt'], 'a+');
    fprintf(fileh2, '%s\r\n', ' ');
    fprintf(fileh2, '%s\r\n', date);
    fprintf(fileh2, '%s\r\n', ['Currently: ' num2str(clock) ' ' tabchar ' in Y M D H M
        S' ]);
    fprintf(fileh2, '%s\r\n', ['Test name: ' testname]);
    fprintf(fileh2, '%s\r\n', ['Read from: ' outdir testname '_results_localextra.txt']);
    fprintf(fileh2, '%s\r\n', 'Reported numeric data: ');
    fprintf(fileh2, '%s\r\n', outstring);
    fprintf(fileh2, '%s\r\n', ' ');
    fclose(fileh2);
    savefigs = 'n';
end
disp('Done!')

```

APPENDIX D
PROCESSED RESULTS

This Appendix contains the processed results produced by the Matlab data processing script for each test.

D.1 TEST #1 -

T01_RCIC_STD_57KW_OLD_ORIFICE_FORCED_END_RESULTS_RCIC

LAND.TXT

Output Saved to C:\Local
Files\RCICLAND_NOTITLES\Export\T01_RCIC_STD_57kW_old_orifice_forced_end\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 4894.684 s, and ending (KEY POINT #11) at t plus 15262.944 s, for a time period of 10368.26 s.
Original Data Record Time: 18000.2876 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 3366.7506 s, T_{bulk} = 57.9366 C and T_{out} = 55.3123 C
Stratification Beginning SP12 Temperature = 57.8114 C
Stratification Beginning Pressure = 18.2573 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 10338.6603 s, T_{bulk} = 95.2465 C and T_{out} = 75.2305 C
Stratification Ending SP12 Temperature = 95.0466 C
Stratification Ending Pressure = 29.6467 psia
Plume detected! Setting t_{plume} (KEY POINT #2) to 3437.0516 s.
At t = 3437.0516 s, the pool pressure is 18.3156 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 58.6463, 58.3923, 60.3963, 58.5985, and 55.3555 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 9.9536 +/- 3.7452 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 9.3379 +/- 3.709 C.
Minimum Steam Quality: 0.99206 at t plus 10341.7605 s
Maximum Steam Quality: 1.0067 at t plus 4320.9661 s
Time-Averaged Steam Quality: 0.99984 +/- 0.0018699
Minimum Turbine Outlet Steam Quality: 0.99912 at t plus 10341.7605 s
Maximum Turbine Outlet Steam Quality: 1.0211 at t plus 1361.7219 s
Time-Averaged Turbine Outlet Steam Quality: 1.012 +/- 0.0034148
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 10278.2598 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.51474 degrees/min at t plus 6986.8076 s and 0.14389 degrees/min at t plus 6458.0983 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.42858 degrees/min at t plus 7873.7213 s and 0.22665 degrees/min at t plus 10163.6563 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.1729 degrees/min at t plus 6986.8076 s and -0.17509 degrees/min at t plus 6095.0926 s, respectively
Max and min smoothed lower level changerates: 1.6104 degrees/min at t plus 9630.8498 s and -0.02954 degrees/min at t plus 9178.0409 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.38396 degrees/min at t plus 9173.4417 s and -1.3687 degrees/min at t plus 9630.8498 s, respectively
Max and min smoothed outlet level changerates: 0.42114 degrees/min at t plus 2760.2659 s and -0.035359 degrees/min at t plus 9570.6484 s, respectively
Max and min smoothed lower-outlet level changerate differences: 1.608 degrees/min at t plus 9630.7498 s and -0.26317 degrees/min at t plus 7352.7135 s, respectively
Max and min smoothed hot (SP8) level changerates: 0.8365 degrees/min at t plus 5010.7006 s and 0.097639 degrees/min at t plus 7472.9144 s, respectively
Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.53428 degrees/min at t plus 5050.9779 s and -0.28931 degrees/min at t plus 7472.9144 s, respectively
The mean steam flow rate was 23.4779 +/- 0.51075 g/s
The mean feedwater flow rate was 22.2345 +/- 0.93409 g/s
The mean water injection to steam flow rate was 0.0037187 +/- 0.035541 g/s

Mean Smoothed Condensing Region SP8-SP9 delta T is 9.8722 +/- 3.8126 C over the Stratification Period, beginning at 2.0096 C and ending at 15.2092 C
 Mean Smoothed SP8-Upper Pool delta T is 9.2603 +/- 3.7694 C over the Stratification Period, beginning at 1.6629 C and ending at 14.6871 C
 The stratification period begins and ends with Smoothed SP8 readings of 60.0785 and 110.3675 C, respectively
 The stratification period begins and ends with condensing flows of 0.25584 and 0.48511 kg/s, respectively.
 The stratification period begins and ends with condensing+cooling flows of 6.8018 and 0.85851 kg/s, respectively.
 The stratification period had a mean sparger steam enthalpy of 2720.1958 +/- 0.96719 kJ/kg.
 At plume detection, the condensing and condensing+cooling flows are 0.25584 and 6.7861 kg/s, respectively
 The plume period had a mean steam enthalpy of 2720.4826 +/- 0.87007 kJ/kg.
 Maximum Smoothed Top-Mid delta T is 1.4115 degrees C at t plus 5966.8922 s with T_upper = 72.5743 C and T_mid = 71.1628 C
 At t plus 5966.8922 s, Smoothed SP8-SP9 is 9.8021 C and Smoothed SP8-Top is 8.3906 C, where Smoothed SP8 is 80.9649 C and Pool P = 21.0255 psia
 Maximum Smoothed Top-Lower delta T is 10.2558 degrees C at t plus 9492.1469 s with T_upper = 91.9391 C and T_low = 81.6833 C
 At t plus 9492.1469 s, Smoothed SP8-SP9 is 13.8539 C and Smoothed SP8-Top is 13.5498 C, where Smoothed SP8 is 105.4889 C and Pool P = 27.7777 psia
 Maximum Smoothed Mid-Lower delta T is 9.9801 degrees C at t plus 9475.8459 s with T_mid = 91.5156 C and T_low = 81.5355 C
 At t plus 9475.8459 s, Smoothed SP8-SP9 is 14.0551 C and Smoothed SP8-Top is 13.7811 C, where Smoothed SP8 is 105.5707 C and Pool P = 27.7365 psia
 Maximum Smoothed Top-Outlet delta T is 20.6577 degrees C at t plus 10368.26 s with T_upper = 95.8454 C and T_out = 75.1878 C
 At t plus 10368.26 s, Smoothed SP8-SP9 is 14.29 C and Smoothed SP8-Top is 13.7245 C, where Smoothed SP8 is 109.5699 C and Pool P = 29.6855 psia
 Maximum Smoothed Mid-Outlet delta T is 20.0922 degrees C at t plus 10368.26 s with T_mid = 95.2799 C and T_out = 75.1878 C
 At t plus 10368.26 s, Smoothed SP8-SP9 is 14.29 C and Smoothed SP8-Top is 13.7245 C, where Smoothed SP8 is 109.5699 C and Pool P = 29.6855 psia
 Maximum Smoothed Lower-Outlet delta T is 19.2737 degrees C at t plus 10368.26 s with T_low = 94.4615 C and T_out = 75.1878 C
 At t plus 10368.26 s, Smoothed SP8-SP9 is 14.29 C and Smoothed SP8-Top is 13.7245 C, where Smoothed SP8 is 109.5699 C and Pool P = 29.6855 psia
 Maximum Smoothed Condensing Region SP8-SP9 delta T is 15.3759 degrees C at (KEY POINT #14) t plus 10244.7579 s with T_SP8 = 110.1343 C and T_SP9 = 94.7584 C and Pool P = 29.447 psia
 Maximum Smoothed Condensing Region SP8-Upper delta T is 14.8121 degrees C at t plus 10335.5601 s with T_SP8 = 110.4903 C and T_upper = 95.6782 C and Pool P = 29.6334 psia
 Maximum Top-Mid delta T is 2.0598 degrees C at (KEY POINT #4) t plus 7452.6142 s ignoring SP 4, with temperatures of 80.862 and 78.8022 C, respectively, at Set # 2, where Pool P = 23.3349 psia and T_outlet = 72.3473 C
 Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 8339.1279 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.99965 C and a raw SP12 Reading of 84.6904 C.
 Maximum Top-Lower delta T is 11.5433 degrees C at t plus 9566.3481 s, with temperatures of 92.6406 and 81.0973 C, respectively, at Set # 1, where Pool P = 27.9386 psia and T_outlet = 75.1664 C
 Maximum Mid-Low delta T is 10.7936 degrees C at (KEY POINT #6) t plus 9554.6695 s ignoring SP 4, with temperatures of 91.8716 and 81.0779 C, respectively, at Set # 2, where Pool P = 27.9107 psia and T_outlet = 75.1204 C
 Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 9806.8519 s with a Smoothed Mid-Axis Mid-Low Delta T of 3.5957 C and a raw SP12 Reading of 92.8709 C.
 Maximum Top-Outlet delta T is 20.8945 degrees C at t plus 10362.0596 s, with temperatures of 96.1019 and 75.2074 C, respectively, at Set # 2, where Pool P = 29.6753 psia
 Maximum Mid-Outlet delta T is 20.0585 degrees C at t plus 10361.7596 s ignoring SP 4, with temperatures of 95.2658 and 75.2073 C, respectively, at Set # 2, where Pool P = 29.677 psia
 Maximum Lower-Outlet delta T is 20.7106 degrees C at (KEY POINT #8) t plus 10327.2596 s, with temperatures of 95.9922 and 75.2816 C, respectively, at Set # 1, where Pool P = 29.6197 psia

Low-Outlet Reconvergence NOT Detected, setting t to (KEY POINT #10) t plus 10368.26 s with a Smoothed Mid-Axis Low-Outlet Delta T of 19.8329 C and a raw SP12 Reading of 95.203 C.

Minimum SP Pressure is 16.1529 psia at t plus 1.5001 s
 Maximum SP Pressure is 29.6911 psia at t plus 10366.3599 s
 Beginning SP Pressure is 16.153 psia
 Ending SP Pressure is 29.6855 psia

Time-Average SP Pressure is 21.0553 +/- 3.9107 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 70.9431 cm (cold) / 70.9765 cm (hot) at 14.7305 psia
 Beginning Smoothed SP Level is 71.0841 cm (cold) / 71.2098 cm (hot) at 16.1582 psia
 Ending Smoothed SP Level is 72.4754 cm (cold) / 73.2211 cm (hot) at 29.6949 psia
 Minimum Smoothed Cold SP Level is 70.7834 cm at t plus 7792.5197 s and 23.9641 psia
 Minimum Smoothed Hot SP Level is 71.1946 cm at t plus 232.5043 s and 16.2625 psia
 Maximum Smoothed Cold SP Level is 72.4754 cm at t plus 10368.26 s and 29.6949 psia
 Maximum Smoothed Hot SP Level is 73.2211 cm at t plus 10368.26 s and 29.6949 psia
 SP 12 Temperature at the beginning is 39.964 C, and at the end is 95.203 C

At plume detection, the Mixing Number is 43.6834

The Mixing Number ranges from a minimum of 32.1718 at (KEY POINT #12) t plus 0 s to a maximum of 109.8003 at (KEY POINT #13) t plus 10368.26 s; it had a mean value of 58.7259 +/- 22.0058 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy ell

KEY POINT #1 (t plus 0 s with a Mixing Number of 32.1718): 17.2558211 0.040894
 0.00925 0.3937 0.710840769 0.712097661 1.01519585
 1 1 26.5357604 54155.8597 0.0695263055 0.0581485075
 0.0226644245 3.40124572e-006 0.0226644245 40.4304101 120.47864
 103.942449 40.595914 40.5527487 40.8388362 37.3958216
 4.17851387 4.22178976 2.09371415 0.629184762 0.6792901
 0.6792901 4.30050184 1.68103157 0.0382322272 992.059931
 955.488355 0.681179479 0.650383122 0.000647553248 0.000270479623
 1.24041639e-005 1.30301606e-005 1532.07587 1541.23736 474.246369
 485.564903 1.16542603 1.11406685 1.15106685 0.0755556799
 0.0762228145 2716.58504 2715.88089 169.435004 435.744383
 2681.75091 266.309379 2280.84065 170.126564 169.944693
 171.14321 156.760419

KEY POINT #2 (t plus 3437.0516 s with a Mixing Number of 43.6834): 17.5665799
 0.040894 0.00925 0.3937 0.710374428 0.712998794
 1.01382146 1 1 24.0141531 54877.4594
 0.0665160113 0.057463508 0.0230725865 4.83070945e-006 0.0230725865
 58.3923137 122.311476 107.449788 60.3963003 58.6463089
 58.5985271 55.3554831 4.18204086 4.22665414 2.10922984
 0.649274175 0.680494719 0.680494719 3.07843157 1.62188928
 0.0388199629 984.04051 952.880255 0.762727525 0.731662607
 0.000477935578 0.000261125479 1.25243723e-005 1.30903968e-005 1552.88038

1537.4255	475.972813	486.199643	1.31519342	1.26312409
1.30012409	0.18507901	0.203145122	2718.66215	2718.08547
244.522899	450.571129	2687.17238	206.04823	2268.09102
252.904469	245.583697	245.386818	231.82983	
KEY POINT #3 (t plus 3366.7506 s with a Mixing Number of 43.3505):	17.6386555			
0.040894	0.00925	0.3937	0.710379405	0.712990993
1.0143673	1	1	24.2148881	55017.9869
0.0665717272	0.0574791375	0.0231672532	6.22327102e-006	0.0231672532
58.0688746	122.829746	107.370074	60.0784843	58.4155729
58.1582666	55.203572	4.18191547	4.22654054	2.1088654
0.648957099	0.680468986	0.680468986	3.09519397	1.62318692
0.0388062484	984.203223	952.940138	0.760789947	0.728617603
0.000480317719	0.000261331543	1.25216377e-005	1.31105338e-005	1552.65708
1537.51605	475.934048	486.556989	1.31162174	1.25916445
1.29616445	0.182295614	0.200183662	2719.77334	2719.18698
243.169951	450.233948	2687.04998	207.063997	2269.53939
251.574775	244.618403	243.545301	231.194368	
KEY POINT #4 (t plus 7452.6142 s with a Mixing Number of 69.173):	18.1319328			
0.040894	0.00925	0.3937	0.707936929	0.71274093
1.0102738	1	1	19.7776738	56281.3272
0.0628312045	0.0561087689	0.0238151416	3.06885185e-006	0.0238151416
79.1349402	125.069778	114.305865	90.6036668	80.2241776
77.3846683	72.3573978	4.19465181	4.23696678	2.14273739
0.666437906	0.682425312	0.682425312	2.25483791	1.51771554
0.0400647576	972.369776	947.625364	0.945040919	0.91690608
0.000358244147	0.000244450229	1.27599419e-005	1.31746584e-005	1557.3837
1528.97781	479.222442	486.751393	1.65383151	1.60864466
1.64564466	0.457781062	0.718068767	2720.72883	2720.33768
331.41299	479.608684	2697.55098	148.195694	2241.12015
379.58001	335.981106	324.0739	303.006611	
KEY POINT #5 (t plus 8339.1279 s with a Mixing Number of 80.5104):	18.3093169			
0.040894	0.00925	0.3937	0.708762907	0.71422025
1.00887905	1	1	18.6384739	56766.7416
0.0617746777	0.0556834012	0.0240481243	5.88887413e-006	0.0240481243
84.8695651	125.657033	116.437483	97.3228528	85.5268849
79.916849	74.7938285	4.1997156	4.24039598	2.15406253
0.670130489	0.682912903	0.682912903	2.09251742	1.48811062
0.0404791787	968.74203	945.949806	1.00840711	0.982580472
0.000333893971	0.000239659208	1.28333106e-005	1.31897866e-005	1555.56445
1526.09206	480.197977	486.693789	1.77260774	1.72896679
1.76596679	0.575721569	0.921043594	2720.70377	2720.35638
355.491465	488.652396	2700.71537	133.16093	2232.05138
407.871983	358.250896	334.704092	313.225851	
KEY POINT #6 (t plus 9554.6695 s with a Mixing Number of 99.3881):	18.3895432			
0.040894	0.00925	0.3937	0.718371455	0.725035608
1.00701982	1	1	16.890259	56866.2239
0.0604458649	0.0550331683	0.0241534965	3.72002901e-006	0.0241534965
91.9633418	126.865082	119.677305	106.124497	92.3536258
83.3681791	75.1373421	4.20692153	4.24581678	2.17214005
0.674101689	0.683553123	0.683553123	1.91911998	1.44540672
0.041135305	964.032568	943.365551	1.11125998	1.0889339
0.000307512753	0.000232702522	1.2944914e-005	1.32244051e-005	1551.70731
1521.47813	481.648204	486.772365	1.96643602	1.92452031
1.96152031	0.755809157	1.25684188	2721.21549	2720.93021
385.323449	502.412953	2705.46519	117.089504	2218.80254
445.018453	386.964121	349.203963	314.681405	
KEY POINT #7 (t plus 9806.8519 s with a Mixing Number of 102.572):	18.407053			
0.040894	0.00925	0.3937	0.720701084	0.72763533
1.00635676	1	1	16.5674133	56943.5922
0.0602536952	0.0549071003	0.0241764945	9.66189958e-006	0.0241764945
92.9788172	126.790955	120.302892	106.517533	93.5908866
89.0284098	75.1883188	4.20803739	4.246893	2.17575328
0.674617652	0.683662825	0.683662825	1.89646538	1.43746483
0.041265737	963.339163	942.861345	1.13206278	1.11148367
0.000304034613	0.000231402408	1.29664749e-005	1.3219012e-005	1551.01828
1520.55602	481.923665	486.565893	2.00578542	1.9639646
2.0009646	0.785060525	1.27391976	2720.64147	2720.36699

389.59907	505.072181	2706.37385	115.473111	2215.56929
446.681888	392.17359	372.98551	314.898252	
KEY POINT #8 (t plus 10327.2596 s with a Mixing Number of 109.2173):	18.58154			
0.040894	0.00925	0.3937	0.724506992	0.73192618
1.00623696	1	1	16.1290073	57325.8322
0.0598498501	0.0546630386	0.024405672	5.4998842e-006	0.024405672
95.1045834	127.847475	121.511683	110.105122	95.6966334
94.4333493	75.2535103	4.21044538	4.24899995	2.18284911
0.675655022	0.683862103	0.683862103	1.85063812	1.42238708
0.0415212623	961.871625	941.882333	1.17314987	1.15231688
0.000296974031	0.000228928367	1.3008145e-005	1.32553417e-005	1549.4661
1518.74605	482.451697	486.997925	2.08364016	2.04194878
2.07894878	0.849351508	1.43882957	2722.09007	2721.82992
398.552879	510.212511	2708.12165	111.659632	2211.87756
461.854986	401.044584	395.728321	315.177788	
KEY POINT #9 (t plus 10338.6603 s with a Mixing Number of 109.4056):	18.5721544			
0.040894	0.00925	0.3937	0.724568522	0.732003484
1.00627554	1	1	16.1114471	57286.8215
0.0598396197	0.0546583968	0.0243933447	5.06130544e-006	0.0243933447
95.1582909	127.909408	121.534644	110.36749	95.6804195
94.4714337	75.2521771	4.21050758	4.24904033	2.18298536
0.675680464	0.683865727	0.683865727	1.84950751	1.42210405
0.0415261608	961.834251	941.863676	1.1739418	1.15296955
0.000296799393	0.000228881853	1.30089366e-005	1.32576684e-005	1549.4249
1518.71131	482.461672	487.035396	2.0851425	2.04345378
2.08045378	0.851030785	1.45154757	2722.20699	2721.94741
398.779128	510.310176	2708.15475	111.531048	2211.89681
462.965059	400.97642	395.888759	315.172321	
KEY POINT #10 (t plus 10368.26 s with a Mixing Number of 109.8003):	18.5700451			
0.040894	0.00925	0.3937	0.72475433	0.732210997
1.00632765	1	1	16.0858766	57262.5274
0.0598164465	0.0546463309	0.0243905742	8.33388687e-006	0.0243905742
95.2799187	128.021027	121.594322	109.569922	95.8454466
94.4614741	75.1877502	4.21064853	4.24914532	2.18333974
0.675737975	0.683875117	0.683875117	1.8469519	1.421369
0.0415389009	961.749585	941.815174	1.17600216	1.1548261
0.000296404587	0.000228761037	1.30109942e-005	1.32617867e-005	1549.33137
1518.62095	482.487591	487.098213	2.08905148	2.04739441
2.08439441	0.854843934	1.41317028	2722.40565	2722.14689
399.291552	510.564029	2708.24075	111.272477	2211.84162
459.591503	401.671685	395.847133	314.902596	
KEY POINT #11 (t plus 10368.26 s with a Mixing Number of 109.8003):	18.5700451			
0.040894	0.00925	0.3937	0.72475433	0.732210997
1.00632765	1	1	16.0858766	57262.5274
0.0598164465	0.0546463309	0.0243905742	8.33388687e-006	0.0243905742
95.2799187	128.021027	121.594322	109.569922	95.8454466
94.4614741	75.1877502	4.21064853	4.24914532	2.18333974
0.675737975	0.683875117	0.683875117	1.8469519	1.421369
0.0415389009	961.749585	941.815174	1.17600216	1.1548261
0.000296404587	0.000228761037	1.30109942e-005	1.32617867e-005	1549.33137
1518.62095	482.487591	487.098213	2.08905148	2.04739441
2.08439441	0.854843934	1.41317028	2722.40565	2722.14689
399.291552	510.564029	2708.24075	111.272477	2211.84162
459.591503	401.671685	395.847133	314.902596	
KEY POINT #12 (t plus 0 s with a Mixing Number of 32.1718):	17.2558211			0.040894
0.00925	0.3937	0.710840769	0.712097661	1.01519585
1	1	26.5357604	54155.8597	0.0695263055
0.0226644245	3.40124572e-006	0.0226644245	40.4304101	120.47864
103.942449	40.595914	40.5527487	40.8388362	37.3958216
4.17851387	4.22178976	2.09371415	0.629184762	0.6792901
0.6792901	4.30050184	1.68103157	0.0382322272	992.059931
955.488355	0.681179479	0.650383122	0.000647553248	0.000270479623
1.24041639e-005	1.30301606e-005	1532.07587	1541.23736	474.246369
485.564903	1.16542603	1.11406685	1.15106685	0.0755556799
0.0762228145	2716.58504	2715.88089	169.435004	435.744383
2681.75091	266.309379	2280.84065	170.126564	169.944693
171.14321	156.760419			

KEY POINT #13 (t plus 10368.26 s with a Mixing Number of 109.8003): 18.5700451

0.040894	0.00925	0.3937	0.72475433	0.732210997
1.00632765	1	1	16.0858766	57262.5274
0.0598164465	0.0546463309	0.0243905742	8.33388687e-006	0.0243905742
95.2799187	128.021027	121.594322	109.569922	95.8454466
94.4614741	75.1877502	4.21064853	4.24914532	2.18333974
0.675737975	0.683875117	0.683875117	1.8469519	1.421369
0.0415389009	961.749585	941.815174	1.17600216	1.1548261
0.000296404587	0.000228761037	1.30109942e-005	1.32617867e-005	1549.33137
1518.62095	482.487591	487.098213	2.08905148	2.04739441
2.08439441	0.854843934	1.41317028	2722.40565	2722.14689
399.291552	510.564029	2708.24075	111.272477	2211.84162
459.591503	401.671685	395.847133	314.902596	

KEY POINT #14 (t plus 10244.7579 s with a Mixing Number of 108.1998): 18.5266147

0.040894	0.00925	0.3937	0.72401168	0.731375443
1.00596487	1	1	16.1562722	57230.2374
0.0599157545	0.0546999129	0.0243335312	6.68839932e-006	0.0243335312
94.7584316	127.390561	121.329246	110.134312	95.4699985
93.2670483	75.2146423	4.21004651	4.24867963	2.18176849
0.67549005	0.683833097	0.683833097	1.85795679	1.42464035
0.0414823999	962.112078	942.030492	1.16687283	1.14702864
0.000298103909	0.000229298584	1.30018552e-005	1.32382359e-005	1549.72897
1519.02159	482.372361	486.724635	2.07173444	2.03006904
2.06706904	0.838594252	1.44023996	2721.23287	2720.97184
397.094589	509.436532	2707.85854	112.341944	2211.79634
461.977606	400.089318	390.818449	315.013916	

End

D.2 TEST #2 - T02_RCIC_STD_57KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T02_RCIC_STD_57kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 2098.241 s, and ending (KEY POINT #11) at t plus 14976.2446 s, for a time period of 12878.0036 s.
Original Data Record Time: 17235.4818 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 3929.9628 s, T_bulk = 59.101 C and T_out = 56.673 C
Stratification Beginning SP12 Temperature = 58.8905 C
Stratification Beginning Pressure = 17.1325 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 12176.6925 s, T_bulk = 96.9752 C and T_out = 75.692 C
Stratification Ending SP12 Temperature = 96.8511 C
Stratification Ending Pressure = 29.2965 psia
Plume detected! Setting t_plume (KEY POINT #2) to 3545.8568 s.
At t = 3545.8568 s, the pool pressure is 16.8474 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 57.6073, 57.5885, 59.5907, 57.7115, and 55.3163 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 10.3245 +/- 3.9134 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 9.8447 +/- 3.796 C.
Minimum Steam Quality: 0.99468 at t plus 12849.403 s
Maximum Steam Quality: 1.0128 at t plus 1017.4172 s
Time-Averaged Steam Quality: 1.005 +/- 0.0022442
Minimum Turbine Outlet Steam Quality: 0.99783 at t plus 12849.403 s
Maximum Turbine Outlet Steam Quality: 1.0229 at t plus 623.0106 s
Time-Averaged Turbine Outlet Steam Quality: 1.0118 +/- 0.0039172
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 12788.0044 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.40631 degrees/min at t plus 8035.0266 s and 0.16646 degrees/min at t plus 11923.091 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.37305 degrees/min at t plus 320.1063 s and 0.17868 degrees/min at t plus 11868.3888 s, respectively

Max and min smoothed upper-mid level changerate differences: 0.12699 degrees/min at t plus 5053.08 s and -0.12147 degrees/min at t plus 5259.9839 s, respectively
 Max and min smoothed lower level changerates: 1.2298 degrees/min at t plus 10380.1647 s and 0.017432 degrees/min at t plus 9885.4564 s, respectively
 Max and min smoothed mid-lower level changerate differences: 0.30459 degrees/min at t plus 9885.1564 s and -0.99422 degrees/min at t plus 10380.1647 s, respectively
 Max and min smoothed outlet level changerates: 2.9767 degrees/min at t plus 12566.1988 s and -0.036845 degrees/min at t plus 10665.47 s, respectively
 Max and min smoothed lower-outlet level changerate differences: 1.2078 degrees/min at t plus 10380.0647 s and -2.7451 degrees/min at t plus 12566.0988 s, respectively
 Max and min smoothed hot (SP8) level changerates: 0.75677 degrees/min at t plus 5506.2869 s and -0.6814 degrees/min at t plus 12788.0044 s, respectively
 Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.46131 degrees/min at t plus 5506.2869 s and -0.97449 degrees/min at t plus 12788.0044 s, respectively

The mean steam flow rate was 23.4613 +/- 1.079 g/s
 The mean feedwater flow rate was 25.0392 +/- 2.212 g/s
 The mean water injection to steam flow rate was 0.003927 +/- 0.035595 g/s
 Mean Smoothed Condensing Region SP8-SP9 delta T is 10.6969 +/- 3.5926 C over the Stratification Period, beginning at 2.278 C and ending at 15.3024 C
 Mean Smoothed SP8-Upper Pool delta T is 10.1997 +/- 3.4994 C over the Stratification Period, beginning at 2.0959 C and ending at 14.5742 C
 The stratification period begins and ends with Smoothed SP8 readings of 61.5964 and 112.478 C, respectively
 The stratification period begins and ends with condensing flows of 0.26707 and 0.52925 kg/s, respectively.
 The stratification period begins and ends with condensing+cooling flows of 5.8361 and 0.84231 kg/s, respectively.
 The stratification period had a mean sparger steam enthalpy of 2718.9485 +/- 1.3255 kJ/kg.
 At plume detection, the condensing and condensing+cooling flows are 0.25821 and 6.6148 kg/s, respectively
 The plume period had a mean steam enthalpy of 2719.0269 +/- 1.3145 kJ/kg.
 Maximum Smoothed Top-Mid delta T is 1.1552 degrees C at t plus 12463.8209 s with T_upper = 99.3145 C and T_mid = 98.1594 C
 At t plus 12463.8209 s, Smoothed SP8-SP9 is 14.0873 C and Smoothed SP8-Top is 12.9321 C, where Smoothed SP8 is 112.2467 C and Pool P = 29.8925 psia
 Maximum Smoothed Top-Lower delta T is 8.5506 degrees C at t plus 10131.7605 s with T_upper = 89.665 C and T_low = 81.1145 C
 At t plus 10131.7605 s, Smoothed SP8-SP9 is 14.2503 C and Smoothed SP8-Top is 13.8028 C, where Smoothed SP8 is 103.4678 C and Pool P = 25.3731 psia
 Maximum Smoothed Mid-Lower delta T is 8.1068 degrees C at t plus 10129.9604 s with T_mid = 89.2103 C and T_low = 81.1035 C
 At t plus 10129.9604 s, Smoothed SP8-SP9 is 14.2595 C and Smoothed SP8-Top is 13.819 C, where Smoothed SP8 is 103.4699 C and Pool P = 25.3717 psia
 Maximum Smoothed Top-Outlet delta T is 22.158 degrees C at t plus 12166.1939 s with T_upper = 97.8491 C and T_out = 75.6912 C
 At t plus 12166.1939 s, Smoothed SP8-SP9 is 15.1393 C and Smoothed SP8-Top is 14.4672 C, where Smoothed SP8 is 112.3164 C and Pool P = 29.2696 psia
 Maximum Smoothed Mid-Outlet delta T is 21.5082 degrees C at t plus 12157.9924 s with T_mid = 97.1573 C and T_out = 75.6491 C
 At t plus 12157.9924 s, Smoothed SP8-SP9 is 14.8815 C and Smoothed SP8-Top is 14.2554 C, where Smoothed SP8 is 112.0388 C and Pool P = 29.2534 psia
 Maximum Smoothed Lower-Outlet delta T is 21.7369 degrees C at t plus 12062.891 s with T_low = 97.2259 C and T_out = 75.489 C
 At t plus 12062.891 s, Smoothed SP8-SP9 is 14.4427 C and Smoothed SP8-Top is 13.7744 C, where Smoothed SP8 is 111.0992 C and Pool P = 29.0656 psia
 Maximum Smoothed Condensing Region SP8-SP9 delta T is 15.3957 degrees C at (KEY POINT #14) t plus 12173.3923 s with T_SP8 = 112.5654 C and T_SP9 = 97.1696 C and Pool P = 29.2841 psia
 Maximum Smoothed Condensing Region SP8-Upper delta T is 14.6746 degrees C at t plus 12173.3923 s with T_SP8 = 112.5654 C and T_upper = 97.8907 C and Pool P = 29.2841 psia
 Maximum Top-Mid delta T is 1.4105 degrees C at (KEY POINT #4) t plus 6366.4011 s ignoring SP 4, with temperatures of 71.0791 and 69.6686 C, respectively, at Set # 2, where Pool P = 19.4128 psia and T_outlet = 65.9976 C
 Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 6366.4011 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.99578 C and a raw SP12 Reading of 69.6686 C.

Maximum Top-Lower delta T is 9.8872 degrees C at t plus 10389.4643 s, with temperatures of 90.814 and 80.9268 C, respectively, at Set # 2, where Pool P = 25.8877 psia and T_{outlet} = 75.1347 C

Maximum Mid-Low delta T is 9.2559 degrees C at (KEY POINT #6) t plus 10389.5643 s ignoring SP 4, with temperatures of 90.1813 and 80.9254 C, respectively, at Set # 2, where Pool P = 25.8871 psia and T_{outlet} = 75.1374 C

Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 10476.3662 s with a Smoothed Mid-Axis Mid-Low Delta T of 3.0829 C and a raw SP12 Reading of 90.5594 C.

Maximum Top-Outlet delta T is 22.4053 degrees C at t plus 12180.4927 s, with temperatures of 98.0775 and 75.6723 C, respectively, at Set # 1, where Pool P = 29.2976 psia

Maximum Mid-Outlet delta T is 21.3857 degrees C at t plus 12172.8923 s ignoring SP 4, with temperatures of 97.0182 and 75.6325 C, respectively, at Set # 2, where Pool P = 29.283 psia

Maximum Lower-Outlet delta T is 22.5979 degrees C at (KEY POINT #8) t plus 12150.792 s, with temperatures of 98.1573 and 75.5594 C, respectively, at Set # 1, where Pool P = 29.2292 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 12655.0008 s with a Smoothed Mid-Axis Low-Outlet Delta T of 7.5317 C and a raw SP12 Reading of 98.9045 C.

Minimum SP Pressure is 15.021 psia at t plus 14.6008 s

Maximum SP Pressure is 30.8387 psia at t plus 12878.0036 s

Beginning SP Pressure is 15.028 psia

Ending SP Pressure is 30.8387 psia

Time-Average SP Pressure is 20.7374 +/- 4.6514 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 78.062 cm (cold) / 78.2033 cm (hot) at 14.6198 psia

Beginning Smoothed SP Level is 77.9323 cm (cold) / 78.1145 cm (hot) at 15.0245 psia

Ending Smoothed SP Level is 77.8519 cm (cold) / 78.9101 cm (hot) at 30.8374 psia

Minimum Smoothed Cold SP Level is 76.6822 cm at t plus 9807.555 s and 24.7146 psia

Minimum Smoothed Hot SP Level is 77.4352 cm at t plus 9285.7471 s and 23.679 psia

Maximum Smoothed Cold SP Level is 77.9323 cm at t plus 1.9001 s and 15.0252 psia

Maximum Smoothed Hot SP Level is 78.9101 cm at t plus 12878.0036 s and 30.8374 psia

SP 12 Temperature at the beginning is 40.0277 C, and at the end is 99.8193 C

At plume detection, the Mixing Number is 45.0613

The Mixing Number ranges from a minimum of 33.3326 at (KEY POINT #12) t plus 0 s to a maximum of 138.0096 at (KEY POINT #13) t plus 12878.0036 s; it had a mean value of 68.9277 +/- 29.4538 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction v1, Sparger fluid velocity (m/s) v1, Two phase Re re_{tp}, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_{mid} Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_{mid} Vapor Pressure p4, T_{Plume} Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 33.3326): 20.4407065 0.040894

0.00925	0.3937	0.779323037	0.78114485	1.01583551
1	1	33.4106111	64315.6065	0.0695239701
0.0268475692	2.89403617e-006	0.0268475692	40.4447578	119.481328
102.147658	40.4779476	40.3956775	40.3300343	38.0154017
4.17853301	4.21940564	2.08617393	0.629198854	0.678615984
0.678615984	4.29928124	1.71298998	0.0379435701	992.051354

956.80174	0.642282317	0.611868784	0.000647380988	0.000275503822	
1.23427452e-005	1.29968805e-005	1532.08722	1543.04963	473.346672	
485.184939	1.09441404	1.03590518	1.07290518	0.0756133143	
0.0757467822	2715.70744	2714.59117	169.488037	428.164019	
2678.94885	258.675982	2287.54342	169.626721	169.281448	
169.010255	159.342433				
KEY POINT #2 (t plus 3545.8568 s with a Mixing Number of 45.0613):					17.0980732
0.040894	0.00925	0.3937	0.774251536	0.77782142	
1.01437511	1	1	25.1543862	53625.4588	
0.0666543777	0.0578988016	0.0224572327	3.30255128e-006	0.0224572327	
57.5884917	120.796019	105.224264	59.5907247	57.6073494	
57.7115322	55.3163089	4.18175389	4.22353585	2.09926281	
0.64847851	0.679747572	0.679747572	3.12040063	1.65892247	
0.0384433414	984.439928	954.541528	0.710116	0.679825282	
0.000483890924	0.000266991582	1.24480689e-005	1.30387436e-005	1552.30037	
1539.88533	474.882234	485.568719	1.21843599	1.1617673	
1.1987673	0.178227526	0.195710166	2716.61079	2715.97805	
241.152843	441.160976	2683.74072	200.008133	2275.44982	
249.526468	241.230265	241.668892	231.657426		
KEY POINT #3 (t plus 3929.9628 s with a Mixing Number of 46.6199):					17.2182201
0.040894	0.00925	0.3937	0.773909323	0.777684851	
1.01448632	1	1	24.9655168	53919.1583	
0.0663561845	0.0578091447	0.022615038	4.16771383e-006	0.022615038	
59.3183846	121.355029	105.683579	61.5963731	59.5004877	
59.6213177	56.7012398	4.18243309	4.22417038	2.10128489	
0.650168455	0.679906659	0.679906659	3.03129404	1.65114079	
0.0385200139	983.567396	954.200467	0.720724989	0.6898072	
0.000471221349	0.000265761443	1.24638092e-005	1.30588443e-005	1553.47546	
1539.38928	475.108716	485.863188	1.23790854	1.18084268	
1.21784268	0.193249648	0.214666293	2717.54356	2716.92028	
248.389013	443.102493	2684.45138	194.713479	2274.44107	
257.917658	249.149224	249.657542	237.449675		
KEY POINT #4 (t plus 6366.4011 s with a Mixing Number of 59.5309):					17.6517064
0.040894	0.00925	0.3937	0.771597097	0.776836182	
1.01265051	1	1	22.7900364	55110.1103	
0.0644064815	0.057132581	0.0231843947	5.53168716e-006	0.0231843947	
70.4163904	122.649972	109.134231	79.1966002	71.0299707	
70.5403739	65.9699288	4.18828341	4.22908818	2.11706265	
0.659962259	0.681020711	0.681020711	2.54874932	1.59495301	
0.0391137419	977.557622	951.608309	0.804617413	0.774720923	
0.000401615219	0.000256839297	1.25821823e-005	1.30983023e-005	1557.70958	
1535.47034	476.786755	486.127572	1.3925608	1.33857323	
1.37557323	0.317668188	0.458931685	2718.50573	2717.98634	
294.848815	457.698387	2689.74975	162.849572	2260.80734	
331.650093	297.417399	295.369567	276.237069		
KEY POINT #5 (t plus 6366.4011 s with a Mixing Number of 59.5309):					17.6517064
0.040894	0.00925	0.3937	0.771597097	0.776836182	
1.01265051	1	1	22.7900364	55110.1103	
0.0644064815	0.057132581	0.0231843947	5.53168716e-006	0.0231843947	
70.4163904	122.649972	109.134231	79.1966002	71.0299707	
70.5403739	65.9699288	4.18828341	4.22908818	2.11706265	
0.659962259	0.681020711	0.681020711	2.54874932	1.59495301	
0.0391137419	977.557622	951.608309	0.804617413	0.774720923	
0.000401615219	0.000256839297	1.25821823e-005	1.30983023e-005	1557.70958	
1535.47034	476.786755	486.127572	1.3925608	1.33857323	
1.37557323	0.317668188	0.458931685	2718.50573	2717.98634	
294.848815	457.698387	2689.74975	162.849572	2260.80734	
331.650093	297.417399	295.369567	276.237069		
KEY POINT #6 (t plus 10389.5643 s with a Mixing Number of 101.2825):					18.1662026
0.040894	0.00925	0.3937	0.766980885	0.775200659	
1.00781491	1	1	17.8698105	56358.6549	
0.0607506161	0.0554773728	0.0238601528	4.62477143e-006	0.0238601528	
90.3476697	125.541221	117.466444	104.312626	90.9430938	
85.1550588	75.0186114	4.20520845	4.24209009	2.15968964	
0.673249347	0.683129374	0.683129374	1.95623718	1.47425568	
0.0406840861	965.122498	945.133956	1.04020118	1.01678324	
0.000313191468	0.000237408291	1.28687445e-005	1.31814482e-005	1552.71808	

1524.65623	480.662839	486.381443	1.8323919	1.78456563
1.82156563	0.711141829	1.18053541	2719.81591	2719.49658
378.517041	493.020714	2702.2318	114.503673	2226.7952
437.355907	381.019801	356.696271	314.172469	
KEY POINT #7 (t plus 10476.3662 s with a Mixing Number of 102.1378):	18.2451682			
0.040894	0.00925	0.3937	0.767048816	0.775341886
1.00800428	1	1	17.8537151	56543.0263
0.0606872241	0.0554392316	0.0239638691	3.46070345e-006	0.0239638691
90.6842878	125.92333	117.656684	104.964976	91.1503275
87.199227	75.0508422	4.20556484	4.24240609	2.16074159
0.673428715	0.683168053	0.683168053	1.94839641	1.47172436
0.0407223221	964.895693	944.982617	1.04616726	1.02207316
0.000311992833	0.000236996423	1.28752969e-005	1.31955779e-005	1552.51115
1524.38774	480.748352	486.600797	1.84362374	1.79577757
1.83277757	0.720261872	1.20755557	2720.50904	2720.19028
379.933517	493.828557	2702.51137	113.89504	2226.68048
440.111337	381.892283	365.284616	314.308464	
KEY POINT #8 (t plus 12150.792 s with a Mixing Number of 124.9287):	18.3967156			
0.040894	0.00925	0.3937	0.774506634	0.784257862
1.00595646	1	1	16.1029805	56849.8624
0.0594655753	0.0547267846	0.024162917	2.60579392e-006	0.024162917
97.1171366	127.252007	121.196254	112.099614	97.7386992
97.0049835	75.6274089	4.21283709	4.24844665	2.18098291
0.676578993	0.683811712	0.683811712	1.80916264	1.42628789
0.041454137	960.458396	942.138406	1.16231414	1.14256485
0.000290550384	0.000229569169	1.29972703e-005	1.32333704e-005	1547.84291
1519.22193	482.314448	486.661696	2.06309051	2.01590208
2.05290208	0.914190784	1.53784957	2721.02293	2720.76362
407.027036	508.870904	2707.66659	101.843868	2212.15202
470.293543	409.644526	406.555925	316.742934	
KEY POINT #9 (t plus 12176.6925 s with a Mixing Number of 125.0643):	18.4266372			
0.040894	0.00925	0.3937	0.774688595	0.784459429
1.00600526	1	1	16.1033029	56925.3987
0.059454396	0.0547150309	0.024202217	1.92789535e-006	0.024202217
97.1755392	127.358866	121.25443	112.477966	97.9037866
97.1450586	75.7681241	4.21290677	4.24854851	2.18132633
0.676605296	0.683821092	0.683821092	1.80798517	1.42556668
0.0414664932	960.417304	942.09121	1.1643065	1.14436802
0.00029036777	0.000229450732	1.29992759e-005	1.32373056e-005	1547.79481
1519.13435	482.33979	486.721667	2.06686804	2.01967949
2.05667949	0.916131977	1.55725035	2721.21325	2720.95394
407.273365	509.118326	2707.75057	101.844961	2212.09493
471.895644	410.340439	407.146317	317.333092	
KEY POINT #10 (t plus 12655.0008 s with a Mixing Number of 133.4362):	18.3302025			
0.040894	0.00925	0.3937	0.777489783	0.787815423
1.00497512	1	1	15.4795526	56647.8362
0.0590909045	0.0544990916	0.0240755563	3.85227378e-006	0.0240755563
99.0700238	127.35117	122.321983	112.031872	100.022111
99.8606177	91.2361347	4.21521885	4.25043273	2.18769058
0.677432515	0.683986349	0.683986349	1.77057858	1.41247365
0.0416951577	959.073343	941.222556	1.2013598	1.18434531
0.000284551655	0.000227297492	1.30360843e-005	1.32325496e-005	1546.16608
1517.51205	482.802522	486.435734	2.13719639	2.09022054
2.12722054	0.980981298	1.53439702	2720.45046	2720.21085
415.262156	513.65979	2709.28734	98.3976337	2206.79067
470.012139	419.274702	418.596425	382.282066	
KEY POINT #11 (t plus 12878.0036 s with a Mixing Number of 138.0096):	18.3550464			
0.040894	0.00925	0.3937	0.778519357	0.789100504
1.00510617	1	1	15.3131202	56639.7123
0.0589014853	0.0544122981	0.0241081871	3.98772412e-006	0.0241081871
100.053871	127.904521	122.750407	113.305965	101.032183
100.851041	96.3918084	4.21645048	4.25119695	2.19027808
0.677844433	0.68404902	0.68404902	1.75173411	1.40729389
0.0417879538	958.368397	940.872581	1.21649476	1.19884663
0.000281612039	0.000226443991	1.30508583e-005	1.32523849e-005	1545.2763
1516.85292	482.986991	486.711946	2.1659633	2.12616504
2.16316504	1.01613104	1.60040925	2721.3413	2721.10681

419.412594	515.482946	2709.90173	96.0703515	2205.85835
475.40958	423.536934	422.775575	403.984819	
KEY POINT #12 (t plus 0 s with a Mixing Number of 33.3326):	20.4407065	0.040894		
0.00925	0.3937	0.779323037	0.78114485	1.01583551
1	1	33.4106111	64315.6065	0.0695239701
0.0268475692	2.89403617e-006	0.0268475692	40.4447578	119.481328
102.147658	40.4779476	40.3956775	40.3300343	38.0154017
4.17853301	4.21940564	2.08617393	0.629198854	0.678615984
0.678615984	4.29928124	1.71298998	0.0379435701	992.051354
956.80174	0.642282317	0.611868784	0.000647380988	0.000275503822
1.23427452e-005	1.29968805e-005	1532.08722	1543.04963	473.346672
485.184939	1.09441404	1.03590518	1.07290518	0.0756133143
0.0757467822	2715.70744	2714.59117	169.488037	428.164019
2678.94885	258.675982	2287.54342	169.626721	169.281448
169.010255	159.342433			
KEY POINT #13 (t plus 12878.0036 s with a Mixing Number of 138.0096):	18.3550464			
0.040894	0.00925	0.3937	0.778519357	0.789100504
1.00510617	1	1	15.3131202	56639.7123
0.0589014853	0.0544122981	0.0241081871	3.98772412e-006	0.0241081871
100.053871	127.904521	122.750407	113.305965	101.032183
100.851041	96.3918084	4.21645048	4.25119695	2.19027808
0.677844433	0.68404902	0.68404902	1.75173411	1.40729389
0.0417879538	958.368397	940.872581	1.21649476	1.19884663
0.000281612039	0.000226443991	1.30508583e-005	1.32523849e-005	1545.2763
1516.85292	482.986991	486.711946	2.1659633	2.12616504
2.16316504	1.01613104	1.60040925	2721.3413	2721.10681
419.412594	515.482946	2709.90173	96.0703515	2205.85835
475.40958	423.536934	422.775575	403.984819	
KEY POINT #14 (t plus 12173.3923 s with a Mixing Number of 125.0495):	18.4248759			
0.040894	0.00925	0.3937	0.774667349	0.784433846
1.00600622	1	1	16.1052489	56920.8484
0.0594555237	0.054716488	0.0241999037	1.95006229e-006	0.0241999037
97.1696482	127.352804	121.247218	112.565384	97.8907387
97.1195014	75.7433818	4.21289976	4.24853588	2.18128374
0.67660264	0.683819931	0.683819931	1.80810388	1.42565604
0.0414649609	960.421446	942.097061	1.16405937	1.14412144
0.000290386178	0.000229465407	1.29990272e-005	1.32370985e-005	1547.79965
1519.14521	482.336649	486.719271	2.06639947	2.01921538
2.05621538	0.915936017	1.56176135	2721.20514	2720.94576
407.248512	509.087655	2707.74016	101.839143	2212.11748
472.265744	410.285423	407.038613	317.229338	

End

D.3 TEST #3 - T03_RCIC_STD_157KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T03_RCIC_STD_157kw\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1869.6379 s, and ending (KEY POINT #11) at t plus 8547.2479 s, for a time period of 6677.6099 s.
Original Data Record Time: 10624.0827 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 2445.4389 s, T_bulk = 72.3374 C and T_out = 69.2204 C
Stratification Beginning SP12 Temperature = 71.8924 C
Stratification Beginning Pressure = 19.2092 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 6176.2003 s, T_bulk = 122.185 C and T_out = 80.2982 C
Stratification Ending SP12 Temperature = 121.8844 C
Stratification Ending Pressure = 48.0791 psia
Plume detected! Setting t_plume (KEY POINT #2) to 1087.8182 s.
At t = 1087.8182 s, the pool pressure is 16.2342 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 54.6606, 54.7606, 56.7615, 54.3952, and 51.9724 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 9.5434 +/- 2.5003 C.

Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 8.7138 +/- 2.0978 C.

Minimum Steam Quality: 0.99337 at t plus 176.1021 s
Maximum Steam Quality: 1.0011 at t plus 2569.341 s
Time-Averaged Steam Quality: 0.99782 +/- 0.0010239
Minimum Turbine Outlet Steam Quality: 1.003 at t plus 6615.9084 s
Maximum Turbine Outlet Steam Quality: 1.0276 at t plus 2379.1381 s
Time-Averaged Turbine Outlet Steam Quality: 1.019 +/- 0.0066167
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 6587.6078 s; using 300 s smoothing

Max and min smoothed upper level changerates: 1.0663 degrees/min at t plus 3189.1514 s and 0.50493 degrees/min at t plus 2875.2465 s, respectively
Max and min smoothed mid (SP9) level changerates: 1.0573 degrees/min at t plus 3237.3522 s and 0.62261 degrees/min at t plus 6283.4024 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.19443 degrees/min at t plus 1985.7866 s and -0.241 degrees/min at t plus 2875.5455 s, respectively
Max and min smoothed lower level changerates: 1.4786 degrees/min at t plus 3815.9613 s and 0.094281 degrees/min at t plus 3327.9543 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.86976 degrees/min at t plus 3327.4533 s and -0.60293 degrees/min at t plus 3815.7623 s, respectively
Max and min smoothed outlet level changerates: 7.0042 degrees/min at t plus 6468.1059 s and -0.17395 degrees/min at t plus 3795.5621 s, respectively
Max and min smoothed lower-outlet level changerate differences: 1.6313 degrees/min at t plus 3815.3622 s and -6.3115 degrees/min at t plus 6468.705 s, respectively
Max and min smoothed hot (SP8) level changerates: 1.553 degrees/min at t plus 1559.0252 s and 0.13839 degrees/min at t plus 2936.648 s, respectively
Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.82583 degrees/min at t plus 1648.1263 s and -0.59259 degrees/min at t plus 2936.648 s, respectively

The mean steam flow rate was 65.8486 +/- 3.0439 g/s
The mean feedwater flow rate was 65.8823 +/- 9.1956 g/s
The mean water injection to steam flow rate was 0.0031783 +/- 0.036458 g/s
Mean Smoothed Condensing Region SP8-SP9 delta T is 10.6358 +/- 0.8358 C over the Stratification Period, beginning at 11.8855 C and ending at 11.4474 C
Mean Smoothed SP8-Upper Pool delta T is 9.6111 +/- 0.73211 C over the Stratification Period, beginning at 10.6821 C and ending at 10.2441 C
The stratification period begins and ends with Smoothed SP8 readings of 84.4036 and 133.5181 C, respectively
The stratification period begins and ends with condensing flows of 1.035 and 2.1936 kg/s, respectively.
The stratification period begins and ends with condensing+cooling flows of 3.2797 and 2.9542 kg/s, respectively.
The stratification period had a mean sparger steam enthalpy of 2744.5577 +/- 1.5748 kJ/kg. At plume detection, the condensing and condensing+cooling flows are 0.6876 and 18.3343 kg/s, respectively
The plume period had a mean steam enthalpy of 2745.8367 +/- 1.6447 kJ/kg.

Maximum Smoothed Top-Mid delta T is 1.6781 degrees C at t plus 2725.6439 s with T_upper = 77.9279 C and T_mid = 76.2498 C
At t plus 2725.6439 s, Smoothed SP8-SP9 is 12.7747 C and Smoothed SP8-Top is 11.0966 C, where Smoothed SP8 is 89.0245 C and Pool P = 20.1329 psia
Maximum Smoothed Top-Lower delta T is 6.7008 degrees C at t plus 3678.7604 s with T_upper = 90.9028 C and T_low = 84.202 C
At t plus 3678.7604 s, Smoothed SP8-SP9 is 10.1671 C and Smoothed SP8-Top is 9.1887 C, where Smoothed SP8 is 100.0914 C and Pool P = 24.992 psia
Maximum Smoothed Mid-Lower delta T is 5.7477 degrees C at t plus 3694.3553 s with T_mid = 90.1508 C and T_low = 84.4031 C
At t plus 3694.3553 s, Smoothed SP8-SP9 is 10.2035 C and Smoothed SP8-Top is 9.2788 C, where Smoothed SP8 is 100.3543 C and Pool P = 25.0879 psia
Maximum Smoothed Top-Outlet delta T is 43.0534 degrees C at t plus 6052.1992 s with T_upper = 122.2823 C and T_out = 79.2289 C
At t plus 6052.1992 s, Smoothed SP8-SP9 is 11.3286 C and Smoothed SP8-Top is 9.7474 C, where Smoothed SP8 is 132.0297 C and Pool P = 46.6739 psia
Maximum Smoothed Mid-Outlet delta T is 41.9165 degrees C at t plus 6135.4999 s with T_mid = 121.6639 C and T_out = 79.7474 C
At t plus 6135.4999 s, Smoothed SP8-SP9 is 10.9465 C and Smoothed SP8-Top is 9.9234 C, where Smoothed SP8 is 132.6104 C and Pool P = 47.6132 psia
Maximum Smoothed Lower-Outlet delta T is 41.9804 degrees C at t plus 6154.501 s with T_low = 121.9601 C and T_out = 79.9796 C

At t plus 6154.501 s, Smoothed SP8-SP9 is 11.1521 C and Smoothed SP8-Top is 10.0929 C, where Smoothed SP8 is 133.0235 C and Pool P = 47.8228 psia

Maximum Smoothed Condensing Region SP8-SP9 delta T is 12.9716 degrees C at (KEY POINT #14) t plus 2669.2437 s with T_SP8 = 88.4751 C and T_SP9 = 75.5035 C and Pool P = 19.9292 psia

Maximum Smoothed Condensing Region SP8-Upper delta T is 11.8308 degrees C at t plus 2641.4711 s with T_SP8 = 87.9551 C and T_upper = 76.1242 C and Pool P = 19.8345 psia

Maximum Top-Mid delta T is 2.1445 degrees C at (KEY POINT #4) t plus 3106.8497 s ignoring SP 4, with temperatures of 82.8674 and 80.7229 C, respectively, at Set # 2, where Pool P = 21.7754 psia and T_outlet = 75.3324 C

Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 3449.5553 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.99976 C and a raw SP12 Reading of 86.4684 C.

Maximum Top-Lower delta T is 8.9259 degrees C at t plus 5260.3849 s, with temperatures of 113.4904 and 104.5645 C, respectively, at Set # 1, where Pool P = 38.2723 psia and T_outlet = 78.1327 C

Maximum Mid-Low delta T is 5.4803 degrees C at (KEY POINT #6) t plus 3805.0606 s ignoring SP 4, with temperatures of 91.8564 and 86.3762 C, respectively, at Set # 2, where Pool P = 25.7943 psia and T_outlet = 77.0472 C

Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 5005.9813 s with a Smoothed Mid-Axis Mid-Low Delta T of 1.8263 C and a raw SP12 Reading of 108.6931 C.

Maximum Top-Outlet delta T is 43.7645 degrees C at t plus 6121.9001 s, with temperatures of 123.3603 and 79.5958 C, respectively, at Set # 1, where Pool P = 47.4626 psia

Maximum Mid-Outlet delta T is 41.9691 degrees C at t plus 6141.7003 s ignoring SP 4, with temperatures of 121.7249 and 79.7558 C, respectively, at Set # 2, where Pool P = 47.6681 psia

Maximum Lower-Outlet delta T is 43.1039 degrees C at (KEY POINT #8) t plus 6128.2005 s, with temperatures of 122.7634 and 79.6595 C, respectively, at Set # 1, where Pool P = 47.5188 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 6541.2061 s with a Smoothed Mid-Axis Low-Outlet Delta T of 14.3615 C and a raw SP12 Reading of 125.7854 C.

Minimum SP Pressure is 15.1197 psia at t plus 3.0012 s

Maximum SP Pressure is 54.3209 psia at t plus 6677.6099 s

Beginning SP Pressure is 15.1236 psia

Ending SP Pressure is 54.3209 psia

Time-Average SP Pressure is 27.2369 +/- 11.5335 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 76.4803 cm (cold) / 76.6011 cm (hot) at 14.6614 psia

Beginning Smoothed SP Level is 76.4544 cm (cold) / 76.6249 cm (hot) at 15.1256 psia

Ending Smoothed SP Level is 75.3066 cm (cold) / 76.8603 cm (hot) at 54.2807 psia

Minimum Smoothed Cold SP Level is 75.23 cm at t plus 6461.2076 s and 51.4663 psia

Minimum Smoothed Hot SP Level is 76.3754 cm at t plus 1119.518 s and 16.2771 psia

Maximum Smoothed Cold SP Level is 76.4544 cm at t plus 0 s and 15.1256 psia

Maximum Smoothed Hot SP Level is 76.8603 cm at t plus 6677.6099 s and 54.2807 psia

SP 12 Temperature at the beginning is 40.3721 C, and at the end is 127.344 C

At plume detection, the Mixing Number is 39.3712

The Mixing Number ranges from a minimum of 32.8326 at (KEY POINT #12) t plus 0 s to a maximum of 244.6429 at (KEY POINT #13) t plus 6677.6099 s; it had a mean value of 94.5084 +/- 60.4538 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m2-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction v1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m3) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool

Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 32.8326): 44.45715697 0.040894
0.00925 0.3937 0.7645444334 0.7662493128 1.021496738
1 1 71.42501977 136985.6705 0.06949097261
0.05829777189 0.05839165072 -3.35227866e-007 0.05839165072 40.64740562
126.727252 103.1744119 41.27567523 40.56635291 40.4214568
37.64528885 4.178530783 4.220760891 2.090455176 0.629455079
0.6790064352 0.6790064352 4.281386266 1.694561878 0.03810772194
991.975184 956.0521556 0.6643062258 0.6224275734 0.0006449492585
0.0002726092404 1.237787288e-005 1.327168726e-005 1532.426014
1542.024491 473.8626944 489.753328 1.134586311 1.042875723
1.079875723 0.0764314079 0.07901649333 2733.981454 2728.87992
170.3354241 432.4999959 2680.554091 262.1645718 2301.481458
172.9606689 169.9952384 169.3928835 157.7964957

KEY POINT #2 (t plus 1087.8182 s with a Mixing Number of 39.3712): 46.74300179
0.040894 0.00925 0.3937 0.7610310003 0.7640678527
1.023245013 1 1 70.28150504 142449.6568
0.06713847375 0.05787353564 0.06139396264 2.001334565e-006 0.06139396264
54.7605962 130.6875257 105.3537514 56.76149746 54.66055371
54.39519899 51.97239649 4.180783563 4.223714257 2.09983104
0.6456174127 0.6797926789 0.6797926789 3.275806228 1.656721278
0.03846490139 985.8291053 954.4454734 0.7130938784 0.6651042191
0.0005058663071 0.000266643747 1.245250587e-005 1.341883412e-005
1550.057317 1539.746104 474.9461558 491.9930651 1.223899817
1.119360808 1.156360808 0.1558150762 0.1714054988 2741.001413
2736.061923 229.3251009 441.7082851 2683.94119 212.3831841
2299.293128 237.6910933 228.9053987 227.7990104 217.6748042

KEY POINT #3 (t plus 2445.4389 s with a Mixing Number of 53.0731): 52.09388404
0.040894 0.00925 0.3937 0.7616601133 0.7669129859
1.023440139 1 1 67.98616653 156945.1232
0.06403021805 0.0570059269 0.06842200646 4.754216195e-006 0.06842200646
72.51803594 134.9852449 109.7772262 84.40355148 73.72149447
72.83068442 69.28191302 4.189691092 4.230034258 2.12011983
0.6616155537 0.6812125693 0.6812125693 2.47205555 1.584909902
0.03922791118 976.342914 951.1194777 0.8210921042 0.7662956507
0.0003903749382 0.0002552368328 1.260426217e-005 1.357370813e-005
1557.897218 1534.703064 477.0948152 494.0944985 1.42306412
1.324876319 1.361876319 0.3475885813 0.5652740411 2747.62984
2743.007721 303.6514488 460.4201973 2690.728973 156.7687485
2287.209643 353.5026752 308.692698 304.962844 290.1017527

KEY POINT #4 (t plus 3106.8497 s with a Mixing Number of 63.688): 50.68421931
0.040894 0.00925 0.3937 0.757742679 0.7643108011
1.021069599 1 1 59.34988308 152621.8533
0.06253380263 0.0563658121 0.06657050141 2.881790241e-006 0.06657050141
80.75799554 135.4007651 113.0129727 90.95896909 81.89980702
80.70057296 75.2567058 4.196046508 4.23493907 2.13608295
0.6675201431 0.6821037115 0.6821037115 2.206703835 1.536286421
0.03981988967 971.3556753 948.6320332 0.9082054852 0.8540271818
0.0003510493169 0.0002474431515 1.271546807e-005 1.358049597e-005
1556.965813 1530.669102 478.6226023 493.8360496 1.585026419
1.501499681 1.538499681 0.4888888945 0.7277758718 2745.945225
2742.422817 338.2137397 474.1271125 2695.616917 135.9133729
2271.818113 381.0660413 343.004056 337.9742229 315.1476092

KEY POINT #5 (t plus 3449.5553 s with a Mixing Number of 72.8553): 51.26459703
0.040894 0.00925 0.3937 0.7566944695 0.764012636
1.019897568 1 1 55.73736589 154064.7752
0.0614855568 0.05590914161 0.06733279067 3.494004896e-006 0.06733279067
86.42398186 136.2711778 115.3074648 96.56036014 87.3247286
81.85379728 76.34362366 4.201236062 4.238564662 2.148003469
0.6710489928 0.6826610134 0.6826610134 2.052149185 1.503650593
0.04025780879 967.7266249 946.8405085 0.9744009555 0.9198005039
0.0003277827342 0.0002421771801 1.279440976e-005 1.360735722e-005

1554.840513	1527.636849	479.6829172	493.9993607	1.70880165
1.627899042	1.664899042	0.6117455533	0.8958553255	2746.225107
2743.118453	362.0128331	483.857161	2699.04167	121.8443279
2262.367946	404.6521669	365.7961584	342.8237309	319.7141489
KEY POINT #6 (t plus 3805.0606 s with a Mixing Number of 83.6055): 51.74712805				
0.040894	0.00925	0.3937	0.756182663	0.7643272184
1.018613016	1	1	51.83232013	155151.5716
0.0604770775	0.05539388775	0.0679665645	4.350520548e-006	0.0679665645
91.79816411	137.3012319	117.882749	102.1521825	92.71302772
86.63746248	77.09783897	4.206773389	4.242782747	2.161996349
0.6740089052	0.6832134732	0.6832134732	1.922886109	1.468728513
0.040767902	964.1406186	944.8025745	1.05329277	0.9984202952
0.0003080846628	0.000236508718	1.28830837e-005	1.36392241e-005	
1551.788744	1524.067462	480.8497907	494.1923263	1.857043868
1.778706343	1.815706343	0.7511380511	1.094588445	2746.628407
2743.941818	384.6173511	494.7886103	2702.843262	110.1712592
2251.839797	428.2369226	388.4651306	362.9229256	322.8884428
KEY POINT #7 (t plus 5005.9813 s with a Mixing Number of 135.5389): 52.18186199				
0.040894	0.00925	0.3937	0.75621858	0.7675074262
1.013265484	1	1	38.44184736	155173.285
0.05723678458	0.05337413688	0.06853755991	4.893649213e-006	0.06853755991
108.6045161	141.1156567	127.8461739	118.5916717	109.6351462
107.1182444	78.05024085	4.22805103	4.260647399	2.222545719
0.6809253282	0.6846352846	0.6846352846	1.603271374	1.348806503
0.04293800339	952.0625002	936.6497795	1.408606361	1.357520291
0.0002582059864	0.0002167371381	1.322666703e-005	1.375188432e-005	
1536.330998	1508.664187	485.126383	494.5436371	2.532994133
2.464610446	2.501610446	1.367837446	1.89964743	2747.499215
2746.02144	455.5394377	537.1951244	2717.103894	81.65568671
2210.304091	497.8423634	459.8965295	449.2583392	326.9370637
KEY POINT #8 (t plus 6128.2005 s with a Mixing Number of 203.6331): 50.39769459				
0.040894	0.00925	0.3937	0.7540170605	0.7679887075
1.007481314	1	1	28.1878444	148946.7363
0.0546520603	0.05144079316	0.0661941694	5.168097216e-006	0.0661941694
121.5659852	144.3413081	137.2018108	132.5030047	122.592497
121.4549084	79.69085632	4.248797605	4.279819496	2.289129878
0.6839457009	0.6849587875	0.6849587875	1.421672689	1.254896261
0.04528298518	941.8926339	928.6091816	1.824580727	1.788062566
0.0002288522575	0.0002008384284	1.354968057e-005	1.383691495e-005	
1518.929367	1492.0062	488.7861368	494.1055377	3.337826103
3.277281869	3.314281869	2.087194627	2.911151264	2746.69063
2745.896076	510.5292251	577.1977965	2729.791845	66.66857145
2169.492834	557.1100532	514.8904025	510.0585537	333.8829227
KEY POINT #9 (t plus 6176.2003 s with a Mixing Number of 207.0519): 50.22912624				
0.040894	0.00925	0.3937	0.7537674572	0.7678566839
1.007014383	1	1	27.75994153	148499.7704
0.05454996775	0.05135835995	0.06597276558	4.081462731e-006	0.06597276558
122.0706752	144.2738438	137.5970359	133.5180795	123.2739319
122.2137843	80.42524476	4.249686933	4.28068411	2.292155225
0.6840240722	0.6849513055	0.6849513055	1.415486782	1.251274108
0.04538900002	941.482039	928.2613227	1.844110315	1.809522317
0.0002278349083	0.0002002160896	1.356332873e-005	1.383214184e-005	
1518.163507	1491.257558	488.932975	493.9253971	3.375900397
3.315763064	3.352763064	2.120467653	2.999359788	2746.173291
2745.402677	512.6764514	578.8919549	2730.311794	66.21550345
2167.281337	561.4478286	517.7900127	513.2858903	336.9667753
KEY POINT #10 (t plus 6541.2061 s with a Mixing Number of 232.705): 50.0122673				
0.040894	0.00925	0.3937	0.7525180501	0.767565761
1.005101376	1	1	25.36292152	147551.3269
0.05377488114	0.05072604026	0.06568793515	4.399974615e-006	0.06568793515
125.8853462	145.3914209	140.6191354	136.2002259	127.3316562
126.4962125	111.2730171	4.256617391	4.28744909	2.315861033
0.6845228969	0.684838091	0.684838091	1.370605422	1.224422746
0.04621890652	938.3434337	925.5794557	1.999059671	1.971997478
0.0002204122916	0.000195578144	1.366768871e-005	1.386095064e-005	
1512.169001	1485.4154	490.0347414	493.6782601	3.678778217
3.620489487	3.657489487	2.386209555	3.242888959	2745.815148

2745.17187	528.9217242	591.8584595	2734.242761	62.93673532
2153.956689	572.9333599	535.0789017	531.523521	466.9155592
KEY POINT #11 (t plus 6677.6099 s with a Mixing Number of 244.6429):	50.67704985			
0.040894	0.00925	0.3937	0.7530662534	0.7686028714
1.004590928	1	1	24.89705353	149301.2138
0.05345042976	0.05048464587	0.06656108479	5.784484202e-006	0.06656108479
127.4734669	146.035546	141.7684685	137.6157713	128.8423165
128.093888	122.3372651	4.2596166	4.290094498	2.325142272
0.6846814085	0.6847691413	0.6847691413	1.352854629	1.214591517
0.04654356902	937.0178074	924.5493162	2.060659443	2.035640638
0.0002174548792	0.000193868641	1.370737618e-005	1.388057889e-005	
1509.564724	1483.139371	490.4439584	493.7257911	3.799557658
3.742524598	3.779524598	2.504543433	3.377713952	2746.156124
2745.53626	535.6924421	596.7954643	2735.716628	61.10302216
2149.360659	578.9985853	541.5238442	538.3367807	513.8435572
KEY POINT #12 (t plus 0 s with a Mixing Number of 32.8326):	44.45715697			0.040894
0.00925	0.3937	0.7645444334	0.7662493128	1.021496738
1	1	71.42501977	136985.6705	0.06949097261
0.05829777189	0.05839165072	-3.35227866e-007	0.05839165072	40.64740562
126.727252	103.1744119	41.27567523	40.56635291	40.4214568
37.64528885	4.178530783	4.220760891	2.090455176	0.629455079
0.6790064352	0.6790064352	4.281386266	1.694561878	0.03810772194
991.975184	956.0521556	0.6643062258	0.6224275734	0.0006449492585
0.0002726092404	1.237787288e-005	1.327168726e-005	1532.426014	
1542.024491	473.8626944	489.753328	1.134586311	1.042875723
1.079875723	0.0764314079	0.07901649333	2733.981454	2728.87992
170.3354241	432.4999959	2680.554091	262.1645718	2301.481458
172.9606689	169.9952384	169.3928835	157.7964957	
KEY POINT #13 (t plus 6677.6099 s with a Mixing Number of 244.6429):	50.67704985			
0.040894	0.00925	0.3937	0.7530662534	0.7686028714
1.004590928	1	1	24.89705353	149301.2138
0.05345042976	0.05048464587	0.06656108479	5.784484202e-006	0.06656108479
127.4734669	146.035546	141.7684685	137.6157713	128.8423165
128.093888	122.3372651	4.2596166	4.290094498	2.325142272
0.6846814085	0.6847691413	0.6847691413	1.352854629	1.214591517
0.04654356902	937.0178074	924.5493162	2.060659443	2.035640638
0.0002174548792	0.000193868641	1.370737618e-005	1.388057889e-005	
1509.564724	1483.139371	490.4439584	493.7257911	3.799557658
3.742524598	3.779524598	2.504543433	3.377713952	2746.156124
2745.53626	535.6924421	596.7954643	2735.716628	61.10302216
2149.360659	578.9985853	541.5238442	538.3367807	513.8435572
KEY POINT #14 (t plus 2669.2437 s with a Mixing Number of 56.6651):	50.57188974			
0.040894	0.00925	0.3937	0.7600253188	0.7656385249
1.022610007	1	1	64.03448581	152428.8767
0.0634919205	0.0568324002	0.06642296367	2.277784566e-006	0.06642296367
75.50352556	134.8908344	110.6566877	88.47510171	76.81459209
75.64341276	70.99070421	4.191833765	4.231343531	2.124362354
0.6638617744	0.681467031	0.681467031	2.369719358	1.571381752
0.03938590761	974.5760457	950.4479358	0.8440676863	0.7897873048
0.0003752930546	0.0002530744311	1.26344724e-005	1.356755297e-005	
1557.865356	1533.635061	477.5137842	493.8951837	1.465673045
1.374448755	1.411448755	0.3941569399	0.6621467603	2746.537814
2742.437399	316.1668913	464.1440213	2692.064109	147.97713
2282.393793	370.6124693	321.6619546	316.7547323	297.2623747

End

D.4 TEST #4 - T04_RCIC_STD_107KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T04_RCIC_STD_107kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1721.1344 s, and ending (KEY POINT #11) at t
plus 10637.7904 s, for a time period of 8916.656 s.
Original Data Record Time: 11590.724 s

Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus
 2678.6462 s, $T_{bulk} = 65.2079$ C and $T_{out} = 62.5368$ C
 Stratification Beginning SP12 Temperature = 65.1796 C
 Stratification Beginning Pressure = 17.4645 psia
 Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus
 8051.2415 s, $T_{bulk} = 115.4315$ C and $T_{out} = 73.8345$ C
 Stratification Ending SP12 Temperature = 115.3675 C
 Stratification Ending Pressure = 41.4152 psia
 Plume detected! Setting t_plume (KEY POINT #2) to 2016.8354 s.
 At t = 2016.8354 s, the pool pressure is 16.4355 psia while the Smoothed Upper, Mid, SP8,
 Lower, and Outlet Temperatures are 59.297, 59.4284, 61.4291, 59.2957, and 56.321
 C, respectively.
 Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9
 temperatures were 10.7153 +/- 2.4439 C.
 Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper
 temperatures were 9.846 +/- 2.2417 C.
 Minimum Steam Quality: 0.99488 at t plus 6.3004 s
 Maximum Steam Quality: 1.0059 at t plus 1243.5221 s
 Time-Averaged Steam Quality: 1.0015 +/- 0.0014775
 Minimum Turbine Outlet Steam Quality: 1.0003 at t plus 8888.9555 s
 Maximum Turbine Outlet Steam Quality: 1.0269 at t plus 1243.5221 s
 Time-Averaged Turbine Outlet Steam Quality: 1.0166 +/- 0.0065728
 Smoothed Changerates may not fully include test beginning and end periods, analysis
 ending at t plus 8826.6569 s; using 300 s smoothing
 Max and min smoothed upper level changerates: 0.82359 degrees/min at t plus 3634.1629 s
 and 0.33562 degrees/min at t plus 7201.9259 s, respectively
 Max and min smoothed mid (SP9) level changerates: 0.8436 degrees/min at t plus 3856.9686
 s and 0.39538 degrees/min at t plus 7744.1359 s, respectively
 Max and min smoothed upper-mid level changerate differences: 0.39545 degrees/min at t
 plus 3586.0621 s and -0.21489 degrees/min at t plus 3849.6672 s, respectively
 Max and min smoothed lower level changerates: 3.3758 degrees/min at t plus 6273.3088 s
 and -0.010467 degrees/min at t plus 5121.79 s, respectively
 Max and min smoothed mid-lower level changerate differences: 0.69735 degrees/min at t
 plus 5121.3899 s and -2.8874 degrees/min at t plus 6284.5115 s, respectively
 Max and min smoothed outlet level changerates: 8.0358 degrees/min at t plus 8357.8461 s
 and -0.024187 degrees/min at t plus 5361.5937 s, respectively
 Max and min smoothed lower-outlet level changerate differences: 3.3129 degrees/min at t
 plus 6273.3088 s and -7.5257 degrees/min at t plus 8355.1469 s, respectively
 Max and min smoothed hot (SP8) level changerates: 1.2931 degrees/min at t plus 2402.0414
 s and 0.071089 degrees/min at t plus 8268.3439 s, respectively
 Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.76384 degrees/min
 at t plus 2402.5414 s and -0.4205 degrees/min at t plus 3756.0658 s, respectively
 The mean steam flow rate was 45.3195 +/- 1.2552 g/s
 The mean feedwater flow rate was 45.1489 +/- 3.8097 g/s
 The mean water injection to steam flow rate was 0.0092897 +/- 0.036998 g/s
 Mean Smoothed Condensing Region SP8-SP9 delta T is 11.4647 +/- 1.1155 C over the
 Stratification Period, beginning at 7.5605 C and ending at 12.0327 C
 Mean Smoothed SP8-Upper Pool delta T is 10.5088 +/- 1.1639 C over the Stratification
 Period, beginning at 7.2295 C and ending at 10.8785 C
 The stratification period begins and ends with Smoothed SP8 readings of 73.2543 and
 127.6498 C, respectively
 The stratification period begins and ends with condensing flows of 0.62296 and 1.4225
 kg/s, respectively.
 The stratification period begins and ends with condensing+cooling flows of 3.5097 and
 1.9911 kg/s, respectively.
 The stratification period had a mean sparger steam enthalpy of 2736.939 +/- 0.89115 kJ/kg.
 At plume detection, the condensing and condensing+cooling flows are 0.56225 and 13.574
 kg/s, respectively
 The plume period had a mean steam enthalpy of 2737.8397 +/- 0.44888 kJ/kg.
 Maximum Smoothed Top-Mid delta T is 2.4105 degrees C at t plus 3711.2643 s with $T_{upper} =$
 76.8628 C and $T_{mid} = 74.4523$ C
 At t plus 3711.2643 s, Smoothed SP8-SP9 is 11.1711 C and Smoothed SP8-Top is 8.7606 C,
 where Smoothed SP8 is 85.6234 C and Pool P = 19.9646 psia
 Maximum Smoothed Top-Lower delta T is 19.6247 degrees C at t plus 6010.7408 s with
 $T_{upper} = 101.2917$ C and $T_{low} = 81.667$ C
 At t plus 6010.7408 s, Smoothed SP8-SP9 is 12.2069 C and Smoothed SP8-Top is 11.3904 C,
 where Smoothed SP8 is 112.6821 C and Pool P = 29.9824 psia

Maximum Smoothed Mid-Lower delta T is 18.9971 degrees C at t plus 6044.5067 s with T_mid = 100.8166 C and T_low = 81.8195 C
 At t plus 6044.5067 s, Smoothed SP8-SP9 is 11.9788 C and Smoothed SP8-Top is 11.3634 C, where Smoothed SP8 is 112.7954 C and Pool P = 30.1686 psia
 Maximum Smoothed Top-Outlet delta T is 43.1262 degrees C at t plus 7969.5398 s with T_upper = 116.1395 C and T_out = 73.0133 C
 At t plus 7969.5398 s, Smoothed SP8-SP9 is 12.1539 C and Smoothed SP8-Top is 11.0212 C, where Smoothed SP8 is 127.1607 C and Pool P = 40.9125 psia
 Maximum Smoothed Mid-Outlet delta T is 42.061 degrees C at t plus 8017.2396 s with T_mid = 115.4865 C and T_out = 73.4255 C
 At t plus 8017.2396 s, Smoothed SP8-SP9 is 11.9442 C and Smoothed SP8-Top is 10.9914 C, where Smoothed SP8 is 127.4307 C and Pool P = 41.1992 psia
 Maximum Smoothed Lower-Outlet delta T is 42.2788 degrees C at t plus 8003.6398 s with T_low = 115.5709 C and T_out = 73.2921 C
 At t plus 8003.6398 s, Smoothed SP8-SP9 is 12.0048 C and Smoothed SP8-Top is 10.9919 C, where Smoothed SP8 is 127.3376 C and Pool P = 41.1173 psia
 Maximum Smoothed Condensing Region SP8-SP9 delta T is 13.5417 degrees C at (KEY POINT #14) t plus 7113.6249 s with T_SP8 = 122.4688 C and T_SP9 = 108.9271 C and Pool P = 35.9401 psia
 Maximum Smoothed Condensing Region SP8-Upper delta T is 12.5963 degrees C at t plus 7113.6249 s with T_SP8 = 122.4688 C and T_upper = 109.8725 C and Pool P = 35.9401 psia
 Maximum Top-Mid delta T is 3.0644 degrees C at (KEY POINT #4) t plus 3624.5643 s ignoring SP 4, with temperatures of 76.5882 and 73.5238 C, respectively, at Set # 2, where Pool P = 19.7049 psia and T_outlet = 67.3603 C
 Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 4645.2817 s with a Smoothed Mid-Axis Top-Mid Delta T of 1.0212 C and a raw SP12 Reading of 85.7181 C.
 Maximum Top-Lower delta T is 22.445 degrees C at t plus 6218.5097 s, with temperatures of 102.8387 and 80.3937 C, respectively, at Set # 1, where Pool P = 31.1223 psia and T_outlet = 71.9789 C
 Maximum Mid-Low delta T is 20.9285 degrees C at (KEY POINT #6) t plus 6229.0083 s ignoring SP 4, with temperatures of 102.3057 and 81.3772 C, respectively, at Set # 2, where Pool P = 31.1883 psia and T_outlet = 71.8474 C
 Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 6370.8124 s with a Smoothed Mid-Axis Mid-Low Delta T of 6.9655 C and a raw SP12 Reading of 103.5519 C.
 Maximum Top-Outlet delta T is 43.5091 degrees C at t plus 7968.3398 s, with temperatures of 116.4668 and 72.9576 C, respectively, at Set # 1, where Pool P = 40.8988 psia
 Maximum Mid-Outlet delta T is 41.9109 degrees C at t plus 7975.5402 s ignoring SP 4, with temperatures of 114.86 and 72.9491 C, respectively, at Set # 2, where Pool P = 40.951 psia
 Maximum Lower-Outlet delta T is 43.2682 degrees C at (KEY POINT #8) t plus 7991.5401 s, with temperatures of 116.4709 and 73.2027 C, respectively, at Set # 1, where Pool P = 41.0478 psia
 Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 8405.2458 s with a Smoothed Mid-Axis Low-Outlet Delta T of 14.4199 C and a raw SP12 Reading of 117.9138 C.
 Minimum SP Pressure is 14.7156 psia at t plus 15.7999 s
 Maximum SP Pressure is 47.7972 psia at t plus 8916.656 s
 Beginning SP Pressure is 14.7258 psia
 Ending SP Pressure is 47.7972 psia
 Time-Average SP Pressure is 25.6377 +/- 9.8652 psia
 SP Levels are fully corrected and compensated
 Pre-Start SP Level is 75.149 cm (cold) / 75.2718 cm (hot) at 14.5991 psia
 Beginning Smoothed SP Level is 75.2222 cm (cold) / 75.3836 cm (hot) at 14.7188 psia
 Ending Smoothed SP Level is 84.1863 cm (cold) / 86.1615 cm (hot) at 47.7888 psia
 Minimum Smoothed Cold SP Level is 75.1096 cm at t plus 629.01 s and 15.0644 psia
 Minimum Smoothed Hot SP Level is 75.3114 cm at t plus 442.3073 s and 14.9476 psia
 Maximum Smoothed Cold SP Level is 85.8062 cm at t plus 7085.2243 s and 35.7837 psia
 Maximum Smoothed Hot SP Level is 87.4819 cm at t plus 7264.1275 s and 36.7636 psia
 SP 12 Temperature at the beginning is 40.2491 C, and at the end is 122.0172 C
 At plume detection, the Mixing Number is 43.1669
 The Mixing Number ranges from a minimum of 32.2572 at (KEY POINT #12) t plus 0 s to a maximum of 255.7515 at (KEY POINT #13) t plus 8916.656 s; it had a mean value of 101.7014 +/- 65.3588 over the test period.
 Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1,

Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) mdl, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m3) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 32.2572): 34.40181538 0.040894
0.00925 0.3937 0.7522216526 0.7538356888 1.020556529
1 1 57.27315231 106633.2441 0.06952701765
0.05852122721 0.04518459849 1.063212153e-005 0.04518459849 40.4260351
124.6067033 102.0220533 41.00954586 40.42534979 40.22789524
37.81728715 4.178538293 4.219241431 2.085656058 0.6291740867
0.6785673353 0.6785673353 4.3009858 1.715271477 0.03792366743
992.0584844 956.8931131 0.6396294303 0.6008034983 0.000647611347
0.0002758617193 1.23384495e-005 1.319314487e-005 1532.05248
1543.172896 473.2833033 488.5448809 1.089581454 1.014824369
1.051824369 0.07553811317 0.07791241071 2728.307459 2725.027245
169.4079371 427.6336913 2678.752065 258.2257542 2300.673768
171.846159 169.4035685 168.5815964 158.5127097

KEY POINT #2 (t plus 2016.8354 s with a Mixing Number of 43.1669): 34.92123307
0.040894 0.00925 0.3937 0.7637198724 0.7673177211
1.022370601 1 1 52.60794133 106754.6615
0.06633717182 0.05789917199 0.04586682062 1.036059291e-005 0.04586682062
59.4283765 129.5986662 105.2223657 61.42908483 59.29701925
59.29567379 56.32095298 4.182489254 4.223533235 2.099254486
0.6502718707 0.6797469092 0.6797469092 3.025813938 1.658954783
0.03844302561 983.5106873 954.5429359 0.710072415 0.6639514938
0.0004704379545 0.0002669966882 1.244800381e-005 1.337711052e-005
1553.536947 1539.88737 474.8812965 491.3118292 1.218356035
1.133565949 1.170565949 0.1942402031 0.2130276744 2736.673344
2733.905748 248.8450726 441.1529516 2683.737778 192.307879
2295.520392 257.2138703 248.2942457 248.2915633 235.8555574

KEY POINT #3 (t plus 2678.6462 s with a Mixing Number of 48.9515): 34.83387524
0.040894 0.00925 0.3937 0.7746214971 0.779223643
1.022198815 1 1 50.21642406 106192.7673
0.06524385091 0.05763756962 0.04575208167 7.243594906e-006 0.04575208167
65.69376493 130.6504106 106.5612187 73.25431464 66.02483043
65.63601417 62.49393146 4.185492826 4.225395863 2.105198932
0.6560097956 0.6802035598 0.6802035598 2.736992128 1.636473814
0.03866803798 980.1983043 953.5461753 0.7413546004 0.6937847703
0.0004289802231 0.0002634392965 1.249389627e-005 1.341425156e-005
1556.572572 1538.424595 475.5394436 491.7930094 1.275829729
1.203945501 1.240945501 0.2582847625 0.3586180176 2738.030475
2735.508786 275.0648305 446.8131219 2685.8058 171.7482914
2291.217353 306.7266148 276.4491276 274.8246053 261.6799004

KEY POINT #4 (t plus 3624.5643 s with a Mixing Number of 59.493): 34.93264592
0.040894 0.00925 0.3937 0.7953994066 0.8020127387
1.020257726 1 1 45.2137879 106306.2565
0.06378198893 0.05701084426 0.04588181068 6.512104765e-006 0.04588181068
73.89781827 131.489335 109.7522791 85.99930331 75.47625293
72.97017505 67.4294238 4.190655797 4.229997376 2.120000517
0.6626696478 0.6812052172 0.6812052172 2.423793664 1.58529714
0.03922346051 975.5308972 951.1384773 0.8204478518 0.7727201283

0.0003832752131	0.0002552986649	1.260340539e-005	1.343792614e-005	
1557.929276	1534.733048	477.0828903	491.8396249	1.421870485
1.359230226	1.396230226	0.3684980549	0.6017214731	2737.917671
2735.873384	309.4357568	460.3145838	2690.691029	150.8788269
2277.603087	360.2077192	316.0499732	305.5500901	282.3482331
KEY POINT #5 (t plus 4645.2817 s with a Mixing Number of 81.2408): 34.92112247				
0.040894	0.00925	0.3937	0.8190119211	0.828250966
1.017594645	1	1	38.90008026	105956.2387
0.06163749197	0.05610772163	0.04586667536	9.802100608e-006	0.04586667536
85.60790257	132.8739297	114.3111256	96.74004667	86.472661
78.17109105	70.81145043	4.200450543	4.236975112	2.142764793
0.6705661017	0.6824265802	0.6824265802	2.073171896	1.517640948
0.04006576376	968.2571846	947.621253	0.9451932205	0.8979052274
0.0003309642103	0.0002444381887	1.276012292e-005	1.347786974e-005	
1555.214835	1528.970836	479.2248698	491.9560525	1.65411637
1.594827843	1.631827843	0.5926048434	0.9017390056	2738.0957
2736.582484	358.5820237	479.6309925	2697.558831	121.0489688
2258.464708	405.4065633	362.2134334	327.3706936	296.5295385
KEY POINT #6 (t plus 6229.0083 s with a Mixing Number of 137.9235): 34.75329138				
0.040894	0.00925	0.3937	0.8545270816	0.8689713752
1.012140227	1	1	29.08765306	104850.0376
0.05842805582	0.05429689137	0.04564623988	7.521363545e-006	0.04564623988
102.5029149	135.6590304	123.3194877	115.0044135	103.133534
89.09535659	71.88475847	4.219623583	4.252219229	2.19374485
0.678814136	0.6841290414	0.6841290414	1.706503443	1.400478648
0.04191213469	956.5931569	940.4064904	1.236836165	1.194974987
0.0002745265394	0.0002253195482	1.307048472e-005	1.355460741e-005	
1542.920027	1515.970295	483.2309269	491.9364943	2.204662026
2.150553579	2.187553579	1.108178404	1.692013842	2738.183049
2737.336957	429.7445418	517.9051974	2710.715739	88.16065558
2220.277851	482.6069751	432.4045148	373.2814169	301.0706533
KEY POINT #7 (t plus 6370.8124 s with a Mixing Number of 142.763): 34.55550981				
0.040894	0.00925	0.3937	0.8555736982	0.8704090631
1.01163804	1	1	28.25422642	104215.0657
0.05822015396	0.05414374541	0.04538646636	8.958663403e-006	0.04538646636
103.5739645	135.8623059	124.0736408	116.1709322	104.367005
97.51265443	72.0393395	4.2210432	4.253586647	2.198391619
0.6792173666	0.6842294283	0.6842294283	1.68743126	1.391559939
0.04207832679	955.8097495	939.7866875	1.264214688	1.223262321
0.0002715282839	0.0002238455075	1.309649711e-005	1.355958477e-005	
1541.8416	1514.788173	483.5522627	491.8948769	2.256812451
2.203031053	2.240031053	1.150544667	1.75738407	2738.08423
2737.285928	434.2686266	521.1161509	2711.790771	86.84752438
2216.968079	487.5554721	437.6152482	408.7089062	301.722479
KEY POINT #8 (t plus 7991.5401 s with a Mixing Number of 205.3155): 35.25266162				
0.040894	0.00925	0.3937	0.8545491691	0.8726889905
1.00686591	1	1	22.60800895	105675.7284
0.05592699423	0.0524881249	0.04630213096	1.068039694e-005	0.04630213096
115.2179803	138.8443543	132.1546108	127.3980117	116.2705098
115.3695778	73.19203933	4.238144568	4.269173936	2.252014138
0.6827102144	0.6849042168	0.6849042168	1.504842452	1.303536968
0.04397926731	946.9628101	932.9931443	1.589453642	1.559659382
0.0002424106344	0.000209126632	1.33753981e-005	1.364194377e-005	
1528.005266	1501.249046	486.8553624	491.7737341	2.881365416
2.829725527	2.866725527	1.703830436	2.498815276	2738.428411
2737.917289	483.5606425	555.5935966	2723.035826	72.03295414
2182.834815	535.3086623	488.0210915	484.2044374	306.6025861
KEY POINT #9 (t plus 8051.2415 s with a Mixing Number of 207.827): 35.20540065				
0.040894	0.00925	0.3937	0.8540015799	0.8721979013
1.00671896	1	1	22.37746022	105498.2817
0.05584735139	0.05242481555	0.04624005668	1.0692646e-005	0.04624005668
115.6170491	138.9976133	132.4610877	127.6497742	116.771276
115.8657729	73.75350182	4.238785684	4.269799808	2.254187739
0.6828016163	0.6849155093	0.6849155093	1.499305715	1.300452701
0.0440558161	946.6491522	932.7300266	1.602996852	1.573616544
0.0002415145379	0.0002086046804	1.338597988e-005	1.364656969e-005	
1527.465631	1500.704762	486.9755299	491.7888471	2.907554438

2.85602991	2.89302991	1.726092028	2.517969354	2738.5098
2738.00905	485.2539555	556.90385	2723.4521	71.6498945
2181.60595	536.3829494	490.1463423	486.3095733	308.9572528
KEY POINT #10 (t plus 8405.2458 s with a Mixing Number of 225.698): 34.94308821				
0.040894	0.00925	0.3937	0.849664637	0.8685311569
1.005289487	1	1	21.01984588	104657.0783
0.05533662492	0.05204083332	0.04589552596	9.229719687e-006	0.04589552596
118.1680825	139.4084348	134.3160722	129.2548024	119.3937725
118.7195412	103.3680065	4.242976403	4.273644077	2.267564464
0.6833415888	0.6849617792	0.6849617792	1.464914922	1.282152795
0.04452629745	944.6273076	931.1289622	1.686962751	1.662719868
0.0002359280832	0.0002054980818	1.345003082e-005	1.365376019e-005	
1523.914819	1497.363362	487.694802	491.4921922	3.070212789
3.019526207	3.056526207	1.874096352	2.642904076	2737.828183
2737.386349	496.0841327	564.8386593	2725.955152	68.7545266
2172.989524	543.2342437	501.2847667	498.4254787	433.4646691
KEY POINT #11 (t plus 8916.656 s with a Mixing Number of 255.7515): 35.04922075				
0.040894	0.00925	0.3937	0.8418626439	0.8616154854
1.003650211	1	1	19.37441085	104691.1598
0.05452979159	0.05142895909	0.04603492431	9.012404901e-006	0.04603492431
122.1703529	140.7152566	137.258567	132.6789999	123.6338255
123.2272372	118.978596	4.249870726	4.279943377	2.289563268
0.6840375006	0.6849578175	0.6849578175	1.414269088	1.254374494
0.04529817388	941.3986284	928.5592682	1.827375008	1.80940121
0.000227633534	0.0002007488277	1.355164051e-005	1.369077233e-005	
1518.004914	1491.898912	488.8072625	491.4340818	3.343272323
3.29491943	3.33191943	2.127090052	2.926292478	2738.09877
2737.723402	513.0986043	577.4410635	2729.866594	64.34245921
2160.657707	557.8627244	519.3188957	517.5924596	499.5475351
KEY POINT #12 (t plus 0 s with a Mixing Number of 32.2572): 34.40181538 0.040894				
0.00925	0.3937	0.7522216526	0.7538356888	1.020556529
1	1	57.27315231	106633.2441	0.06952701765
0.05852122721	0.04518459849	1.063212153e-005	0.04518459849	40.4260351
124.6067033	102.0220533	41.00954586	40.42534979	40.22789524
37.81728715	4.178538293	4.219241431	2.085656058	0.6291740867
0.6785673353	0.6785673353	4.3009858	1.715271477	0.03792366743
992.0584844	956.8931131	0.6396294303	0.6008034983	0.000647611347
0.0002758617193	1.23384495e-005	1.319314487e-005	1532.05248	
1543.172896	473.2833033	488.5448809	1.089581454	1.014824369
1.051824369	0.07553811317	0.07791241071	2728.307459	2725.027245
169.4079371	427.6336913	2678.752065	258.2257542	2300.673768
171.846159	169.4035685	168.5815964	158.5127097	
KEY POINT #13 (t plus 8916.656 s with a Mixing Number of 255.7515): 35.04922075				
0.040894	0.00925	0.3937	0.8418626439	0.8616154854
1.003650211	1	1	19.37441085	104691.1598
0.05452979159	0.05142895909	0.04603492431	9.012404901e-006	0.04603492431
122.1703529	140.7152566	137.258567	132.6789999	123.6338255
123.2272372	118.978596	4.249870726	4.279943377	2.289563268
0.6840375006	0.6849578175	0.6849578175	1.414269088	1.254374494
0.04529817388	941.3986284	928.5592682	1.827375008	1.80940121
0.000227633534	0.0002007488277	1.355164051e-005	1.369077233e-005	
1518.004914	1491.898912	488.8072625	491.4340818	3.343272323
3.29491943	3.33191943	2.127090052	2.926292478	2738.09877
2737.723402	513.0986043	577.4410635	2729.866594	64.34245921
2160.657707	557.8627244	519.3188957	517.5924596	499.5475351
KEY POINT #14 (t plus 7113.6249 s with a Mixing Number of 168.4359): 34.79428343				
0.040894	0.00925	0.3937	0.8580402853	0.8745200367
1.009412978	1	1	25.38457855	104653.0809
0.05717334687	0.05338016654	0.04570008033	6.330933059e-006	0.04570008033
108.9270743	137.1877066	127.8167278	122.4687829	109.8724974
107.4931699	72.25716339	4.228520776	4.260590843	2.222351265
0.6810242178	0.6846327354	0.6846327354	1.598156455	1.349128592
0.044293110763	951.8171674	936.6744992	1.407430088	1.370875765
0.0002573910139	0.0002167909646	1.322565074e-005	1.35961351e-005	
1535.952154	1508.713333	485.1143128	491.8531995	2.530736843
2.477954732	2.514954732	1.382848779	2.147018096	2738.227453

2737.583076	456.9042782	537.0695117	2717.062847	80.16523352
2201.157941	514.310077	460.9014351	450.8438134	302.6573393

End

D.5 TEST #5 - T05_SRV_STD_157KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T05_SRV_STD_157kw\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 2283.0426 s, and ending (KEY POINT #11) at t plus 6993.515 s, for a time period of 4710.4724 s.
Original Data Record Time: 9615.556 s
No Bulk Pool to Outlet Thermal Stratification Detected (KEY POINT #3), 0 0 0 0 0 0.
No Bulk Pool to Outlet Destratification Detected (KEY POINT #9), 0 0 0 0 0 0.
No Plume detected, setting t_plume (KEY POINT #2) to the end at 4710.4724 s.
At t = 4710.4724 s, the pool pressure is 32.5391 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 105.7249, 106.8742, 106.4698, 105.2811, and 102.8122 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were -0.40439 +/- 0 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 0.74496 +/- 0 C.
Minimum Steam Quality: 1.0089 at t plus 4709.8724 s
Maximum Steam Quality: 1.0217 at t plus 664.11 s
Time-Averaged Steam Quality: 1.017 +/- 0.0028703
SRV Alignment, no RCIC Turbine 0 0 0 0 0 0
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 4620.4713 s; using 300 s smoothing
Max and min smoothed upper level changerates: 1.1176 degrees/min at t plus 3715.9565 s and 0.69649 degrees/min at t plus 4138.4627 s, respectively
Max and min smoothed mid (SP9) level changerates: 1.3449 degrees/min at t plus 3650.9568 s and 0.53674 degrees/min at t plus 4342.9674 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.25342 degrees/min at t plus 4343.6675 s and -0.30281 degrees/min at t plus 3565.5539 s, respectively
Max and min smoothed lower level changerates: 1.0132 degrees/min at t plus 384.807 s and 0.58094 degrees/min at t plus 552.9086 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.63315 degrees/min at t plus 3650.9568 s and -0.38044 degrees/min at t plus 4505.9687 s, respectively
Max and min smoothed outlet level changerates: 1.0635 degrees/min at t plus 1267.9205 s and 0.7041 degrees/min at t plus 213.8042 s, respectively
Max and min smoothed lower-outlet level changerate differences: 0.2568 degrees/min at t plus 2236.8339 s and -0.22594 degrees/min at t plus 1358.9207 s, respectively
Max and min smoothed hot (SP8) level changerates: 1.1427 degrees/min at t plus 3712.9564 s and 0.663 degrees/min at t plus 4102.6637 s, respectively
Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.45887 degrees/min at t plus 4342.9674 s and -0.33179 degrees/min at t plus 3945.0606 s, respectively
The mean steam flow rate was 66.4143 +/- 2.0659 g/s
The mean feedwater flow rate was 65.5882 +/- 3.517 g/s
The mean water injection to steam flow rate was 0.0027372 +/- 0.03749 g/s
No stratification; 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0.
At plume detection, the condensing and condensing+cooling flows are 2.0687 and -93.0779 kg/s, respectively
The plume period had a mean steam enthalpy of 2740.5797 +/- 0 kJ/kg.
Maximum Smoothed Top-Mid delta T is 0.78185 degrees C at t plus 3541.8546 s with T_upper = 89.7499 C and T_mid = 88.9681 C
At t plus 3541.8546 s, Smoothed SP8-SP9 is 0.83515 C and Smoothed SP8-Top is 0.053292 C, where Smoothed SP8 is 89.8032 C and Pool P = 24.2712 psia
Maximum Smoothed Top-Lower delta T is 1.6622 degrees C at t plus 4130.3633 s with T_upper = 98.4533 C and T_low = 96.7911 C
At t plus 4130.3633 s, Smoothed SP8-SP9 is -1.7152 C and Smoothed SP8-Top is -0.20891 C, where Smoothed SP8 is 98.2444 C and Pool P = 28.0202 psia
Maximum Smoothed Mid-Lower delta T is 3.1906 degrees C at t plus 4222.5665 s with T_mid = 101.2668 C and T_low = 98.0762 C

At t plus 4222.5665 s, Smoothed SP8-SP9 is -2.2607 C and Smoothed SP8-Top is -0.32095 C, where Smoothed SP8 is 99.0062 C and Pool P = 28.6706 psia
Maximum Smoothed Top-Outlet delta T is 3.6183 degrees C at t plus 3791.1588 s with T_upper = 94.1787 C and T_out = 90.5604 C
At t plus 3791.1588 s, Smoothed SP8-SP9 is -0.5268 C and Smoothed SP8-Top is -0.21835 C, where Smoothed SP8 is 93.9603 C and Pool P = 25.7636 psia
Maximum Smoothed Mid-Outlet delta T is 4.9228 degrees C at t plus 4128.0641 s with T_mid = 99.9653 C and T_out = 95.0425 C
At t plus 4128.0641 s, Smoothed SP8-SP9 is -1.7364 C and Smoothed SP8-Top is -0.19411 C, where Smoothed SP8 is 98.2288 C and Pool P = 27.9945 psia
Maximum Smoothed Lower-Outlet delta T is 3.7321 degrees C at t plus 2357.2368 s with T_low = 74.0511 C and T_out = 70.319 C
At t plus 2357.2368 s, Smoothed SP8-SP9 is -0.19088 C and Smoothed SP8-Top is -0.072027 C, where Smoothed SP8 is 72.8295 C and Pool P = 19.1811 psia
Maximum Smoothed Condensing Region SP8-SP9 delta T is 0.83709 degrees C at (KEY POINT #14) t plus 3541.4546 s with T_SP8 = 89.8009 C and T_SP9 = 88.9638 C and Pool P = 24.2743 psia
Maximum Smoothed Condensing Region SP8-Upper delta T is 0.84595 degrees C at t plus 4681.9728 s with T_SP8 = 106.0622 C and T_upper = 105.2162 C and Pool P = 32.2835 psia
Maximum Top-Mid delta T is 2.5727 degrees C at (KEY POINT #4) t plus 4140.8628 s ignoring SP 4, with temperatures of 98.4093 and 95.8366 C, respectively, at Set # 2, where Pool P = 28.086 psia and T_outlet = 95.0966 C
Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 4631.3719 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.99936 C and a raw SP12 Reading of 102.7251 C.
Maximum Top-Lower delta T is 2.7721 degrees C at t plus 3907.5615 s, with temperatures of 96.4098 and 93.6377 C, respectively, at Set # 1, where Pool P = 26.4991 psia and T_outlet = 92.3452 C
Maximum Mid-Low delta T is 2.3395 degrees C at (KEY POINT #6) t plus 3943.0615 s ignoring SP 4, with temperatures of 95.6497 and 93.3102 C, respectively, at Set # 2, where Pool P = 26.7444 psia and T_outlet = 92.5376 C
Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 3943.0615 s with a Smoothed Mid-Axis Mid-Low Delta T of 0.79846 C and a raw SP12 Reading of 95.6497 C.
Maximum Top-Outlet delta T is 4.5212 degrees C at t plus 3799.0583 s, with temperatures of 95.0318 and 90.5106 C, respectively, at Set # 1, where Pool P = 25.818 psia
Maximum Mid-Outlet delta T is 3.4159 degrees C at t plus 3206.2514 s ignoring SP 4, with temperatures of 85.5874 and 82.1715 C, respectively, at Set # 2, where Pool P = 22.5307 psia
Maximum Lower-Outlet delta T is 5.0378 degrees C at (KEY POINT #8) t plus 2533.0399 s, with temperatures of 77.6333 and 72.5955 C, respectively, at Set # 1, where Pool P = 19.7508 psia
Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 3342.0522 s with a Smoothed Mid-Axis Low-Outlet Delta T of 1.6785 C and a raw SP12 Reading of 86.378 C.
Minimum SP Pressure is 15.0498 psia at t plus 6.0014 s
Maximum SP Pressure is 32.5412 psia at t plus 4710.3724 s
Beginning SP Pressure is 15.053 psia
Ending SP Pressure is 32.5391 psia
Time-Average SP Pressure is 20.7278 +/- 4.9594 psia
SP Levels are fully corrected and compensated
Pre-Start SP Level is 74.671 cm (cold) / 74.7459 cm (hot) at 14.7681 psia
Beginning Smoothed SP Level is 75.0613 cm (cold) / 75.2106 cm (hot) at 15.056 psia
Ending Smoothed SP Level is 82.5067 cm (cold) / 83.8763 cm (hot) at 32.5357 psia
Minimum Smoothed Cold SP Level is 75.0613 cm at t plus 0 s and 15.056 psia
Minimum Smoothed Hot SP Level is 75.2106 cm at t plus 0 s and 15.056 psia
Maximum Smoothed Cold SP Level is 82.5067 cm at t plus 4710.4724 s and 32.5357 psia
Maximum Smoothed Hot SP Level is 83.8763 cm at t plus 4710.4724 s and 32.5357 psia
SP 12 Temperature at the beginning is 40.3181 C, and at the end is 103.7826 C
At plume detection, the Mixing Number is 149.4012
The Mixing Number ranges from a minimum of 31.1574 at (KEY POINT #12) t plus 0 s to a maximum of 149.4012 at (KEY POINT #13) t plus 4710.4724 s; it had a mean value of 65.8746 +/- 32.9617 over the test period.
Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m2-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsurf Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2,

Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m3) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 31.1574): 47.54424134 0.040894
 0.00925 0.3937 0.7506133521 0.7521064616 1.024438211
 1 1 83.92839407 146048.7934 0.06968941165
 0.05879519799 0.06244633988 3.044993839e-006 0.06244633988 39.42664906
 127.628845 100.6049258 39.17344169 39.28004953 40.50803044
 38.04103763 4.178550113 4.217412545 2.079900522 0.6279028921
 0.6780050525 0.6780050525 4.391199227 1.741431674 0.03770177697
 992.4365854 957.9190884 0.6103121585 0.5665133976 0.0006598527259
 0.0002799582589 1.229000858e-005 1.331249756e-005 1530.352222
 1544.530942 472.5647139 490.677592 1.036269744 1.038071277
 1.075071277 0.0716165664 0.07065138186 2738.674818 2731.630843
 165.234021 421.6518015 2676.525757 256.4177805 2317.023017
 164.1759801 164.6199373 169.7542085 159.4497483

KEY POINT #2 (t plus 4710.4724 s with a Mixing Number of 149.4012): 52.79278682
 0.040894 0.00925 0.3937 0.8250667473 0.8387634285
 1.013521767 1 44.59055455 158688.6305
 0.05757629867 0.05433400504 0.06933997085 4.075365052e-006 0.06933997085
 106.8742062 136.9111331 123.1365496 106.4698188 105.7248547
 105.2810707 102.8122458 4.225607371 4.251889708 2.1926267
 0.6803649513 0.6841037185 0.6841037185 1.631205396 1.402661442
 0.04187210046 953.3509838 940.5564721 1.230267464 1.184015094
 0.0002626403455 0.0002256798681 1.306417533e-005 1.360468117e-005
 1538.28092 1516.25491 483.1526471 492.826399 2.192160864
 2.243256817 2.280256817 1.28958277 1.27183639 2742.100312
 2740.111995 448.2095102 517.1264666 2710.454327 68.91695641
 2224.973846 446.500846 443.3524884 441.4806741 431.0614571

KEY POINT #3 (t plus 4710.4724 s with a Mixing Number of 149.4012): 52.79278682
 0.040894 0.00925 0.3937 0.8250667473 0.8387634285
 1.013521767 1 44.59055455 158688.6305
 0.05757629867 0.05433400504 0.06933997085 4.075365052e-006 0.06933997085
 106.8742062 136.9111331 123.1365496 106.4698188 105.7248547
 105.2810707 102.8122458 4.225607371 4.251889708 2.1926267
 0.6803649513 0.6841037185 0.6841037185 1.631205396 1.402661442
 0.04187210046 953.3509838 940.5564721 1.230267464 1.184015094
 0.0002626403455 0.0002256798681 1.306417533e-005 1.360468117e-005
 1538.28092 1516.25491 483.1526471 492.826399 2.192160864
 2.243256817 2.280256817 1.28958277 1.27183639 2742.100312
 2740.111995 448.2095102 517.1264666 2710.454327 68.91695641
 2224.973846 446.500846 443.3524884 441.4806741 431.0614571

KEY POINT #4 (t plus 4140.8628 s with a Mixing Number of 118.4471): 52.11513321
 0.040894 0.00925 0.3937 0.8144559701 0.8260306021
 1.016158952 1 51.00796889 157222.63
 0.05892830093 0.0552861249 0.0684499159 3.205348664e-006 0.0684499159
 99.91473021 135.2083189 118.4195748 98.27768585 98.57437509
 96.9716582 95.26911076 4.216317618 4.243682128 2.164996565
 0.677776608 0.6833189652 0.6833189652 1.754345042 1.461666867
 0.0408767653 958.4544402 944.3741549 1.070370661 1.021753557
 0.0002820124429 0.000235358036 1.290157657e-005 1.355527673e-005
 1545.366108 1523.301601 481.0899033 492.7048239 1.889232339

1.936399458	1.973399458	1.011097587	0.9534113086	2741.887487
2739.285674	418.8116685	497.0687634	2703.629957	78.25709482
2244.818724	411.9110555	413.1601559	406.40951	399.2423864
KEY POINT #5 (t plus 4631.3719 s with a Mixing Number of 141.1264): 52.58302094				
0.040894	0.00925	0.3937	0.8242110077	0.8376323304
1.013894763	1	1	45.32355922	158136.6166
0.05786229243	0.05446704956	0.0690644567	3.787425311e-006	0.0690644567
105.4113601	136.6749286	122.4801908	105.350684	104.6201209
104.1289876	101.9570451	4.223560409	4.250714402	2.188643847
0.6798710961	0.6840097352	0.6840097352	1.655638935	1.410555943
0.04172935634	954.4428619	941.0934094	1.206931014	1.160233341
0.0002665099936	0.0002269816097	1.304153986e-005	1.35979263e-005	
1539.892751	1517.269182	482.870725	492.816656	2.147782884
2.198324342	2.235324342	1.226337153	1.223770151	2742.070133
2740.015908	442.0262975	514.3330018	2709.514382	72.30670434
2227.737131	441.7700309	438.6836294	436.612595	427.4496449
KEY POINT #6 (t plus 3943.0615 s with a Mixing Number of 106.6984): 51.89367419				
0.040894	0.00925	0.3937	0.8087494557	0.8194334824
1.017022921	1	1	53.37752382	156742.6625
0.05950351797	0.05559916443	0.06815904354	5.128113214e-006	0.06815904354
96.9188568	134.6550634	116.8584568	95.85216243	95.87126545
94.48388725	92.53087467	4.212637394	4.241086008	2.15635199
0.6764805712	0.6830029498	0.6830029498	1.813134486	1.482408596
0.04056262489	960.5847953	945.6165739	1.021318454	0.9722739989
0.000291159703	0.0002387335324	1.284780619e-005	1.353900641e-005	
1547.973324	1525.507972	480.3886419	492.6481364	1.796870921
1.843925686	1.880925686	0.9076257829	0.8729753024	2741.82175
2738.97259	406.1787011	490.4393639	2701.336659	84.26066277
2251.382386	401.6857853	401.7649424	395.9259475	387.7098416
KEY POINT #7 (t plus 3943.0615 s with a Mixing Number of 106.6984): 51.89367419				
0.040894	0.00925	0.3937	0.8087494557	0.8194334824
1.017022921	1	1	53.37752382	156742.6625
0.05950351797	0.05559916443	0.06815904354	5.128113214e-006	0.06815904354
96.9188568	134.6550634	116.8584568	95.85216243	95.87126545
94.48388725	92.53087467	4.212637394	4.241086008	2.15635199
0.6764805712	0.6830029498	0.6830029498	1.813134486	1.482408596
0.04056262489	960.5847953	945.6165739	1.021318454	0.9722739989
0.000291159703	0.0002387335324	1.284780619e-005	1.353900641e-005	
1547.973324	1525.507972	480.3886419	492.6481364	1.796870921
1.843925686	1.880925686	0.9076257829	0.8729753024	2741.82175
2738.97259	406.1787011	490.4393639	2701.336659	84.26066277
2251.382386	401.6857853	401.7649424	395.9259475	387.7098416
KEY POINT #8 (t plus 2533.0399 s with a Mixing Number of 56.4897): 50.86911311				
0.040894	0.00925	0.3937	0.7670491235	0.7727829526
1.022596251	1	1	71.29258427	154535.4238
0.06354688101	0.05746005749	0.06681334768	3.472584229e-007	0.06681334768
75.1998292	131.9270975	107.4673844	75.37922743	75.26905303
76.56243922	72.88556452	4.191609008	4.226679237	2.109310365
0.6636385136	0.6805003893	0.6805003893	2.379685076	1.621603114
0.03882299255	974.7498859	952.8670327	0.76315577	0.7135297173
0.000376764785	0.000261080032	1.252497593e-005	1.346125995e-005	
1557.883552	1537.405492	475.9813672	492.4799376	1.315982919
1.361739251	1.398739251	0.3891918089	0.3921183795	2742.819756
2737.737123	314.8928563	450.6455605	2687.19939	135.7527042
2292.174195	315.6448356	315.1816468	320.6065329	305.19943
KEY POINT #9 (t plus 4710.4724 s with a Mixing Number of 149.4012): 52.79278682				
0.040894	0.00925	0.3937	0.8250667473	0.8387634285
1.013521767	1	1	44.59055455	158688.6305
0.05757629867	0.05433400504	0.06933997085	4.075365052e-006	0.06933997085
106.8742062	136.9111331	123.1365496	106.4698188	105.7248547
105.2810707	102.8122458	4.225607371	4.251889708	2.1926267
0.6803649513	0.6841037185	0.6841037185	1.631205396	1.402661442
0.04187210046	953.3509838	940.5564721	1.230267464	1.184015094
0.0002626403455	0.0002256798681	1.306417533e-005	1.360468117e-005	
1538.28092	1516.25491	483.1526471	492.826399	2.192160864
2.243256817	2.280256817	1.28958277	1.27183639	2742.100312

2740.111995	448.2095102	517.1264666	2710.454327	68.91695641
2224.973846	446.500846	443.3524884	441.4806741	431.0614571
KEY POINT #10 (t plus 3342.0522 s with a Mixing Number of 77.2018): 51.91286615				
0.040894	0.00925	0.3937	0.7900475777	0.7983412379
1.019641495	1	1	61.74788683	157261.1676
0.06140255559	0.05649129865	0.06818425096	4.929869221e-006	0.06818425096
86.86907812	133.2701251	112.3804627	86.8016403	86.75533771
86.8464076	84.34237182	4.201680752	4.233961286	2.132885535
0.6713061609	0.6819392307	0.6819392307	2.040765808	1.545546272
0.03970184905	967.4257134	949.1218659	0.8906134961	0.8407837455
0.0003260549149	0.0002489320436	1.269371842e-005	1.349935766e-005	
1554.617513	1531.480109	478.3269277	492.5587395	1.552231557
1.599130461	1.636130461	0.6224009815	0.6207766505	2742.14691
2738.334109	363.8806394	471.4464167	2694.666738	107.5657773
2270.700494	363.5972894	363.4014172	363.7867907	353.272279
KEY POINT #11 (t plus 4710.4724 s with a Mixing Number of 149.4012): 52.79278682				
0.040894	0.00925	0.3937	0.8250667473	0.8387634285
1.013521767	1	1	44.59055455	158688.6305
0.05757629867	0.05433400504	0.06933997085	4.075365052e-006	0.06933997085
106.8742062	136.9111331	123.1365496	106.4698188	105.7248547
105.2810707	102.8122458	4.225607371	4.251889708	2.1926267
0.6803649513	0.6841037185	0.6841037185	1.631205396	1.402661442
0.04187210046	953.3509838	940.5564721	1.230267464	1.184015094
0.0002626403455	0.0002256798681	1.306417533e-005	1.360468117e-005	
1538.28092	1516.25491	483.1526471	492.826399	2.192160864
2.243256817	2.280256817	1.28958277	1.27183639	2742.100312
2740.111995	448.2095102	517.1264666	2710.454327	68.91695641
2224.973846	446.500846	443.3524884	441.4806741	431.0614571
KEY POINT #12 (t plus 0 s with a Mixing Number of 31.1574): 47.54424134 0.040894				
0.00925	0.3937	0.7506133521	0.7521064616	1.024438211
1	1	83.92839407	146048.7934	0.06968941165
0.05879519799	0.06244633988	3.044993839e-006	0.06244633988	39.42664906
127.628845	100.6049258	39.17344169	39.28004953	40.50803044
38.04103763	4.178550113	4.217412545	2.079900522	0.6279028921
0.6780050525	0.6780050525	4.391199227	1.741431674	0.03770177697
992.4365854	957.9190884	0.6103121585	0.5665133976	0.0006598572759
0.0002799582589	1.229000858e-005	1.331249756e-005	1530.352222	
1544.530942	472.5647139	490.677592	1.036269744	1.038071277
1.075071277	0.0716165664	0.07065138186	2738.674818	2731.630843
165.234021	421.6518015	2676.525757	256.4177805	2317.023017
164.1759801	164.6199373	169.7542085	159.4497483	
KEY POINT #13 (t plus 4710.4724 s with a Mixing Number of 149.4012): 52.79278682				
0.040894	0.00925	0.3937	0.8250667473	0.8387634285
1.013521767	1	1	44.59055455	158688.6305
0.05757629867	0.05433400504	0.06933997085	4.075365052e-006	0.06933997085
106.8742062	136.9111331	123.1365496	106.4698188	105.7248547
105.2810707	102.8122458	4.225607371	4.251889708	2.1926267
0.6803649513	0.6841037185	0.6841037185	1.631205396	1.402661442
0.04187210046	953.3509838	940.5564721	1.230267464	1.184015094
0.0002626403455	0.0002256798681	1.306417533e-005	1.360468117e-005	
1538.28092	1516.25491	483.1526471	492.826399	2.192160864
2.243256817	2.280256817	1.28958277	1.27183639	2742.100312
2740.111995	448.2095102	517.1264666	2710.454327	68.91695641
2224.973846	446.500846	443.3524884	441.4806741	431.0614571
KEY POINT #14 (t plus 3541.4546 s with a Mixing Number of 82.059): 51.94271667				
0.040894	0.00925	0.3937	0.796075022	0.8050500203
1.018812688	1	1	58.98946833	157209.2581
0.06101065933	0.05621069089	0.06822345773	4.693175845e-006	0.06822345773
88.96381937	133.6961586	113.7936472	89.80090978	89.74437531
89.59501424	87.45537811	4.203782956	4.23615876	2.140081854
0.6724930684	0.682300243	0.682300243	1.989045894	1.525016272
0.03996716632	966.0407231	948.0250553	0.9303054679	0.8806027813
0.0003181942528	0.0002456279455	1.274231976e-005	1.351157993e-005	
1553.515953	1529.653232	478.985529	492.5890744	1.626285214
1.673286091	1.710286091	0.6746536415	0.6965335951	2742.017752
2738.537994	372.6900333	477.4366641	2696.786065	104.7466308
2264.581088	376.2093445	375.9703219	375.3450412	366.3549461

End

D.6 TEST #6 - T06_RCIC_1ATM_107KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T06_RCIC_1ATM_107kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1599.5375 s, and ending (KEY POINT #11) at t plus 8065.6533 s, for a time period of 6466.1158 s.
Original Data Record Time: 9753.6069 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 2493.7446 s, T_bulk = 63.412 C and T_out = 60.8315 C
Stratification Beginning SP12 Temperature = 63.1484 C
Stratification Beginning Pressure = 15.1555 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 5339.3954 s, T_bulk = 89.5236 C and T_out = 69.9724 C
Stratification Ending SP12 Temperature = 89.4619 C
Stratification Ending Pressure = 15.181 psia
Plume detected! Setting t_plume (KEY POINT #2) to 1918.9338 s.
At t = 1918.9338 s, the pool pressure is 15.1571 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 58.6399, 58.5941, 60.5965, 58.3806, and 55.4551 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 7.8818 +/- 2.0516 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 7.2439 +/- 1.7663 C.
Minimum Steam Quality: 0.99162 at t plus 94.3014 s
Maximum Steam Quality: 1.0031 at t plus 5586.8996 s
Time-Averaged Steam Quality: 0.99951 +/- 0.0015948
Minimum Turbine Outlet Steam Quality: 1.0143 at t plus 94.3014 s
Maximum Turbine Outlet Steam Quality: 1.0263 at t plus 5586.8996 s
Time-Averaged Turbine Outlet Steam Quality: 1.0222 +/- 0.0018929
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 6376.1137 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.96096 degrees/min at t plus 3451.7614 s and 0.30004 degrees/min at t plus 3205.6574 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.75056 degrees/min at t plus 3658.5653 s and 0.42427 degrees/min at t plus 5030.4897 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.39309 degrees/min at t plus 3403.2597 s and -0.23998 degrees/min at t plus 3209.1566 s, respectively
Max and min smoothed lower level changerates: 1.4287 degrees/min at t plus 4462.3792 s and 0.060317 degrees/min at t plus 3534.5632 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.65558 degrees/min at t plus 3535.8632 s and -0.84751 degrees/min at t plus 4462.5802 s, respectively
Max and min smoothed outlet level changerates: 4.7683 degrees/min at t plus 5506.398 s and -0.05232 degrees/min at t plus 4351.1779 s, respectively
Max and min smoothed lower-outlet level changerate differences: 1.4138 degrees/min at t plus 4461.9792 s and -4.2263 degrees/min at t plus 5510.7972 s, respectively
Max and min smoothed hot (SP8) level changerates: 1.2455 degrees/min at t plus 2443.2437 s and 0.066375 degrees/min at t plus 6093.6085 s, respectively
Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.72779 degrees/min at t plus 2443.2437 s and -0.4286 degrees/min at t plus 6074.4074 s, respectively
The mean steam flow rate was 44.9518 +/- 1.3555 g/s
The mean feedwater flow rate was 43.7802 +/- 1.868 g/s
The mean water injection to steam flow rate was 0.01029 +/- 0.039484 g/s
Mean Smoothed Condensing Region SP8-SP9 delta T is 8.7257 +/- 0.72648 C over the Stratification Period, beginning at 6.0436 C and ending at 9.6791 C
Mean Smoothed SP8-Upper Pool delta T is 7.9596 +/- 0.66496 C over the Stratification Period, beginning at 5.4626 C and ending at 9.0724 C
The stratification period begins and ends with Smoothed SP8 readings of 69.6529 and 99.7966 C, respectively
The stratification period begins and ends with condensing flows of 0.63452 and 2.1519 kg/s, respectively.
The stratification period begins and ends with condensing+cooling flows of 4.261 and 2.6272 kg/s, respectively.

The stratification period had a mean sparger steam enthalpy of 2729.5634 +/- 0.65645 kJ/kg.

At plume detection, the condensing and condensing+cooling flows are 0.55711 and 12.9775 kg/s, respectively

The plume period had a mean steam enthalpy of 2732.1083 +/- 1.025 kJ/kg.

Maximum Smoothed Top-Mid delta T is 1.5269 degrees C at t plus 3550.3621 s with T_upper = 74.565 C and T_mid = 73.0381 C

At t plus 3550.3621 s, Smoothed SP8-SP9 is 9.4824 C and Smoothed SP8-Top is 7.9555 C, where Smoothed SP8 is 82.5205 C and Pool P = 15.1573 psia

Maximum Smoothed Top-Lower delta T is 6.6943 degrees C at t plus 4232.5961 s with T_upper = 81.3674 C and T_low = 74.6731 C

At t plus 4232.5961 s, Smoothed SP8-SP9 is 8.5001 C and Smoothed SP8-Top is 7.7335 C, where Smoothed SP8 is 89.101 C and Pool P = 15.1691 psia

Maximum Smoothed Mid-Lower delta T is 5.9296 degrees C at t plus 4232.1781 s with T_mid = 80.5969 C and T_low = 74.6673 C

At t plus 4232.1781 s, Smoothed SP8-SP9 is 8.4809 C and Smoothed SP8-Top is 7.7178 C, where Smoothed SP8 is 89.0778 C and Pool P = 15.1673 psia

Maximum Smoothed Top-Outlet delta T is 20.766 degrees C at t plus 5289.9936 s with T_upper = 90.436 C and T_out = 69.67 C

At t plus 5289.9936 s, Smoothed SP8-SP9 is 9.8309 C and Smoothed SP8-Top is 9.0926 C, where Smoothed SP8 is 99.5286 C and Pool P = 15.1808 psia

Maximum Smoothed Mid-Outlet delta T is 20.2587 degrees C at t plus 5395.0956 s with T_mid = 90.8427 C and T_out = 70.5839 C

At t plus 5395.0956 s, Smoothed SP8-SP9 is 9.375 C and Smoothed SP8-Top is 8.9039 C, where Smoothed SP8 is 100.2176 C and Pool P = 15.1956 psia

Maximum Smoothed Lower-Outlet delta T is 20.6483 degrees C at t plus 5395.5956 s with T_low = 91.2408 C and T_out = 70.5926 C

At t plus 5395.5956 s, Smoothed SP8-SP9 is 9.363 C and Smoothed SP8-Top is 8.893 C, where Smoothed SP8 is 100.2128 C and Pool P = 15.195 psia

Maximum Smoothed Condensing Region SP8-SP9 delta T is 10.4338 degrees C at (KEY POINT #14) t plus 3127.2559 s with T_SP8 = 79.4793 C and T_SP9 = 69.0454 C and Pool P = 15.1563 psia

Maximum Smoothed Condensing Region SP8-Upper delta T is 9.5321 degrees C at t plus 3136.3554 s with T_SP8 = 79.4261 C and T_upper = 69.8939 C and Pool P = 15.1555 psia

Maximum Top-Mid delta T is 2.3688 degrees C at (KEY POINT #4) t plus 3569.0641 s ignoring SP 4, with temperatures of 75.3338 and 72.965 C, respectively, at Set # 2, where Pool P = 15.1694 psia and T_outlet = 67.1666 C

Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 3966.5699 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.99998 C and a raw SP12 Reading of 77.8254 C.

Maximum Top-Lower delta T is 8.9937 degrees C at t plus 4514.1802 s, with temperatures of 84.616 and 75.6223 C, respectively, at Set # 1, where Pool P = 15.1688 psia and T_outlet = 69.1517 C

Maximum Mid-Low delta T is 5.8648 degrees C at (KEY POINT #6) t plus 4193.1748 s ignoring SP 4, with temperatures of 80.2104 and 74.3457 C, respectively, at Set # 2, where Pool P = 15.17 psia and T_outlet = 69.1945 C

Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 4695.5836 s with a Smoothed Mid-Axis Mid-Low Delta T of 1.9542 C and a raw SP12 Reading of 85.2056 C.

Maximum Top-Outlet delta T is 21.1036 degrees C at t plus 5315.694 s, with temperatures of 90.8701 and 69.7665 C, respectively, at Set # 1, where Pool P = 15.1828 psia

Maximum Mid-Outlet delta T is 19.7169 degrees C at t plus 5322.3954 s ignoring SP 4, with temperatures of 89.557 and 69.84 C, respectively, at Set # 2, where Pool P = 15.1831 psia

Maximum Lower-Outlet delta T is 21.028 degrees C at (KEY POINT #8) t plus 5257.9937 s, with temperatures of 90.5616 and 69.5336 C, respectively, at Set # 1, where Pool P = 15.1821 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 5539.1978 s with a Smoothed Mid-Axis Low-Outlet Delta T of 7.0017 C and a raw SP12 Reading of 90.9571 C.

Minimum SP Pressure is 14.7959 psia at t plus 6.2004 s

Maximum SP Pressure is 15.6309 psia at t plus 6465.0158 s

Beginning SP Pressure is 14.8049 psia

Ending SP Pressure is 15.6182 psia

Time-Average SP Pressure is 15.1743 +/- 0.10582 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 74.9717 cm (cold) / 75.1028 cm (hot) at 14.5875 psia

Beginning Smoothed SP Level is 75.3484 cm (cold) / 75.5116 cm (hot) at 14.8063 psia

Ending Smoothed SP Level is 75.3997 cm (cold) / 76.3364 cm (hot) at 15.6264 psia

Minimum Smoothed Cold SP Level is 75.1008 cm at t plus 5040.0893 s and 15.1765 psia
 Minimum Smoothed Hot SP Level is 75.5034 cm at t plus 70.301 s and 14.8437 psia
 Maximum Smoothed Cold SP Level is 75.4637 cm at t plus 602.6105 s and 15.1555 psia
 Maximum Smoothed Hot SP Level is 76.3364 cm at t plus 6466.1158 s and 15.6264 psia
 SP 12 Temperature at the beginning is 39.8306 C, and at the end is 99.2528 C
 At plume detection, the Mixing Number is 42.0583

The Mixing Number ranges from a minimum of 32.6675 at (KEY POINT #12) t plus 0 s to a maximum of 339.06 at (KEY POINT #13) t plus 6466.1158 s; it had a mean value of 77.987 +/- 59.9332 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 32.6675): 33.61870469 0.040894
 0.00925 0.3937 0.7534840865 0.7551155468 1.016568729
 1 1 55.13415808 105535.6918 0.06948997517
 0.05850248938 0.04415603236 1.30037419e-005 0.04415603236 40.65352911
 120.2664974 102.1188035 41.08179104 40.5275699 40.42258324
 38.16358448 4.178536186 4.219367887 2.086054846 0.6294616587
 0.6786048255 0.6786048255 4.280823669 1.713513567 0.0379389945
 991.970851 956.8227373 0.6416720905 0.6099413941 0.0006448704157
 0.000275585966 1.234175832e-005 1.302690385e-005 1532.432611
 1543.077992 473.3321193 485.7047149 1.09330231 1.020855477
 1.057855477 0.07645624698 0.07821080753 2719.23734 2716.197565
 170.3590631 428.0421877 2678.90365 257.6831246 2291.195152
 172.1485713 169.8312334 169.3956408 159.9602884

KEY POINT #2 (t plus 1918.9338 s with a Mixing Number of 42.0583): 33.45125815
 0.040894 0.00925 0.3937 0.7537078809 0.7570505922
 1.020980174 1 1 53.8606921 103272.4104
 0.06648122034 0.05831841176 0.04393610197 8.724162092e-006 0.04393610197
 58.59412055 126.054289 103.0681018 60.59654989 58.63986414
 58.38062962 55.4550783 4.182169612 4.220619497 2.090007905
 0.6494597851 0.678966605 0.678966605 3.068143935 1.696451731
 0.03809060441 983.93085 956.1299873 0.6619977253 0.6211932874
 0.0004764598966 0.0002729063999 1.237423471e-005 1.324609104e-005
 1552.979448 1542.13208 473.8094299 489.333797 1.130371167
 1.04499655 1.08199655 0.1868339728 0.2050301651 2730.459643
 2727.558669 245.3484843 432.0509805 2680.388163 186.7024962
 2298.408662 253.7238059 245.5383592 244.4571567 232.2276902

KEY POINT #3 (t plus 2493.7446 s with a Mixing Number of 45.9298): 33.68444255
 0.040894 0.00925 0.3937 0.7530948631 0.7569987348
 1.02141015 1 1 54.73122245 103909.6369
 0.0560982779 0.05836399032 0.04424237487 1.154103052e-005 0.04424237487
 63.60934281 126.313333 102.8332465 69.65293169 64.1903773
 63.49384354 60.94127534 4.184431795 4.220308015 2.089023095
 0.6541578791 0.6788781255 0.6788781255 2.827767606 1.700641516
 0.03805288878 981.3195405 956.3017498 0.6569210442 0.6156125871

0.0004420687324	0.0002735649437	1.236619828e-005	1.325662984e-005	
1555.740417	1542.368578	473.6916256	489.534141	1.121105112
1.044972593	1.081972593	0.2352397427	0.3073525482	2731.167499
2728.171993	266.3284342	431.0590927	2680.021373	164.7306585
2300.108407	291.6273889	268.7584065	265.8466366	255.1710969
KEY POINT #4 (t plus 3569.0641 s with a Mixing Number of 56.7012): 34.85513898				
0.040894	0.00925	0.3937	0.7521688828	0.7574785317
1.022208004	1	1	57.09371824	107291.888
0.06389554859	0.05839787366	0.04578001024	1.043834163e-005	0.04578001024
73.26725229	127.0386625	102.6585705	82.15160653	74.69531829
72.01815678	67.07823504	4.190275291	4.22007713	2.088293553
0.6621755194	0.6788118816	0.6788118816	2.445683516	1.703770991
0.03802492611	975.889492	956.4293394	0.6531658099	0.6106291096
0.0003864833787	0.0002740566004	1.236022187e-005	1.328493775e-005	
1557.870333	1542.543421	473.6038871	490.0258855	1.114254166
1.045374669	1.082374669	0.3588144316	0.5169964432	2732.963342
2729.703649	306.7679731	430.3214161	2679.748366	123.553443
2302.641926	344.0261592	312.7513202	301.5359269	280.8521765
KEY POINT #5 (t plus 3966.5699 s with a Mixing Number of 64.8484): 34.96515093				
0.040894	0.00925	0.3937	0.7519153274	0.7577651514
1.022146017	1	1	57.23322137	107647.9383
0.06305193824	0.05839493091	0.04592450394	9.267380662e-006	0.04592450394
77.92571556	126.9837462	102.6737438	86.57575871	78.77495782
73.44954442	68.50865109	4.19378925	4.22009716	2.088356827
0.6655743347	0.6788176507	0.6788176507	2.29205247	1.703498696
0.03802735211	973.0908454	956.4182616	0.6534913156	0.6110473239
0.0003637596471	0.0002740138293	1.236074098e-005	1.328278929e-005	
1557.511258	1542.528269	473.6115126	489.9884393	1.114847902
1.045904264	1.082904264	0.4357009338	0.6153617654	2732.862684
2729.587042	326.2962707	430.3854931	2679.772088	104.0892224
2302.477191	362.6050211	329.8567486	307.5333403	286.8409587
KEY POINT #6 (t plus 4193.1748 s with a Mixing Number of 70.0039): 34.99259878				
0.040894	0.00925	0.3937	0.7517180741	0.7578512293
1.022360935	1	1	57.3155004	107657.5204
0.06263106329	0.05839467626	0.04596055494	1.215585658e-005	0.04596055494
80.22797372	127.2242593	102.6750568	88.67529704	80.86306193
74.38103294	69.17260048	4.195692773	4.220098893	2.088362303
0.6671445102	0.6788181497	0.6788181497	2.222279991	1.703475138
0.03802756206	971.6662224	956.417303	0.6535194885	0.6106873975
0.0003533580689	0.0002740101288	1.236078591e-005	1.329203319e-005	
1557.021773	1542.526957	473.6121725	490.1430529	1.114899291
1.045870676	1.082870676	0.478541111	0.6672463991	2733.357516
2730.07245	335.9536255	430.3910378	2679.77414	94.43741239
2302.966478	371.4284606	338.6170838	311.4369582	289.6211384
KEY POINT #7 (t plus 4695.5836 s with a Mixing Number of 85.5049): 35.0999542				
0.040894	0.00925	0.3937	0.7513841272	0.7582466336
1.022493344	1	1	57.49639955	107939.7222
0.06171630615	0.05839321068	0.04610155947	9.817189291e-006	0.04610155947
85.18389499	127.3787229	102.6826134	93.78764876	85.98766825
83.05586048	69.38512022	4.20016547	4.22010887	2.088393822
0.6702831646	0.6788210217	0.6788210217	2.08432122	1.703339566
0.03802877049	968.5087162	956.4117857	0.6536816508	0.6106022099
0.0003326262818	0.000273988833	1.236104444e-005	1.329795462e-005	
1555.298702	1542.519408	473.6159698	490.241374	1.115195091
1.046142706	1.083142706	0.5828593551	0.8090277951	2733.687485
2730.381649	356.7580465	430.4229494	2679.785954	73.66490296
2303.264536	392.932797	360.1330076	347.8234947	290.5111107
KEY POINT #8 (t plus 5257.9937 s with a Mixing Number of 107.9094): 35.2597335				
0.040894	0.00925	0.3937	0.7510906657	0.7585561098
1.022469635	1	1	57.69857671	108431.0911
0.06090789267	0.05838729727	0.04631141943	1.203898719e-005	0.04631141943
89.51128175	127.3806203	102.7131017	98.94114857	90.24512486
89.57608434	69.60450552	4.204491708	4.220149137	2.088521038
0.6727588085	0.6788326019	0.6788326019	1.976055595	1.702792796
0.03803364752	965.6525158	956.3895225	0.6543362554	0.6112611702
0.0003161877582	0.0002739029419	1.236208754e-005	1.32979529e-005	
1553.077594	1542.488934	473.6312888	490.2384031	1.116389203

1.046972782	1.083972782	0.688897302	0.9764525467	2733.703283
2730.374157	374.9430744	430.551703	2679.833613	55.60862864
2303.15158	414.6403209	378.0274807	375.216933	291.4299087
KEY POINT #9 (t plus 5339.3954 s with a Mixing Number of 112.1973): 35.25567187				
0.040894	0.00925	0.3937	0.7511954324	0.75873113
1.02250456	1	1	57.67630645	108402.9345
0.06079392943	0.0583848113	0.04630608473	1.437555777e-005	0.04630608473
90.11750747	127.4314054	102.7259183	99.79659508	90.72415477
90.09711114	69.97792266	4.20512923	4.220166071	2.08857454
0.6730861886	0.6788374666	0.6788374666	1.961713226	1.70256305
0.0380356984	965.24515	956.3801624	0.6546115947	0.6114576163
0.0003139979786	0.0002738668498	1.236252604e-005	1.32998747e-005	
1552.714991	1542.476115	473.6377276	490.2693031	1.116891495
1.047370107	1.084370107	0.7049615784	1.006840251	2733.798535
2730.471978	377.4921695	430.6058283	2679.853647	53.11365884
2303.192706	418.2467698	380.0420831	377.4077928	292.9937872
KEY POINT #10 (t plus 5539.1978 s with a Mixing Number of 129.8136): 35.2706178				
0.040894	0.00925	0.3937	0.7513709795	0.7591961707
1.022353578	1	1	57.57518572	108487.8471
0.06041295463	0.05837495693	0.04632571526	1.187598661e-005	0.04632571526
92.13743023	127.3104675	102.776719	100.9247491	92.50645738
92.55809907	83.96140689	4.207309496	4.220233225	2.088786734
0.6741428818	0.6788567289	0.6788567289	1.915293874	1.701653012
0.03804383142	963.8751112	956.3430545	0.6557038816	0.6127580707
0.0003068901237	0.0002737238764	1.236426416e-005	1.329509879e-005	
1551.417776	1542.425258	473.6632435	490.1845114	1.118884257
1.049351473	1.086351473	0.7607584011	1.048108636	2733.523662
2730.20876	385.988547	430.8203662	2679.933043	44.83181918
2302.703296	423.0044448	387.539928	387.7599112	351.629311
KEY POINT #11 (t plus 6466.1158 s with a Mixing Number of 339.06): 35.97569466				
0.040894	0.00925	0.3937	0.7539972924	0.7633644226
1.022374924	1	1	57.3638417	110452.1493
0.05894224473	0.05823659944	0.04725178892	1.136963162e-005	0.04725178892
99.84236027	127.9957525	103.4893393	103.0199205	99.91495031
99.92173244	96.34699752	4.216424056	4.221181203	2.091785599
0.6776988425	0.679123618	0.679123618	1.755841693	1.688987857
0.03815859551	958.4731683	955.8212934	0.6711833089	0.6273002295
0.0002822135219	0.0002717323632	1.238865181e-005	1.331970511e-005	
1545.256895	1541.703826	474.0202583	490.5264999	1.147149309
1.077405201	1.114405201	1.008487765	1.128465065	2734.617122
2731.326512	418.441991	433.8302292	2681.045248	15.38823823
2300.786893	2680.500638	418.7467874	418.7780137	403.7164348
KEY POINT #12 (t plus 0 s with a Mixing Number of 32.6675): 33.61870469 0.040894				
0.00925	0.3937	0.7534840865	0.7551155468	1.016568729
1	1	55.13415808	105535.6918	0.06948997517
0.05850248938	0.04415603236	1.30037419e-005	0.04415603236	40.65352911
120.2664974	102.1188035	41.08179104	40.5275699	40.42258324
38.16358448	4.178536186	4.219367887	2.086054846	0.6294616587
0.6786048255	0.6786048255	4.280823669	1.713513567	0.0379389945
991.970851	956.8227373	0.6416720905	0.6099413941	0.0006448704157
0.000275585966	1.234175832e-005	1.302690385e-005	1532.432611	
1543.077992	473.3321193	485.7047149	1.09330231	1.020855477
1.057855477	0.07645624698	0.07821080753	2719.23734	2716.197565
170.3590631	428.0421877	2678.90365	257.6831246	2291.195152
172.1485713	169.8312334	169.3956408	159.9602884	
KEY POINT #13 (t plus 6466.1158 s with a Mixing Number of 339.06): 35.97569466				
0.040894	0.00925	0.3937	0.7539972924	0.7633644226
1.022374924	1	1	57.3638417	110452.1493
0.05894224473	0.05823659944	0.04725178892	1.136963162e-005	0.04725178892
99.84236027	127.9957525	103.4893393	103.0199205	99.91495031
99.92173244	96.34699752	4.216424056	4.221181203	2.091785599
0.6776988425	0.679123618	0.679123618	1.755841693	1.688987857
0.03815859551	958.4731683	955.8212934	0.6711833089	0.6273002295
0.0002822135219	0.0002717323632	1.238865181e-005	1.331970511e-005	
1545.256895	1541.703826	474.0202583	490.5264999	1.147149309
1.077405201	1.114405201	1.008487765	1.128465065	2734.617122

2731.326512	418.441991	433.8302292	2681.045248	15.38823823
2300.786893	2680.500638	418.7467874	418.7780137	403.7164348
KEY POINT #14 (t plus 3127.2559 s with a Mixing Number of 51.324): 34.21651105				
0.040894	0.00925	0.3937	0.7525615571	0.7572260426
1.021783813	1	1	55.96267997	105468.0082
0.06465073079	0.05839631101	0.04494121303	1.022471405e-005	0.04494121303
69.04542817	126.5739472	102.6666278	79.4792623	69.96616991
69.900613	64.41381573	4.187481144	4.220087766	2.08832715
0.6588343493	0.6788149454	0.6788149454	2.601114413	1.703626386
0.03802621429	978.3262467	956.423457	0.6533386437	0.611555697
0.0004092444748	0.0002740338866	1.236049753e-005	1.32670563e-005	
1557.433417	1542.535375	473.6079365	489.7254432	1.114569419
1.044979033	1.081979033	0.2993478644	0.4642375266	2731.893413
2728.761592	289.0833655	430.3554423	2679.760963	141.2720768
2301.537971	332.8124276	292.937828	292.6661358	269.7000898

End

D.7 TEST #7 -

T07_RCIC_040GPM_1ATM_107KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T07_RCIC_040GPM_1ATM_107kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1060.8267 s, and ending (KEY POINT #11) at t plus 6992.932 s, for a time period of 5932.1053 s.
Original Data Record Time: 9933.5122 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 2306.6409 s, T_bulk = 62.4304 C and T_out = 59.8726 C
Stratification Beginning SP12 Temperature = 62.3943 C
Stratification Beginning Pressure = 15.2119 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 5115.3906 s, T_bulk = 87.477 C and T_out = 75.872 C
Stratification Ending SP12 Temperature = 87.3474 C
Stratification Ending Pressure = 15.2371 psia
Plume detected! Setting t_plume (KEY POINT #2) to 1577.3292 s.
At t = 1577.3292 s, the pool pressure is 15.2115 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 55.7306, 55.8196, 57.8205, 55.5877, and 53.5748 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 7.5076 +/- 1.9013 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 7.0083 +/- 1.6631 C.
Minimum Steam Quality: 0.51464 at t plus 430.4086 s
Maximum Steam Quality: 0.69599 at t plus 5886.9037 s
Time-Averaged Steam Quality: 0.5947 +/- 0.028316
Minimum Turbine Outlet Steam Quality: 0.56058 at t plus 430.4086 s
Maximum Turbine Outlet Steam Quality: 0.73594 at t plus 5886.9037 s
Time-Averaged Turbine Outlet Steam Quality: 0.63837 +/- 0.027843
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 5842.1031 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.76703 degrees/min at t plus 2.9012 s and 0.35867 degrees/min at t plus 5572.4977 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.74181 degrees/min at t plus 0 s and 0.4422 degrees/min at t plus 5008.5895 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.1515 degrees/min at t plus 4918.4873 s and -0.32795 degrees/min at t plus 5520.8978 s, respectively
Max and min smoothed lower level changerates: 1.0368 degrees/min at t plus 5185.4916 s and 0.21497 degrees/min at t plus 3813.4911 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.41708 degrees/min at t plus 3813.4911 s and -0.54314 degrees/min at t plus 5185.4916 s, respectively
Max and min smoothed outlet level changerates: 3.003 degrees/min at t plus 5245.093 s and 0.044062 degrees/min at t plus 4669.0831 s, respectively

Max and min smoothed lower-outlet level changerate differences: 0.79912 degrees/min at t plus 4664.1818 s and -2.0592 degrees/min at t plus 5238.8166 s, respectively
 Max and min smoothed hot (SP8) level changerates: 1.0569 degrees/min at t plus 2182.5398 s and 0.19047 degrees/min at t plus 5801.6018 s, respectively
 Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.56343 degrees/min at t plus 2182.5398 s and -0.44703 degrees/min at t plus 5501.0976 s, respectively
 The mean steam flow rate was 45.4318 +/- 2.288 g/s
 The mean feedwater flow rate was 43.9783 +/- 6.5187 g/s
 The mean water injection to steam flow rate was 24.4514 +/- 1.938 g/s
 Mean Smoothed Condensing Region SP8-SP9 delta T is 8.398 +/- 0.5925 C over the Stratification Period, beginning at 6.4057 C and ending at 9.6157 C
 Mean Smoothed SP8-Upper Pool delta T is 7.7858 +/- 0.49303 C over the Stratification Period, beginning at 6.3481 C and ending at 8.6376 C
 The stratification period begins and ends with Smoothed SP8 readings of 68.5801 and 97.0486 C, respectively
 The stratification period begins and ends with condensing flows of 0.58206 and 1.7117 kg/s, respectively.
 The stratification period begins and ends with condensing+cooling flows of 3.9852 and 2.6253 kg/s, respectively.
 The stratification period had a mean sparger steam enthalpy of 1853.8155 +/- 31.3013 kJ/kg.
 At plume detection, the condensing and condensing+cooling flows are 0.49165 and 12.8538 kg/s, respectively
 The plume period had a mean steam enthalpy of 1855.171 +/- 28.7074 kJ/kg.
 Maximum Smoothed Top-Mid delta T is 1.6167 degrees C at t plus 5399.2958 s with T_upper = 91.4565 C and T_mid = 89.8397 C
 At t plus 5399.2958 s, Smoothed SP8-SP9 is 9.6572 C and Smoothed SP8-Top is 8.0405 C, where Smoothed SP8 is 99.4969 C and Pool P = 15.2537 psia
 Maximum Smoothed Top-Lower delta T is 3.516 degrees C at t plus 4330.1777 s with T_upper = 81.6498 C and T_low = 78.1338 C
 At t plus 4330.1777 s, Smoothed SP8-SP9 is 8.4271 C and Smoothed SP8-Top is 7.6149 C, where Smoothed SP8 is 89.2647 C and Pool P = 15.2228 psia
 Maximum Smoothed Mid-Lower delta T is 2.8565 degrees C at t plus 4493.78 s with T_mid = 82.3186 C and T_low = 79.4621 C
 At t plus 4493.78 s, Smoothed SP8-SP9 is 8.3456 C and Smoothed SP8-Top is 7.8892 C, where Smoothed SP8 is 90.6643 C and Pool P = 15.2244 psia
 Maximum Smoothed Top-Outlet delta T is 12.7765 degrees C at t plus 5041.0883 s with T_upper = 87.993 C and T_out = 75.2165 C
 At t plus 5041.0883 s, Smoothed SP8-SP9 is 9.5834 C and Smoothed SP8-Top is 8.5166 C, where Smoothed SP8 is 96.5096 C and Pool P = 15.2369 psia
 Maximum Smoothed Mid-Outlet delta T is 11.794 degrees C at t plus 5004.2892 s with T_mid = 86.5799 C and T_out = 74.7859 C
 At t plus 5004.2892 s, Smoothed SP8-SP9 is 9.6996 C and Smoothed SP8-Top is 8.8064 C, where Smoothed SP8 is 96.2795 C and Pool P = 15.2373 psia
 Maximum Smoothed Lower-Outlet delta T is 11.5539 degrees C at t plus 5003.4892 s with T_low = 86.3334 C and T_out = 74.7795 C
 At t plus 5003.4892 s, Smoothed SP8-SP9 is 9.7073 C and Smoothed SP8-Top is 8.8108 C, where Smoothed SP8 is 96.2799 C and Pool P = 15.2359 psia
 Maximum Smoothed Condensing Region SP8-SP9 delta T is 9.827 degrees C at (KEY POINT #14) t plus 5224.0168 s with T_SP8 = 98.1009 C and T_SP9 = 88.2739 C and Pool P = 15.2371 psia
 Maximum Smoothed Condensing Region SP8-Upper delta T is 9.0174 degrees C at t plus 4980.2878 s with T_SP8 = 96.188 C and T_upper = 87.1706 C and Pool P = 15.2362 psia
 Maximum Top-Mid delta T is 1.9252 degrees C at (KEY POINT #4) t plus 2874.8504 s ignoring SP 4, with temperatures of 68.4544 and 66.5292 C, respectively, at Set # 2, where Pool P = 15.2104 psia and T_outlet = 63.9168 C
 Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 2899.0508 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.99986 C and a raw SP12 Reading of 66.8159 C.
 Maximum Top-Lower delta T is 5.4951 degrees C at t plus 4646.0817 s, with temperatures of 83.8844 and 78.3893 C, respectively, at Set # 1, where Pool P = 15.2234 psia and T_outlet = 73.991 C
 Maximum Mid-Low delta T is 3.3858 degrees C at (KEY POINT #6) t plus 4256.1744 s ignoring SP 4, with temperatures of 80.0133 and 76.6275 C, respectively, at Set # 3, where Pool P = 15.2232 psia and T_outlet = 72.7493 C

Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 4734.0838 s with a Smoothed Mid-Axis Mid-Low Delta T of 1.1282 C and a raw SP12 Reading of 84.3611 C.

Maximum Top-Outlet delta T is 13.3329 degrees C at t plus 4994.3887 s, with temperatures of 87.8401 and 74.5072 C, respectively, at Set # 1, where Pool P = 15.2372 psia

Maximum Mid-Outlet delta T is 12.0255 degrees C at t plus 4994.3887 s ignoring SP 4, with temperatures of 86.5327 and 74.5072 C, respectively, at Set # 2, where Pool P = 15.2372 psia

Maximum Lower-Outlet delta T is 13.2484 degrees C at (KEY POINT #8) t plus 5026.4885 s, with temperatures of 88.1312 and 74.8828 C, respectively, at Set # 1, where Pool P = 15.2383 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 5271.0925 s with a Smoothed Mid-Axis Low-Outlet Delta T of 4.4094 C and a raw SP12 Reading of 88.5184 C.

Minimum SP Pressure is 14.6906 psia at t plus 6.2004 s

Maximum SP Pressure is 15.3891 psia at t plus 5929.5041 s

Beginning SP Pressure is 14.697 psia

Ending SP Pressure is 15.386 psia

Time-Average SP Pressure is 15.1885 +/- 0.11567 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 75.9557 cm (cold) / 76.0986 cm (hot) at 14.588 psia

Beginning Smoothed SP Level is 76.2437 cm (cold) / 76.4121 cm (hot) at 14.6922 psia

Ending Smoothed SP Level is 76.4278 cm (cold) / 77.3165 cm (hot) at 15.3713 psia

Minimum Smoothed Cold SP Level is 76.2437 cm at t plus 0 s and 14.6922 psia

Minimum Smoothed Hot SP Level is 76.4121 cm at t plus 0 s and 14.6922 psia

Maximum Smoothed Cold SP Level is 76.7899 cm at t plus 818.5158 s and 15.202 psia

Maximum Smoothed Hot SP Level is 77.3177 cm at t plus 5920.2056 s and 15.3701 psia

SP 12 Temperature at the beginning is 39.8405 C, and at the end is 94.0427 C

At plume detection, the Mixing Number is 43.2166

The Mixing Number ranges from a minimum of 34.4199 at (KEY POINT #12) t plus 0 s to a maximum of 178.8432 at (KEY POINT #13) t plus 5932.1053 s; it had a mean value of 66.7905 +/- 32.89 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) gl, Sparger Diameter (m) dl, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vfl, Sparger fluid velocity (m/s) vl, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 34.4199): 62.76991779 0.040894

0.00925	0.3937	0.7624370901	0.7641214556	0.648764989
0.648764989	0.9996254285	61.55938181	205822.7268	0.06951847535
0.05832044601	0.0555986307	0.02684566771	0.08244429841	40.47851248
103.0576225	103.0576225	40.58445142	40.28685713	40.1624464
37.19098989	4.178538489	4.220605573	2.089963867	0.6292403337
0.6789626714	0.6789626714	4.296398612	1.696638245	0.03808891862
992.0403828	956.1376567	0.6617705245	1.019664525	0.0006469887267
0.0002729357233	1.23738761e-005	1.247147513e-005	1532.139931	
1542.142667	473.8041774	467.4131047	1.129956371	1.012991595
1.049991595	0.07574905557	0.07617644636	1894.456827	1890.667269
169.6270536	432.0067208	2680.371804	262.3796672	1462.450106
170.0697236	168.8247087	168.3079537	155.8954722	

KEY POINT #2 (t plus 1577.3292 s with a Mixing Number of 43.2166): 51.10309333

0.040894	0.00925	0.3937	0.766728267	0.7699845671
0.6268761988	0.6268761988	0.9995831832	47.85805592	167259.007
0.06695767876	0.05825010069	0.04343259296	0.02368807286	0.06712066583
55.81959573	103.4198521	103.4198521	57.82050192	55.73063612
55.58766588	53.57483893	4.181146414	4.221088276	2.091491346
0.6466987074	0.679097866	0.679097866	3.216176	1.690214612
0.03814734919	985.3113718	955.8722703	0.6696609527	1.067805458
0.0004974465507	0.0002719254043	1.238627331e-005	1.249445358e-005	
1550.929933	1541.77483	473.9855214	466.9259323	1.144367513
1.048799342	1.085799342	0.1639082329	0.180182513	1844.668807
1842.378413	233.7467359	433.5367076	2680.936926	199.7899717
1411.132099	242.1135202	233.3733403	232.7785423	224.3672795

KEY POINT #3 (t plus 2306.6409 s with a Mixing Number of 48.3286): 52.74878944

0.040894	0.00925	0.3937	0.7657557584	0.7697192457
0.620167995	0.620167995	0.9995717839	48.94692571	172626.0615
0.06586046953	0.05825930359	0.0441288739	0.02515330919	0.06928218309
62.17443278	103.3724809	103.3724809	68.5801356	62.23208255
62.2839657	59.78796539	4.183729505	4.221024986	2.091290973
0.6528519828	0.6790802765	0.6790802765	2.893244126	1.691051936
0.03813968921	982.0826811	955.9070101	0.6686247357	1.077673187
0.000451477602	0.0002720571473	1.238465189e-005	1.249584783e-005	
1555.072045	1541.823154	473.961831	466.7066371	1.142474287
1.048754655	1.085754655	0.2204112751	0.2933369334	1829.576386
1827.180584	260.3249775	433.3366104	2680.863063	173.0116328
1396.239776	287.1353383	260.56475	260.7847388	250.3472428

KEY POINT #4 (t plus 2874.8504 s with a Mixing Number of 53.5496): 54.16368689

0.040894	0.00925	0.3937	0.7654008946	0.7700640185
0.6167691088	0.6167691088	0.9995658142	50.01174278	177242.2243
0.06496983811	0.0582625183	0.04490332478	0.02623723621	0.07114056099
67.24619402	103.3559322	103.3559322	75.81384014	67.74017525
67.41812704	63.793274	4.186402534	4.221002888	2.091221019
0.657333878	0.6790741254	0.6790741254	2.672622532	1.691344641
0.03813701459	979.3366184	955.9191437	0.668263051	1.083019385
0.0004196455834	0.0002721031975	1.238408547e-005	1.249685181e-005	
1557.018101	1541.84002	473.9535532	466.5968483	1.141813517
1.048756398	1.085756398	0.2766674432	0.39928527	1821.999968
1819.498793	281.5503986	433.266709	2680.837257	151.7163104
1388.733259	317.4414962	283.6170751	282.27167	267.1036424

KEY POINT #5 (t plus 2899.0508 s with a Mixing Number of 53.7305): 54.31838199

0.040894	0.00925	0.3937	0.7653804714	0.7700664586
0.615162394	0.615162394	0.9995629045	50.02945279	177739.2359
0.0649432215	0.05826315751	0.04491120394	0.02643253922	0.07134374317
67.39662208	103.3526416	103.3526416	76.085473	67.92278376
67.606076	63.94730632	4.186490049	4.220998495	2.091207112
0.6574611195	0.6790729019	0.6790729019	2.666517426	1.691402855
0.03813648285	979.2529463	955.9215563	0.6681911516	1.085728085
0.0004187592736	0.000272112356	1.238397284e-005	1.249749894e-005	
1557.058268	1541.843372	473.9519071	466.5462897	1.141682165
1.048761852	1.085761852	0.2785061563	0.4038203416	1818.382029
1815.879083	282.1801579	433.2528097	2680.832126	151.0726518
1385.129219	318.5802477	284.3816115	283.0585287	267.7481985

KEY POINT #6 (t plus 4256.1744 s with a Mixing Number of 76.163): 54.59438101

0.040894	0.00925	0.3937	0.7641417585	0.7706478762
0.6339950069	0.6339950069	0.9995965088	51.80618872	178762.9746
0.06263583904	0.05826142447	0.04596260457	0.02574364577	0.07170625034
80.20192902	103.3615631	103.3615631	88.34557052	80.75592984
77.59232976	72.76413373	4.195669788	4.221010407	2.091244819
0.6671273502	0.6790762188	0.6790762188	2.223063829	1.691245033
0.03813792459	971.683982	955.9150153	0.6683861006	1.053819676
0.0003534755489	0.0002720875268	1.23842782e-005	1.248906616e-005	
1557.029141	1541.834282	473.9563699	467.1127497	1.142038316
1.04966526	1.08666526	0.4780374088	0.6588645356	1860.913368
1858.229487	335.844652	433.2904937	2680.846038	97.44584173
1427.622874	370.0427642	338.167838	324.8999085	304.6653185

KEY POINT #7 (t plus 4734.0838 s with a Mixing Number of 89.7654): 53.7975338

0.040894	0.00925	0.3937	0.7638674995	0.7710459505
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0.6494145412	0.6494145412	0.9996226137	52.28203177	176247.2085
0.06185243901	0.05826048824	0.04620002663	0.02445961554	0.07065964217
84.45042306	103.3663826	103.3663826	92.5764095	84.92067764
82.7250061	74.3376087	4.19947018	4.221016842	2.091265192
0.6698394606	0.6790780102	0.6790780102	2.103766304	1.691159787
0.03813870352	968.9852408	955.9114815	0.6684914345	1.028987053
0.0003355627319	0.0002720741154	1.238444316e-005	1.248244648e-005	
1555.610807	1541.82937	473.9587807	467.5523541	1.142230753
1.050471252	1.087471252	0.5663176215	0.7733582661	1895.631175
1892.897764	353.6779378	433.3108513	2680.853554	79.63291356
1462.320324	387.8356612	355.651528	346.4349003	311.2589737
KEY POINT #8 (t plus 5026.4885 s with a Mixing Number of 99.9306): 53.37147386				
0.040894	0.00925	0.3937	0.7638845355	0.7714364408
0.6599528996	0.6599528996	0.9996396549	52.68850969	174907.925
0.06141837991	0.05825820487	0.04649273021	0.0236073093	0.07010003951
86.78425901	103.3781367	103.3781367	96.38139181	87.77146406
86.11734418	75.0695407	4.201718606	4.22103254	2.091314887
0.6712274496	0.6790823781	0.6790823781	2.043054019	1.690951921
0.03814060348	967.4645859	955.9028629	0.6687483861	1.012962298
0.0003263792908	0.0002720414118	1.238484547e-005	1.247841144e-005	
1554.554114	1541.817387	473.9646599	467.8448941	1.142700192
1.050576788	1.087576788	0.6203585733	0.8900268658	1919.388233
1916.612154	363.4814245	433.3605008	2680.871883	69.87907629
1486.027733	403.8544871	367.6285443	360.6808623	314.3267263
KEY POINT #9 (t plus 5115.3906 s with a Mixing Number of 103.3045): 53.17275931				
0.040894	0.00925	0.3937	0.7638683343	0.7715189598
0.6637080796	0.6637080796	0.9996458281	52.81687985	174286.1283
0.06129727881	0.05826115097	0.04654049812	0.02329854245	0.06983904057
87.43289801	103.362971	103.362971	97.0486115	88.41103293
87.26862844	75.82156107	4.202363822	4.221012287	2.091250771
0.6716005182	0.6790767421	0.6790767421	2.026745392	1.691220129
0.03813815213	967.037168	955.913983	0.6684168706	1.006737987
0.0003239041914	0.0002720836088	1.238432639e-005	1.247630457e-005	
1554.22638	1541.832847	473.9570742	467.9393254	1.14209453
1.050561372	1.087561372	0.6361208216	0.9119174939	1927.804348
1925.014725	366.2070313	433.2964408	2680.848234	67.08940954
1494.507907	406.6651976	370.316672	365.5181278	317.4790803
KEY POINT #10 (t plus 5271.0925 s with a Mixing Number of 111.1609): 52.52276806				
0.040894	0.00925	0.3937	0.7638635196	0.7717240823
0.6745615611	0.6745615611	0.9996628164	53.03099463	172218.5199
0.0610443191	0.05826199252	0.04660970484	0.02237561352	0.06898531837
88.7843407	103.3586388	103.3586388	98.22514349	90.06847388
89.73277512	83.93812277	4.203736501	4.221006502	2.091232459
0.672360206	0.6790751317	0.6790751317	1.993524517	1.69129676
0.038137452	966.1401222	955.9171593	0.6683221963	0.9904164238
0.0003188512302	0.0002720956647	1.238417811e-005	1.247174856e-005	
1553.496774	1541.837262	473.9549071	468.2218655	1.141921569
1.050880973	1.087880973	0.6700378619	0.9516060051	1952.210261
1949.397975	371.8872345	433.2781419	2680.841478	61.3909074
1518.932119	411.6227609	377.2849346	375.8760637	351.5316616
KEY POINT #11 (t plus 5932.1053 s with a Mixing Number of 178.8432): 46.23888974				
0.040894	0.00925	0.3937	0.7642777677	0.7731653399
0.7887226921	0.7887226921	0.9998127396	54.57513419	152087.9996
0.05984736138	0.05826154971	0.04716247208	0.01356937141	0.06073184349
95.11764944	103.3609184	103.3609184	101.8728813	95.2814624
95.32345981	92.24149602	4.210683342	4.221009546	2.091242094
0.6756071181	0.6790759791	0.6790759791	1.850464876	1.691256437
0.03813782039	961.8194069	955.915488	0.6683720111	0.847251966
0.0002969083971	0.0002720893209	1.238425613e-005	1.24328886e-005	
1549.25959	1541.834939	473.9560474	470.7547676	1.142012576
1.05981119	1.09681119	0.8497597903	1.08386506	2208.96563
2205.987185	398.5330327	433.2877705	2680.845033	34.75473779
1775.67786	427.004853	399.2215177	399.4010307	386.4320368
KEY POINT #12 (t plus 0 s with a Mixing Number of 34.4199): 62.76991779 0.040894				
0.00925	0.3937	0.7624370901	0.7641214556	0.648764989
0.648764989	0.9996254285	61.55938181	205822.7268	0.06951847535
0.05832044601	0.0555986307	0.02684566771	0.08244429841	40.47851248

103.0576225	103.0576225	40.58445142	40.28685713	40.1624464
37.19098989	4.178538489	4.220605573	2.089963867	0.6292403337
0.6789626714	0.6789626714	4.296398612	1.696638245	0.03808891862
992.0403828	956.1376567	0.6617705245	1.019664525	0.0006469887267
0.0002729357233	1.23738761e-005	1.247147513e-005	1532.139931	
1542.142667	473.8041774	467.4131047	1.129956371	1.012991595
1.049991595	0.07574905557	0.07617644636	1894.456827	1890.667269
169.6270536	432.0067208	2680.371804	262.3796672	1462.450106
170.0697236	168.8247087	168.3079537	155.8954722	
KEY POINT #13 (t plus 5932.1053 s with a Mixing Number of 178.8432): 46.23888974				
0.040894	0.00925	0.3937	0.7642777677	0.7731653399
0.7887226921	0.7887226921	0.9998127396	54.57513419	152087.9996
0.05984736138	0.05826154971	0.04716247208	0.01356937141	0.06073184349
95.11764944	103.3609184	103.3609184	101.8728813	95.2814624
95.32345981	92.24149602	4.210683342	4.221009546	2.091242094
0.6756071181	0.6790759791	0.6790759791	1.850464876	1.691256437
0.03813782039	961.8194069	955.915488	0.6683720111	0.847251966
0.0002969083971	0.0002720893209	1.238425613e-005	1.24328886e-005	
1549.25959	1541.834939	473.9560474	470.7547676	1.142012576
1.05981119	1.09681119	0.8497597903	1.08386506	2208.96563
2205.987185	398.5330327	433.2877705	2680.845033	34.75473779
1775.67786	427.004853	399.2215177	399.4010307	386.4320368
KEY POINT #14 (t plus 5224.0168 s with a Mixing Number of 107.9805): 52.25779211				
0.040894	0.00925	0.3937	0.7638343662	0.7716369862
0.6779964433	0.6779964433	0.9996681932	53.05206165	171374.2032
0.0611399602	0.05826425709	0.04662938222	0.02200790707	0.06863728929
88.2739224	103.346981	103.346981	98.1009468	89.44822195
88.66259308	78.98420529	4.203213579	4.220990938	2.09118319
0.6720760672	0.6790707968	0.6790707968	2.005952665	1.691503007
0.03813556817	966.4799353	955.9257064	0.6680674812	0.9850284885
0.0003207433438	0.0002721281121	1.238377909e-005	1.246996404e-005	
1553.779699	1541.849139	473.9490753	468.3052863	1.141456235
1.050582826	1.087582826	0.6570548657	0.9473499918	1959.904429
1957.089908	369.7416805	433.2288994	2680.823298	63.48721885
1526.67553	411.0993324	374.6769044	371.376822	330.7412094

End

D.8 TEST #8 - T08_RCIC_040GPM_107KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T08_RCIC_040GPM_107kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 2044.3429 s, and ending (KEY POINT #11) at t plus 10480.7805 s, for a time period of 8436.4376 s.
Original Data Record Time: 12198.2097 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 2290.736 s, T_{bulk} = 61.5556 C and T_{out} = 59.4322 C
Stratification Beginning SP12 Temperature = 61.2481 C
Stratification Beginning Pressure = 16.4767 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 7496.9238 s, T_{bulk} = 109.8205 C and T_{out} = 74.1689 C
Stratification Ending SP12 Temperature = 109.6427 C
Stratification Ending Pressure = 36.1733 psia
Plume detected! Setting t_{plume} (KEY POINT #2) to 1659.7259 s.
At t = 1659.7259 s, the pool pressure is 15.7153 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 55.9093, 56.0772, 58.0778, 55.7861, and 53.6478 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 10.1925 +/- 2.9825 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 9.4804 +/- 2.8168 C.
Minimum Steam Quality: 0.51672 at t plus 685.5112 s
Maximum Steam Quality: 0.66112 at t plus 8105.1336 s
Time-Averaged Steam Quality: 0.59234 +/- 0.020428
Minimum Turbine Outlet Steam Quality: 0.56247 at t plus 685.5112 s

Maximum Turbine Outlet Steam Quality: 0.67746 at t plus 8105.1336 s
 Time-Averaged Turbine Outlet Steam Quality: 0.62502 +/- 0.015747
 Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 8346.4374 s; using 300 s smoothing
 Max and min smoothed upper level changerates: 0.85108 degrees/min at t plus 3701.0607 s and 0.3597 degrees/min at t plus 6995.7151 s, respectively
 Max and min smoothed mid (SP9) level changerates: 0.69463 degrees/min at t plus 3615.5578 s and 0.39895 degrees/min at t plus 7258.2191 s, respectively
 Max and min smoothed upper-mid level changerate differences: 0.26167 degrees/min at t plus 3374.954 s and -0.16867 degrees/min at t plus 3555.5584 s, respectively
 Max and min smoothed lower level changerates: 2.3212 degrees/min at t plus 5971.3975 s and 0.0072092 degrees/min at t plus 3350.0536 s, respectively
 Max and min smoothed mid-lower level changerate differences: 0.61763 degrees/min at t plus 3605.0002 s and -1.7776 degrees/min at t plus 5971.4996 s, respectively
 Max and min smoothed outlet level changerates: 7.6632 degrees/min at t plus 7786.1273 s and -0.02798 degrees/min at t plus 4186.5685 s, respectively
 Max and min smoothed lower-outlet level changerate differences: 2.2359 degrees/min at t plus 5971.3975 s and -7.144 degrees/min at t plus 7785.6283 s, respectively
 Max and min smoothed hot (SP8) level changerates: 1.0759 degrees/min at t plus 2181.1358 s and 0.22496 degrees/min at t plus 7665.9485 s, respectively
 Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.5205 degrees/min at t plus 2181.1358 s and -0.28715 degrees/min at t plus 3776.562 s, respectively
 The mean steam flow rate was 45.4844 +/- 1.0202 g/s
 The mean feedwater flow rate was 44.9409 +/- 1.271 g/s
 The mean water injection to steam flow rate was 24.8476 +/- 1.115 g/s
 Mean Smoothed Condensing Region SP8-SP9 delta T is 10.9507 +/- 2.1231 C over the Stratification Period, beginning at 6.143 C and ending at 13.4693 C
 Mean Smoothed SP8-Upper Pool delta T is 10.1609 +/- 2.1201 C over the Stratification Period, beginning at 6.0543 C and ending at 12.3153 C
 The stratification period begins and ends with Smoothed SP8 readings of 67.9793 and 123.1198 C, respectively
 The stratification period begins and ends with condensing flows of 0.549 and 1.247 kg/s, respectively.
 The stratification period begins and ends with condensing+cooling flows of 4.2001 and 1.7081 kg/s, respectively.
 The stratification period had a mean sparger steam enthalpy of 1872.7689 +/- 12.1382 kJ/kg.
 At plume detection, the condensing and condensing+cooling flows are 0.49108 and 13.0555 kg/s, respectively
 The plume period had a mean steam enthalpy of 1869.6989 +/- 16.6767 kJ/kg.
 Maximum Smoothed Top-Mid delta T is 1.5818 degrees C at t plus 8335.7358 s with T_upper = 117.7687 C and T_mid = 116.1869 C
 At t plus 8335.7358 s, Smoothed SP8-SP9 is 12.2572 C and Smoothed SP8-Top is 10.6754 C, where Smoothed SP8 is 128.4441 C and Pool P = 41.4713 psia
 Maximum Smoothed Top-Lower delta T is 11.438 degrees C at t plus 5761.6936 s with T_upper = 97.0643 C and T_low = 85.6264 C
 At t plus 5761.6936 s, Smoothed SP8-SP9 is 12.8879 C and Smoothed SP8-Top is 12.2202 C, where Smoothed SP8 is 109.2845 C and Pool P = 27.3769 psia
 Maximum Smoothed Mid-Lower delta T is 10.7702 degrees C at t plus 5761.6936 s with T_mid = 96.3966 C and T_low = 85.6264 C
 At t plus 5761.6936 s, Smoothed SP8-SP9 is 12.8879 C and Smoothed SP8-Top is 12.2202 C, where Smoothed SP8 is 109.2845 C and Pool P = 27.3769 psia
 Maximum Smoothed Top-Outlet delta T is 36.6847 degrees C at t plus 7425.8217 s with T_upper = 110.2833 C and T_out = 73.5986 C
 At t plus 7425.8217 s, Smoothed SP8-SP9 is 13.5258 C and Smoothed SP8-Top is 12.4333 C, where Smoothed SP8 is 122.7166 C and Pool P = 35.7827 psia
 Maximum Smoothed Mid-Outlet delta T is 35.5999 degrees C at t plus 7418.8493 s with T_mid = 109.1478 C and T_out = 73.5479 C
 At t plus 7418.8493 s, Smoothed SP8-SP9 is 13.6406 C and Smoothed SP8-Top is 12.5746 C, where Smoothed SP8 is 122.7884 C and Pool P = 35.7411 psia
 Maximum Smoothed Lower-Outlet delta T is 35.5758 degrees C at t plus 7432.4221 s with T_low = 109.2327 C and T_out = 73.6568 C
 At t plus 7432.4221 s, Smoothed SP8-SP9 is 13.5696 C and Smoothed SP8-Top is 12.4893 C, where Smoothed SP8 is 122.8228 C and Pool P = 35.8225 psia
 Maximum Smoothed Condensing Region SP8-SP9 delta T is 14.2505 degrees C at (KEY POINT #14) t plus 6969.9137 s with T_SP8 = 120.2456 C and T_SP9 = 105.995 C and Pool P = 33.4157 psia

Maximum Smoothed Condensing Region SP8-Upper delta T is 13.363 degrees C at t plus 6445.1106 s with T_SP8 = 116.3356 C and T_upper = 102.9726 C and Pool P = 30.7583 psia
 Maximum Top-Mid delta T is 2.2528 degrees C at (KEY POINT #4) t plus 3584.158 s ignoring SP 4, with temperatures of 75.2131 and 72.9603 C, respectively, at Set # 2, where Pool P = 19.0685 psia and T_outlet = 67.756 C
 Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 4528.174 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.99985 C and a raw SP12 Reading of 83.6957 C.
 Maximum Top-Lower delta T is 14.3987 degrees C at t plus 5941.0208 s, with temperatures of 98.8861 and 84.4874 C, respectively, at Set # 1, where Pool P = 28.2713 psia and T_outlet = 70.9469 C
 Maximum Mid-Low delta T is 11.7386 degrees C at (KEY POINT #6) t plus 5770.8931 s ignoring SP 4, with temperatures of 96.41 and 84.6714 C, respectively, at Set # 2, where Pool P = 27.4266 psia and T_outlet = 70.7088 C
 Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 6037.4233 s with a Smoothed Mid-Axis Mid-Low Delta T of 3.9117 C and a raw SP12 Reading of 98.7858 C.
 Maximum Top-Outlet delta T is 37.2082 degrees C at t plus 7431.7221 s, with temperatures of 110.7704 and 73.5622 C, respectively, at Set # 1, where Pool P = 35.8096 psia
 Maximum Mid-Outlet delta T is 35.6618 degrees C at t plus 7396.9201 s ignoring SP 4, with temperatures of 108.9664 and 73.3046 C, respectively, at Set # 2, where Pool P = 35.6445 psia
 Maximum Lower-Outlet delta T is 36.8155 degrees C at (KEY POINT #8) t plus 7430.621 s, with temperatures of 110.3773 and 73.5618 C, respectively, at Set # 1, where Pool P = 35.8104 psia
 Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 7818.7272 s with a Smoothed Mid-Axis Low-Outlet Delta T of 12.2654 C and a raw SP12 Reading of 111.8494 C.
 Minimum SP Pressure is 14.6753 psia at t plus 61.8995 s
 Maximum SP Pressure is 42.2321 psia at t plus 8436.0375 s
 Beginning SP Pressure is 14.6832 psia
 Ending SP Pressure is 42.2311 psia
 Time-Average SP Pressure is 23.6178 +/- 8.2121 psia
 SP Levels are fully corrected and compensated
 Pre-Start SP Level is 75.5226 cm (cold) / 75.6601 cm (hot) at 14.6978 psia
 Beginning Smoothed SP Level is 75.7776 cm (cold) / 75.9411 cm (hot) at 14.6894 psia
 Ending Smoothed SP Level is 83.6256 cm (cold) / 85.4091 cm (hot) at 42.2433 psia
 Minimum Smoothed Cold SP Level is 75.7691 cm at t plus 145.5033 s and 14.6974 psia
 Minimum Smoothed Hot SP Level is 75.9392 cm at t plus 33.1999 s and 14.6897 psia
 Maximum Smoothed Cold SP Level is 83.6945 cm at t plus 7358.0208 s and 35.419 psia
 Maximum Smoothed Hot SP Level is 85.4091 cm at t plus 8436.4376 s and 42.2433 psia
 SP 12 Temperature at the beginning is 40.0358 C, and at the end is 116.7484 C
 At plume detection, the Mixing Number is 43.5377
 The Mixing Number ranges from a minimum of 34.185 at (KEY POINT #12) t plus 0 s to a maximum of 223.004 at (KEY POINT #13) t plus 8433.2384 s; it had a mean value of 94.7469 +/- 55.3088 over the test period.
 Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8,

Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 34.185): 53.72431041 0.040894
0.00925 0.3937 0.7577762961 0.7594107385 0.6152278213
0.6152278213 0.9995760134 50.96844979 176262.2459 0.06952849958
0.05843773759 0.04564824051 0.02491522739 0.07056346789 40.41693034
102.452972 102.452972 40.55870406 40.27360842 40.00712038
37.61120412 4.178538843 4.219806227 2.087438042 0.6291624666
0.6787334333 0.6787334333 4.301829735 1.70746906 0.03799210993
992.0628711 956.5793401 0.6487682168 1.054069932 0.0006477263726
0.0002746373352 1.235318831e-005 1.246439326e-005 1532.03691
1542.748058 473.5004852 466.2084479 1.106234776 1.012797239
1.049797239 0.07550156658 0.07607238244 1816.297344 1813.699562
169.3697131 429.4532049 2679.426806 260.0834918 1386.84414
169.96212 168.7693311 167.6589008 157.6513844

KEY POINT #2 (t plus 1659.7259 s with a Mixing Number of 43.5377): 52.28111092
0.040894 0.00925 0.3937 0.7664612406 0.7697324921
0.6211750017 0.6211750017 0.9995606342 47.18911133 170650.8854
0.06691360516 0.05808454857 0.04408799687 0.0245799202 0.06866791707
56.07723374 104.271131 104.271131 58.07779441 55.90925758
55.78607262 53.64782984 4.181226652 4.222234033 2.095123787
0.6469618358 0.679409304 0.679409304 3.201927145 1.675306591
0.03828596276 985.1867307 955.2462701 0.6885061668 1.10790624
0.0004954346741 0.0002695774029 1.241541883e-005 1.252840702e-005
1551.142337 1540.895226 474.4099509 467.0754777 1.178833702
1.083257124 1.120257124 0.165930582 0.1823718932 1833.977881
1831.751069 234.8268931 437.1330752 2682.262049 202.3061822
1396.844806 243.192404 234.1231086 233.6110263 224.6753562

KEY POINT #3 (t plus 2290.736 s with a Mixing Number of 48.6299): 52.55772476
0.040894 0.00925 0.3937 0.7752490371 0.7793552202
0.6266878639 0.6266878639 0.9995543761 46.13245975 171020.2019
0.06591937549 0.05786340586 0.04449091525 0.02454031651 0.06903123177
61.83631569 105.4056553 105.4056553 67.97932698 61.92498151
61.63627103 59.27000849 4.183551217 4.223785875 2.100059212
0.6525443204 0.6798107027 0.6798107027 2.909016881 1.65584059
0.03847355566 982.2641222 954.4069497 0.7142903852 1.139278613
0.0004537442821 0.0002665045502 1.245428451e-005 1.256749537e-005
1554.915511 1539.69016 474.9717621 467.6681173 1.226095615
1.135761498 1.172761498 0.2170352809 0.285726708 1849.148881
1847.020678 258.917686 441.9276765 2684.02152 183.0099905
1407.221205 284.6268984 259.2872053 258.0823037 248.1881914

KEY POINT #4 (t plus 3584.158 s with a Mixing Number of 62.797): 52.68799233
0.040894 0.00925 0.3937 0.7894662381 0.7957639283
0.6400902514 0.6400902514 0.999524489 41.90766409 169668.7323
0.06384662748 0.05712861208 0.04533634359 0.02386598636 0.06920232995
73.53903298 109.1543943 109.1543943 82.61570887 74.30705287
72.2578697 67.66618872 4.190408938 4.229117703 2.117157954
0.6623962235 0.6810268018 0.6810268018 2.436195686 1.594636098
0.03911730497 975.7418303 951.5930071 0.805129927 1.257240017
0.000385100081 0.0002567887673 1.258287462e-005 1.269899721e-005
1557.921933 1535.446452 476.7964372 469.4585556 1.393509102
1.314641765 1.351641765 0.3629615203 0.526652352 1888.219354
1886.463102 307.9286456 457.7837289 2689.780498 149.8550833
1430.435625 345.9955389 311.1458005 302.5620871 283.3357794

KEY POINT #5 (t plus 4528.174 s with a Mixing Number of 80.946): 53.6500332
0.040894 0.00925 0.3937 0.7917778743 0.7997669357
0.630992654 0.630992654 0.9994378883 37.13089726 170708.0342
0.06197993025 0.05633737692 0.04575401368 0.02471189582 0.0704659095
83.76224041 113.1561774 113.1561774 93.16928573 84.68226876
77.51456894 69.36786971 4.198725819 4.235161741 2.136812139
0.6694415377 0.6821402982 0.6821402982 2.122234569 1.534205998
0.03984677406 969.4486187 948.5208896 0.9122272578 1.444889221
0.0003383674083 0.0002471083282 1.272039308e-005 1.285214529e-005
1555.973863 1530.483983 478.6893431 470.5592211 1.592529782
1.517919296 1.554919296 0.5511563485 0.7906506141 1877.609074
1876.23037 350.8249702 474.7341319 2695.831682 123.9091617
1402.874942 390.3663939 354.6869766 324.6113402 290.4775158

KEY POINT #6 (t plus 5770.8931 s with a Mixing Number of 118.6919): 54.72733836

0.040894	0.00925	0.3937	0.821934091	0.833500857
0.6223704691	0.6223704691	0.9992879696	30.76480826	170866.641
0.0595855964	0.0550535703	0.04650052478	0.02538035659	0.07188088137
96.48960771	119.5759872	119.5759872	109.4204607	97.08317546
85.80243676	70.76936609	4.212112216	4.245643388	2.171558638
0.6762890265	0.6835349339	0.6835349339	1.821925746	1.446701991
0.04111429597	960.8962966	943.4470521	1.107920078	1.77889418
0.0002925250624	0.0002329143688	1.294142239e-005	1.309804981e-005	
1548.33611	1521.626524	481.6034511	472.2978806	1.96012287
1.891211702	1.928211702	0.8935473575	1.406072249	1874.219714
1873.273241	404.3741308	501.9823402	2705.317763	97.60820939
1372.237374	458.9479807	406.8732271	359.4237917	296.3774566

KEY POINT #7 (t plus 6037.4233 s with a Mixing Number of 128.3454): 54.54818148

0.040894	0.00925	0.3937	0.8272183083	0.839618162
0.6208302011	0.6208302011	0.9992514288	29.32208913	169594.3486
0.05912013134	0.05476530632	0.04634022377	0.02530534643	0.0716455702
98.91801372	121.0055404	121.0055404	112.4051565	99.54028795
94.61053138	71.10890471	4.215053716	4.248113313	2.17985958
0.677362164	0.6837806943	0.6837806943	1.773542525	1.428657865
0.04141370538	959.1782718	942.2930258	1.155801955	1.860310199
0.0002850095595	0.0002299582413	1.299069559e-005	1.315311125e-005	
1546.280246	1519.50843	482.23128	472.6630067	2.050746277
1.983352398	2.020352398	0.9756414115	1.553501364	1874.330888
1873.471103	414.6133615	508.0598338	2707.391096	93.44647227
1366.271054	471.5847514	417.2352433	396.4697426	297.8071228

KEY POINT #8 (t plus 7430.621 s with a Mixing Number of 177.1392): 54.02916768

0.040894	0.00925	0.3937	0.8369291415	0.8524069313
0.6230186294	0.6230186294	0.9990914903	23.93491903	164753.3665
0.05711178159	0.05337908213	0.04642663935	0.0245372392	0.07096387855
109.2398885	127.8220237	127.8220237	122.7755747	110.320628
109.2087661	73.6428534	4.228983875	4.260601013	2.222386231
0.6811176741	0.6846331946	0.6846331946	1.593239661	1.349070651
0.04293234762	951.5792457	936.6700536	1.407641583	2.257336555
0.0002566062498	0.000216781282	1.322583352e-005	1.341076562e-005	
1535.577245	1508.704496	485.1164839	474.6445853	2.531142697
2.469033752	2.506033752	1.397535866	2.167662947	1895.831968
1895.259088	458.2264389	537.0921031	2717.07023	78.86566423
1358.739865	515.6135902	462.7964923	458.0961365	308.4622795

KEY POINT #9 (t plus 7496.9238 s with a Mixing Number of 179.4484): 54.12980052

0.040894	0.00925	0.3937	0.8369085534	0.8525346678
0.6197716266	0.6197716266	0.9990703524	23.64279262	164880.2502
0.0570309056	0.05331450834	0.04632629647	0.02476975691	0.07109605339
109.650488	128.1372799	128.1372799	123.1197805	110.804489
109.6635286	74.27756467	4.229586459	4.261207751	2.224473142
0.6812406383	0.6846599641	0.6846599641	1.586825236	1.345631849
0.04300633452	951.2672672	936.4052007	1.420277714	2.289484216
0.0002555828677	0.0002162063686	1.32367143e-005	1.342540455e-005	
1535.088732	1508.177198	485.2455256	474.5837894	2.555397986
2.49352322	2.53052322	1.417008656	2.19101784	1889.523195
1888.964213	459.9647629	538.4370334	2717.509327	78.47227056
1351.086162	517.0786703	464.8454628	460.0212303	311.1239816

KEY POINT #10 (t plus 7818.7272 s with a Mixing Number of 192.6342): 52.32604733

0.040894	0.00925	0.3937	0.836706884	0.8530505304
0.6504355915	0.6504355915	0.9991471506	22.93661151	158952.7681
0.05655951107	0.05298960091	0.04644880316	0.02227813503	0.06872693819
112.0362717	129.7205377	129.7205377	124.8840163	113.1896579
112.3856205	99.47162513	4.233169009	4.264295021	2.235116955
0.6819143481	0.6847776336	0.6847776336	1.550582439	1.328665042
0.04338306765	949.4388671	935.0686793	1.485126728	2.281332938
0.0002497808169	0.0002133623726	1.329136461e-005	1.346199506e-005	
1532.153603	1505.492808	485.8876409	476.3081907	2.680083639
2.619498381	2.656498381	1.534621052	2.313966246	1960.098142
1959.572054	470.069007	545.1945269	2719.702727	75.12551995
1414.903615	524.5913384	474.9512825	471.5492497	416.9996506

KEY POINT #11 (t plus 8436.4376 s with a Mixing Number of 222.9409): 54.00500197

0.040894	0.00925	0.3937	0.83625599	0.85409058
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0.6657485431	0.6657485431	0.9991195732	21.99650688	162601.1362
0.05556218624	0.05227234482	0.04793883523	0.0229933032	0.07093213843
117.0431362	133.198449	133.198449	128.7958563	118.5570557
118.1676518	114.8017052	4.241117599	4.27131634	2.259459609
0.6831107929	0.6849384351	0.6849384351	1.4798746	1.293103368
0.04424135742	945.521179	932.0953496	1.635961297	2.455162643
0.0002383613016	0.0002073590732	1.341143962e-005	1.35821963e-005	
1525.49409	1499.3862	487.2630998	477.8560994	2.9713541
2.912575501	2.949575501	1.807600497	2.606677198	2001.482666
2000.998819	491.3044963	560.0570577	2724.450471	68.75256133
1441.425608	541.2705742	497.7259029	496.0760129	481.8069935
KEY POINT #12 (t plus 0 s with a Mixing Number of 34.185):	53.72431041			0.040894
0.00925	0.3937	0.7577762961	0.7594107385	0.6152278213
0.6152278213	0.9995760134	50.96844979	176262.2459	0.06952849958
0.05843773759	0.04564824051	0.02491522739	0.07056346789	40.41693034
102.452972	102.452972	40.55870406	40.27360842	40.00712038
37.61120412	4.178538843	4.219806227	2.087438042	0.6291624666
0.6787334333	0.6787334333	4.301829735	1.70746906	0.03799210993
992.0628711	956.5793401	0.6487682168	1.054069932	0.0006477263726
0.0002746373352	1.235318831e-005	1.246439326e-005	1532.03691	
1542.748058	473.5004852	466.2084479	1.106234776	1.012797239
1.049797239	0.07550156658	0.07607238244	1816.297344	1813.699562
169.3697131	429.4532049	2679.426806	260.0834918	1386.84414
169.96212	168.7693311	167.6589008	157.6513844	
KEY POINT #13 (t plus 8433.2384 s with a Mixing Number of 223.004):	54.53360289			
0.040894	0.00925	0.3937	0.8362537688	0.8540776755
0.6588858279	0.6588858279	0.9990925676	21.99292637	164135.6216
0.05556530433	0.05227558577	0.0479378614	0.02368856075	0.07162642214
117.0275663	133.1827864	133.1827864	128.7969579	118.5379646
118.1624395	114.7926244	4.241092144	4.271283968	2.259347005
0.6831074821	0.6849380103	0.6849380103	1.480084054	1.293258441
0.04423739607	945.5335147	932.1088551	1.635255465	2.479597939
0.0002383953136	0.0002073853834	1.341089881e-005	1.358691754e-005	
1525.515664	1499.414341	487.2570141	477.5652006	2.969987218
2.910874258	2.947874258	1.806693896	2.606763663	1986.592099
1986.10841	491.2383425	559.9900666	2724.429311	68.75172411
1426.602032	541.2751538	497.6447669	496.0537771	481.7683927
KEY POINT #14 (t plus 6969.9137 s with a Mixing Number of 160.6076):	54.82757732			
0.040894	0.00925	0.3937	0.8361723611	0.8507478675
0.6088828619	0.6088828619	0.9990959047	25.27295277	168101.9254
0.057748293	0.05382773325	0.04607279185	0.02593974703	0.07201253888
105.9950486	125.6261661	125.6261661	120.2455708	106.9515011
105.4718306	72.66685253	4.224350717	4.256447563	2.208147451
0.6800762099	0.6844158434	0.6844158434	1.645848745	1.37359626
0.04242635029	954.0194914	938.5030926	1.322116246	2.169417156
0.0002649644055	0.0002208675259	1.315005766e-005	1.333785405e-005	
1539.275482	1512.310231	484.2068131	473.4494984	2.367336754
2.303463459	2.340463459	1.25125868	2.002153376	1859.545156
1858.906434	444.4995253	527.7297917	2713.990442	83.23026636
1331.815364	504.8522431	448.5393068	442.290792	304.3595185

End

D.9 TEST #9 - T09_RCIC_14PSIG_107KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T09_RCIC_14PSIG_107kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1785.2361 s, and ending (KEY POINT #11) at t plus 11121.3801 s, for a time period of 9336.144 s.
Original Data Record Time: 12508.3004 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 1231.6184 s, T_bulk = 51.446 C and T_out = 46.6852 C
Stratification Beginning SP12 Temperature = 51.3612 C
Stratification Beginning Pressure = 30.9121 psia

Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 9306.5423 s, $T_{bulk} = 127.6598$ C and $T_{out} = 65.9489$ C
 Stratification Ending SP12 Temperature = 127.5488 C
 Stratification Ending Pressure = 72.0254 psia
 Plume detected! Setting t_plume (KEY POINT #2) to 863.2124 s.
 At t = 863.2124 s, the pool pressure is 30.4636 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 48.6881, 48.7419, 50.7443, 49.1189, and 43.8525 C, respectively.

Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 15.0062 +/- 3.9978 C.

Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 13.6782 +/- 3.7886 C.

Minimum Steam Quality: 0.98945 at t plus 8926.3376 s
 Maximum Steam Quality: 1.0028 at t plus 1557.1231 s
 Time-Averaged Steam Quality: 0.99725 +/- 0.0023927
 Minimum Turbine Outlet Steam Quality: 0.99147 at t plus 8926.3376 s
 Maximum Turbine Outlet Steam Quality: 1.0122 at t plus 1557.1231 s
 Time-Averaged Turbine Outlet Steam Quality: 1.0034 +/- 0.0048722
 Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 9246.2429 s; using 300 s smoothing

Max and min smoothed upper level changerates: 0.8275 degrees/min at t plus 2863.1438 s and 0.357 degrees/min at t plus 9239.5435 s, respectively
 Max and min smoothed mid (SP9) level changerates: 0.88415 degrees/min at t plus 3745.6562 s and 0.37111 degrees/min at t plus 2919.885 s, respectively
 Max and min smoothed upper-mid level change rate differences: 0.38408 degrees/min at t plus 2863.9438 s and -0.27744 degrees/min at t plus 3744.8562 s, respectively
 Max and min smoothed lower level changerates: 3.102 degrees/min at t plus 7515.3159 s and -0.19145 degrees/min at t plus 2218.7339 s, respectively
 Max and min smoothed mid-lower level change rate differences: 0.69331 degrees/min at t plus 2218.7339 s and -2.5958 degrees/min at t plus 7515.3159 s, respectively
 Max and min smoothed outlet level changerates: 0.70738 degrees/min at t plus 667.6102 s and 0.012087 degrees/min at t plus 3460.4519 s, respectively
 Max and min smoothed lower-outlet level change rate differences: 3.0035 degrees/min at t plus 7515.3159 s and -0.54718 degrees/min at t plus 2114.0309 s, respectively
 Max and min smoothed hot (SP8) level changerates: 1.4205 degrees/min at t plus 1724.7257 s and 0.12903 degrees/min at t plus 8107.6237 s, respectively
 Max and min smoothed hot-mid (SP8-SP9) level change rate differences: 0.90237 degrees/min at t plus 1724.7257 s and -0.41519 degrees/min at t plus 3557.1535 s, respectively

The mean steam flow rate was 43.4815 +/- 1.1074 g/s
 The mean feedwater flow rate was 43.4205 +/- 1.6892 g/s
 The mean water injection to steam flow rate was 0.0027484 +/- 0.038867 g/s
 Mean Smoothed Condensing Region SP8-SP9 delta T is 15.5421 +/- 3.1807 C over the Stratification Period, beginning at 4.0088 C and ending at 14.8862 C
 Mean Smoothed SP8-Upper Pool delta T is 14.1602 +/- 3.1092 C over the Stratification Period, beginning at 3.4709 C and ending at 14.2405 C
 The stratification period begins and ends with Smoothed SP8 readings of 55.7904 and 142.5166 C, respectively
 The stratification period begins and ends with condensing flows of 0.31847 and 0.8453 kg/s, respectively.
 The stratification period begins and ends with condensing+cooling flows of 6.3985 and 1.4057 kg/s, respectively.

The stratification period had a mean sparger steam enthalpy of 2733.0317 +/- 1.8199 kJ/kg. At plume detection, the condensing and condensing+cooling flows are 0.30716 and 12.9002 kg/s, respectively
 The plume period had a mean steam enthalpy of 2733.0351 +/- 1.8789 kJ/kg.

Maximum Smoothed Top-Mid delta T is 3.7619 degrees C at t plus 3411.8522 s with $T_{upper} = 74.5053$ C and $T_{mid} = 70.7434$ C
 At t plus 3411.8522 s, Smoothed SP8-SP9 is 17.2901 C and Smoothed SP8-Top is 13.5282 C, where Smoothed SP8 is 88.0335 C and Pool P = 35.7393 psia
 Maximum Smoothed Top-Lower delta T is 27.7551 degrees C at t plus 7050.8083 s with $T_{upper} = 111.3447$ C and $T_{low} = 83.5895$ C
 At t plus 7050.8083 s, Smoothed SP8-SP9 is 17.7157 C and Smoothed SP8-Top is 17.2516 C, where Smoothed SP8 is 128.5963 C and Pool P = 54.7955 psia
 Maximum Smoothed Mid-Lower delta T is 27.2911 degrees C at t plus 7050.9083 s with $T_{mid} = 110.8813$ C and $T_{low} = 83.5902$ C

At t plus 7050.9083 s, Smoothed SP8-SP9 is 17.7079 C and Smoothed SP8-Top is 17.244 C, where Smoothed SP8 is 128.5892 C and Pool P = 54.7959 psia
Maximum Smoothed Top-Outlet delta T is 62.3497 degrees C at t plus 9298.3438 s with T_upper = 128.3087 C and T_out = 65.9591 C
At t plus 9298.3438 s, Smoothed SP8-SP9 is 14.8796 C and Smoothed SP8-Top is 14.135 C, where Smoothed SP8 is 142.4437 C and Pool P = 71.9578 psia
Maximum Smoothed Mid-Outlet delta T is 61.8155 degrees C at t plus 9336.144 s with T_mid = 127.8872 C and T_out = 66.0718 C
At t plus 9336.144 s, Smoothed SP8-SP9 is 14.656 C and Smoothed SP8-Top is 14.1326 C, where Smoothed SP8 is 142.5433 C and Pool P = 72.2619 psia
Maximum Smoothed Lower-Outlet delta T is 60.9292 degrees C at t plus 9332.5438 s with T_low = 126.9894 C and T_out = 66.0602 C
At t plus 9332.5438 s, Smoothed SP8-SP9 is 14.7466 C and Smoothed SP8-Top is 14.2285 C, where Smoothed SP8 is 142.6 C and Pool P = 72.2426 psia
Maximum Smoothed Condensing Region SP8-SP9 delta T is 18.5497 degrees C at (KEY POINT #14) t plus 3487.1534 s with T_SP8 = 89.9851 C and T_SP9 = 71.4354 C and Pool P = 35.9873 psia
Maximum Smoothed Condensing Region SP8-Upper delta T is 17.9235 degrees C at t plus 6529.1004 s with T_SP8 = 124.7097 C and T_upper = 106.7862 C and Pool P = 51.1953 psia
Maximum Top-Mid delta T is 5.0676 degrees C at (KEY POINT #4) t plus 2954.044 s ignoring SP 4, with temperatures of 70.9112 and 65.8436 C, respectively, at Set # 2, where Pool P = 34.4004 psia and T_outlet = 56.6531 C
Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 5793.2884 s with a Smoothed Mid-Axis Top-Mid Delta T of 1.6889 C and a raw SP12 Reading of 97.9773 C.
Maximum Top-Lower delta T is 29.9102 degrees C at t plus 7110.2087 s, with temperatures of 111.8397 and 81.9296 C, respectively, at Set # 2, where Pool P = 55.2218 psia and T_outlet = 62.6679 C
Maximum Mid-Low delta T is 29.399 degrees C at (KEY POINT #6) t plus 7110.3097 s ignoring SP 4, with temperatures of 111.322 and 81.923 C, respectively, at Set # 2, where Pool P = 55.225 psia and T_outlet = 62.6726 C
Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 7719.7385 s with a Smoothed Mid-Axis Mid-Low Delta T of 9.7901 C and a raw SP12 Reading of 116.277 C.
Maximum Top-Outlet delta T is 62.8564 degrees C at t plus 9322.2432 s, with temperatures of 128.7874 and 65.931 C, respectively, at Set # 1, where Pool P = 72.1576 psia
Maximum Mid-Outlet delta T is 61.8181 degrees C at t plus 9335.944 s ignoring SP 4, with temperatures of 127.9223 and 66.1041 C, respectively, at Set # 2, where Pool P = 72.2539 psia
Maximum Lower-Outlet delta T is 61.9354 degrees C at (KEY POINT #8) t plus 9198.5651 s, with temperatures of 127.6744 and 65.7391 C, respectively, at Set # 1, where Pool P = 71.1036 psia
Low-Outlet Reconvergence NOT Detected, setting t to (KEY POINT #10) t plus 9336.144 s with a Smoothed Mid-Axis Low-Outlet Delta T of 61.5178 C and a raw SP12 Reading of 127.9371 C.
Minimum SP Pressure is 29.6403 psia at t plus 2.2341 s
Maximum SP Pressure is 72.2619 psia at t plus 9336.144 s
Beginning SP Pressure is 29.643 psia
Ending SP Pressure is 72.2619 psia
Time-Average SP Pressure is 44.313 +/- 12.7652 psia
SP Levels are fully corrected and compensated
Pre-Start SP Level is 84.3452 cm (cold) / 84.5256 cm (hot) at 28.7816 psia
Beginning Smoothed SP Level is 84.8555 cm (cold) / 85.0933 cm (hot) at 29.6403 psia
Ending Smoothed SP Level is 83.0104 cm (cold) / 85.0647 cm (hot) at 72.2683 psia
Minimum Smoothed Cold SP Level is 83.0104 cm at t plus 9336.144 s and 72.2683 psia
Minimum Smoothed Hot SP Level is 85.0647 cm at t plus 9336.144 s and 72.2683 psia
Maximum Smoothed Cold SP Level is 85.3284 cm at t plus 2849.542 s and 34.118 psia
Maximum Smoothed Hot SP Level is 86.3905 cm at t plus 5309.1817 s and 43.6737 psia
SP 12 Temperature at the beginning is 40.432 C, and at the end is 127.9371 C
At plume detection, the Mixing Number is 44.8139
The Mixing Number ranges from a minimum of 40.6672 at (KEY POINT #12) t plus 0 s to a maximum of 227.6333 at (KEY POINT #13) t plus 9336.144 s; it had a mean value of 101.5207 +/- 55.3862 over the test period.
Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat

Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) kl, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m3) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Lower Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 40.6672): 33.76693435 0.040894
 0.00925 0.3937 0.8485546192 0.8509330776 1.006321913
 1 1 29.08978363 104078.2906 0.06956789776
 0.05461064697 0.04435072261 2.873584963e-006 0.04435072261 40.17477116
 128.1872887 121.7707737 40.95337758 40.39381282 40.10855865
 35.78166995 4.178287122 4.24945629 2.184389716 0.6289091084
 0.683902644 0.683902644 4.32283105 1.419200572 0.04157663592
 992.1991288 941.6716776 1.182111113 1.160858486 0.0006506656297
 0.0002284045199 1.301707796e-005 1.326756047e-005 1531.796404
 1518.353279 482.5641462 487.1692282 2.100644111 2.043628264
 2.080628264 0.07453512326 0.07768109615 2723.231497 2722.385281
 168.4491613 511.3146326 2708.494898 342.8654713 2211.916864
 171.7024015 169.3628751 168.1741013 150.098729

KEY POINT #2 (t plus 863.2124 s with a Mixing Number of 44.8139): 32.6807584
 0.040894 0.00925 0.3937 0.8499949505 0.853339833
 1.00818448 1 1 27.6033057 99949.3041
 0.0681547526 0.0544380914 0.0429240995 1.64553121e-006 0.0429240995
 48.7418885 130.923766 122.623128 50.7443126 48.6880715
 49.1189473 43.8525311 4.17904386 4.25096942 2.18950736
 0.639169894 0.684030619 0.684030619 3.65170825 1.40882831
 0.0417603234 988.656179 940.976636 1.21198238 1.18398903
 0.000558515788 0.000226696926 1.3046469e-005 1.3371248e-005 1544.07468
 1517.04922 482.932261 488.858548 2.15738425 2.10005754
 2.13705754 0.116004907 0.128147623 2728.4444 2727.68245
 204.252012 514.941273 2709.71935 310.689261 2213.50312
 212.620629 204.025637 205.829326 183.826502

KEY POINT #3 (t plus 1231.6184 s with a Mixing Number of 46.6016): 32.716868
 0.040894 0.00925 0.3937 0.850691483 0.854592475
 1.00848238 1 1 27.290695 99854.8597
 0.0676438943 0.0543455994 0.0429715272 2.25075822e-006 0.0429715272
 51.7815561 131.670552 123.079385 55.7903787 52.3194826
 52.67409 46.7207198 4.17970493 4.25178691 2.19227802
 0.642524488 0.684095728 0.684095728 3.45331433 1.40334508
 0.0418596129 987.279239 940.603309 1.22822066 1.19889148
 0.000530860207 0.000225792683 1.30622038e-005 1.33986829e-005 1547.42652
 1516.34367 483.12816 489.261057 2.18826638 2.13094974
 2.16794974 0.134854788 0.163680226 2729.72339 2728.97861
 216.958526 516.883142 2710.37259 299.924617 2212.84025
 233.716477 219.205479 220.690697 195.813983

KEY POINT #4 (t plus 2954.044 s with a Mixing Number of 57.9211): 33.37585138
 0.040894 0.00925 0.3937 0.8532480159 0.8602631332
 1.007630461 1 1 25.23634313 101276.1001
 0.06511002431 0.05367185635 0.04383705998 4.269703282e-006 0.04383705998
 66.45283314 134.0109917 126.3901786 81.35163822 69.31646446
 64.25081069 56.7564521 4.185657708 4.257878355 2.213042816
 0.6567264215 0.6844976072 0.6844976072 2.704917272 1.364947777
 0.04260056052 979.8315702 937.8676479 1.351384425 1.322660023
 0.0004243994049 0.0002194293518 1.317642005e-005 1.347674392e-005

1557.022434	1511.069028	484.5254664	490.0238924	2.423321546
2.371756258	2.408756258	0.2671392587	0.5007010359	2732.36862
2731.731747	278.3384693	530.9861625	2715.06621	252.6476932
2201.382457	340.7738457	290.3256494	269.1243844	237.7814188
KEY POINT #5 (t plus 5793.2884 s with a Mixing Number of 107.8478): 34.11235112				
0.040894	0.00925	0.3937	0.8497175675	0.8630182943
1.002367204	1	1	19.30114921	102516.8077
0.05920094968	0.05163672361	0.04480440558	-2.770918988e-007	
0.04480440558	98.49738588	138.5053254	136.2612536	115.4003738
99.55306462	79.10375697	60.86295201	4.214252361	4.277780275
2.281999753	0.6772500231	0.6849697532	0.6849697532	1.781643145
1.263622223	0.04503300884	959.5342859	929.4343473	1.778771606
1.767363165	0.0002863183686	0.0002023346097	1.351720083e-005	1.360743198e-005
1546.900173	1493.773399	488.43414	490.1455943	3.248610425
3.200048958	3.237048958	0.9609907668	1.713975674	2734.023852
2733.651318	412.9323082	573.1674781	2728.54909	160.2351699
2160.856374	484.3601303	417.3806177	331.4105876	255.0240284
KEY POINT #6 (t plus 7110.3097 s with a Mixing Number of 147.3186): 33.3599877				
0.040894	0.00925	0.3937	0.838709315	0.854676993
0.998997339	0.998997339	0.999997731	15.9558964	99393.1252
0.0566826981	0.0503765366	0.043816224	4.84494435e-007	0.043816224
111.414024	142.282429	142.282429	129.079417	111.831217
85.1110821	62.6422973	4.23192498	4.29129066	2.32934001
0.681815622	0.68473371	0.68473371	1.5597958	1.21026093
0.0466903822	949.976688	924.086836	2.08869387	2.09078548
0.000251302457	0.000193113569	1.37251232e-005	1.37255301e-005	1533.19981
1482.11198	490.625201	490.603461	3.85459128	3.80724395
3.84424395	1.50320024	2.62901209	2734.48343	2734.22884
467.521238	599.004243	2736.37189	131.483005	2135.47919
542.540031	469.285669	356.670271	262.517738	
KEY POINT #7 (t plus 7719.7385 s with a Mixing Number of 167.2513): 33.0524828				
0.040894	0.00925	0.3937	0.835208479	0.85248605
0.997012214	0.997012214	0.999992707	14.6936239	97799.0762
0.0556916471	0.0498006115	0.0434123358	8.39660351e-007	0.0434123358
116.396253	145.012503	145.012503	133.187222	117.031524
109.39799	63.5500628	4.23974749	4.29778355	2.35212747
0.683045332	0.684498048	0.684498048	1.48855648	1.18791931
0.0474872888	946.093939	921.611333	2.24278278	2.24948741
0.000239814177	0.000189197161	1.38193856e-005	1.38206646e-005	1526.6686
1476.55597	491.569745	491.502462	4.15778018	4.11098529
4.14798529	1.77024594	2.97037429	2733.66715	2733.45125
488.646656	610.747901	2739.81244	122.101245	2122.91925
560.087642	491.33916	459.016078	266.340688	
KEY POINT #8 (t plus 9198.5651 s with a Mixing Number of 222.4009): 31.339967				
0.040894	0.00925	0.3937	0.830598794	0.850836238
0.995288335	0.995288335	0.999986342	11.8089978	91260.2105
0.0535709685	0.0484336709	0.0411630552	5.13564559e-006	0.0411630552
126.884045	151.440702	151.440702	141.690248	127.602321
125.768352	65.7619254	4.25817273	4.3140334	2.4090229
0.684699365	0.683630181	0.683630181	1.35932459	1.13944741
0.0494795821	937.572284	915.656556	2.64176705	2.65423684
0.000218574666	0.00018056435	1.40412678e-005	1.40435421e-005	1510.8241
1462.82701	493.672313	493.556926	4.94772622	4.90229787
4.93929787	2.46008028	3.79123779	2737.84075	2737.7013
533.261502	638.475552	2747.63897	105.214051	2099.3652
596.533164	536.319363	528.51314	275.661192	
KEY POINT #9 (t plus 9306.5423 s with a Mixing Number of 226.0249): 31.8489377				
0.040894	0.00925	0.3937	0.830208997	0.850672155
0.995410686	0.995410686	0.99998653	11.8579833	92632.8756
0.0534183137	0.0483305874	0.0418315558	3.960987e-006	0.0418315558
127.630394	151.922626	151.922626	142.516573	128.276043
126.724289	65.9780009	4.25959031	4.31530828	2.41347066
0.684769566	0.683547546	0.683547546	1.35107332	1.13603328
0.0496356447	936.947969	915.202966	2.6738275	2.68611893
0.000217197858	0.000179948386	1.40578975e-005	1.4060132e-005	1509.59222
1461.76163	493.823047	493.709989	5.01147465	4.96596092
5.00296092	2.51649072	3.87987471	2738.6777	2738.53709

536.444451	640.558792	2748.20976	104.114341	2098.11891
600.082623	539.193878	532.586861	276.570678	
KEY POINT #10 (t plus 9336.144 s with a Mixing Number of 227.6333):	31.930864			
0.040894	0.00925	0.3937	0.830104244	0.85064691
0.995511991	0.995511991	0.999986786	11.8526515	92842.8601
0.0533657316	0.0483037315	0.0419391608	4.6456069e-006	0.0419391608
127.887219	152.048116	152.048116	142.543257	128.410618
126.944755	66.071764	4.26008296	4.31564159	2.41463298
0.68479195	0.683525629	0.683525629	1.34826082	1.13514907
0.0496764382	936.732307	915.08469	2.68222676	2.69428329
0.000216727741	0.000179788675	1.40622276e-005	1.40644176e-005	1509.16392
1461.4834	493.862139	493.751414	5.02818173	4.98272056
5.01972056	2.5361433	3.88276448	2739.04111	2738.90063
537.539618	641.10136	2748.35801	103.561742	2097.93975
600.198208	539.768437	533.526757	276.964446	
KEY POINT #11 (t plus 9336.144 s with a Mixing Number of 227.6333):	31.930864			
0.040894	0.00925	0.3937	0.830104244	0.85064691
0.995511991	0.995511991	0.999986786	11.8526515	92842.8601
0.0533657316	0.0483037315	0.0419391608	4.6456069e-006	0.0419391608
127.887219	152.048116	152.048116	142.543257	128.410618
126.944755	66.071764	4.26008296	4.31564159	2.41463298
0.68479195	0.683525629	0.683525629	1.34826082	1.13514907
0.0496764382	936.732307	915.08469	2.68222676	2.69428329
0.000216727741	0.000179788675	1.40622276e-005	1.40644176e-005	1509.16392
1461.4834	493.862139	493.751414	5.02818173	4.98272056
5.01972056	2.5361433	3.88276448	2739.04111	2738.90063
537.539618	641.10136	2748.35801	103.561742	2097.93975
600.198208	539.768437	533.526757	276.964446	
KEY POINT #12 (t plus 0 s with a Mixing Number of 40.6672):	33.76693435			0.040894
0.00925	0.3937	0.8485546192	0.8509330776	1.006321913
1	1	29.08978363	104078.2906	0.06956789776
0.05461064697	0.04435072261	2.873584963e-006	0.04435072261	40.17477116
128.1872887	121.7707737	40.95337758	40.39381282	40.10855865
35.78166995	4.178287122	4.24945629	2.184389716	0.6289091084
0.683902644	0.683902644	4.32283105	1.419200572	0.04157663592
992.1991288	941.6716776	1.182111113	1.160858486	0.0006506656297
0.0002284045199	1.301707796e-005	1.326756047e-005	1531.796404	
1518.353279	482.5641462	487.1692282	2.100644111	2.043628264
2.080628264	0.07453512326	0.07768109615	2723.231497	2722.385281
168.4491613	511.3146326	2708.494898	342.8654713	2211.916864
171.7024015	169.3628751	168.1741013	150.098729	
KEY POINT #13 (t plus 9336.144 s with a Mixing Number of 227.6333):	31.930864			
0.040894	0.00925	0.3937	0.830104244	0.85064691
0.995511991	0.995511991	0.999986786	11.8526515	92842.8601
0.0533657316	0.0483037315	0.0419391608	4.6456069e-006	0.0419391608
127.887219	152.048116	152.048116	142.543257	128.410618
126.944755	66.071764	4.26008296	4.31564159	2.41463298
0.68479195	0.683525629	0.683525629	1.34826082	1.13514907
0.0496764382	936.732307	915.08469	2.68222676	2.69428329
0.000216727741	0.000179788675	1.40622276e-005	1.40644176e-005	1509.16392
1461.4834	493.862139	493.751414	5.02818173	4.98272056
5.01972056	2.5361433	3.88276448	2739.04111	2738.90063
537.539618	641.10136	2748.35801	103.561742	2097.93975
600.198208	539.768437	533.526757	276.964446	
KEY POINT #14 (t plus 3487.1534 s with a Mixing Number of 62.9271):	33.59573585			
0.040894	0.00925	0.3937	0.853087058	0.8611924652
1.006902591	1	1	24.32605045	101791.6099
0.06422432382	0.05337635945	0.04412586425	4.462237049e-006	0.04412586425
71.43539144	134.6822165	127.8353201	89.98507493	75.11532501
67.55597884	57.87352082	4.188702783	4.26062655	2.222474032
0.6608319386	0.6846343461	0.6846343461	2.510844745	1.348925204
0.04293546128	977.0210177	936.6588916	1.408172695	1.381199685
0.0003961241669	0.0002167569756	1.322629242e-005	1.349682968e-005	
1558.029679	1508.682305	485.1219343	490.0944751	2.532161907
2.481098945	2.518098945	0.3318913955	0.7014258766	2732.727755
2732.135999	299.2100883	537.1488235	2717.088765	237.9387352
2195.578932	377.0462199	314.6275604	282.9666881	242.4615249

End

D.10 TEST #10 - T10_RCIC_10PSIG_157KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T10_RCIC_10PSIG_157kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1972.1408 s, and ending (KEY POINT #11) at t plus 8424.3438 s, for a time period of 6452.203 s.
Original Data Record Time: 10330.6779 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 1916.9306 s, T_bulk = 66.152 C and T_out = 63.0554 C
Stratification Beginning SP12 Temperature = 65.9766 C
Stratification Beginning Pressure = 29.2395 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 6423.3044 s, T_bulk = 132.5826 C and T_out = 78.5434 C
Stratification Ending SP12 Temperature = 133.7023 C
Stratification Ending Pressure = 74.314 psia
Plume detected! Setting t_plume (KEY POINT #2) to 1165.6177 s.
At t = 1165.6177 s, the pool pressure is 27.5849 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 55.863, 55.8709, 57.8771, 55.3824, and 52.4329 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 10.9224 +/- 2.9501 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 9.9327 +/- 2.6307 C.
Minimum Steam Quality: 0.98553 at t plus 0.50003 s
Maximum Steam Quality: 1.0025 at t plus 3712.3603 s
Time-Averaged Steam Quality: 0.99903 +/- 0.0016174
Minimum Turbine Outlet Steam Quality: 0.99869 at t plus 6360.4018 s
Maximum Turbine Outlet Steam Quality: 1.0206 at t plus 1419.2222 s
Time-Averaged Turbine Outlet Steam Quality: 1.0127 +/- 0.005388
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 6362.2019 s; using 300 s smoothing
Max and min smoothed upper level changerates: 1.3845 degrees/min at t plus 3065.2483 s and 0.66302 degrees/min at t plus 6279.0011 s, respectively
Max and min smoothed mid (SP9) level changerates: 1.2455 degrees/min at t plus 3279.2766 s and 0.64553 degrees/min at t plus 42.3004 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.57573 degrees/min at t plus 3021.6488 s and -0.24031 degrees/min at t plus 3293.5524 s, respectively
Max and min smoothed lower level changerates: 3.9956 degrees/min at t plus 6080.9978 s and 0.10504 degrees/min at t plus 3136.4504 s, respectively
Max and min smoothed mid-lower level changerate differences: 1.0207 degrees/min at t plus 3255.2522 s and -3.2352 degrees/min at t plus 6080.9978 s, respectively
Max and min smoothed outlet level changerates: 1.2034 degrees/min at t plus 922.8158 s and -0.055276 degrees/min at t plus 4047.0655 s, respectively
Max and min smoothed lower-outlet level changerate differences: 3.9659 degrees/min at t plus 6080.9978 s and -0.34609 degrees/min at t plus 3136.3504 s, respectively
Max and min smoothed hot (SP8) level changerates: 1.8571 degrees/min at t plus 1997.0322 s and 0.30683 degrees/min at t plus 3022.8479 s, respectively
Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 1.0434 degrees/min at t plus 1996.9562 s and -0.51214 degrees/min at t plus 3110.5499 s, respectively
The mean steam flow rate was 65.4446 +/- 3.2311 g/s
The mean feedwater flow rate was 64.2034 +/- 8.469 g/s
The mean water injection to steam flow rate was 0.0020395 +/- 0.038746 g/s
Mean Smoothed Condensing Region SP8-SP9 delta T is 12.0158 +/- 1.1432 C over the Stratification Period, beginning at 8.0814 C and ending at 9.9239 C
Mean Smoothed SP8-Upper Pool delta T is 10.8785 +/- 1.197 C over the Stratification Period, beginning at 7.4879 C and ending at 9.3168 C
The stratification period begins and ends with Smoothed SP8 readings of 74.1375 and 143.6922 C, respectively
The stratification period begins and ends with condensing flows of 0.6247 and 1.7129 kg/s, respectively.

The stratification period begins and ends with condensing+cooling flows of 4.652 and 3.3957 kg/s, respectively.

The stratification period had a mean sparger steam enthalpy of 2749.7712 +/- 1.412 kJ/kg. At plume detection, the condensing and condensing+cooling flows are 0.54326 and 19.2421 kg/s, respectively

The plume period had a mean steam enthalpy of 2750.1193 +/- 1.3926 kJ/kg.

Maximum Smoothed Top-Mid delta T is 2.861 degrees C at t plus 3209.1506 s with T_upper = 86.2736 C and T_mid = 83.4126 C

At t plus 3209.1506 s, Smoothed SP8-SP9 is 11.7256 C and Smoothed SP8-Top is 8.8646 C, where Smoothed SP8 is 95.1382 C and Pool P = 34.6579 psia

Maximum Smoothed Top-Lower delta T is 27.5226 degrees C at t plus 5602.6905 s with T_upper = 124.1762 C and T_low = 96.6537 C

At t plus 5602.6905 s, Smoothed SP8-SP9 is 11.1787 C and Smoothed SP8-Top is 10.0628 C, where Smoothed SP8 is 134.239 C and Pool P = 60.8373 psia

Maximum Smoothed Mid-Lower delta T is 26.5378 degrees C at t plus 5625.3898 s with T_mid = 123.3843 C and T_low = 96.8465 C

At t plus 5625.3898 s, Smoothed SP8-SP9 is 10.939 C and Smoothed SP8-Top is 10.0063 C, where Smoothed SP8 is 134.3233 C and Pool P = 61.2028 psia

Maximum Smoothed Top-Outlet delta T is 56.2813 degrees C at t plus 6452.203 s with T_upper = 134.8783 C and T_out = 78.597 C

At t plus 6452.203 s, Smoothed SP8-SP9 is 10.0443 C and Smoothed SP8-Top is 9.2832 C, where Smoothed SP8 is 144.1615 C and Pool P = 74.7639 psia

Maximum Smoothed Mid-Outlet delta T is 55.5202 degrees C at t plus 6452.203 s with T_mid = 134.1172 C and T_out = 78.597 C

At t plus 6452.203 s, Smoothed SP8-SP9 is 10.0443 C and Smoothed SP8-Top is 9.2832 C, where Smoothed SP8 is 144.1615 C and Pool P = 74.7639 psia

Maximum Smoothed Lower-Outlet delta T is 52.1101 degrees C at t plus 6452.203 s with T_low = 130.707 C and T_out = 78.597 C

At t plus 6452.203 s, Smoothed SP8-SP9 is 10.0443 C and Smoothed SP8-Top is 9.2832 C, where Smoothed SP8 is 144.1615 C and Pool P = 74.7639 psia

Maximum Smoothed Condensing Region SP8-SP9 delta T is 15.0367 degrees C at (KEY POINT #14) t plus 2719.0435 s with T_SP8 = 91.8245 C and T_SP9 = 76.7878 C and Pool P = 32.01 psia

Maximum Smoothed Condensing Region SP8-Upper delta T is 14.0666 degrees C at t plus 2719.0435 s with T_SP8 = 91.8245 C and T_upper = 77.7579 C and Pool P = 32.01 psia

Maximum Top-Mid delta T is 3.9524 degrees C at (KEY POINT #4) t plus 3144.4509 s ignoring SP 4, with temperatures of 85.8823 and 81.9299 C, respectively, at Set # 2, where Pool P = 34.2614 psia and T_outlet = 75.1862 C

Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 3931.4639 s with a Smoothed Mid-Axis Top-Mid Delta T of 1.3172 C and a raw SP12 Reading of 96.3293 C.

Maximum Top-Lower delta T is 32.341 degrees C at t plus 5791.0942 s, with temperatures of 126.8237 and 94.4827 C, respectively, at Set # 1, where Pool P = 63.8087 psia and T_outlet = 78.2266 C

Maximum Mid-Low delta T is 28.9671 degrees C at (KEY POINT #6) t plus 5714.7929 s ignoring SP 4, with temperatures of 124.5781 and 95.611 C, respectively, at Set # 2, where Pool P = 62.5867 psia and T_outlet = 78.0357 C

Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 6203.1998 s with a Smoothed Mid-Axis Mid-Low Delta T of 9.6535 C and a raw SP12 Reading of 131.1013 C.

Maximum Top-Outlet delta T is 56.636 degrees C at t plus 6434.803 s, with temperatures of 135.1033 and 78.4673 C, respectively, at Set # 1, where Pool P = 74.4924 psia

Maximum Mid-Outlet delta T is 55.4838 degrees C at t plus 6437.1032 s ignoring SP 4, with temperatures of 133.896 and 78.4122 C, respectively, at Set # 2, where Pool P = 74.525 psia

Maximum Lower-Outlet delta T is 54.9649 degrees C at (KEY POINT #8) t plus 6450.903 s, with temperatures of 133.5889 and 78.624 C, respectively, at Set # 3, where Pool P = 74.7499 psia

Low-Outlet Reconvergence NOT Detected, setting t to (KEY POINT #10) t plus 6452.203 s with a Smoothed Mid-Axis Low-Outlet Delta T of 52.1669 C and a raw SP12 Reading of 134.0296 C.

Minimum SP Pressure is 25.9227 psia at t plus 0 s

Maximum SP Pressure is 74.7675 psia at t plus 6451.904 s

Beginning SP Pressure is 25.9227 psia

Ending SP Pressure is 74.7639 psia

Time-Average SP Pressure is 40.3044 +/- 14.1225 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 80.1156 cm (cold) / 80.2746 cm (hot) at 24.665 psia

Beginning Smoothed SP Level is 81.0583 cm (cold) / 81.2619 cm (hot) at 25.9319 psia
 Ending Smoothed SP Level is 81.0978 cm (cold) / 83.2189 cm (hot) at 74.7735 psia
 Minimum Smoothed Cold SP Level is 81.0583 cm at t plus 0 s and 25.9319 psia
 Minimum Smoothed Hot SP Level is 81.2619 cm at t plus 0 s and 25.9319 psia
 Maximum Smoothed Cold SP Level is 83.1427 cm at t plus 3236.4521 s and 34.8253 psia
 Maximum Smoothed Hot SP Level is 84.3811 cm at t plus 4253.4953 s and 43.0168 psia
 SP 12 Temperature at the beginning is 39.7463 C, and at the end is 134.0296 C

At plume detection, the Mixing Number is 46.2584

The Mixing Number ranges from a minimum of 38.6305 at (KEY POINT #12) t plus 2.5011 s to a maximum of 252.9774 at (KEY POINT #13) t plus 6452.203 s; it had a mean value of 99.0716 +/- 60.5542 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 41.1958): 257.3335301 0.040894
 0.00925 0.3937 0.8105830862 0.8126194415 0.9838296021
 0.9838296021 0.999981729 241.0381455 816781.0739 0.0695738875
 0.05541243958 0.3379912399 4.038358636e-006 0.3379912399 40.1379383
 117.7902705 117.7902705 40.70699012 40.11092407 40.05886316
 36.43836618 4.178350449 4.242628517 2.161482433 0.628849109
 0.6831949643 0.6831949643 4.32628639 1.469952462 0.04074923736
 992.2023808 944.8762526 1.050373147 1.067617759 0.000651113729
 0.0002367080021 1.287989823e-005 1.288398779e-005 1531.692757
 1524.198641 480.8083173 480.5581457 1.851544355 1.787944945
 1.824944945 0.07438906537 0.0766734004 2725.097645 2666.998257
 168.2726106 494.3958618 2702.707536 326.1232512 2230.701783
 170.6503075 168.1582294 167.943802 152.819856

KEY POINT #2 (t plus 1165.6177 s with a Mixing Number of 46.2584): 49.1132336
 0.040894 0.00925 0.3937 0.8205645728 0.824634847
 1.017625724 1 1 46.11465092 146958.3118
 0.06694890457 0.05497971799 0.0645071115 2.709577341e-006 0.0645071115
 55.87090261 138.1830239 119.9426414 57.87708811 55.86297469
 55.38237326 52.43291771 4.180971248 4.24627207 2.173667669
 0.6467949388 0.6836002001 0.6836002001 3.213067018 1.442026556
 0.04119047656 985.3226842 943.1519023 1.120045228 1.065069248
 0.0004970604584 0.0002321494304 1.295405844e-005 1.366670963e-005
 1551.115574 1521.088247 481.7652195 494.3649894 1.983047923
 1.901624553 1.938624553 0.1643092829 0.1806620894 2746.794799
 2744.668238 234.0336685 503.5407506 2705.850927 269.5070821
 2243.254048 242.4221823 233.9990787 231.992713 219.6668265

KEY POINT #3 (t plus 1916.9306 s with a Mixing Number of 53.4326): 49.20223294
 0.040894 0.00925 0.3937 0.8253830445 0.8311087707
 1.017533227 1 1 43.92808279 146663.826
 0.06517999864 0.05463916443 0.06462400649 1.504310264e-006 0.06462400649
 66.05614466 139.6641609 121.6297645 74.13754097 66.64960553
 65.81865718 63.07675956 4.18551385 4.249207722 2.183550381

0.6563662249	0.6838806746	0.6838806746	2.721559526	1.420932861
0.04154647237	980.035506	941.7863618	1.177227158	1.120089363
0.0004267910264	0.0002286893433	1.301221616e-005	1.371896649e-005	
1556.835112	1518.567251	482.5029778	494.9959654	2.091375776
2.016286841	2.053286841	0.2624803447	0.3722368402	2748.752112
2746.822436	276.6487359	510.7147904	2708.29182	234.0660545
2238.037322	310.4935079	279.13137	275.6562331	264.1861035
KEY POINT #4 (t plus 3144.4509 s with a Mixing Number of 70.9155): 50.87332857				
0.040894	0.00925	0.3937	0.8313617057	0.8407891344
1.01539176	1	1	39.21006123	150840.509
0.06223235455	0.053655728	0.06681888441	-4.914349453e-007	
0.06681888441	82.39601961	141.9854557	126.4691629	94.07735194
85.08668145	80.13992228	75.09412564	4.197296317	4.25802714
2.213552472	0.6686282908	0.6845056858	0.6845056858	2.159805289
1.364060771	0.04261868221	970.3591151	937.8018131	1.354439727
1.297446441	0.0003440564616	0.000219281682	1.317914559e-005	1.379214319e-005
1556.626537	1510.939897	484.5582786	495.4662667	2.429170194
2.363198391	2.400198391	0.5220629254	0.8177588869	2750.327959
2748.790531	345.156262	531.3228751	2715.177169	186.1666131
2219.005084	394.2529497	356.4517461	335.6904219	314.5356505
KEY POINT #5 (t plus 3931.4639 s with a Mixing Number of 94.5454): 52.79563695				
0.040894	0.00925	0.3937	0.8306661632	0.8427682819
1.012922759	1	1	35.14669514	155809.0478
0.05959657143	0.05264387607	0.06934371432	1.094732897e-006	0.06934371432
96.43217726	144.1397939	131.3998553	108.9569306	97.8740747
84.57606543	77.27605605	4.211847223	4.267643702	2.246705244
0.6763105373	0.6848719841	0.6848719841	1.823029717	1.311207577
0.04379217078	960.9764841	933.6394181	1.556493023	1.502174535
0.0002927300403	0.0002104227526	1.334933942e-005	1.385686395e-005	
1548.556602	1502.579991	486.5578233	495.6872556	2.817684379
2.75408574	2.79108574	0.8916775873	1.384245073	2751.280435
2750.045145	404.1977432	552.3677171	2722.007414	148.1699739
2198.912718	457.0506856	410.2707583	354.3408568	323.7139194
KEY POINT #6 (t plus 5714.7929 s with a Mixing Number of 195.0669): 50.64139732				
0.040894	0.00925	0.3937	0.8143423413	0.8327188869
1.004119071	1	1	21.78800405	147558.2536
0.05402257286	0.04941850634	0.06651425745	2.978211043e-006	0.06651425745
124.6695233	150.548969	146.8165806	135.7664646	125.6489051
98.83053988	78.09219538	4.254158455	4.302205246	2.367637153
0.6844298253	0.68429867	0.68429867	1.384521688	1.17374697
0.04802983535	939.390677	919.9580091	2.349513506	2.324382936
0.0002227486227	0.0001866934385	1.388166781e-005	1.403465582e-005	
1514.304701	1472.794005	492.1770741	495.1169771	4.368440455
4.315326961	4.352326961	2.298725171	3.202457234	2751.270067
2750.79535	523.7958379	618.5186749	2742.048379	94.72283707
2132.751392	571.1240105	527.9619841	414.4217996	327.2610664
KEY POINT #7 (t plus 6203.1998 s with a Mixing Number of 233.173): 50.56742029				
0.040894	0.00925	0.3937	0.8123511693	0.8326517055
1.002155027	1	1	19.36275597	146537.7098
0.0527093552	0.04848393899	0.06641709332	4.412215866e-006	0.06641709332
131.0822197	153.1033332	151.2055536	141.5771159	131.8442462
122.9422286	78.30448987	4.266452192	4.313414281	2.406861873
0.6849880612	0.683669616	0.683669616	1.314393552	1.141123993
0.04940377733	934.0087767	915.8775158	2.626235757	2.611755251
0.0002110287073	0.0001808664207	1.403315323e-005	1.411175382e-005	
1503.621234	1463.345031	493.5984149	495.143807	4.916857548
4.865317528	4.902317528	2.791227949	3.779230508	2752.281449
2751.906532	551.1526357	637.4592949	2747.359641	86.3066592
2114.822154	596.0455124	554.4032111	516.489923	328.1952522
KEY POINT #8 (t plus 6450.903 s with a Mixing Number of 252.8339): 51.14267371				
0.040894	0.00925	0.3937	0.8109885354	0.8321955778
1.001374747	1	1	18.52145709	147730.5167
0.0520856965	0.04802346033	0.06717265214	2.925668418e-006	0.06717265214
134.0996809	154.5479284	153.3561834	144.1102798	134.8586189
130.6840064	78.5953019	4.272620604	4.319148973	2.426850764
0.6850927627	0.6832873392	0.6832873392	1.284183636	1.126049382
0.05010550744	931.4161109	913.8477628	2.771043231	2.76138648

0.0002059122483	0.0001781404835	1.41073606e-005	1.415705126e-005	
1498.255113	1458.56305	494.2657226	495.2520296	5.204999524
5.153982016	5.190982016	3.050867162	4.055535615	2753.128484
2752.785439	564.0549508	646.7595487	2749.894162	82.7045979
2106.368935	606.9369943	567.297062	549.474537	329.4377951
KEY POINT #9 (t plus 6423.3044 s with a Mixing Number of 250.3901): 51.16210873				
0.040894	0.00925	0.3937	0.8112077353	0.8323074586
1.001539273	1	1	18.64275535	147806.5434
0.05215435689	0.04807266997	0.0671981788	4.572812691e-006	0.0671981788
133.7683343	154.464291	153.1267197	143.6922164	134.3754158
130.0756522	78.53382515	4.271930547	4.318529308	2.42469403
0.6850862333	0.6833304363	0.6833304363	1.287419313	1.127630339
0.05002972968	931.7027597	914.065282	2.7552949	2.744529408
0.0002064624502	0.0001784274406	1.409944372e-005	1.415514649e-005	
1498.855055	1459.077992	494.1954396	495.2998064	5.17362747
5.122445185	5.159445185	3.021435686	4.008849231	2753.211876
2752.864324	562.6372597	645.7666301	2749.62591	83.12937042
2107.445246	605.1395057	565.2299081	546.8778219	329.1774789
KEY POINT #10 (t plus 6452.203 s with a Mixing Number of 252.9774): 51.13763826				
0.040894	0.00925	0.3937	0.8109780487	0.832189445
1.001377363	1	1	18.51524771	147711.4225
0.05208206345	0.04802132927	0.0671660384	3.141450903e-006	0.0671660384
134.1172077	154.5600938	153.3661185	144.1615285	134.8782838
130.7070469	78.59696661	4.272657249	4.319175845	2.426944274
0.6850930617	0.6832854607	0.6832854607	1.284013007	1.125981078
0.05010879331	931.4009179	913.8383397	2.771726713	2.762049465
0.000205883213	0.0001781280798	1.410770338e-005	1.415748724e-005	
1498.223257	1458.540729	494.2687607	495.256942	5.206361271
5.155452495	5.192452495	3.052430398	4.061288672	2753.145316
2752.802502	564.1299337	646.8025425	2749.905765	82.67260879
2106.342774	607.1572176	567.3812115	549.5729167	329.4448934
KEY POINT #11 (t plus 6452.203 s with a Mixing Number of 252.9774): 51.13763826				
0.040894	0.00925	0.3937	0.8109780487	0.832189445
1.001377363	1	1	18.51524771	147711.4225
0.05208206345	0.04802132927	0.0671660384	3.141450903e-006	0.0671660384
134.1172077	154.5600938	153.3661185	144.1615285	134.8782838
130.7070469	78.59696661	4.272657249	4.319175845	2.426944274
0.6850930617	0.6832854607	0.6832854607	1.284013007	1.125981078
0.05010879331	931.4009179	913.8383397	2.771726713	2.762049465
0.000205883213	0.0001781280798	1.410770338e-005	1.415748724e-005	
1498.223257	1458.540729	494.2687607	495.256942	5.206361271
5.155452495	5.192452495	3.052430398	4.061288672	2753.145316
2752.802502	564.1299337	646.8025425	2749.905765	82.67260879
2106.342774	607.1572176	567.3812115	549.5729167	329.4448934
KEY POINT #12 (t plus 2.5011 s with a Mixing Number of 38.6305): 39.40112862				
0.040894	0.00925	0.3937	0.8105904393	0.8126271725
1.009952704	1	1	38.61207197	121336.5071
0.0695674414	0.05541210227	0.05175087876	3.57555551e-006	0.05175087876
40.17757731	128.0891226	117.7919521	40.73250617	40.13704332
40.10490675	36.44859844	4.178350003	4.24263132	2.16149177
0.6288994247	0.6831953017	0.6831953017	4.322730487	1.469930186
0.04074957652	992.1872013	944.8749132	1.050426178	1.020505995
0.0006506306831	0.0002367043755	1.287995615e-005	1.327934842e-005	
1531.759797	1524.196257	480.8090717	488.053821	1.851644238
1.78806451	1.82506451	0.07454626102	0.07677723164	2726.179522
2724.68863	168.4382468	494.4030033	2702.710004	325.9647565
2231.776518	170.756933	168.2673755	168.1361986	152.8626227
KEY POINT #13 (t plus 6452.203 s with a Mixing Number of 252.9774): 51.13763826				
0.040894	0.00925	0.3937	0.8109780487	0.832189445
1.001377363	1	1	18.51524771	147711.4225
0.05208206345	0.04802132927	0.0671660384	3.141450903e-006	0.0671660384
134.1172077	154.5600938	153.3661185	144.1615285	134.8782838
130.7070469	78.59696661	4.272657249	4.319175845	2.426944274
0.6850930617	0.6832854607	0.6832854607	1.284013007	1.125981078
0.05010879331	931.4009179	913.8383397	2.771726713	2.762049465
0.000205883213	0.0001781280798	1.410770338e-005	1.415748724e-005	
1498.223257	1458.540729	494.2687607	495.256942	5.206361271

5.155452495	5.192452495	3.052430398	4.061288672	2753.145316
2752.802502	564.1299337	646.8025425	2749.905765	82.67260879
2106.342774	607.1572176	567.3812115	549.5729167	329.4448934
KEY POINT #14 (t plus 2719.0435 s with a Mixing Number of 63.8539): 50.35810645				
0.040894	0.00925	0.3937	0.8300810069	0.837959011
1.016525651	1	1	41.39879462	149576.2235
0.06325900197	0.0540880934	0.0661421729	-7.132868137e-008	
0.0661421729	76.78777623	141.1606023	124.3474068	91.82445469
77.757858	77.16956636	71.59102345	4.192634712	4.254086628
2.200093324	0.6648331172	0.6842642768	0.6842642768	2.327823526
1.388353817	0.0421391175	973.8366231	939.5610909	1.274273454
1.216413488	0.0003691268802	0.0002233148978	1.310594076e-005	1.376785933e-005
1557.891245	1514.355551	483.6683652	495.4015744	2.275990406
2.207587238	2.244587238	0.4157471496	0.7518799169	2750.083318
2748.369458	321.6177763	522.2820334	2712.179969	200.6642571
2227.801285	384.760959	325.683984	323.2199838	299.8448517

End

D.11 TEST #11 -

T11_RCIC_040GPM_15PSIG_107KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T11_RCIC_040GPM_15PSIG_107kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1720.5394 s, and ending (KEY POINT #11) at t plus 13127.1358 s, for a time period of 11406.5964 s.
Original Data Record Time: 14133.5534 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 474.7432 s, T_{bulk} = 44.7957 C and T_{out} = 41.8025 C
Stratification Beginning SP12 Temperature = 44.8096 C
Stratification Beginning Pressure = 30.6351 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 10855.9869 s, T_{bulk} = 142.6046 C and T_{out} = 79.3774 C
Stratification Ending SP12 Temperature = 142.3466 C
Stratification Ending Pressure = 93.9264 psia
Plume detected! Setting t_{plume} (KEY POINT #2) to 63.4006 s.
At t = 63.4006 s, the pool pressure is 30.255 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 41.9098, 41.9583, 43.9636, 42.6139, and 37.9249 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 14.4716 +/- 3.928 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 13.1285 +/- 3.7928 C.
Minimum Steam Quality: 0.48095 at t plus 173.7019 s
Maximum Steam Quality: 0.64477 at t plus 10597.7832 s
Time-Averaged Steam Quality: 0.573 +/- 0.018701
Minimum Turbine Outlet Steam Quality: 0.50262 at t plus 173.7019 s
Maximum Turbine Outlet Steam Quality: 0.6546 at t plus 5559.395 s
Time-Averaged Turbine Outlet Steam Quality: 0.58546 +/- 0.017517
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 11316.5953 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.78977 degrees/min at t plus 2178.7366 s and 0.35376 degrees/min at t plus 10039.4732 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.85454 degrees/min at t plus 4461.7762 s and 0.37284 degrees/min at t plus 121.4019 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.31384 degrees/min at t plus 2313.3383 s and -0.24154 degrees/min at t plus 4372.2751 s, respectively
Max and min smoothed lower level changerates: 3.2834 degrees/min at t plus 7374.3268 s and -0.465 degrees/min at t plus 1461.9236 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.98842 degrees/min at t plus 1461.9236 s and -2.7773 degrees/min at t plus 7374.3268 s, respectively
Max and min smoothed outlet level changerates: 1.5524 degrees/min at t plus 11223.794 s and 0.01224 degrees/min at t plus 2811.0468 s, respectively

Max and min smoothed lower-outlet level changerate differences: 3.1244 degrees/min at t plus 7374.3268 s and -1.1057 degrees/min at t plus 11312.095 s, respectively
 Max and min smoothed hot (SP8) level changerates: 1.6029 degrees/min at t plus 2539.8443 s and 0.064231 degrees/min at t plus 2336.1386 s, respectively
 Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 1.0535 degrees/min at t plus 2539.8443 s and -0.48684 degrees/min at t plus 4821.6818 s, respectively
 The mean steam flow rate was 43.6958 +/- 1.0217 g/s
 The mean feedwater flow rate was 43.0951 +/- 1.8745 g/s
 The mean water injection to steam flow rate was 24.8662 +/- 1.5428 g/s
 Mean Smoothed Condensing Region SP8-SP9 delta T is 14.9345 +/- 3.2237 C over the Stratification Period, beginning at 4.2025 C and ending at 12.4052 C
 Mean Smoothed SP8-Upper Pool delta T is 13.5533 +/- 3.193 C over the Stratification Period, beginning at 4.0696 C and ending at 11.5742 C
 The stratification period begins and ends with Smoothed SP8 readings of 50.0135 and 154.9343 C, respectively
 The stratification period begins and ends with condensing flows of 0.26462 and 1.0086 kg/s, respectively.
 The stratification period begins and ends with condensing+cooling flows of 6.028 and 1.6314 kg/s, respectively.
 The stratification period had a mean sparger steam enthalpy of 1842.6926 +/- 31.658 kJ/kg.
 At plume detection, the condensing and condensing+cooling flows are 0.25075 and 12.7902 kg/s, respectively
 The plume period had a mean steam enthalpy of 1839.1216 +/- 36.3323 kJ/kg.
 Maximum Smoothed Top-Mid delta T is 4.2898 degrees C at t plus 3193.6537 s with T_upper = 74.4347 C and T_mid = 70.1449 C
 At t plus 3193.6537 s, Smoothed SP8-SP9 is 16.9027 C and Smoothed SP8-Top is 12.6129 C, where Smoothed SP8 is 87.0476 C and Pool P = 36.1484 psia
 Maximum Smoothed Top-Lower delta T is 27.8172 degrees C at t plus 6776.0996 s with T_upper = 111.4737 C and T_low = 83.6565 C
 At t plus 6776.0996 s, Smoothed SP8-SP9 is 17.4617 C and Smoothed SP8-Top is 16.8828 C, where Smoothed SP8 is 128.3566 C and Pool P = 55.1412 psia
 Maximum Smoothed Mid-Lower delta T is 27.2384 degrees C at t plus 6776.0996 s with T_mid = 110.8949 C and T_low = 83.6565 C
 At t plus 6776.0996 s, Smoothed SP8-SP9 is 17.4617 C and Smoothed SP8-Top is 16.8828 C, where Smoothed SP8 is 128.3566 C and Pool P = 55.1412 psia
 Maximum Smoothed Top-Outlet delta T is 64.9496 degrees C at t plus 10477.7813 s with T_upper = 140.3277 C and T_out = 75.378 C
 At t plus 10477.7813 s, Smoothed SP8-SP9 is 12.4129 C and Smoothed SP8-Top is 11.7965 C, where Smoothed SP8 is 152.1242 C and Pool P = 89.2598 psia
 Maximum Smoothed Mid-Outlet delta T is 64.3334 degrees C at t plus 10478.5813 s with T_mid = 139.7161 C and T_out = 75.3826 C
 At t plus 10478.5813 s, Smoothed SP8-SP9 is 12.4223 C and Smoothed SP8-Top is 11.8063 C, where Smoothed SP8 is 152.1383 C and Pool P = 89.271 psia
 Maximum Smoothed Lower-Outlet delta T is 63.9533 degrees C at t plus 10466.6817 s with T_low = 139.3108 C and T_out = 75.3575 C
 At t plus 10466.6817 s, Smoothed SP8-SP9 is 12.6062 C and Smoothed SP8-Top is 11.9386 C, where Smoothed SP8 is 152.2335 C and Pool P = 89.1229 psia
 Maximum Smoothed Condensing Region SP8-SP9 delta T is 19.116 degrees C at (KEY POINT #14) t plus 3728.6633 s with T_SP8 = 95.6193 C and T_SP9 = 76.5034 C and Pool P = 37.9149 psia
 Maximum Smoothed Condensing Region SP8-Upper delta T is 18.1473 degrees C at t plus 5969.2014 s with T_SP8 = 121.7678 C and T_upper = 103.6205 C and Pool P = 49.3167 psia
 Maximum Top-Mid delta T is 5.5814 degrees C at (KEY POINT #4) t plus 3224.7534 s ignoring SP 4, with temperatures of 75.834 and 70.2526 C, respectively, at Set # 2, where Pool P = 36.2443 psia and T_outlet = 53.0573 C
 Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 5152.1887 s with a Smoothed Mid-Axis Top-Mid Delta T of 1.8604 C and a raw SP12 Reading of 93.3204 C.
 Maximum Top-Lower delta T is 30.3173 degrees C at t plus 6783.017 s, with temperatures of 111.5853 and 81.268 C, respectively, at Set # 1, where Pool P = 55.1801 psia and T_outlet = 62.5785 C
 Maximum Mid-Low delta T is 28.9055 degrees C at (KEY POINT #6) t plus 7006.5198 s ignoring SP 4, with temperatures of 112.8796 and 83.9741 C, respectively, at Set # 2, where Pool P = 56.878 psia and T_outlet = 63.3334 C
 Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 7583.1307 s with a Smoothed Mid-Axis Mid-Low Delta T of 9.6295 C and a raw SP12 Reading of 117.6405 C.

Maximum Top-Outlet delta T is 65.3332 degrees C at t plus 10472.581 s, with temperatures of 140.7526 and 75.4194 C, respectively, at Set # 1, where Pool P = 89.1915 psia
 Maximum Mid-Outlet delta T is 64.3771 degrees C at t plus 10500.7806 s ignoring SP 4, with temperatures of 139.7928 and 75.4157 C, respectively, at Set # 2, where Pool P = 89.5158 psia
 Maximum Lower-Outlet delta T is 65.1433 degrees C at (KEY POINT #8) t plus 10246.2761 s, with temperatures of 139.0592 and 73.9158 C, respectively, at Set # 1, where Pool P = 86.599 psia
 Low-Outlet Reconvergence NOT Detected, setting t to (KEY POINT #10) t plus 11406.5964 s with a Smoothed Mid-Axis Low-Outlet Delta T of 54.392 C and a raw SP12 Reading of 146.2414 C.

Minimum SP Pressure is 30.2004 psia at t plus 0.72404 s
 Maximum SP Pressure is 100.6833 psia at t plus 11406.5964 s
 Beginning SP Pressure is 30.2119 psia
 Ending SP Pressure is 100.6833 psia

Time-Average SP Pressure is 53.757 +/- 20.796 psia
 SP Levels are fully corrected and compensated

Pre-Start SP Level is 82.4117 cm (cold) / 82.5908 cm (hot) at 29.1824 psia
 Beginning Smoothed SP Level is 82.9202 cm (cold) / 83.1472 cm (hot) at 30.2062 psia
 Ending Smoothed SP Level is 80.5492 cm (cold) / 83.0359 cm (hot) at 100.6793 psia
 Minimum Smoothed Cold SP Level is 80.5491 cm at t plus 11406.0984 s and 100.6731 psia
 Minimum Smoothed Hot SP Level is 83.0307 cm at t plus 11373.0965 s and 100.2564 psia
 Maximum Smoothed Cold SP Level is 83.3973 cm at t plus 2763.147 s and 34.9134 psia
 Maximum Smoothed Hot SP Level is 84.4218 cm at t plus 5168.8306 s and 44.3343 psia
 SP 12 Temperature at the beginning is 40.068 C, and at the end is 146.2414 C

At plume detection, the Mixing Number is 41.7762

The Mixing Number ranges from a minimum of 41.5283 at (KEY POINT #12) t plus 0 s to a maximum of 385.9168 at (KEY POINT #13) t plus 11406.5964 s; it had a mean value of 146.4924 +/- 98.3745 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 41.5283): 51.93560575 0.040894
 0.00925 0.3937 0.8292021165 0.8314723941 0.5678812083
 0.5678812083 0.9990263334 24.49114808 160309.6877 0.06936023809
 0.05447575745 0.04253736055 0.02567675743 0.06821411798 41.44894025
 122.4372006 122.4372006 43.20682017 41.18381806 42.35866673
 37.28460024 4.178284794 4.250637801 2.188384554 0.6305141057
 0.6840034086 0.6840034086 4.210964235 1.411076474 0.04172005549
 991.706868 941.1285134 1.205415076 2.120586817 0.0006354455189
 0.0002270673634 1.304005738e-005 1.324844863e-005 1533.905345
 1517.335238 482.8522016 470.7387834 2.144901972 2.082642456
 2.119642456 0.07974254461 0.08744027887 1761.420997 1760.821181
 173.7764499 514.1500638 2709.452706 340.3736138 1247.270934
 181.1214253 172.6671929 177.5791424 156.3821675

KEY POINT #2 (t plus 63.4006 s with a Mixing Number of 41.7762): 52.61513672

0.040894	0.00925	0.3937	0.8292696849	0.8315887113
0.5559115839	0.5559115839	0.9989765036	24.25836821	162258.9805
0.06927697149	0.05446677636	0.04234170292	0.02676493581	0.06910663873
41.95833511	122.4815396	122.4815396	43.96357087	41.90983264
42.61393157	37.92485553	4.178297667	4.250716806	2.188651986
0.6311474355	0.6840099333	0.6840099333	4.167536662	1.410539619
0.04172964823	991.5060769	941.0923079	1.206978599	2.168947897
0.0006295219457	0.0002269789203	1.304158637e-005	1.326055047e-005	
1534.718463	1517.267109	482.871306	470.1628244	2.14787332
2.085970308	2.122970308	0.08191054673	0.09094621882	1735.251852
1734.663384	175.9051431	514.3387413	2709.516316	338.4335981
1220.913111	184.2837109	175.7009867	178.6460119	159.0576867

KEY POINT #3 (t plus 474.7432 s with a Mixing Number of 43.7712): 51.33043566

0.040894	0.00925	0.3937	0.830087817	0.8328879139
0.5758816793	0.5758816793	0.9990458803	24.2529995	158331.561
0.06864265726	0.05439235052	0.04219816355	0.02522110197	0.06741926552
45.81099419	122.8488183	122.8488183	50.01345847	45.94381784
46.99629622	41.78658835	4.178589633	4.251373143	2.190875153
0.6357972284	0.6840631211	0.6840631211	3.861164322	1.406110038
0.04180935325	989.9275043	940.7920789	1.219992952	2.11645721
0.0005874990823	0.0002262487881	1.305425215e-005	1.325766526e-005	
1540.36334	1516.70087	483.0292642	471.2241486	2.172615558
2.111791551	2.148791551	0.1000176194	0.1235952177	1780.055528
1779.46732	192.0054128	515.9017811	2710.042669	323.8963683
1264.153747	209.5671263	192.5589469	196.9599582	175.1953679

KEY POINT #4 (t plus 3224.7534 s with a Mixing Number of 63.3311): 52.07016481

0.040894	0.00925	0.3937	0.8336091063	0.8411033843
0.586075699	0.586075699	0.9989302471	21.51585712	158275.194
0.06435663462	0.05331658078	0.04315959317	0.02523125958	0.06839085276
70.69552728	128.1271651	128.1271651	88.00389459	74.81594398
66.4096137	53.08174763	4.188210457	4.261188243	2.224406018
0.6602463609	0.6846591225	0.6846591225	2.538124355	1.345741867
0.04300395541	977.4486877	936.4137049	1.419870877	2.420083222
0.0004001201435	0.0002162247695	1.323636519e-005	1.345351262e-005	
1557.952988	1508.194154	485.2413915	473.0124331	2.554616845
2.498971444	2.535971444	0.3215121482	0.6502718104	1815.975171
1815.512239	296.1126575	538.393788	2717.495251	242.2812213
1277.581292	368.7194436	313.374239	278.1695573	222.4300301

KEY POINT #5 (t plus 5152.1887 s with a Mixing Number of 99.533): 52.70975744

0.040894	0.00925	0.3937	0.8326729697	0.8442138637
0.5895572808	0.5895572808	0.9987272322	18.26131982	157264.6774
0.06005935976	0.05196519464	0.04414188843	0.02508902861	0.06923091704
94.00314999	134.6807034	134.6807034	111.2705446	95.19391211
77.55693127	57.66649982	4.208948793	4.274411169	2.270238551
0.6751822515	0.6849664285	0.6849664285	1.874035833	1.278628578
0.04462023499	962.6837394	930.8125245	1.70387594	2.886415547
0.0003006251194	0.0002048978481	1.34626218e-005	1.37062744e-005	
1550.497167	1496.697095	487.8345582	474.6299318	3.103035722
3.050342207	3.087342207	0.8155151569	1.496030663	1840.20274
1839.869264	393.9931732	566.3992819	2726.443816	172.4061087
1273.803458	466.8592252	399.0045484	324.9117587	241.6439652

KEY POINT #6 (t plus 7006.5198 s with a Mixing Number of 155.698): 53.15762646

0.040894	0.00925	0.3937	0.8206589521	0.8360486108
0.5801127467	0.5801127467	0.9983184452	14.37905228	154598.1809
0.05637965217	0.05015047135	0.04431866146	0.02550050308	0.06981916454
112.9432554	143.3556339	143.3556339	130.0252859	113.3300644
86.35842006	63.19041769	4.234258261	4.293814953	2.338199593
0.6822254692	0.6846505861	0.6846505861	1.537178842	1.201346856
0.04700021231	948.7978033	923.1174981	2.148219385	3.696879699
0.0002476709005	0.0001915552576	1.376217967e-005	1.406114848e-005	
1531.271547	1479.947654	491.0001605	475.6336504	3.971577048
3.92174186	3.95874186	1.581384021	2.704640547	1841.851983
1841.645226	474.0028645	603.618507	2737.73248	129.6156425
1238.233476	546.5806218	475.6396037	361.9181448	264.8203122

KEY POINT #7 (t plus 7583.1307 s with a Mixing Number of 175.9764): 52.70112555

0.040894	0.00925	0.3937	0.8181472306	0.8348711691
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0.5850008498	0.5850008498	0.9982259704	13.39137841	152145.4219
0.05541557117	0.04957152589	0.04433906145	0.02488051814	0.0692195796
117.7746581	146.0947941	146.0947941	134.3366933	118.1825392
108.6498921	65.08122911	4.242006963	4.300423474	2.361388916
0.68333638	0.684382594	0.684382594	1.470046117	1.179362041
0.04781123481	945.0024882	920.6211524	2.306334208	3.935451895
0.0002368067759	0.0001876872958	1.385675044e-005	1.416513097e-005	
1524.752808	1474.307707	491.9357011	476.3344456	4.283153498
4.234302588	4.271302588	1.850617233	3.072061513	1859.152845
1858.973516	494.5010357	615.4086878	2741.157443	120.9076521
1243.744157	565.0065684	496.2302015	455.8619367	272.7574635
KEY POINT #8 (t plus 10246.2761 s with a Mixing Number of 302.0953): 55.28498864				
0.040894	0.00925	0.3937	0.809506126	0.831768112
0.5709957639	0.5709957639	0.9973792704	9.961627705	153674.0249
0.05127119922	0.04681982019	0.04617651441	0.02643680517	0.07261331958
138.0146118	158.9422389	158.9422389	151.0355301	138.6521086
137.3992973	73.99768946	4.280887045	4.334828344	2.481116227
0.6851061293	0.682068899	0.682068899	1.247388765	1.089492721
0.05201825679	928.0168591	908.4819177	3.177235941	5.5497947
0.0001996300485	0.0001714275726	1.430002946e-005	1.471181826e-005	
1491.082157	1445.682276	495.9089759	476.6845576	6.016877622
5.970558302	6.007558302	3.416508093	4.894634273	1861.765071
1861.665837	580.8517064	670.9782099	2756.260978	90.12650354
1190.786861	636.7928755	583.580078	578.2192406	310.2324316
KEY POINT #9 (t plus 10855.9869 s with a Mixing Number of 342.8635): 52.23001898				
0.040894	0.00925	0.3937	0.8072732135	0.8309211749
0.5972873996	0.5972873996	0.9974535251	9.12320242	144316.8037
0.05032461126	0.04613184635	0.04515227767	0.02344853338	0.06860081105
142.5291179	162.1130047	162.1130047	154.93431	143.3601392
142.3655315	79.44118949	4.291116817	4.344256783	2.51342093
0.6848850461	0.681233463	0.681233463	1.20811269	1.070306512
0.05316346884	923.991349	905.3754189	3.428179521	5.724965486
0.000192821205	0.0001678373651	1.44093389e-005	1.480003951e-005	
1482.259285	1438.078809	496.7836284	478.8213197	6.520752269
6.475347192	6.512347192	3.881233046	5.424903593	1924.200493
1924.11726	600.2331255	684.7670515	2759.731648	84.53392598
1239.433441	653.6576813	603.7988324	599.5323504	333.0905744
KEY POINT #10 (t plus 11406.5964 s with a Mixing Number of 385.9168): 50.1687406				
0.040894	0.00925	0.3937	0.8054920922	0.8303586289
0.5999331189	0.5999331189	0.9973039573	8.247569074	137601.7783
0.04950970951	0.04553063065	0.04328649632	0.02260695657	0.06589345288
146.3864884	164.8713265	164.8713265	157.5307597	146.9636104
146.2390726	91.74867797	4.30035866	4.352786477	2.542409057
0.6845226314	0.6804225959	0.6804225959	1.177001578	1.054477431
0.05419589534	920.4830717	902.636879	3.659169545	6.082851826
0.0001873527957	0.0001648347041	1.450439759e-005	1.490969451e-005	
1474.359774	1431.294321	497.5100956	479.1831393	6.985879604
6.941593621	6.978593621	4.317457839	5.802804908	1936.24337
1936.175347	616.8326195	696.7881222	2762.663777	79.95550274
1239.455247	664.919533	619.3137714	616.199846	384.8115022
KEY POINT #11 (t plus 11406.5964 s with a Mixing Number of 385.9168): 50.1687406				
0.040894	0.00925	0.3937	0.8054920922	0.8303586289
0.5999331189	0.5999331189	0.9973039573	8.247569074	137601.7783
0.04950970951	0.04553063065	0.04328649632	0.02260695657	0.06589345288
146.3864884	164.8713265	164.8713265	157.5307597	146.9636104
146.2390726	91.74867797	4.30035866	4.352786477	2.542409057
0.6845226314	0.6804225959	0.6804225959	1.177001578	1.054477431
0.05419589534	920.4830717	902.636879	3.659169545	6.082851826
0.0001873527957	0.0001648347041	1.450439759e-005	1.490969451e-005	
1474.359774	1431.294321	497.5100956	479.1831393	6.985879604
6.941593621	6.978593621	4.317457839	5.802804908	1936.24337
1936.175347	616.8326195	696.7881222	2762.663777	79.95550274
1239.455247	664.919533	619.3137714	616.199846	384.8115022
KEY POINT #12 (t plus 0 s with a Mixing Number of 41.5283): 51.93560575 0.040894				
0.00925	0.3937	0.8292021165	0.8314723941	0.5678812083
0.5678812083	0.9990263334	24.49114808	160309.6877	0.06936023809
0.05447575745	0.04253736055	0.02567675743	0.06821411798	41.44894025

122.4372006	122.4372006	43.20682017	41.18381806	42.35866673
37.28460024	4.178284794	4.250637801	2.188384554	0.6305141057
0.6840034086	0.6840034086	4.210964235	1.411076474	0.04172005549
991.706868	941.1285134	1.205415076	2.120586817	0.0006354455189
0.0002270673634	1.304005738e-005	1.324844863e-005	1533.905345	
1517.335238	482.8522016	470.7387834	2.144901972	2.082642456
2.119642456	0.07974254461	0.08744027887	1761.420997	1760.821181
173.7764499	514.1500638	2709.452706	340.3736138	1247.270934
181.1214253	172.6671929	177.5791424	156.3821675	
KEY POINT #13 (t plus 11406.5964 s with a Mixing Number of 385.9168): 50.1687406				
0.040894	0.00925	0.3937	0.8054920922	0.8303586289
0.5999331189	0.5999331189	0.9973039573	8.247569074	137601.7783
0.04950970951	0.04553063065	0.04328649632	0.02260695657	0.06589345288
146.3864884	164.8713265	164.8713265	157.5307597	146.9636104
146.2390726	91.74867797	4.30035866	4.352786477	2.542409057
0.6845226314	0.6804225959	0.6804225959	1.177001578	1.054477431
0.05419589534	920.4830717	902.636879	3.659169545	6.082851826
0.0001873527957	0.0001648347041	1.450439759e-005	1.490969451e-005	
1474.359774	1431.294321	497.5100956	479.1831393	6.985879604
6.941593621	6.978593621	4.317457839	5.802804908	1936.24337
1936.175347	616.8326195	696.7881222	2762.663777	79.95550274
1239.455247	664.919533	619.3137714	616.199846	384.8115022
KEY POINT #14 (t plus 3728.6633 s with a Mixing Number of 70.0468): 51.71263843				
0.040894	0.00925	0.3937	0.8331180342	0.84159306
0.5938811055	0.5938811055	0.9989195901	20.78552986	156614.3522
0.06331065192	0.0530192329	0.04337256963	0.02454869495	0.06792126458
76.50338008	129.576347	129.576347	95.61934406	80.1998285
70.46600166	53.73312429	4.192325115	4.264011067	2.234136314
0.664651186	0.6847680729	0.6847680729	2.336890743	1.330189573
0.04334839948	974.0263263	935.1908406	1.479123968	2.487915332
0.0003704906374	0.0002136184302	1.328638713e-005	1.350282785e-005	
1557.999209	1505.739773	485.8295737	473.734237	2.668527836
2.613634496	2.650634496	0.4108821901	0.8655603746	1836.657733
1836.225695	320.4580645	544.5788928	2719.503789	224.1208283
1292.07884	400.7639162	335.9588855	295.1622079	225.1626045

End

D.12 TEST #12 - T12_RCIC_5PSIG_107KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T12_RCIC_5PSIG_107kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1804.8372 s, and ending (KEY POINT #11) at t plus 12746.8131 s, for a time period of 10941.9759 s.
Original Data Record Time: 14288.3382 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 2625.7422 s, T_bulk = 63.4675 C and T_out = 60.0729 C
Stratification Beginning SP12 Temperature = 63.2378 C
Stratification Beginning Pressure = 23.6034 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 10146.3644 s, T_bulk = 130.4416 C and T_out = 76.0545 C
Stratification Ending SP12 Temperature = 130.314 C
Stratification Ending Pressure = 64.5798 psia
Plume detected! Setting t_plume (KEY POINT #2) to 1987.1317 s.
At t = 1987.1317 s, the pool pressure is 22.6159 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 58.161, 58.0852, 60.0925, 58.0885, and 54.4546 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 12.0007 +/- 2.561 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 11.0272 +/- 2.3492 C.
Minimum Steam Quality: 0.98998 at t plus 10912.0752 s
Maximum Steam Quality: 1.0061 at t plus 3455.8547 s
Time-Averaged Steam Quality: 1.0001 +/- 0.0027551
Minimum Turbine Outlet Steam Quality: 0.99215 at t plus 10912.0752 s

Maximum Turbine Outlet Steam Quality: 1.0206 at t plus 2252.4358 s
 Time-Averaged Turbine Outlet Steam Quality: 1.0093 +/- 0.0070392
 Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 10851.9747 s; using 300 s smoothing
 Max and min smoothed upper level changerates: 0.72556 degrees/min at t plus 3837.4615 s and 0.34665 degrees/min at t plus 8694.4393 s, respectively
 Max and min smoothed mid (SP9) level changerates: 0.82435 degrees/min at t plus 5060.2814 s and 0.37529 degrees/min at t plus 10152.2637 s, respectively
 Max and min smoothed upper-mid level changerate differences: 0.288 degrees/min at t plus 3491.5557 s and -0.22808 degrees/min at t plus 5059.5804 s, respectively
 Max and min smoothed lower level changerates: 3.9973 degrees/min at t plus 7440.4466 s and -0.11894 degrees/min at t plus 3422.3538 s, respectively
 Max and min smoothed mid-lower level changerate differences: 0.68162 degrees/min at t plus 5509.9901 s and -3.5466 degrees/min at t plus 7440.4466 s, respectively
 Max and min smoothed outlet level changerates: 5.706 degrees/min at t plus 10779.9746 s and -0.020841 degrees/min at t plus 4164.7662 s, respectively
 Max and min smoothed lower-outlet level changerate differences: 3.9164 degrees/min at t plus 7440.4466 s and -5.2007 degrees/min at t plus 10777.3755 s, respectively
 Max and min smoothed hot (SP8) level changerates: 1.37 degrees/min at t plus 2604.743 s and 0.16669 degrees/min at t plus 9222.1495 s, respectively
 Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.83882 degrees/min at t plus 2534.64 s and -0.31375 degrees/min at t plus 4438.4719 s, respectively
 The mean steam flow rate was 44.6559 +/- 0.83056 g/s
 The mean feedwater flow rate was 43.7258 +/- 1.8014 g/s
 The mean water injection to steam flow rate was 0.0030939 +/- 0.036284 g/s
 Mean Smoothed Condensing Region SP8-SP9 delta T is 12.6626 +/- 1.1657 C over the Stratification Period, beginning at 7.3739 C and ending at 11.5956 C
 Mean Smoothed SP8-Upper Pool delta T is 11.6236 +/- 1.1461 C over the Stratification Period, beginning at 7.0097 C and ending at 10.6215 C
 The stratification period begins and ends with Smoothed SP8 readings of 71.0506 and 141.8864 C, respectively
 The stratification period begins and ends with condensing flows of 0.46557 and 1.2492 kg/s, respectively.
 The stratification period begins and ends with condensing+cooling flows of 3.4858 and 1.9138 kg/s, respectively.
 The stratification period had a mean sparger steam enthalpy of 2737.3289 +/- 1.2347 kJ/kg. At plume detection, the condensing and condensing+cooling flows are 0.42606 and 12.9278 kg/s, respectively
 The plume period had a mean steam enthalpy of 2737.5098 +/- 1.129 kJ/kg.
 Maximum Smoothed Top-Mid delta T is 2.3721 degrees C at t plus 4318.67 s with T_upper = 81.1101 C and T_mid = 78.7379 C
 At t plus 4318.67 s, Smoothed SP8-SP9 is 13.3206 C and Smoothed SP8-Top is 10.9484 C, where Smoothed SP8 is 92.0585 C and Pool P = 28.112 psia
 Maximum Smoothed Top-Lower delta T is 26.12 degrees C at t plus 7175.8164 s with T_upper = 109.9648 C and T_low = 83.8448 C
 At t plus 7175.8164 s, Smoothed SP8-SP9 is 14.061 C and Smoothed SP8-Top is 13.3846 C, where Smoothed SP8 is 123.3494 C and Pool P = 43.0219 psia
 Maximum Smoothed Mid-Lower delta T is 25.491 degrees C at t plus 7108.8356 s with T_mid = 108.8059 C and T_low = 83.3148 C
 At t plus 7108.8356 s, Smoothed SP8-SP9 is 13.5815 C and Smoothed SP8-Top is 13.046 C, where Smoothed SP8 is 122.3873 C and Pool P = 42.5877 psia
 Maximum Smoothed Top-Outlet delta T is 55.7836 degrees C at t plus 9916.7602 s with T_upper = 129.9466 C and T_out = 74.163 C
 At t plus 9916.7602 s, Smoothed SP8-SP9 is 12.1269 C and Smoothed SP8-Top is 10.9029 C, where Smoothed SP8 is 140.8495 C and Pool P = 62.5965 psia
 Maximum Smoothed Mid-Outlet delta T is 54.6949 degrees C at t plus 10002.8262 s with T_mid = 129.4256 C and T_out = 74.7307 C
 At t plus 10002.8262 s, Smoothed SP8-SP9 is 11.84 C and Smoothed SP8-Top is 10.9513 C, where Smoothed SP8 is 141.2657 C and Pool P = 63.3059 psia
 Maximum Smoothed Lower-Outlet delta T is 54.659 degrees C at t plus 9979.3608 s with T_low = 129.1915 C and T_out = 74.5325 C
 At t plus 9979.3608 s, Smoothed SP8-SP9 is 11.8816 C and Smoothed SP8-Top is 10.9366 C, where Smoothed SP8 is 141.0424 C and Pool P = 63.0955 psia
 Maximum Smoothed Condensing Region SP8-SP9 delta T is 14.6068 degrees C at (KEY POINT #14) t plus 7383.8183 s with T_SP8 = 125.5408 C and T_SP9 = 110.934 C and Pool P = 44.3567 psia

Maximum Smoothed Condensing Region SP8-Upper delta T is 14.0174 degrees C at t plus 6976.313 s with T_SP8 = 122.1298 C and T_upper = 108.1125 C and Pool P = 41.7433 psia

Maximum Top-Mid delta T is 4.0962 degrees C at (KEY POINT #4) t plus 3860.4618 s ignoring SP 4, with temperatures of 77.2292 and 73.133 C, respectively, at Set # 2, where Pool P = 26.6314 psia and T_outlet = 66.5982 C

Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 5546.8143 s with a Smoothed Mid-Axis Top-Mid Delta T of 1.365 C and a raw SP12 Reading of 92.5302 C.

Maximum Top-Lower delta T is 28.2301 degrees C at t plus 7267.5177 s, with temperatures of 110.4139 and 82.1838 C, respectively, at Set # 1, where Pool P = 43.6193 psia and T_outlet = 70.9363 C

Maximum Mid-Low delta T is 26.9159 degrees C at (KEY POINT #6) t plus 7132.716 s ignoring SP 4, with temperatures of 108.9358 and 82.0198 C, respectively, at Set # 2, where Pool P = 42.7502 psia and T_outlet = 70.8574 C

Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 7568.5219 s with a Smoothed Mid-Axis Mid-Low Delta T of 8.9696 C and a raw SP12 Reading of 112.2591 C.

Maximum Top-Outlet delta T is 56.0469 degrees C at t plus 9937.9614 s, with temperatures of 130.2269 and 74.18 C, respectively, at Set # 1, where Pool P = 62.7758 psia

Maximum Mid-Outlet delta T is 54.8058 degrees C at t plus 9971.2614 s ignoring SP 4, with temperatures of 129.2698 and 74.464 C, respectively, at Set # 2, where Pool P = 63.0442 psia

Maximum Lower-Outlet delta T is 55.8925 degrees C at (KEY POINT #8) t plus 9958.5596 s, with temperatures of 130.2648 and 74.3723 C, respectively, at Set # 1, where Pool P = 62.9523 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 10826.4753 s with a Smoothed Mid-Axis Low-Outlet Delta T of 18.6259 C and a raw SP12 Reading of 134.8564 C.

Minimum SP Pressure is 20.7345 psia at t plus 3.3002 s

Maximum SP Pressure is 72.0881 psia at t plus 10941.8769 s

Beginning SP Pressure is 20.7411 psia

Ending SP Pressure is 72.0878 psia

Time-Average SP Pressure is 37.6823 +/- 15.285 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 76.8408 cm (cold) / 76.9744 cm (hot) at 19.8052 psia

Beginning Smoothed SP Level is 77.2727 cm (cold) / 77.4443 cm (hot) at 20.7443 psia

Ending Smoothed SP Level is 80.5617 cm (cold) / 82.7283 cm (hot) at 72.0942 psia

Minimum Smoothed Cold SP Level is 77.081 cm at t plus 2589.7431 s and 23.5424 psia

Minimum Smoothed Hot SP Level is 77.432 cm at t plus 1352.9224 s and 21.8473 psia

Maximum Smoothed Cold SP Level is 80.5617 cm at t plus 10941.9759 s and 72.0942 psia

Maximum Smoothed Hot SP Level is 82.7283 cm at t plus 10941.9759 s and 72.0942 psia

SP 12 Temperature at the beginning is 40.0548 C, and at the end is 135.7365 C

At plume detection, the Mixing Number is 45.1143

The Mixing Number ranges from a minimum of 35.5449 at (KEY POINT #12) t plus 0 s to a maximum of 324.5116 at (KEY POINT #13) t plus 10941.9759 s; it had a mean value of 121.5718 +/- 82.5853 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8,

Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 35.5449): 36.74278043 0.040894
0.00925 0.3937 0.7727272112 0.7744428647 1.013830827
1 1 44.37054148 113638.555 0.06960802964
0.05669326994 0.04825930734 5.369110399e-006 0.04825930734 39.9279
126.0464525 111.3605831 40.254814 39.90993725 39.77263922
36.10383451 4.178441517 4.232404205 2.127809291 0.6285635417
0.6816640914 0.6816640914 4.345415173 1.560724542 0.03951391151
992.2673163 949.9080109 0.8628299974 0.8281816502 0.0006536814121
0.0002513677393 1.265866011e-005 1.322226654e-005 1531.278148
1532.764912 477.8471204 487.9843209 1.500526546 1.430270643
1.467270643 0.07356088776 0.074853381 2725.885401 2723.916656
167.363289 467.1253442 2693.129181 299.7620551 2258.760057
168.7292794 167.2867256 166.7161371 151.389944

KEY POINT #2 (t plus 1987.1317 s with a Mixing Number of 45.1143): 33.29175894
0.040894 0.00925 0.3937 0.7715302102 0.7751237984
1.016584172 1 1 37.48203207 101441.1898
0.06656891855 0.05619593154 0.04372660989 3.167943558e-006 0.04372660989
58.08518687 131.3749932 113.867857 60.09252345 58.16104109
58.08848508 54.4545953 4.181854431 4.236275444 2.140465022
0.6489886753 0.6823185531 0.6823185531 3.094284458 1.523953972
0.03998125798 984.2091035 947.9672189 0.9324287261 0.8882701672
0.0004802069524 0.0002454566712 1.274487264e-005 1.34209111e-005
1552.719641 1529.555812 479.0199123 491.0507761 1.630252629
1.559633422 1.596633422 0.1824351316 0.2003137005 2735.104591
2733.699689 243.2635295 477.7513178 2696.896994 234.4877882
2257.353274 251.6587243 243.5793071 243.2788414 228.0886855

KEY POINT #3 (t plus 2625.7422 s with a Mixing Number of 49.3637): 33.61592801
0.040894 0.00925 0.3937 0.7708277044 0.7751013837
1.016298871 1 1 36.51856141 102231.1524
0.06559803438 0.05597040308 0.04415238537 1.444633323e-006 0.04415238537
63.67671048 132.136723 115.0003254 71.05056892 64.04086639
63.92397438 60.01292945 4.184337002 4.238072154 2.146378258
0.6542487518 0.6825899803 0.6825899803 2.824616495 1.507934193
0.04019829595 981.3083273 947.081646 0.965320339 0.9205463359
0.0004416474617 0.0002428700441 1.278383898e-005 1.344687728e-005
1555.870825 1528.050889 479.5421062 491.3414066 1.69178831
1.627515465 1.664515465 0.2359562517 0.3264581152 2736.037677
2734.704072 266.658778 482.5541904 2698.585267 215.8954124
2253.483487 297.5286262 268.1811498 267.6949246 251.3368011

KEY POINT #4 (t plus 3860.4618 s with a Mixing Number of 60.3683): 34.06822742
0.040894 0.00925 0.3937 0.7796344099 0.7859375877
1.014495487 1 1 33.10467625 103279.5676
0.06374329296 0.0552690297 0.0447464519 4.273279688e-006 0.0447464519
74.11243538 133.536148 118.5046793 87.11077406 76.09323829
71.92660993 66.51598939 4.190706084 4.243825352 2.165474868
0.6628561015 0.6833353839 0.6833353839 2.416362139 1.460554098
0.04089410502 975.4246439 944.3061223 1.073098502 1.029204475
0.0003822029881 0.0002351765713 1.290450855e-005 1.348946481e-005
1558.01297 1523.179502 481.1278694 491.5744006 1.894376909
1.836611955 1.873611955 0.371843793 0.6282517547 2736.832152
2735.736232 310.3737676 497.4302896 2703.754489 187.0565221
2239.401862 364.9147252 318.6748099 301.2167717 278.5638509

KEY POINT #5 (t plus 5546.8143 s with a Mixing Number of 92.0947): 34.43303698
0.040894 0.00925 0.3937 0.7906587965 0.8002630366
1.010668877 1 1 27.16584348 103852.991
0.06032226132 0.05391272745 0.04522560608 4.422981698e-006 0.04522560608
92.61678931 135.9567038 125.2090808 104.5746443 93.59585103
80.81217003 69.59510311 4.207562137 4.255672873 2.205501345
0.6744534338 0.6843684348 0.6843684348 1.904461967 1.378370474
0.04233206922 963.6029847 938.8489405 1.306355243 1.267636122
0.0003052767544 0.0002216601867 1.313566733e-005 1.355863323e-005
1551.333592 1512.981773 484.0318918 491.6803025 2.337220857
2.282916234 2.319916234 0.774525943 1.191327526 2737.476894
2736.738911 388.1002074 525.9525779 2713.401289 137.8523705
2211.524316 438.4991295 392.2189047 338.5045382 291.4917108

KEY POINT #6 (t plus 7132.716 s with a Mixing Number of 143.9185): 34.46850236

0.040894	0.00925	0.3937	0.7936001899	0.8066328841
1.005989782	1	1	21.23532754	103235.9045
0.05715875109	0.05220730897	0.0452721876	2.997454564e-006	0.0452721876
109.0012555	139.3065764	133.512651	122.9519762	109.5888518
83.6218816	70.87250423	4.228517124	4.271967187	2.261724238
0.681073495	0.6849463852	0.6849463852	1.596958703	1.290001963
0.04432101024	951.7833198	931.8242013	1.650172542	1.623275386
0.0002572169424	0.0002068326237	1.342228873e-005	1.365372777e-005	
1535.964741	1498.820462	487.3849742	491.6797796	2.99888237
2.947339621	2.984339621	1.386320156	2.179606568	2738.284207
2737.833268	457.2522208	561.4010518	2724.874534	104.1488309
2176.883156	516.3967744	459.7358935	350.3496907	296.895603

KEY POINT #7 (t plus 7568.5219 s with a Mixing Number of 158.2462): 34.3890483

0.040894	0.00925	0.3937	0.7938815699	0.807855654
1.004616318	1	1	19.91050393	102853.8601
0.0565048281	0.05176533495	0.04516782974	3.336132587e-006	0.04516782974
112.3122155	140.0556361	135.6429571	126.0869207	112.9788216
103.5110444	71.34661629	4.23346829	4.27645375	2.27736597
0.6820171859	0.6849717051	0.6849717051	1.546469392	1.269440818
0.04487045054	949.2498497	929.9747411	1.749164601	1.727308783
0.0002491382079	0.0002033299301	1.349584978e-005	1.367285331e-005	
1531.914511	1494.924005	488.2007929	491.5174487	3.191019716
3.139932432	3.176932432	1.548726575	2.400972138	2738.082828
2737.6864	471.2747516	570.5191536	2727.728037	99.24440201
2167.563674	529.7467747	474.095921	434.0739845	298.8907521

KEY POINT #8 (t plus 9958.5596 s with a Mixing Number of 261.9274): 33.8784854

0.040894	0.00925	0.3937	0.800058681	0.818971741
0.998511898	0.998511898	0.999996177	14.3369466	99756.094
0.0531357949	0.0493827721	0.0444972378	3.20031273e-006	0.0444972378
129.008753	146.985007	146.985007	141.201043	130.014237
128.781019	74.3651954	4.26245004	4.30262348	2.36910341
0.684836973	0.68427829	0.68427829	1.33616756	1.17244715
0.0480811409	935.750247	919.802946	2.35968188	2.36318952
0.000214678633	0.000186463012	1.3887482e-005	1.38881418e-005	1507.1028
1472.43914	492.233088	492.198757	4.38853673	4.33986951
4.37686951	2.62343172	3.73953596	2739.30187	2739.09632
542.274986	619.244574	2742.25557	76.9695882	2120.05729
594.398726	546.560632	541.305561	311.640434	

KEY POINT #9 (t plus 10146.3644 s with a Mixing Number of 272.7161): 33.7373221

0.040894	0.00925	0.3937	0.80105839	0.820408721
0.99812994	0.99812994	0.999995074	13.9384004	99111.0164
0.0528723374	0.0491861279	0.0443118289	5.00569437e-006	0.0443118289
130.290749	147.910974	147.910974	141.886355	131.264903
130.258845	76.0622183	4.26496933	4.30493956	2.37722021
0.684922898	0.684160874	0.684160874	1.32261417	1.16537081
0.0483652152	934.664461	918.948275	2.41621708	2.42073209
0.000212402167	0.00018520611	1.39194458e-005	1.39202896e-005	1504.91087
1470.47712	492.538947	492.495272	4.50035097	4.45187066
4.48887066	2.7261803	3.81212433	2739.61938	2739.4251
547.748586	623.236722	2743.38992	75.488136	2116.38266
597.345492	551.903108	547.613738	318.761594	

KEY POINT #10 (t plus 10826.4753 s with a Mixing Number of 316.6516): 33.7994594

0.040894	0.00925	0.3937	0.805137114	0.826409671
0.996083561	0.996083561	0.999988672	12.7629043	98437.3687
0.0518835953	0.048444757	0.0443934421	7.07100109e-006	0.0443934421
135.073787	151.388851	151.388851	146.045237	136.198714
135.540262	116.178688	4.27476849	4.31389672	2.40854587
0.685082622	0.683638927	0.683638927	1.27479818	1.1398165
0.0494628474	930.551659	915.705299	2.638336	2.64867951
0.000204301608	0.000180630873	1.40394785e-005	1.40413657e-005	1496.38835
1462.94134	493.656038	493.56026	4.9409062	4.89285723
4.92985723	3.13873719	4.27734725	2739.47927	2739.31638
568.200615	638.251449	2747.57742	70.0508339	2101.22782
615.236284	573.009621	570.196096	487.784473	

KEY POINT #11 (t plus 10941.9759 s with a Mixing Number of 324.5116): 33.8222319

0.040894	0.00925	0.3937	0.805616916	0.827282965
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0.995951535	0.995951535	0.999988108	12.5829594	98361.1404
0.0517192222	0.0483191405	0.0444233524	5.24397076e-006	0.0444233524
135.864726	151.976117	151.976117	146.494795	137.019546
136.57758	126.636173	4.27645083	4.31545029	2.4139659
0.685084829	0.683538224	0.683538224	1.26728929	1.13565613
0.0496530254	929.862223	915.152558	2.67740518	2.68825666
0.000203018976	0.000179880273	1.40597433e-005	1.40617153e-005	1494.92768
1461.64307	493.839718	493.739969	5.01859076	4.97072011
5.00772011	3.21158048	4.33025108	2739.89923	2739.7409
571.58748	640.790061	2748.27297	69.2025816	2099.10917
617.174567	576.526302	574.637673	532.215095	
KEY POINT #12 (t plus 0 s with a Mixing Number of 35.5449): 36.74278043 0.040894				
0.00925	0.3937	0.7727272112	0.7744428647	1.013830827
1	1	44.37054148	113638.555	0.06960802964
0.05669326994	0.04825930734	5.369110399e-006	0.04825930734	39.9279
126.0464525	111.3605831	40.254814	39.90993725	39.77263922
36.10383451	4.178441517	4.232404205	2.127809291	0.6285635417
0.6816640914	0.6816640914	4.345415173	1.560724542	0.03951391151
992.2673163	949.9080109	0.8628299974	0.8281816502	0.0006536814121
0.0002513677393	1.265866011e-005	1.322226654e-005	1531.278148	
1532.764912	477.8471204	487.9843209	1.500526546	1.430270643
1.467270643	0.07356088776	0.074853381	2725.885401	2723.916656
167.363289	467.1253442	2693.129181	299.7620551	2258.760057
168.7292794	167.2867256	166.7161371	151.389944	
KEY POINT #13 (t plus 10941.9759 s with a Mixing Number of 324.5116): 33.8222319				
0.040894	0.00925	0.3937	0.805616916	0.827282965
0.995951535	0.995951535	0.999988108	12.5829594	98361.1404
0.0517192222	0.0483191405	0.0444233524	5.24397076e-006	0.0444233524
135.864726	151.976117	151.976117	146.494795	137.019546
136.57758	126.636173	4.27645083	4.31545029	2.4139659
0.685084829	0.683538224	0.683538224	1.26728929	1.13565613
0.0496530254	929.862223	915.152558	2.67740518	2.68825666
0.000203018976	0.000179880273	1.40597433e-005	1.40617153e-005	1494.92768
1461.64307	493.839718	493.739969	5.01859076	4.97072011
5.00772011	3.21158048	4.33025108	2739.89923	2739.7409
571.58748	640.790061	2748.27297	69.2025816	2099.10917
617.174567	576.526302	574.637673	532.215095	
KEY POINT #14 (t plus 7383.8183 s with a Mixing Number of 152.1046): 34.41087195				
0.040894	0.00925	0.3937	0.7938741069	0.8074155397
1.005154846	1	1	20.44412048	102990.2414
0.05677762086	0.05195012748	0.04519649372	5.799062777e-006	0.04519649372
110.9339614	139.7053262	134.7533076	125.5407513	111.6783634
91.50775207	71.15887068	4.231376691	4.274564362	2.270772759
0.6816401499	0.6849671802	0.6849671802	1.567080965	1.277929664
0.04463899697	950.310315	930.7494492	1.707259845	1.683383111
0.0002524439164	0.000204778734	1.346512889e-005	1.366341294e-005	
1533.637215	1496.564061	487.862322	491.56291	3.109605074
3.058322128	3.095322128	1.479321997	2.361143755	2738.092542
2737.67458	465.4355102	566.710063	2726.540985	101.2745527
2171.382479	527.4163405	468.5845405	383.4956641	298.1040412

End

D.13 TEST #13 - T13_RCIC_060GPM_157KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T13_RCIC_060GPM_157kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1153.361 s, and ending (KEY POINT #11) at t plus 7513.9608 s, for a time period of 6360.5998 s.
Original Data Record Time: 8911.3997 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 3199.024 s, T_bulk = 81.1327 C and T_out = 77.3373 C
Stratification Beginning SP12 Temperature = 80.8037 C
Stratification Beginning Pressure = 21.7017 psia

Bulk Pool to Outlet Thermal De-stratification Detected beginning (KEY POINT #9) at t plus 5571.0937 s, $T_{bulk} = 111.7117$ C and $T_{out} = 97.7167$ C
 Stratification Ending SP12 Temperature = 111.5393 C
 Stratification Ending Pressure = 38.1043 psia
 Plume detected! Setting t_plume (KEY POINT #2) to 1018.6153 s.
 At t = 1018.6153 s, the pool pressure is 16.1023 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 53.4058, 53.5204, 55.521, 53.463, and 50.9301 C, respectively.

Over the Plume Period (Plume Detected to De-stratification), the mean Smoothed SP8-SP9 temperatures were 8.6421 +/- 2.3538 C.

Over the Plume Period (Plume Detected to De-stratification), the mean Smoothed SP8-Upper temperatures were 8.0558 +/- 1.9998 C.

Minimum Steam Quality: 0.4776 at t plus 975.4158 s
 Maximum Steam Quality: 0.65776 at t plus 6062.2557 s
 Time-Averaged Steam Quality: 0.57917 +/- 0.026335
 Minimum Turbine Outlet Steam Quality: 0.53952 at t plus 8.7985 s
 Maximum Turbine Outlet Steam Quality: 0.69331 at t plus 3889.8615 s
 Time-Averaged Turbine Outlet Steam Quality: 0.62617 +/- 0.020513
 Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 6270.6127 s; using 300 s smoothing

Max and min smoothed upper level changerates: 0.95174 degrees/min at t plus 2358.5369 s and 0.48002 degrees/min at t plus 3233.0499 s, respectively
 Max and min smoothed mid (SP9) level changerates: 0.84057 degrees/min at t plus 1042.8176 s and 0.65574 degrees/min at t plus 3114.5481 s, respectively
 Max and min smoothed upper-mid level changerate differences: 0.20087 degrees/min at t plus 3504.8492 s and -0.28873 degrees/min at t plus 3236.3511 s, respectively
 Max and min smoothed lower level changerates: 0.96347 degrees/min at t plus 5036.1781 s and 0.46431 degrees/min at t plus 3532.9571 s, respectively
 Max and min smoothed mid-lower level changerate differences: 0.33485 degrees/min at t plus 3504.9555 s and -0.23404 degrees/min at t plus 5851.4937 s, respectively
 Max and min smoothed outlet level changerates: 2.52 degrees/min at t plus 5775.9884 s and 0.14181 degrees/min at t plus 5182.7804 s, respectively
 Max and min smoothed lower-outlet level changerate differences: 0.79635 degrees/min at t plus 3504.1781 s and -1.7096 degrees/min at t plus 5772.3892 s, respectively
 Max and min smoothed hot (SP8) level changerates: 1.5381 degrees/min at t plus 1293.323 s and 0.12144 degrees/min at t plus 3350.1496 s, respectively
 Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.7968 degrees/min at t plus 1293.323 s and -0.68511 degrees/min at t plus 3350.1496 s, respectively

The mean steam flow rate was 66.3496 +/- 2.8728 g/s
 The mean feedwater flow rate was 65.9029 +/- 5.1252 g/s
 The mean water injection to steam flow rate was 37.2206 +/- 2.5764 g/s
 Mean Smoothed Condensing Region SP8-SP9 delta T is 9.7609 +/- 0.60457 C over the Stratification Period, beginning at 11.2459 C and ending at 11.3529 C
 Mean Smoothed SP8-Upper Pool delta T is 9.0995 +/- 0.50194 C over the Stratification Period, beginning at 10.0585 C and ending at 10.3437 C
 The stratification period begins and ends with Smoothed SP8 readings of 92.6317 and 122.9118 C, respectively
 The stratification period begins and ends with condensing flows of 1.1417 and 1.9366 kg/s, respectively.
 The stratification period begins and ends with condensing+cooling flows of 3.2953 and 3.1314 kg/s, respectively.
 The stratification period had a mean sparger steam enthalpy of 1894.2557 +/- 19.3759 kJ/kg.

At plume detection, the condensing and condensing+cooling flows are 0.67833 and 19.5277 kg/s, respectively
 The plume period had a mean steam enthalpy of 1875.6918 +/- 34.8119 kJ/kg.

Maximum Smoothed Top-Mid delta T is 2.0194 degrees C at t plus 3122.0476 s with $T_{upper} = 82.4213$ C and $T_{mid} = 80.4018$ C
 At t plus 3122.0476 s, Smoothed SP8-SP9 is 11.2371 C and Smoothed SP8-Top is 9.2177 C, where Smoothed SP8 is 91.639 C and Pool P = 21.3521 psia
 Maximum Smoothed Top-Lower delta T is 1.9689 degrees C at t plus 4804.5198 s with $T_{upper} = 102.7278$ C and $T_{low} = 100.759$ C
 At t plus 4804.5198 s, Smoothed SP8-SP9 is 9.3617 C and Smoothed SP8-Top is 8.7014 C, where Smoothed SP8 is 111.4292 C and Pool P = 31.4083 psia
 Maximum Smoothed Mid-Lower delta T is 1.3277 degrees C at t plus 4906.0786 s with $T_{mid} = 103.3844$ C and $T_{low} = 102.0567$ C

At t plus 4906.0786 s, Smoothed SP8-SP9 is 9.4573 C and Smoothed SP8-Top is 9.0328 C, where Smoothed SP8 is 112.8417 C and Pool P = 32.1988 psia
Maximum Smoothed Top-Outlet delta T is 14.7353 degrees C at t plus 5564.1933 s with T_upper = 112.4328 C and T_out = 97.6974 C
At t plus 5564.1933 s, Smoothed SP8-SP9 is 11.1986 C and Smoothed SP8-Top is 10.2377 C, where Smoothed SP8 is 122.6705 C and Pool P = 38.0501 psia
Maximum Smoothed Mid-Outlet delta T is 13.9066 degrees C at t plus 5545.6872 s with T_mid = 111.266 C and T_out = 97.3594 C
At t plus 5545.6872 s, Smoothed SP8-SP9 is 11.0086 C and Smoothed SP8-Top is 10.2369 C, where Smoothed SP8 is 122.2745 C and Pool P = 37.875 psia
Maximum Smoothed Lower-Outlet delta T is 13.8156 degrees C at t plus 5550.0124 s with T_low = 111.235 C and T_out = 97.4193 C
At t plus 5550.0124 s, Smoothed SP8-SP9 is 11.0193 C and Smoothed SP8-Top is 10.2016 C, where Smoothed SP8 is 122.3374 C and Pool P = 37.9125 psia
Maximum Smoothed Condensing Region SP8-SP9 delta T is 12.063 degrees C at (KEY POINT #14) t plus 5602.2614 s with T_SP8 = 123.9847 C and T_SP9 = 111.9217 C and Pool P = 38.3914 psia
Maximum Smoothed Condensing Region SP8-Upper delta T is 10.8268 degrees C at t plus 5602.2614 s with T_SP8 = 123.9847 C and T_upper = 113.1578 C and Pool P = 38.3914 psia
Maximum Top-Mid delta T is 2.1806 degrees C at (KEY POINT #4) t plus 3055.3448 s ignoring SP 4, with temperatures of 81.0088 and 78.8282 C, respectively, at Set # 2, where Pool P = 21.0859 psia and T_outlet = 75.8334 C
Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 3562.9558 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.99986 C and a raw SP12 Reading of 85.8618 C.
Maximum Top-Lower delta T is 4.1874 degrees C at t plus 4900.5763 s, with temperatures of 104.0672 and 99.8798 C, respectively, at Set # 1, where Pool P = 32.1562 psia and T_outlet = 94.7165 C
Maximum Mid-Low delta T is 1.8741 degrees C at (KEY POINT #6) t plus 4154.1666 s ignoring SP 4, with temperatures of 93.7463 and 91.8721 C, respectively, at Set # 3, where Pool P = 26.8627 psia and T_outlet = 87.6395 C
Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 4866.9784 s with a Smoothed Mid-Axis Mid-Low Delta T of 0.99958 C and a raw SP12 Reading of 102.8403 C.
Maximum Top-Outlet delta T is 15.804 degrees C at t plus 5504.6899 s, with temperatures of 112.6879 and 96.8839 C, respectively, at Set # 2, where Pool P = 37.4688 psia
Maximum Mid-Outlet delta T is 14.133 degrees C at t plus 5525.187 s ignoring SP 4, with temperatures of 111.0699 and 96.9369 C, respectively, at Set # 2, where Pool P = 37.6593 psia
Maximum Lower-Outlet delta T is 15.4438 degrees C at (KEY POINT #8) t plus 5577.996 s, with temperatures of 113.2595 and 97.8157 C, respectively, at Set # 1, where Pool P = 38.1593 psia
Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 5858.3221 s with a Smoothed Mid-Axis Low-Outlet Delta T of 5.1477 C and a raw SP12 Reading of 114.7856 C.
Minimum SP Pressure is 15.1175 psia at t plus 8.2015 s
Maximum SP Pressure is 46.8384 psia at t plus 6360.4188 s
Beginning SP Pressure is 15.1202 psia
Ending SP Pressure is 46.8359 psia
Time-Average SP Pressure is 24.7967 +/- 9.0597 psia
SP Levels are fully corrected and compensated
Pre-Start SP Level is 77.5341 cm (cold) / 77.6896 cm (hot) at 14.6846 psia
Beginning Smoothed SP Level is 78.083 cm (cold) / 78.2655 cm (hot) at 15.1217 psia
Ending Smoothed SP Level is 87.1692 cm (cold) / 89.2987 cm (hot) at 46.854 psia
Minimum Smoothed Cold SP Level is 77.9959 cm at t plus 152.1007 s and 15.2129 psia
Minimum Smoothed Hot SP Level is 78.1933 cm at t plus 152.0007 s and 15.2128 psia
Maximum Smoothed Cold SP Level is 87.9222 cm at t plus 5655.5895 s and 38.943 psia
Maximum Smoothed Hot SP Level is 89.8589 cm at t plus 5809.3203 s and 40.4835 psia
SP 12 Temperature at the beginning is 39.8824 C, and at the end is 121.0224 C
At plume detection, the Mixing Number is 42.0839
The Mixing Number ranges from a minimum of 35.1057 at (KEY POINT #12) t plus 0 s to a maximum of 228.3876 at (KEY POINT #13) t plus 6360.4188 s; it had a mean value of 92.8401 +/- 54.1879 over the test period.
Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m2-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) mdl, Water mdot to Steam md2,

Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m3) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 35.1057): 72.33733181 0.040894
0.00925 0.3937 0.7808298517 0.7826553004 0.5701635263
0.5701635263 0.9994595563 60.22142642 235717.3073 0.06956065388
0.05811295749 0.05759980793 0.03741068084 0.09501048877 40.21931012
104.1251698 104.1251698 40.29314309 40.24535798 40.34995192
37.7428711 4.178533104 4.222036447 2.094496684 0.6289137279
0.6793565299 0.6793565299 4.319516323 1.677844149 0.03826206615
992.142015 955.353835 0.6852446514 1.201189279 0.0006501332037
0.0002699773897 1.241042046e-005 1.25496209e-005 1531.709635
1541.047548 474.3373526 465.3270028 1.172863986 1.04260398
1.07960398 0.07471206981 0.07500619594 1720.455888 1716.829268
168.5465894 436.516365 2682.03514 267.9697755 1283.939523
168.8551029 168.6539255 169.0940743 158.2042309

KEY POINT #2 (t plus 1018.6153 s with a Mixing Number of 42.0839): 79.73348519
0.040894 0.00925 0.3937 0.7841918275 0.7874161421
0.5993320933 0.5993320933 0.9994839835 64.91581663 258437.5035
0.06734944812 0.0576774946 0.06539776017 0.03932710609 0.1047248663
53.52042977 106.3571517 106.3571517 55.5210319 53.40577199
53.46302034 50.93012117 4.180410009 4.225109384 2.104282914
0.6443243916 0.6801353528 0.6801353528 3.348067497 1.639860718
0.03863344048 986.4247146 953.6986151 0.7365155459 1.228259758
0.0005160358788 0.0002639759464 1.248689922e-005 1.261667173e-005
1548.946681 1538.650869 475.4395294 467.1293617 1.266928058
1.110210017 1.147210017 0.1467738362 0.1615909999 1792.393122
1788.179059 224.1396908 445.950232 2685.491284 221.8105412
1346.44289 232.5036316 223.6589235 223.9012346 213.3174734

KEY POINT #3 (t plus 3199.024 s with a Mixing Number of 73.1378): 78.60036489
0.040894 0.00925 0.3937 0.827088748 0.835738498
0.6383092986 0.6383092986 0.9994460014 54.12500339 249787.9652
0.06241841506 0.05623046085 0.06703009744 0.03620648731 0.1032365847
81.38583335 113.6942253 113.6942253 92.63173457 82.5732364
81.9187923 77.45346932 4.19659286 4.236002636 2.139569338
0.667931174 0.6822756111 0.6822756111 2.188587463 1.526441921
0.03994831218 970.9629382 948.1025036 0.9274669913 1.452200646
0.0003483363391 0.0002458577541 1.273889966e-005 1.286804718e-005
1556.784316 1529.783517 478.9394326 470.9905107 1.620982322
1.495943036 1.532943036 0.5013886686 0.7749584921 1896.750174
1893.820658 340.8479071 477.0151241 2696.637393 136.167217
1419.73505 388.1026639 345.8302348 343.0860691 324.3569745

KEY POINT #4 (t plus 3055.3448 s with a Mixing Number of 70.3489): 78.31319136
0.040894 0.00925 0.3937 0.830282147 0.838630428
0.6404936914 0.6404936914 0.9994639652 55.36415909 249433.7438
0.06274486318 0.05637810396 0.06701230836 0.03584709221 0.1028594006
79.60686911 112.9510548 112.9510548 90.82335278 81.16977481
80.12884689 75.81162161 4.195078804 4.234842942 2.135768272
0.6667496782 0.6820878177 0.6820878177 2.240716742 1.53718777
0.03980828383 972.07481 948.6800611 0.9064710328 1.414510627
0.0003561308945 0.0002475881788 1.271333871e-005 1.283923979e-005
1557.2495 1530.748971 478.5937223 470.810054 1.581791161

1.453882874	1.490882874	0.4666496546	0.7240579203	1899.888654
1896.823464	333.3803305	473.864664	2695.524017	140.4843335
1426.02399	380.4919836	339.9365324	335.5716155	317.4698809
KEY POINT #5 (t plus 3562.9558 s with a Mixing Number of 82.2947): 78.6808018				
0.040894	0.00925	0.3937	0.8369041543	0.8468643326
0.6399888069	0.6399888069	0.9994126283	50.952975	248554.3777
0.06156371278	0.05581258119	0.06726035263	0.03608188089	0.1033422335
86.00440224	115.7911657	115.7911657	94.89718631	86.7138773
86.03850496	80.68099041	4.200828978	4.23934483	2.150581658
0.6708021692	0.6827706522	0.6827706522	2.06293852	1.496956642
0.04035209967	968.0029062	946.4599225	0.9888417085	1.544184649
0.0003294167989	0.0002410934009	1.281105942e-005	1.2945146e-005	
1555.03717	1526.979729	479.903967	471.7494561	1.735879289
1.617559047	1.654559047	0.6018410082	0.8428926143	1905.344695
1902.748489	360.2493563	485.9094801	2699.759151	125.6601237
1419.435215	397.6473007	363.2286584	360.3940252	337.9048486
KEY POINT #6 (t plus 4154.1666 s with a Mixing Number of 102.5386): 81.38557064				
0.040894	0.00925	0.3937	0.8570880547	0.869576376
0.617949194	0.617949194	0.992732327	45.34992461	253998.4652
0.06009328646	0.05504216478	0.06733431293	0.03956046259	0.1068947755
93.82451021	119.6326305	119.6326305	103.3755337	94.38922368
93.152287	87.68911109	4.209016036	4.245740296	2.171883558
0.6750293888	0.6835451175	0.6835451175	1.878029586	1.445977536
0.04112603744	962.755382	943.401493	1.1097863	1.794613141
0.0003011927617	0.0002327958885	1.294337442e-005	1.310315605e-005	
1550.389964	1521.543592	481.6284755	472.1421713	1.963650286
1.852303519	1.889303519	0.8101344051	1.142596219	1865.731216
1863.6746	393.1496361	502.2230786	2705.400192	109.0734426
1363.508137	433.4050019	395.5254074	390.3218734	367.3511177
KEY POINT #7 (t plus 4866.9784 s with a Mixing Number of 133.2825): 81.41000556				
0.040894	0.00925	0.3937	0.8748354816	0.8905243483
0.6326333563	0.6326333563	0.9992049156	40.04711567	250607.0048
0.05835931681	0.05401772865	0.06884128129	0.03808558794	0.1069268692
102.8573339	124.6933303	124.6283303	112.2008102	103.1502648
101.7613684	94.49103047	4.220083409	4.254721139	2.202254919
0.6789508406	0.6843070989	0.6843070989	1.700166089	1.384326371
0.04221628403	956.3388347	939.2755753	1.28707563	2.032855655
0.0002735323175	0.0002226478145	1.311787414e-005	1.328446813e-005	
1542.573287	1513.806246	483.8146524	474.198935	2.300412767
2.198430767	2.235430767	1.122052566	1.543019073	1910.140167
1908.536396	431.243703	523.7554192	2712.670947	92.5117162
1386.384748	470.7351373	432.4786879	426.6207806	395.986527
KEY POINT #8 (t plus 5577.996 s with a Mixing Number of 173.6301): 81.43315424				
0.040894	0.00925	0.3937	0.8790444598	0.8976660309
0.6341731268	0.6341731268	0.9990698	34.26702072	246753.8989
0.05663957862	0.05287519518	0.06936528182	0.03759199173	0.1069572736
111.6319282	130.2768597	130.2768597	123.184551	112.673121
111.5669097	98.05870354	4.232544309	4.265395855	2.238921757
0.681806881	0.6848123556	0.6848123556	1.556615732	1.322821267
0.04351750298	949.7541727	934.5965236	1.50847082	2.376429364
0.0002507501966	0.0002123799007	1.331056953e-005	1.349574383e-005	
1532.669484	1504.535297	486.1109031	475.7639829	2.725049909
2.631772927	2.668772927	1.51414276	2.195435462	1926.738278
1925.564049	468.3583703	547.5701947	2720.468724	79.21182438
1379.168083	517.3636645	472.7648646	468.0844833	411.0455327
KEY POINT #9 (t plus 5571.0937 s with a Mixing Number of 173.2918): 81.62358086				
0.040894	0.00925	0.3937	0.879026001	0.897628266
0.6325232183	0.6325232183	0.9990646122	34.3090466	247344.0243
0.05665404493	0.052886144415	0.06936228922	0.0378450976	0.1072073868
111.5588343	130.2236443	130.2236443	122.9117699	112.5680864
111.4395269	97.8642083	4.232433409	4.265290191	2.238556344
0.6817868628	0.6848091829	0.6848091829	1.557709495	1.323377645
0.04350459683	949.8104096	934.6417449	1.506225132	2.379068758
0.0002509255946	0.0002124735066	1.330873243e-005	1.349502874e-005	
1532.760811	1504.627208	486.0896	475.6783574	2.720722327
2.627355227	2.664355227	1.510464933	2.176879609	1923.026279

1921.849169	468.0486825	547.3429201	2720.395559	79.29423764
1375.683359	516.2035996	472.3198226	467.545037	410.2256526
KEY POINT #10 (t plus 5858.3221 s with a Mixing Number of 191.7071): 81.02958849				
0.040894	0.00925	0.3937	0.8788693232	0.8985765194
0.6401204972	0.6401204972	0.9990311987	32.27462076	244020.2349
0.05597880371	0.05239844336	0.06932533138	0.03710188421	0.1064272156
114.9581923	132.5887006	132.5887006	126.431655	116.1818927
115.1252293	109.4955955	4.237725288	4.270061184	2.255095843
0.6826506447	0.6849199057	0.6849199057	1.508484717	1.2991736
0.04408778845	947.1697943	932.6203503	1.608663353	2.510628679
0.0002430001935	0.0002083880818	1.339038605e-005	1.357930007e-005	
1528.357819	1500.477477	487.025455	476.6055677	2.918515906
2.828636144	2.865636144	1.689465301	2.426391369	1945.104613
1944.062962	482.4596034	557.4494818	2723.625204	74.98987835
1387.655132	531.1931038	487.645297	483.1687679	459.3386632
KEY POINT #11 (t plus 6360.5998 s with a Mixing Number of 228.3854): 81.73966194				
0.040894	0.00925	0.3937	0.8716921446	0.8929866852
0.6442137836	0.6442137836	0.9989241853	29.1031679	243239.0575
0.05476938413	0.05149722685	0.07000986484	0.0373499871	0.1073598519
120.9853475	136.9310723	136.9310723	131.7821795	122.5583428
121.8122331	118.482985	4.24778309	4.279229861	2.287067434
0.6838517573	0.6849629318	0.6849629318	1.428871627	1.257392657
0.04521069572	942.3648163	928.84709	1.811298623	2.808617337
0.0002300344327	0.0002012669076	1.354033127e-005	1.374229028e-005	
1519.801814	1492.516971	488.6851829	477.8215237	3.311945067
3.230471351	3.267471351	2.049442799	2.849798079	1964.132765
1963.28577	508.0592448	576.0374656	2729.434893	67.97822077
1388.095299	554.0296867	514.7419685	511.5735207	497.4396923
KEY POINT #12 (t plus 0 s with a Mixing Number of 35.1057): 72.33733181 0.040894				
0.00925	0.3937	0.7808298517	0.7826553004	0.5701635263
0.5701635263	0.9994595563	60.22142642	235717.3073	0.06956065388
0.05811295749	0.05759980793	0.03741068084	0.09501048877	40.21931012
104.1251698	104.1251698	40.29314309	40.24535798	40.34995192
37.7428711	4.178533104	4.222036447	2.094496684	0.6289137279
0.6793565299	0.6793565299	4.319516323	1.677844149	0.03826206615
992.142015	955.353835	0.6852446514	1.201189279	0.0006501332037
0.0002699773897	1.241042046e-005	1.25496209e-005	1531.709635	
1541.047548	474.3373526	465.3270028	1.172863986	1.04260398
1.07960398	0.07471206981	0.07500619594	1720.455888	1716.829268
168.5465894	436.516365	2682.03514	267.9697755	1283.939523
168.8551029	168.6539255	169.0940743	158.2042309	
KEY POINT #13 (t plus 6360.4188 s with a Mixing Number of 228.3876): 81.79855667				
0.040894	0.00925	0.3937	0.8716961393	0.8929901776
0.6436696067	0.6436696067	0.9989216584	29.10030622	243406.428
0.05476972671	0.05149741168	0.07000448238	0.03743272404	0.1074372064
120.9836511	136.9301854	136.9301854	131.7799441	122.5574967
121.8084465	118.4774826	4.247780142	4.279227933	2.287060691
0.6838514763	0.6849629441	0.6849629441	1.428892781	1.257400856
0.04521045935	942.3661933	928.8478689	1.81125524	2.810917385
0.0002300379033	0.0002012683142	1.354030064e-005	1.374273557e-005	
1519.804347	1492.518641	488.6848517	477.7961241	3.311860549
3.230320229	3.267320229	2.049333322	2.849609453	1962.958661
1962.111833	508.0520281	576.0336647	2729.433723	67.98163656
1386.924996	554.0201351	514.7383612	511.55742	497.4163327
KEY POINT #14 (t plus 5602.2614 s with a Mixing Number of 175.1179): 80.96252231				
0.040894	0.00925	0.3937	0.87912557	0.8978501224
0.6382605065	0.6382605065	0.9990809962	34.10470173	245253.7431
0.05658221369	0.05283572866	0.06937591034	0.03696321809	0.1063391284
111.9216594	130.4686336	130.4686336	123.984668	113.1578182
111.7512014	98.73915934	4.232985513	4.26577728	2.240241172
0.6818855132	0.6848235283	0.6848235283	1.552296009	1.3208208
0.0435640952	949.5309532	934.4334583	1.516586021	2.373940196
0.0002500571187	0.0002120432223	1.331719002e-005	1.349982e-005	
1532.305682	1504.203514	486.1875799	475.990379	2.740691674
2.647693843	2.684693843	1.528793465	2.250608116	1936.073105
1934.909974	469.5858831	548.389279	2720.732203	78.80339593
1387.683826	520.7673299	474.8184728	468.8656627	413.9143411

End

D.14 TEST #14 - T14_RCIC_1ATM_157KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T14_RCIC_1ATM_157kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1430.7658 s, and ending (KEY POINT #11) at t plus 5973.2456 s, for a time period of 4542.4798 s.
Original Data Record Time: 7605.868 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 2385.5384 s, T_bulk = 72.2546 C and T_out = 69.8949 C
Stratification Beginning SP12 Temperature = 72.1899 C
Stratification Beginning Pressure = 15.2821 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 3512.8539 s, T_bulk = 87.3483 C and T_out = 79.9994 C
Stratification Ending SP12 Temperature = 87.269 C
Stratification Ending Pressure = 15.3239 psia
Plume detected! Setting t_plume (KEY POINT #2) to 939.7137 s.
At t = 939.7137 s, the pool pressure is 15.2785 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 53.6278, 53.6193, 55.6206, 53.5167, and 50.472 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 7.7273 +/- 2.8802 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 7.0634 +/- 2.3856 C.
Minimum Steam Quality: 0.99376 at t plus 214.2033 s
Maximum Steam Quality: 1.0011 at t plus 2078.8349 s
Time-Averaged Steam Quality: 0.99814 +/- 0.0011321
Minimum Turbine Outlet Steam Quality: 1.0231 at t plus 301.6032 s
Maximum Turbine Outlet Steam Quality: 1.0314 at t plus 2843.8467 s
Time-Averaged Turbine Outlet Steam Quality: 1.0283 +/- 0.0013266
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 4452.4727 s; using 300 s smoothing
Max and min smoothed upper level changerates: 1.0549 degrees/min at t plus 2431.7411 s and 0.52368 degrees/min at t plus 3902.7412 s, respectively
Max and min smoothed mid (SP9) level changerates: 1.0083 degrees/min at t plus 3780.3622 s and 0.69765 degrees/min at t plus 2892.1464 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.27929 degrees/min at t plus 2430.14 s and -0.41692 degrees/min at t plus 3819.5625 s, respectively
Max and min smoothed lower level changerates: 1.237 degrees/min at t plus 3544.1847 s and 0.13441 degrees/min at t plus 2964.9506 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.5982 degrees/min at t plus 2964.9506 s and -0.4986 degrees/min at t plus 3544.3577 s, respectively
Max and min smoothed outlet level changerates: 2.048 degrees/min at t plus 3586.2571 s and 0.16499 degrees/min at t plus 3041.1499 s, respectively
Max and min smoothed lower-outlet level changerate differences: 0.47951 degrees/min at t plus 3326.8523 s and -0.91416 degrees/min at t plus 3645.9575 s, respectively
Max and min smoothed hot (SP8) level changerates: 1.5337 degrees/min at t plus 1436.8222 s and -0.1319 degrees/min at t plus 2779.445 s, respectively
Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.66698 degrees/min at t plus 1473.7233 s and -0.94887 degrees/min at t plus 2779.445 s, respectively
The mean steam flow rate was 66.7509 +/- 1.9931 g/s
The mean feedwater flow rate was 65.2437 +/- 10.6112 g/s
The mean water injection to steam flow rate was 0.0044022 +/- 0.036477 g/s
Mean Smoothed Condensing Region SP8-SP9 delta T is 9.3352 +/- 1.4951 C over the Stratification Period, beginning at 11.7322 C and ending at 8.8525 C
Mean Smoothed SP8-Upper Pool delta T is 8.1288 +/- 1.2972 C over the Stratification Period, beginning at 10.5514 C and ending at 7.3814 C
The stratification period begins and ends with Smoothed SP8 readings of 84.2197 and 96.0967 C, respectively
The stratification period begins and ends with condensing flows of 1.2354 and 2.5113 kg/s, respectively.
The stratification period begins and ends with condensing+cooling flows of 3.2204 and 4.2691 kg/s, respectively.

The stratification period had a mean sparger steam enthalpy of 2740.7147 +/- 0.47705 kJ/kg.

At plume detection, the condensing and condensing+cooling flows are 0.74581 and 19.6402 kg/s, respectively

The plume period had a mean steam enthalpy of 2746.5465 +/- 0.90679 kJ/kg.

Maximum Smoothed Top-Mid delta T is 2.1669 degrees C at t plus 3673.2361 s with T_upper = 91.3566 C and T_mid = 89.1897 C

At t plus 3673.2361 s, Smoothed SP8-SP9 is 9.1197 C and Smoothed SP8-Top is 6.9529 C, where Smoothed SP8 is 98.3095 C and Pool P = 15.3386 psia

Maximum Smoothed Top-Lower delta T is 2.3477 degrees C at t plus 3194.5517 s with T_upper = 84.2374 C and T_low = 81.8897 C

At t plus 3194.5517 s, Smoothed SP8-SP9 is 7.9919 C and Smoothed SP8-Top is 6.8497 C, where Smoothed SP8 is 91.0871 C and Pool P = 15.295 psia

Maximum Smoothed Mid-Lower delta T is 1.2055 degrees C at t plus 3194.4507 s with T_mid = 83.094 C and T_low = 81.8885 C

At t plus 3194.4507 s, Smoothed SP8-SP9 is 7.9967 C and Smoothed SP8-Top is 6.8546 C, where Smoothed SP8 is 91.0908 C and Pool P = 15.2951 psia

Maximum Smoothed Top-Outlet delta T is 8.6602 degrees C at t plus 3485.9544 s with T_upper = 88.4181 C and T_out = 79.7579 C

At t plus 3485.9544 s, Smoothed SP8-SP9 is 8.5905 C and Smoothed SP8-Top is 7.0794 C, where Smoothed SP8 is 95.4975 C and Pool P = 15.3088 psia

Maximum Smoothed Mid-Outlet delta T is 7.1662 degrees C at t plus 3498.4611 s with T_mid = 87.0714 C and T_out = 79.9052 C

At t plus 3498.4611 s, Smoothed SP8-SP9 is 8.6779 C and Smoothed SP8-Top is 7.2166 C, where Smoothed SP8 is 95.7493 C and Pool P = 15.3232 psia

Maximum Smoothed Lower-Outlet delta T is 8.0647 degrees C at t plus 3550.5561 s with T_low = 88.908 C and T_out = 80.8432 C

At t plus 3550.5561 s, Smoothed SP8-SP9 is 8.8533 C and Smoothed SP8-Top is 7.155 C, where Smoothed SP8 is 96.4661 C and Pool P = 15.317 psia

Maximum Smoothed Condensing Region SP8-SP9 delta T is 11.7926 degrees C at (KEY POINT #14) t plus 2395.237 s with T_SP8 = 84.4204 C and T_SP9 = 72.6278 C and Pool P = 15.2815 psia

Maximum Smoothed Condensing Region SP8-Upper delta T is 10.7336 degrees C at t plus 2338.3387 s with T_SP8 = 83.3316 C and T_upper = 72.598 C and Pool P = 15.282 psia

Maximum Top-Mid delta T is 2.1893 degrees C at (KEY POINT #4) t plus 2815.9571 s ignoring SP 4, with temperatures of 79.5373 and 77.348 C, respectively, at Set # 2, where Pool P = 15.2813 psia and T_outlet = 73.9644 C

Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 3033.9485 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.99909 C and a raw SP12 Reading of 81.057 C.

Maximum Top-Lower delta T is 3.6819 degrees C at t plus 3204.9513 s, with temperatures of 84.7409 and 81.059 C, respectively, at Set # 1, where Pool P = 15.2932 psia and T_outlet = 76.6853 C

Maximum Mid-Low delta T is 1.5494 degrees C at (KEY POINT #6) t plus 2869.2461 s ignoring SP 4, with temperatures of 79.4408 and 77.8913 C, respectively, at Set # 2, where Pool P = 15.2926 psia and T_outlet = 74.8448 C

Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 2869.2461 s with a Smoothed Mid-Axis Mid-Low Delta T of 0.87727 C and a raw SP12 Reading of 79.4408 C.

Maximum Top-Outlet delta T is 9.2384 degrees C at t plus 3509.7677 s, with temperatures of 89.2142 and 79.9758 C, respectively, at Set # 1, where Pool P = 15.3219 psia

Maximum Mid-Outlet delta T is 7.3478 degrees C at t plus 3482.1562 s ignoring SP 4, with temperatures of 86.9776 and 79.6297 C, respectively, at Set # 2, where Pool P = 15.3095 psia

Maximum Lower-Outlet delta T is 9.1259 degrees C at (KEY POINT #8) t plus 3468.7574 s, with temperatures of 88.6267 and 79.5008 C, respectively, at Set # 1, where Pool P = 15.3093 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 3622.2572 s with a Smoothed Mid-Axis Low-Outlet Delta T of 3.0404 C and a raw SP12 Reading of 88.3963 C.

Minimum SP Pressure is 14.8214 psia at t plus 0 s

Maximum SP Pressure is 16.1784 psia at t plus 4540.0857 s

Beginning SP Pressure is 14.8214 psia

Ending SP Pressure is 16.1773 psia

Time-Average SP Pressure is 15.3248 +/- 0.19934 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 76.5369 cm (cold) / 76.679 cm (hot) at 14.6967 psia

Beginning Smoothed SP Level is 77.0125 cm (cold) / 77.189 cm (hot) at 14.8271 psia

Ending Smoothed SP Level is 76.5917 cm (cold) / 77.5982 cm (hot) at 16.1809 psia

Minimum Smoothed Cold SP Level is 76.5896 cm at t plus 4506.6758 s and 16.0872 psia
 Minimum Smoothed Hot SP Level is 77.189 cm at t plus 0 s and 14.8271 psia
 Maximum Smoothed Cold SP Level is 77.2669 cm at t plus 253.9025 s and 15.039 psia
 Maximum Smoothed Hot SP Level is 77.7039 cm at t plus 4414.0685 s and 15.9325 psia
 SP 12 Temperature at the beginning is 40.3354 C, and at the end is 99.9414 C
 At plume detection, the Mixing Number is 38.4286
 The Mixing Number ranges from a minimum of 32.7622 at (KEY POINT #12) t plus 0 s to a maximum of 269.8203 at (KEY POINT #13) t plus 4542.4798 s; it had a mean value of 71.0913 +/- 48.8964 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 32.7622): 51.68433553 0.040894
 0.00925 0.3937 0.7701249014 0.7718899222 1.024235576
 1 1 83.92824409 157890.1249 0.06947577248
 0.05831310271 0.06788409051 2.580138907e-006 0.06788409051 40.74070806
 129.7014415 103.0954497 41.23768898 40.48075873 40.53160571
 36.98498522 4.178535923 4.220655847 2.090122876 0.6295715819
 0.6789768643 0.6789768643 4.273203676 1.695965174 0.03809500515
 991.9390833 956.1099702 0.6625909544 0.6158391672 0.0006438349814
 0.0002728299009 1.237517059e-005 1.338639271e-005 1532.577289
 1542.104435 473.8231357 491.6751017 1.131454261 1.022295431
 1.059295431 0.07681063294 0.07885807988 2741.962786 2734.918836
 170.7234708 432.1664867 2680.430854 261.4430159 2309.7963
 172.8001242 169.6357584 169.8513222 155.0354764

KEY POINT #2 (t plus 939.7137 s with a Mixing Number of 38.4286): 49.93733229
 0.040894 0.00925 0.3937 0.7719410612 0.7749879592
 1.025120957 1 1 78.85692072 151773.4879
 0.06733265553 0.05813285873 0.06558951278 4.40988611e-006 0.06558951278
 53.61931614 131.5413858 104.0228906 55.6205902 53.6278319
 53.51666926 50.47203371 4.180451639 4.221898273 2.094058314
 0.6444254045 0.6793193955 0.6793193955 3.34218182 1.67962685
 0.03824535321 986.3730864 955.429152 0.6829667152 0.6333076331
 0.0005152043504 0.000270258311 1.240691821e-005 1.345516463e-005
 1549.028541 1541.153915 474.2864376 492.7253399 1.168695724
 1.053611392 1.090611392 0.1474778971 0.1623605684 2744.510918
 2738.292504 224.548243 436.0842365 2681.876064 211.5359935
 2308.426681 232.9150807 224.5823906 224.1206724 211.3979466

KEY POINT #3 (t plus 2385.5384 s with a Mixing Number of 52.7606): 50.52048095
 0.040894 0.00925 0.3937 0.7694142275 0.7748411098
 1.026400347 1 1 80.54056473 152986.0769
 0.06403569433 0.05816718617 0.06635544149 4.539657237e-006 0.06635544149
 72.48753625 132.8034539 103.8464134 84.21972121 73.66834724
 72.87503887 69.73709809 4.18972946 4.221660402 2.093303978
 0.6615777318 0.6792550232 0.6792550232 2.47319225 1.682711672
 0.038216578 976.3492833 955.5589976 0.679050752 0.6273104422

0.0003905285376	0.0002707442682	1.240087577e-005	1.350439589e-005	
1557.846882	1541.336725	474.1985031	493.5531724	1.16153237
1.0535973	1.0905973	0.3471379438	0.5611966416	2747.390345
2740.903563	303.501629	435.338657	2681.601446	131.8370279
2312.051688	352.7093828	308.4480177	305.1266727	291.9857295
KEY POINT #4 (t plus 2815.9571 s with a Mixing Number of 60.755): 52.97387942				
0.040894	0.00925	0.3937	0.76962915	0.7760553945
1.026688415	1	1	84.315753	160238.9813
0.06296802301	0.05815273214	0.06957782448	4.625619141e-006	0.06957782448
78.38588448	133.1923778	103.9207302	87.29106089	79.76984434
79.61901279	73.96807416	4.194159106	4.221760489	2.093621323
0.665894357	0.6792821773	0.6792821773	2.277826759	1.681411242
0.03822868605	972.8109713	955.5043349	0.6806975815	0.6283215094
0.000361643883	0.0002705394332	1.240342024e-005	1.351926858e-005	
1557.431108	1541.259852	474.2355464	493.7905376	1.16454452
1.054047631	1.091047631	0.4439955205	0.6326458435	2748.770161
2741.661015	328.2268588	435.6526248	2681.717113	107.425766
2313.117536	365.6112619	334.0308412	333.4008543	309.710583
KEY POINT #5 (t plus 3033.9485 s with a Mixing Number of 66.0511): 51.08709283				
0.040894	0.00925	0.3937	0.7685845317	0.7754151755
1.026475613	1	1	81.7122398	154700.2051
0.0625113863	0.0581854147	0.06709965018	3.682968269e-006	0.06709965018
80.8800474	132.8014496	103.7526712	88.14028669	81.72731111
80.39914744	75.78873963	4.196250079	4.221534327	2.092904338
0.6675766847	0.6792206757	0.6792206757	2.203224108	1.684354866
0.03820132493	971.2601439	955.627913	0.6769780938	0.6252416655
0.0003505084343	0.0002710030433	1.239766638e-005	1.350454302e-005	
1556.848326	1541.433461	474.1517506	493.5643481	1.157742069
1.054519486	1.091519486	0.4912981595	0.6536906142	2747.610195
2740.933305	338.6903954	434.942634	2681.455499	96.25223858
2312.667561	369.1802963	342.2446925	336.6739489	317.3418075
KEY POINT #6 (t plus 2869.2461 s with a Mixing Number of 62.0954): 51.65704772				
0.040894	0.00925	0.3937	0.7690867632	0.7756043304
1.026787801	1	1	82.54453613	156248.5741
0.06285894018	0.05817432249	0.06784824972	4.603241341e-006	0.06784824972
78.98321447	133.2015352	103.8097165	86.98020428	79.93021694
80.19684936	74.74341286	4.194648064	4.221611025	2.093147445
0.6663049238	0.6792415901	0.6792415901	2.259552713	1.683354547
0.03821060431	972.4422902	955.5859803	0.6782387624	0.6258506604
0.0003589219108	0.0002708455167	1.239961938e-005	1.351988856e-005	
1557.313033	1541.374625	474.1802046	493.8110579	1.160047378
1.054203789	1.091203789	0.454960054	0.6250853515	2748.532983
2741.719383	330.7323144	435.1836259	2681.544319	104.4513115
2313.349357	364.3050337	334.703677	335.8251321	312.9600719
KEY POINT #7 (t plus 2869.2461 s with a Mixing Number of 62.0954): 51.65704772				
0.040894	0.00925	0.3937	0.7690867632	0.7756043304
1.026787801	1	1	82.54453613	156248.5741
0.06285894018	0.05817432249	0.06784824972	4.603241341e-006	0.06784824972
78.98321447	133.2015352	103.8097165	86.98020428	79.93021694
80.19684936	74.74341286	4.194648064	4.221611025	2.093147445
0.6663049238	0.6792415901	0.6792415901	2.259552713	1.683354547
0.03821060431	972.4422902	955.5859803	0.6782387624	0.6258506604
0.0003589219108	0.0002708455167	1.239961938e-005	1.351988856e-005	
1557.313033	1541.374625	474.1802046	493.8110579	1.160047378
1.054203789	1.091203789	0.454960054	0.6250853515	2748.532983
2741.719383	330.7323144	435.1836259	2681.544319	104.4513115
2313.349357	364.3050337	334.703677	335.8251321	312.9600719
KEY POINT #8 (t plus 3468.7574 s with a Mixing Number of 82.0868): 51.70324864				
0.040894	0.00925	0.3937	0.768460622	0.7761826512
1.026211766	1	1	82.46212694	156673.4035
0.06144618975	0.05817296579	0.06790893168	4.98967612e-006	0.06790893168
86.63515218	132.5661697	103.8166933	95.08371201	88.11956258
87.04263599	79.53904283	4.201570342	4.22162041	2.093177196
0.6711412026	0.6792441452	0.6792441452	2.046843941	1.683232287
0.03821173976	967.5634903	955.5808509	0.6783930763	0.6270399455
0.0003269542558	0.0002708262622	1.239985824e-005	1.349528766e-005	
1554.628409	1541.367422	474.1836839	493.406188	1.160329582

1.055964693	1.092964693	0.6167817197	0.8486996614	2747.235775
2740.435773	362.8553513	435.2131002	2681.55518	72.35774886
2312.022675	398.3898404	369.0919814	364.5689101	333.0691078
KEY POINT #9 (t plus 3512.8539 s with a Mixing Number of 84.3811): 51.77788195				
0.040894	0.00925	0.3937	0.7684902086	0.776300988
1.026218457	1	1	82.55264555	156892.1765
0.06133252794	0.05817092476	0.06800695779	3.677493156e-006	0.06800695779
87.24420849	132.5832419	103.8271889	96.09673537	88.71534285
87.65512861	80.13347026	4.202173956	4.221634531	2.093221961
0.6714928657	0.679247988	0.679247988	2.031472139	1.683048395
0.03821344813	967.1627128	955.5731338	0.6786252752	0.6272443664
0.0003246222224	0.0002707973009	1.240021758e-005	1.349592282e-005	
1554.324321	1541.356585	474.1889176	493.4156518	1.160754229
1.056235929	1.093235929	0.6315014598	0.880821321	2747.281348
2740.466408	365.4145494	435.2574404	2681.571519	69.84289097
2312.023907	402.6559429	371.5962837	367.1427942	335.5629582
KEY POINT #10 (t plus 3622.2572 s with a Mixing Number of 89.853): 51.94588295				
0.040894	0.00925	0.3937	0.7684206672	0.7764638653
1.026259025	1	1	82.75674152	157370.1901
0.0610878574	0.0581655426	0.06822761643	5.246619366e-006	0.06822761643
88.55206712	132.6537889	103.8548646	97.34215296	90.45933632
90.10421011	85.1801	4.203496462	4.221671778	2.093340043
0.6722316632	0.6792581145	0.6792581145	1.999170155	1.682563688
0.03821795422	966.2960061	955.5527827	0.6792378644	0.6277419406
0.0003197113381	0.0002707209604	1.240116512e-005	1.349858532e-005	
1553.627846	1541.327991	474.2027166	493.4568481	1.161874585
1.057005945	1.094005945	0.664103462	0.9216886986	2747.447358
2740.59868	370.911321	435.3743607	2681.614601	64.46303974
2312.072997	407.9024201	378.9290971	377.4383901	356.7479009
KEY POINT #11 (t plus 4542.4798 s with a Mixing Number of 269.8203): 53.67577785				
0.040894	0.00925	0.3937	0.7659172293	0.775981586
1.026140655	1	1	81.67941967	162121.0012
0.0587272918	0.05789498517	0.07049972346	4.164687906e-006	0.07049972346
100.9566149	133.7946936	105.2438258	103.9708686	101.2145594
101.1894986	97.89145848	4.217840967	4.223562777	2.099348558
0.6781534697	0.6797543993	0.6797543993	1.734891258	1.658589558
0.03844659569	957.6727382	954.5270219	0.7105652181	0.6571906228
0.000278939518	0.0002669389822	1.244873914e-005	1.353937641e-005	
1544.218921	1539.86433	474.8918945	493.9951316	1.21926012
1.115631999	1.152631999	1.049294316	1.166580326	2749.063671
2742.392143	423.1438127	441.2436562	2683.771009	18.09984352
2307.820015	2681.979561	424.230552	424.1274607	410.2262015
KEY POINT #12 (t plus 0 s with a Mixing Number of 32.7622): 51.68433553 0.040894				
0.00925	0.3937	0.7701249014	0.7718899222	1.024235576
1	1	83.92824409	157890.1249	0.06947577248
0.05831310271	0.06788409051	2.580138907e-006	0.06788409051	40.74070806
129.7014415	103.0954497	41.23768898	40.48075873	40.53160571
36.98498522	4.178535923	4.220655847	2.090122876	0.6295715819
0.6789768643	0.6789768643	4.273203676	1.695965174	0.03809500515
991.9390833	956.1099702	0.6625909544	0.6158391672	0.0006438349814
0.0002728299009	1.237517059e-005	1.338639271e-005	1532.577289	
1542.104435	473.8231357	491.6751017	1.131454261	1.022295431
1.059295431	0.07681063294	0.07885807988	2741.962786	2734.918836
170.7234708	432.1664867	2680.430854	261.4430159	2309.7963
172.8001242	169.6357584	169.8513222	155.0354764	
KEY POINT #13 (t plus 4542.4798 s with a Mixing Number of 269.8203): 53.67577785				
0.040894	0.00925	0.3937	0.7659172293	0.775981586
1.026140655	1	1	81.67941967	162121.0012
0.0587272918	0.05789498517	0.07049972346	4.164687906e-006	0.07049972346
100.9566149	133.7946936	105.2438258	103.9708686	101.2145594
101.1894986	97.89145848	4.217840967	4.223562777	2.099348558
0.6781534697	0.6797543993	0.6797543993	1.734891258	1.658589558
0.03844659569	957.6727382	954.5270219	0.7105652181	0.6571906228
0.000278939518	0.0002669389822	1.244873914e-005	1.353937641e-005	
1544.218921	1539.86433	474.8918945	493.9951316	1.21926012
1.115631999	1.152631999	1.049294316	1.166580326	2749.063671

At plume detection, the condensing and condensing+cooling flows are 1.4959 and -421.5113 kg/s, respectively

The plume period had a mean steam enthalpy of 2730.9264 +/- 0 kJ/kg.

Maximum Smoothed Top-Mid delta T is 0.75278 degrees C at t plus 3958.9644 s with T_upper = 77.3937 C and T_mid = 76.641 C

At t plus 3958.9644 s, Smoothed SP8-SP9 is 0.67974 C and Smoothed SP8-Top is -0.073033 C, where Smoothed SP8 is 77.3207 C and Pool P = 20.4281 psia

Maximum Smoothed Top-Lower delta T is 1.5446 degrees C at t plus 5365.3899 s with T_upper = 90.2976 C and T_low = 88.753 C

At t plus 5365.3899 s, Smoothed SP8-SP9 is -1.831 C and Smoothed SP8-Top is -0.31464 C, where Smoothed SP8 is 89.9829 C and Pool P = 24.807 psia

Maximum Smoothed Mid-Lower delta T is 3.1441 degrees C at t plus 5400.9889 s with T_mid = 92.2263 C and T_low = 89.0821 C

At t plus 5400.9889 s, Smoothed SP8-SP9 is -1.8159 C and Smoothed SP8-Top is -0.19133 C, where Smoothed SP8 is 90.4104 C and Pool P = 24.9471 psia

Maximum Smoothed Top-Outlet delta T is 3.3265 degrees C at t plus 4961.4818 s with T_upper = 86.6919 C and T_out = 83.3655 C

At t plus 4961.4818 s, Smoothed SP8-SP9 is -1.145 C and Smoothed SP8-Top is -0.34236 C, where Smoothed SP8 is 86.3496 C and Pool P = 23.3866 psia

Maximum Smoothed Mid-Outlet delta T is 4.7304 degrees C at t plus 5401.0859 s with T_mid = 92.2267 C and T_out = 87.4963 C

At t plus 5401.0859 s, Smoothed SP8-SP9 is -1.8152 C and Smoothed SP8-Top is -0.19126 C, where Smoothed SP8 is 90.4115 C and Pool P = 24.9469 psia

Maximum Smoothed Lower-Outlet delta T is 3.0461 degrees C at t plus 1714.6251 s with T_low = 57.1912 C and T_out = 54.1451 C

At t plus 1714.6251 s, Smoothed SP8-SP9 is -0.47117 C and Smoothed SP8-Top is -0.078093 C, where Smoothed SP8 is 56.0294 C and Pool P = 16.4601 psia

Maximum Smoothed Condensing Region SP8-SP9 delta T is 0.68119 degrees C at (KEY POINT #14) t plus 3958.6604 s with T_SP8 = 77.3176 C and T_SP9 = 76.6364 C and Pool P = 20.427 psia

Maximum Smoothed Condensing Region SP8-Upper delta T is 0.55772 degrees C at t plus 6036.9973 s with T_SP8 = 96.0226 C and T_upper = 95.4649 C and Pool P = 27.5682 psia

Maximum Top-Mid delta T is 2.2723 degrees C at (KEY POINT #4) t plus 5678.2898 s ignoring SP 4, with temperatures of 93.496 and 91.2238 C, respectively, at Set # 2, where Pool P = 26.0339 psia and T_outlet = 89.8876 C

Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 6044.7987 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.99938 C and a raw SP12 Reading of 94.4687 C.

Maximum Top-Lower delta T is 2.4311 degrees C at t plus 5753.7931 s, with temperatures of 94.0925 and 91.6614 C, respectively, at Set # 2, where Pool P = 26.3566 psia and T_outlet = 90.6283 C

Maximum Mid-Low delta T is 2.149 degrees C at (KEY POINT #6) t plus 180.9034 s ignoring SP 4, with temperatures of 43.6847 and 41.5356 C, respectively, at Set # 2, where Pool P = 15.2104 psia and T_outlet = 40.409 C

Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 180.9034 s with a Smoothed Mid-Axis Mid-Low Delta T of 0.14214 C and a raw SP12 Reading of 43.6847 C.

Maximum Top-Outlet delta T is 3.8744 degrees C at t plus 4976.6807 s, with temperatures of 87.3875 and 83.5131 C, respectively, at Set # 1, where Pool P = 23.4261 psia

Maximum Mid-Outlet delta T is 3.887 degrees C at t plus 3502.3553 s ignoring SP 4, with temperatures of 73.7224 and 69.8355 C, respectively, at Set # 2, where Pool P = 19.3279 psia

Maximum Lower-Outlet delta T is 4.0989 degrees C at (KEY POINT #8) t plus 3541.4566 s, with temperatures of 74.6185 and 70.5196 C, respectively, at Set # 1, where Pool P = 19.4227 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 3831.5592 s with a Smoothed Mid-Axis Low-Outlet Delta T of 1.3659 C and a raw SP12 Reading of 74.9839 C.

Minimum SP Pressure is 15.1088 psia at t plus 1.0001 s

Maximum SP Pressure is 38.9981 psia at t plus 8080.2302 s

Beginning SP Pressure is 15.1193 psia

Ending SP Pressure is 38.995 psia

Time-Average SP Pressure is 22.7706 +/- 6.8216 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 76.0129 cm (cold) / 76.146 cm (hot) at 14.6981 psia

Beginning Smoothed SP Level is 76.5224 cm (cold) / 76.69 cm (hot) at 15.113 psia

Ending Smoothed SP Level is 79.3506 cm (cold) / 80.7706 cm (hot) at 39.0016 psia

Minimum Smoothed Cold SP Level is 76.2505 cm at t plus 4578.9729 s and 22.1529 psia

Minimum Smoothed Hot SP Level is 76.6787 cm at t plus 198.2033 s and 15.219 psia

Maximum Smoothed Cold SP Level is 80.6387 cm at t plus 6970.5107 s and 32.1146 psia
 Maximum Smoothed Hot SP Level is 81.8884 cm at t plus 6985.9156 s and 32.2023 psia
 SP 12 Temperature at the beginning is 40.2622 C, and at the end is 112.9122 C
 At plume detection, the Mixing Number is 195.3685
 The Mixing Number ranges from a minimum of 32.4148 at (KEY POINT #12) t plus 0 s to a
 maximum of 195.3685 at (KEY POINT #13) t plus 8080.5292 s; it had a mean value of
 81.9616 +/- 46.0899 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 32.4148): 33.55182244 0.040894
 0.00925 0.3937 0.7652243623 0.7668997726 1.015870168
 1 1 57.74794494 105981.3929 0.06955889984
 0.05879671561 0.04406818678 1.839331257e-006 0.04406818678 40.2300938
 118.0485361 100.5970626 39.9570382 40.11766023 41.23101032
 38.87105828 4.178533141 4.217402518 2.07986903 0.6289273713
 0.6780018637 0.6780018637 4.318308822 1.741579006 0.03770055929
 992.1307755 957.9247558 0.6101525993 0.5810288639 0.0006499655559
 0.0002799812934 1.228973993e-005 1.294631246e-005 1531.727723
 1544.538309 472.5607081 484.4735547 1.035980073 1.042002762
 1.079002762 0.07475496621 0.07367530141 2715.633756 2712.298931
 168.5915961 421.6186176 2676.513373 253.0270215 2294.015138
 167.4506237 168.1202823 172.7755478 162.9184026

KEY POINT #2 (t plus 8080.5292 s with a Mixing Number of 195.3685): 36.82799728
 0.040894 0.00925 0.3937 0.7935061475 0.8077063997
 1.005470095 1 1 25.57441478 111676.9483
 0.05623358903 0.05310204147 0.04837123425 8.544358399e-006 0.04837123425
 113.678492 134.5574126 129.1731795 113.6174221 113.9351938
 113.776728 111.2981221 4.235716719 4.263220091 2.231406392
 0.6823377877 0.6847401125 0.6847401125 1.52657253 1.334474092
 0.04325184706 948.1577854 935.5319428 1.462443396 1.440287214
 0.0002459177967 0.0002143375009 1.32724701e-005 1.348572058e-005
 1530.038224 1506.427662 485.6667753 489.6155469 2.636431467
 2.689068211 2.726068211 1.620144448 1.616895565 2731.504134
 2730.850083 477.0278822 542.8577658 2718.94667 65.82988358
 2188.646368 476.7692114 478.1140272 477.4452816 466.9543239

KEY POINT #3 (t plus 8080.5292 s with a Mixing Number of 195.3685): 36.82799728
 0.040894 0.00925 0.3937 0.7935061475 0.8077063997
 1.005470095 1 1 25.57441478 111676.9483
 0.05623358903 0.05310204147 0.04837123425 8.544358399e-006 0.04837123425
 113.678492 134.5574126 129.1731795 113.6174221 113.9351938
 113.776728 111.2981221 4.235716719 4.263220091 2.231406392
 0.6823377877 0.6847401125 0.6847401125 1.52657253 1.334474092
 0.04325184706 948.1577854 935.5319428 1.462443396 1.440287214
 0.0002459177967 0.0002143375009 1.32724701e-005 1.348572058e-005
 1530.038224 1506.427662 485.6667753 489.6155469 2.636431467

2.689068211	2.726068211	1.620144448	1.616895565	2731.504134
2730.850083	477.0278822	542.8577658	2718.94667	65.82988358
2188.646368	476.7692114	478.1140272	477.4452816	466.9543239
KEY POINT #4 (t plus 5678.2898 s with a Mixing Number of 103.4476): 35.761256				
0.040894	0.00925	0.3937	0.7821444864	0.7913360181
1.013120626	1	1	37.29900747	109544.1864
0.06004540175	0.05576334802	0.04697013736	6.585544827e-006	0.04697013736
94.07662257	129.7422211	116.0375963	92.98676881	92.90841221
91.56097603	89.99737093	4.209316204	4.239744441	2.151904
0.6751490465	0.6828254629	0.6828254629	1.872504458	1.493570594
0.04040040562	962.5691675	946.2656363	0.9962651249	0.9589067486
0.0003003384726	0.0002405446947	1.281954291e-005	1.3350054e-005	
1550.193323	1526.642571	480.0162515	489.5441399	1.749809034
1.794954505	1.831954505	0.817736807	0.7852932384	2730.553453
2729.162237	394.2064324	486.9552264	2700.124076	92.74879398
2243.598227	389.6195667	389.2885347	383.6222231	377.049705
KEY POINT #5 (t plus 6044.7987 s with a Mixing Number of 115.1503): 35.92716371				
0.040894	0.00925	0.3937	0.7915825059	0.8017350244
1.012014591	1	1	35.30662708	109911.6328
0.05944053984	0.05539098731	0.0471880466	6.604680018e-006	0.0471880466
97.24791458	130.3509709	117.8972057	96.07147321	95.55059515
95.11499599	93.44987066	4.213020881	4.242806876	2.162076764
0.6766311273	0.6832163576	0.6832163576	1.806489448	1.468537378
0.04077082211	960.3552305	944.7910535	1.053749771	1.017718067
0.0002901307698	0.0002364775931	1.288358167e-005	1.336715137e-005	
1547.710565	1524.046935	480.8562711	489.5646117	1.857904784
1.903239769	1.940239769	0.918542338	0.8800081974	2730.639422
2729.392864	407.5694596	494.8500079	2702.864473	87.28054836
2235.789414	402.6139199	400.4190498	398.5875199	391.5815792
KEY POINT #6 (t plus 180.9034 s with a Mixing Number of 33.148): 33.23039871				
0.040894	0.00925	0.3937	0.7649774413	0.7667936222
1.017320634	1	1	57.15347246	104428.6649
0.06923962653	0.05876693718	0.04364601714	4.768104543e-006	0.04364601714
42.18651832	119.8091053	100.7513252	41.82716732	41.70396736
42.96699292	40.40062134	4.178557388	4.217599462	2.080487747
0.6313759588	0.678064283	0.678064283	4.148720663	1.738693019
0.03772447515	991.3665264	957.8135181	0.6132891097	0.5814874851
0.0006268676586	0.0002795300137	1.229501074e-005	1.301293975e-005	
1534.908721	1544.393438	472.6392575	485.6049565	1.041675199
1.048727235	1.085727235	0.0828980668	0.0813474899	2719.071926
2715.805406	176.7671833	422.2696472	2676.756268	245.5024639
2296.802279	175.2656169	174.7493208	180.0300361	169.3103241
KEY POINT #7 (t plus 180.9034 s with a Mixing Number of 33.148): 33.23039871				
0.040894	0.00925	0.3937	0.7649774413	0.7667936222
1.017320634	1	1	57.15347246	104428.6649
0.06923962653	0.05876693718	0.04364601714	4.768104543e-006	0.04364601714
42.18651832	119.8091053	100.7513252	41.82716732	41.70396736
42.96699292	40.40062134	4.178557388	4.217599462	2.080487747
0.6313759588	0.678064283	0.678064283	4.148720663	1.738693019
0.03772447515	991.3665264	957.8135181	0.6132891097	0.5814874851
0.0006268676586	0.0002795300137	1.229501074e-005	1.301293975e-005	
1534.908721	1544.393438	472.6392575	485.6049565	1.041675199
1.048727235	1.085727235	0.0828980668	0.0813474899	2719.071926
2715.805406	176.7671833	422.2696472	2676.756268	245.5024639
2296.802279	175.2656169	174.7493208	180.0300361	169.3103241
KEY POINT #8 (t plus 3541.4566 s with a Mixing Number of 57.3728): 34.50061791				
0.040894	0.00925	0.3937	0.7635368906	0.7688516703
1.017902958	1	1	48.42890934	106507.6921
0.06392259955	0.05755200661	0.04531436933	7.081764497e-006	0.04531436933
73.11688288	126.3396472	106.9982346	72.95975306	72.88947597
73.3049675	70.59705352	4.190105063	4.226012498	2.107172788
0.6620762699	0.6803479425	0.6803479425	2.450804953	1.629267886
0.03874249727	975.9846459	953.2190997	0.7518045389	0.7125085028
0.0003872503856	0.0002622966815	1.250888321e-005	1.324663262e-005	
1557.920538	1537.936026	475.7529268	488.9278303	1.29506641
1.339138946	1.376138946	0.3565371776	0.3541705808	2728.887412

2726.542053	306.1617137	448.6612356	2686.478505	142.499522
2280.226176	305.5033318	305.2074935	306.9512793	295.6106832
KEY POINT #9 (t plus 8080.5292 s with a Mixing Number of 195.3685): 36.82799728				
0.040894	0.00925	0.3937	0.7935061475	0.8077063997
1.005470095	1	1	25.57441478	111676.9483
0.05623358903	0.05310204147	0.04837123425	8.544358399e-006	0.04837123425
113.678492	134.5574126	129.1731795	113.6174221	113.9351938
113.776728	111.2981221	4.235716719	4.263220091	2.231406392
0.6823377877	0.6847401125	0.6847401125	1.52657253	1.334474092
0.04325184706	948.1577854	935.5319428	1.462443396	1.440287214
0.0002459177967	0.0002143375009	1.32724701e-005	1.348572058e-005	
1530.038224	1506.427662	485.6667753	489.6155469	2.636431467
2.689068211	2.726068211	1.620144448	1.616895565	2731.504134
2730.850083	477.0278822	542.8577658	2718.94667	65.82988358
2188.646368	476.7692114	478.1140272	477.4452816	466.9543239
KEY POINT #10 (t plus 3831.5592 s with a Mixing Number of 60.8046): 34.70579838				
0.040894	0.00925	0.3937	0.7634351623	0.7691326628
1.017520698	1	1	47.06630177	106991.2331
0.06347681424	0.05734861253	0.04558386085	4.053825826e-006	0.04558386085
75.58695426	126.8972779	108.0353399	75.91332896	75.77629346
75.8695081	73.63971545	4.191894021	4.22749301	2.111924069
0.6639233239	0.6806814122	0.6806814122	2.366861963	1.612421284
0.03892122342	974.5188688	952.4395163	0.7770835446	0.7374466126
0.0003748698926	0.0002596208188	1.254446299e-005	1.326518891e-005	
1557.861238	1536.75489	476.2568891	489.1248792	1.341676101
1.386264217	1.423264217	0.3955302184	0.4009412916	2729.444691
2727.229454	316.517565	453.0482398	2688.070308	136.5306748
2276.396451	317.8857336	317.3098998	317.7034799	308.3614513
KEY POINT #11 (t plus 8080.5292 s with a Mixing Number of 195.3685): 36.82799728				
0.040894	0.00925	0.3937	0.7935061475	0.8077063997
1.005470095	1	1	25.57441478	111676.9483
0.05623358903	0.05310204147	0.04837123425	8.544358399e-006	0.04837123425
113.678492	134.5574126	129.1731795	113.6174221	113.9351938
113.776728	111.2981221	4.235716719	4.263220091	2.231406392
0.6823377877	0.6847401125	0.6847401125	1.52657253	1.334474092
0.04325184706	948.1577854	935.5319428	1.462443396	1.440287214
0.0002459177967	0.0002143375009	1.32724701e-005	1.348572058e-005	
1530.038224	1506.427662	485.6667753	489.6155469	2.636431467
2.689068211	2.726068211	1.620144448	1.616895565	2731.504134
2730.850083	477.0278822	542.8577658	2718.94667	65.82988358
2188.646368	476.7692114	478.1140272	477.4452816	466.9543239
KEY POINT #12 (t plus 0 s with a Mixing Number of 32.4148): 33.55182244 0.040894				
0.00925	0.3937	0.7652243623	0.7668997726	1.015870168
1	1	57.74794494	105981.3929	0.06955889984
0.05879671561	0.04406818678	1.839331257e-006	0.04406818678	40.2300938
118.0485361	100.5970626	39.9570382	40.11766023	41.23101032
38.87105828	4.178533141	4.217402518	2.07986903	0.6289273713
0.6780018637	0.6780018637	4.318308822	1.741579006	0.03770055929
992.1307755	957.9247558	0.6101525993	0.5810288639	0.0006499655559
0.0002799812934	1.228973993e-005	1.294631246e-005	1531.727723	
1544.538309	472.5607081	484.4735547	1.035980073	1.042002762
1.079002762	0.07475496621	0.07367530141	2715.633756	2712.298931
168.5915961	421.6186176	2676.513373	253.0270215	2294.015138
167.4506237	168.1202823	172.7755478	162.9184026	
KEY POINT #13 (t plus 8080.5292 s with a Mixing Number of 195.3685): 36.82799728				
0.040894	0.00925	0.3937	0.7935061475	0.8077063997
1.005470095	1	1	25.57441478	111676.9483
0.05623358903	0.05310204147	0.04837123425	8.544358399e-006	0.04837123425
113.678492	134.5574126	129.1731795	113.6174221	113.9351938
113.776728	111.2981221	4.235716719	4.263220091	2.231406392
0.6823377877	0.6847401125	0.6847401125	1.52657253	1.334474092
0.04325184706	948.1577854	935.5319428	1.462443396	1.440287214
0.0002459177967	0.0002143375009	1.32724701e-005	1.348572058e-005	
1530.038224	1506.427662	485.6667753	489.6155469	2.636431467
2.689068211	2.726068211	1.620144448	1.616895565	2731.504134
2730.850083	477.0278822	542.8577658	2718.94667	65.82988358
2188.646368	476.7692114	478.1140272	477.4452816	466.9543239

KEY POINT #14 (t plus 3958.6604 s with a Mixing Number of 62.3619): 34.80153111

0.040894	0.00925	0.3937	0.7633234248	0.7691920613
1.017264298	1	1	46.43733665	107243.0228
0.06328649215	0.05725372688	0.0457095997	2.663509935e-006	0.0457095997
76.63643658	127.0723494	108.518331	77.3176262	77.38820582
76.76706078	74.67350222	4.192692033	4.228190764	2.114169298
0.6646827353	0.6808323184	0.6808323184	2.332705774	1.604695727
0.03900543883	973.8865081	952.0748345	0.7890895551	0.7494736244
0.0003698123407	0.0002583915374	1.256103916e-005	1.327054923e-005	
1557.762919	1536.194466	476.490303	489.159937	1.363849315
1.408566135	1.445566135	0.4131522933	0.424940232	2729.529375
2727.372949	320.9190948	455.0918716	2688.809384	134.1727767
2274.437504	323.7752947	324.0698903	321.4682139	312.6956707

End

D.16 TEST #16 - T16_SRV_15PSIG_107KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T16_SRV_15PSIG_107kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1804.5682 s, and ending (KEY POINT #11) at t plus 9924.8937 s, for a time period of 8120.3254 s.
Original Data Record Time: 13185.4462 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 4231.266 s, T_bulk = 79.2303 C and T_out = 76.3907 C
Stratification Beginning SP12 Temperature = 80.0208 C
Stratification Beginning Pressure = 37.4766 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 8090.7348 s, T_bulk = 112.3248 C and T_out = 110.841 C
Stratification Ending SP12 Temperature = 112.169 C
Stratification Ending Pressure = 56.6525 psia
No Plume detected, setting t_plume (KEY POINT #2) to the end at 8120.3254 s.
At t = 8120.3254 s, the pool pressure is 56.8624 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 113.3683, 114.6837, 112.8655, 112.7627, and 111.0746 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 0 +/- 0 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 0 +/- 0 C.
Minimum Steam Quality: 0.99716 at t plus 7987.1248 s
Maximum Steam Quality: 1.0095 at t plus 1713.328 s
Time-Averaged Steam Quality: 1.0045 +/- 0.0025327
SRV Alignment, no RCIC Turbine 0 0 0 0 0
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 8030.3263 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.72163 degrees/min at t plus 53.8991 s and 0.45607 degrees/min at t plus 6218.6987 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.83863 degrees/min at t plus 4348.8677 s and 0.34817 degrees/min at t plus 5146.4804 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.21007 degrees/min at t plus 4507.9698 s and -0.27599 degrees/min at t plus 4348.7697 s, respectively
Max and min smoothed lower level changerates: 0.83297 degrees/min at t plus 4.2992 s and 0.36669 degrees/min at t plus 3169.2613 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.43272 degrees/min at t plus 4374.4682 s and -0.24998 degrees/min at t plus 5146.4804 s, respectively
Max and min smoothed outlet level changerates: 1.1122 degrees/min at t plus 57.8013 s and 0.3044 degrees/min at t plus 4362.5705 s, respectively
Max and min smoothed lower-outlet level changerate differences: 0.22513 degrees/min at t plus 4273.5674 s and -0.39386 degrees/min at t plus 64.8997 s, respectively
Max and min smoothed hot (SP8) level changerates: 0.75423 degrees/min at t plus 19.1991 s and 0.38328 degrees/min at t plus 7257.4121 s, respectively
Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.233 degrees/min at t plus 4508.1699 s and -0.25396 degrees/min at t plus 4348.7697 s, respectively
The mean steam flow rate was 45.4994 +/- 1.2376 g/s

The mean feedwater flow rate was 45.4051 +/- 1.7748 g/s
 The mean water injection to steam flow rate was 0.0060864 +/- 0.028913 g/s
 Mean Smoothed Condensing Region SP8-SP9 delta T is -0.87944 +/- 0.46871 C over the Stratification Period, beginning at -0.056923 C and ending at -1.8143 C
 Mean Smoothed SP8-Upper Pool delta T is -0.0098849 +/- 0.30891 C over the Stratification Period, beginning at -0.50933 C and ending at -0.57295 C
 The stratification period begins and ends with Smoothed SP8 readings of 78.8443 and 112.5171 C, respectively
 The stratification period begins and ends with condensing flows of 0.4716 and 0.82366 kg/s, respectively.
 The stratification period begins and ends with condensing+cooling flows of -458.1989 and -13.948 kg/s, respectively.
 The stratification period had a mean sparger steam enthalpy of 2734.6286 +/- 1.1606 kJ/kg. At plume detection, the condensing and condensing+cooling flows are 0.83007 and -13.9142 kg/s, respectively
 The plume period had a mean steam enthalpy of 0 +/- 0 kJ/kg.
 Maximum Smoothed Top-Mid delta T is 0.63772 degrees C at t plus 4590.3736 s with T_upper = 82.7355 C and T_mid = 82.0978 C
 At t plus 4590.3736 s, Smoothed SP8-SP9 is 0.27001 C and Smoothed SP8-Top is -0.36771 C, where Smoothed SP8 is 82.3678 C and Pool P = 38.6346 psia
 Maximum Smoothed Top-Lower delta T is 2.0334 degrees C at t plus 5081.2796 s with T_upper = 87.2368 C and T_low = 85.2035 C
 At t plus 5081.2796 s, Smoothed SP8-SP9 is -0.8101 C and Smoothed SP8-Top is -0.23583 C, where Smoothed SP8 is 87.001 C and Pool P = 40.3947 psia
 Maximum Smoothed Mid-Lower delta T is 3.2759 degrees C at t plus 5752.889 s with T_mid = 94.6954 C and T_low = 91.4195 C
 At t plus 5752.889 s, Smoothed SP8-SP9 is -1.2971 C and Smoothed SP8-Top is 0.35431 C, where Smoothed SP8 is 93.3984 C and Pool P = 43.1819 psia
 Maximum Smoothed Top-Outlet delta T is 4.3631 degrees C at t plus 4529.7711 s with T_upper = 82.323 C and T_out = 77.9599 C
 At t plus 4529.7711 s, Smoothed SP8-SP9 is -0.24088 C and Smoothed SP8-Top is -0.32871 C, where Smoothed SP8 is 81.9943 C and Pool P = 38.4438 psia
 Maximum Smoothed Mid-Outlet delta T is 4.6953 degrees C at t plus 4433.2716 s with T_mid = 82.0683 C and T_out = 77.373 C
 At t plus 4433.2716 s, Smoothed SP8-SP9 is -1.1271 C and Smoothed SP8-Top is -0.357 C, where Smoothed SP8 is 80.9412 C and Pool P = 38.1157 psia
 Maximum Smoothed Lower-Outlet delta T is 3.715 degrees C at t plus 0.49802 s with T_low = 39.8273 C and T_out = 36.1124 C
 At t plus 0.49802 s, Smoothed SP8-SP9 is 0.047538 C and Smoothed SP8-Top is 0.026447 C, where Smoothed SP8 is 39.0603 C and Pool P = 30.2156 psia
 Maximum Smoothed Condensing Region SP8-SP9 delta T is 0.31735 degrees C at (KEY POINT #14) t plus 5592.4859 s with T_SP8 = 91.9144 C and T_SP9 = 91.5971 C and Pool P = 42.4639 psia
 Maximum Smoothed Condensing Region SP8-Upper delta T is 0.64225 degrees C at t plus 6470.1021 s with T_SP8 = 99.5712 C and T_upper = 98.929 C and Pool P = 46.6315 psia
 Maximum Top-Mid delta T is 2.3661 degrees C at (KEY POINT #4) t plus 4645.7487 s ignoring SP 4, with temperatures of 84.038 and 81.6718 C, respectively, at Set # 2, where Pool P = 38.8241 psia and T_outlet = 79.2743 C
 Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 4645.7487 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.57623 C and a raw SP12 Reading of 81.6718 C.
 Maximum Top-Lower delta T is 3.0432 degrees C at t plus 4739.1611 s, with temperatures of 85.4137 and 82.3706 C, respectively, at Set # 2, where Pool P = 39.1513 psia and T_outlet = 80.4038 C
 Maximum Mid-Low delta T is 2.9603 degrees C at (KEY POINT #6) t plus 3673.2651 s ignoring SP 4, with temperatures of 75.8089 and 72.8486 C, respectively, at Set # 2, where Pool P = 35.8901 psia and T_outlet = 70.8769 C
 Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 3704.1579 s with a Smoothed Mid-Axis Mid-Low Delta T of 0.99877 C and a raw SP12 Reading of 74.7418 C.
 Maximum Top-Outlet delta T is 5.2852 degrees C at t plus 4532.0722 s, with temperatures of 83.2471 and 77.9619 C, respectively, at Set # 2, where Pool P = 38.4589 psia
 Maximum Mid-Outlet delta T is 5.151 degrees C at t plus 4566.0692 s ignoring SP 4, with temperatures of 83.4165 and 78.2655 C, respectively, at Set # 2, where Pool P = 38.5583 psia
 Maximum Lower-Outlet delta T is 5.5323 degrees C at (KEY POINT #8) t plus 75.4013 s, with temperatures of 43.0812 and 37.5489 C, respectively, at Set # 1, where Pool P = 30.2572 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 2134.6321 s with a Smoothed Mid-Axis Low-Outlet Delta T of 1.8435 C and a raw SP12 Reading of 58.9462 C.

Minimum SP Pressure is 30.2003 psia at t plus 0 s
 Maximum SP Pressure is 56.8624 psia at t plus 8120.3254 s
 Beginning SP Pressure is 30.2003 psia
 Ending SP Pressure is 56.8624 psia
 Time-Average SP Pressure is 39.143 +/- 7.6325 psia

SP Levels are fully corrected and compensated
 Pre-Start SP Level is 75.864 cm (cold) / 76.0054 cm (hot) at 14.8335 psia
 Beginning Smoothed SP Level is 76.1925 cm (cold) / 76.3493 cm (hot) at 30.2028 psia
 Ending Smoothed SP Level is 75.4925 cm (cold) / 76.703 cm (hot) at 56.8681 psia
 Minimum Smoothed Cold SP Level is 75.4925 cm at t plus 8120.3254 s and 56.8681 psia
 Minimum Smoothed Hot SP Level is 76.3412 cm at t plus 619.4104 s and 30.6902 psia
 Maximum Smoothed Cold SP Level is 76.1962 cm at t plus 18.402 s and 30.22 psia
 Maximum Smoothed Hot SP Level is 76.8705 cm at t plus 6885.0088 s and 48.9007 psia
 SP 12 Temperature at the beginning is 40.8347 C, and at the end is 112.3775 C
 At plume detection, the Mixing Number is 149.394

The Mixing Number ranges from a minimum of 38.282 at (KEY POINT #12) t plus 22.3013 s to a maximum of 149.394 at (KEY POINT #13) t plus 8120.3254 s; it had a mean value of 74.5955 +/- 30.9504 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) gl, Sparger Diameter (m) dl, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) mdl, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m3) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 38.319): 44.3605796 0.040894
 0.00925 0.3937 0.7619251712 0.7634931761 1.008895731
 1 1 38.89162781 135791.2244 0.06975803883
 0.05468051817 0.05826480248 4.655889213e-006 0.05826480248 39.00329936
 130.4961371 121.4252109 39.05288599 39.02386558 39.80849208
 36.09512009 4.178305368 4.248848022 2.182336481 0.6274129077
 0.6838484018 0.6838484018 4.429792284 1.423454114 0.04150282888
 992.6414177 941.9525758 1.170171265 1.140711431 0.0006651760972
 0.0002291037043 1.30051637e-005 1.3359343e-005 1529.779916
 1518.876755 482.414109 488.8587796 2.077990093 2.082409074
 2.119409074 0.07000915884 0.0701958067 2729.063701 2727.551142
 163.557849 509.8447015 2707.99697 346.2868525 2219.218999
 163.7650371 163.6422701 166.9237764 151.4119666

KEY POINT #2 (t plus 8120.3254 s with a Mixing Number of 149.394): 36.05060298
 0.040894 0.00925 0.3937 0.7549249485 0.7670296859
 1.000077362 1 1 17.19319712 107347.7353
 0.05603351208 0.05034345021 0.04735017623 3.520047177e-006 0.04735017623
 114.68371 142.5019146 142.4396297 112.8654742 113.3683238
 112.7627435 111.0745672 4.237013257 4.291658164 2.330629777
 0.682650637 0.6847223067 0.6847223067 1.512223791 1.208944387
 0.04673548864 947.430694 923.9451567 2.097329326 2.096950483
 0.0002436434516 0.000192883766 1.373055124e-005 1.373343698e-005
 1528.970363 1481.796563 490.68042 490.7298621 3.871551464

3.920919676	3.957919676	1.674395619	1.577328432	2737.032759
2736.737153	481.3747075	599.6799517	2736.571839	118.3052442
2137.352807	473.6734652	475.8015689	473.2397961	466.0975831
KEY POINT #3 (t plus 4231.266 s with a Mixing Number of 66.7237): 34.66401947				
0.040894	0.00925	0.3937	0.7607574256	0.7669364495
1.007213958	1	1	25.02758509	104896.7706
0.06287391566	0.05334869101	0.0455289869	9.280096401e-006	0.0455289869
78.90126658	135.1255766	127.970421	78.84434366	79.35367094
78.26095509	76.32027532	4.194245032	4.260886288	2.223367241
0.6663301568	0.6846459339	0.6846459339	2.261737997	1.347449409
0.04296713243	972.5529778	936.5454348	1.413578331	1.385314838
0.000359317165	0.0002165102978	1.323095527e-005	1.3513766e-005	
1557.613485	1508.456586	485.1772753	490.3688854	2.542536727
2.584100982	2.621100982	0.4534424971	0.4523908719	2733.626594
2733.000214	330.510699	537.7251631	2717.277018	207.2144641
2195.901431	330.2719516	332.4069234	327.8266823	319.693133
KEY POINT #4 (t plus 4645.7487 s with a Mixing Number of 72.9754): 34.70463831				
0.040894	0.00925	0.3937	0.7602938458	0.7670203497
1.006531353	1	1	24.21679677	104930.7215
0.06200605114	0.05311620872	0.04558233716	5.506747764e-006	0.04558233716
83.62109029	135.5458062	129.1041718	82.773193	83.24570834
81.77420787	79.31345218	4.198339977	4.263085143	2.230940902
0.6694161291	0.6847351453	0.6847351453	2.125861818	1.335210683
0.04323537711	969.5846057	935.5902579	1.459603524	1.433254417
0.0003389640184	0.0002144610418	1.327008806e-005	1.352522367e-005	
1556.247371	1506.545012	485.6388454	490.3402974	2.630969279
2.676991766	2.713991766	0.5480890733	0.5299630445	2733.651741
2733.065287	350.32365	542.5632049	2718.851182	192.2395549
2191.088536	346.7642168	348.7463923	342.5727819	332.2520069
KEY POINT #5 (t plus 4645.7487 s with a Mixing Number of 72.9754): 34.70463831				
0.040894	0.00925	0.3937	0.7602938458	0.7670203497
1.006531353	1	1	24.21679677	104930.7215
0.06200605114	0.05311620872	0.04558233716	5.506747764e-006	0.04558233716
83.62109029	135.5458062	129.1041718	82.773193	83.24570834
81.77420787	79.31345218	4.198339977	4.263085143	2.230940902
0.6694161291	0.6847351453	0.6847351453	2.125861818	1.335210683
0.04323537711	969.5846057	935.5902579	1.459603524	1.433254417
0.0003389640184	0.0002144610418	1.327008806e-005	1.352522367e-005	
1556.247371	1506.545012	485.6388454	490.3402974	2.630969279
2.676991766	2.713991766	0.5480890733	0.5299630445	2733.651741
2733.065287	350.32365	542.5632049	2718.851182	192.2395549
2191.088536	346.7642168	348.7463923	342.5727819	332.2520069
KEY POINT #6 (t plus 3673.2651 s with a Mixing Number of 60.9434): 34.61197423				
0.040894	0.00925	0.3937	0.7613488802	0.7667555898
1.007876458	1	1	25.99946616	104883.3109
0.06379776266	0.0536196849	0.04546062879	7.070678646e-006	0.04546062879
73.81029683	134.5068858	126.6456292	73.4131548	73.79269719
73.37367683	70.8173745	4.190348755	4.258360145	2.214693565
0.662662452	0.6845234818	0.6845234818	2.426556342	1.362083784
0.04265924547	975.6267938	937.6546293	1.361285975	1.331464168
0.0003837360252	0.0002189524378	1.318523506e-005	1.349520779e-005	
1558.132115	1510.65084	484.6314988	490.301495	2.442278696
2.474988281	2.511988281	0.3671409591	0.3610357534	2733.297935
2732.621962	309.1592966	532.0752014	2715.4249	222.9159049
2201.222733	307.4951892	309.084172	307.3312331	296.6261677
KEY POINT #7 (t plus 3704.1579 s with a Mixing Number of 61.1823): 34.61104682				
0.040894	0.00925	0.3937	0.7613384345	0.7667932694
1.007903245	1	1	25.94696822	104854.2599
0.06375703166	0.05360575853	0.04545941069	1.746221588e-006	0.04545941069
74.03625184	134.5999512	126.7137957	73.67496524	74.12457573
73.6263206	71.06364561	4.190510126	4.258488999	2.21513525
0.6628328385	0.6845302626	0.6845302626	2.418798119	1.361321858
0.0426749426	975.4932672	937.5977387	1.36393804	1.333966113
0.0003825927571	0.0002188255057	1.318758738e-005	1.349858508e-005	
1558.130979	1510.538978	484.6597501	490.3480588	2.447357707
2.480508184	2.517508184	0.3706532225	0.3650508229	2733.447783

2732.774538	310.1065918	532.3658314	2715.520531	222.2592397
2201.081951	308.5926634	310.475342	308.3902887	297.6580904
KEY POINT #8 (t plus 75.4013 s with a Mixing Number of 38.5306): 35.84753478				
0.040894	0.00925	0.3937	0.7619300031	0.7635534098
1.006665033	1	1	31.18277905	110459.3638
0.06962218757	0.05466964447	0.04708345906	8.512448644e-006	0.04708345906
39.84075866	128.2544348	121.4790054	39.88009177	40.05476643
41.13794352	37.62064287	4.178281142	4.248942516	2.182655297
0.6284865432	0.6838569353	0.6838569353	4.352806436	1.422790105
0.0415142935	992.3253655	941.9088815	1.172023539	1.149801811
0.0006547381991	0.0002289945975	1.300701836e-005	1.327138811e-005	
1531.235389	1518.795463	482.4374957	487.2908765	2.081503528
2.086313022	2.123313022	0.07321963494	0.07337349706	2723.696655
2722.724289	167.0573453	510.073514	2708.074541	343.0161687
2213.623141	167.2216901	167.9500231	172.4789326	157.7866087
KEY POINT #9 (t plus 8090.7348 s with a Mixing Number of 147.9155): 36.02949803				
0.040894	0.00925	0.3937	0.7550560711	0.7671243342
1.000214567	1	1	17.25080472	107281.7565
0.05610369207	0.05037223553	0.04732245622	2.324124466e-006	0.04732245622
114.3313645	142.4916385	142.3028669	112.5170855	113.0900366
112.5507349	110.8058416	4.236453363	4.291338399	2.329507541
0.6825665827	0.6847322427	0.6847322427	1.517199454	1.210089552
0.04669624114	947.7065634	924.0684223	2.089814952	2.088671694
0.0002444473143	0.0001930836619	1.37258289e-005	1.373383827e-005	
1529.439585	1482.071005	490.632386	490.7819983	3.856792884
3.906146188	3.943146188	1.65521275	1.559267689	2737.154086
2736.856495	479.8808592	599.0920887	2736.397901	119.2112295
2138.061997	472.1973717	474.6220424	472.341129	464.9594918
KEY POINT #10 (t plus 2134.6321 s with a Mixing Number of 48.8233): 33.81595212				
0.040894	0.00925	0.3937	0.7611930161	0.7647329173
1.008730144	1	1	27.68407982	102958.5529
0.06630684574	0.05420962155	0.04441510433	7.477659779e-006	0.04441510433
59.60374331	132.5717101	123.7493822	59.26162889	59.4047838
60.25577366	57.45699693	4.182313381	4.252996931	2.196386318
0.6504981401	0.6841870551	0.6841870551	3.016653988	1.395379004
0.04200664226	983.4643334	940.0534782	1.252383649	1.221700181
0.0004691967411	0.000224477061	1.308531229e-005	1.343132268e-005	
1553.837945	1515.298177	483.4143702	489.7155489	2.234267875
2.249921914	2.286921914	0.1958284513	0.1927402068	2731.228402
2730.461994	249.672399	519.7354234	2711.329065	270.0630244
2211.492978	248.2415944	248.8388668	252.400994	240.700297
KEY POINT #11 (t plus 8120.3254 s with a Mixing Number of 149.394): 36.05060298				
0.040894	0.00925	0.3937	0.7549249485	0.7670296859
1.000077362	1	1	17.19319712	107347.7353
0.05603351208	0.05034345021	0.04735017623	3.520047177e-006	0.04735017623
114.68371	142.5019146	142.4396297	112.8654742	113.3683238
112.7627435	111.0745672	4.237013257	4.291658164	2.330629777
0.682650637	0.6847223067	0.6847223067	1.512223791	1.208944387
0.04673548864	947.430694	923.9451567	2.097329326	2.096950483
0.0002436434516	0.000192883766	1.373055124e-005	1.373343698e-005	
1528.970363	1481.796563	490.68042	490.7298621	3.871551464
3.920919676	3.957919676	1.674395619	1.577328432	2737.032759
2736.737153	481.3747075	599.6799517	2736.571839	118.3052442
2137.352807	473.6734652	475.8015689	473.2397961	466.0975831
KEY POINT #12 (t plus 22.3013 s with a Mixing Number of 38.282): 36.6914694				
0.040894	0.00925	0.3937	0.7619590862	0.7635292677
1.007897604	1	1	32.05781871	112649.4464
0.06970160672	0.05467669584	0.04819191356	2.16703663e-006	0.04819191356
39.35146379	129.4865925	121.4441215	39.40436703	39.37962795
40.26817108	36.79941125	4.17829328	4.248881232	2.182448522
0.6278607088	0.6838514054	0.6838514054	4.397524187	1.423220614
0.04150685803	992.5106521	941.9372172	1.170822132	1.14459189
0.0006608039379	0.0002290653385	1.300581568e-005	1.331973656e-005	
1530.39036	1518.848187	482.4223314	488.1566911	2.079224632
2.083779135	2.120779135	0.07132879089	0.07153117641	2726.411661
2725.383957	165.012706	509.9251362	2708.024241	344.9124302
2216.486525	165.2337512	165.1288748	168.844563	154.3549489

KEY POINT #13 (t plus 8120.3254 s with a Mixing Number of 149.394): 36.05060298

0.040894	0.00925	0.3937	0.7549249485	0.7670296859
1.000077362	1	1	17.19319712	107347.7353
0.05603351208	0.05034345021	0.04735017623	3.520047177e-006	0.04735017623
114.68371	142.5019146	142.4396297	112.8654742	113.3683238
112.7627435	111.0745672	4.237013257	4.291658164	2.330629777
0.682650637	0.6847223067	0.6847223067	1.512223791	1.208944387
0.04673548864	947.430694	923.9451567	2.097329326	2.096950483
0.0002436434516	0.000192883766	1.373055124e-005	1.373343698e-005	
1528.970363	1481.796563	490.68042	490.7298621	3.871551464
3.920919676	3.957919676	1.674395619	1.577328432	2737.032759
2736.737153	481.3747075	599.6799517	2736.571839	118.3052442
2137.352807	473.6734652	475.8015689	473.2397961	466.0975831

KEY POINT #14 (t plus 5592.4859 s with a Mixing Number of 85.9426): 35.04969306

0.040894	0.00925	0.3937	0.7597075376	0.7678458401
1.004927473	1	1	22.36067903	105656.9768
0.06051505711	0.05248947684	0.04603554465	6.715335324e-006	0.04603554465
91.5970835	136.9333324	132.1480642	91.91443568	91.78281763
90.01722745	88.77808657	4.206296146	4.269160595	2.25196782
0.6739678965	0.6849039643	0.6849039643	1.927273843	1.303603043
0.04397763579	964.322973	932.9987604	1.589165351	1.567698629
0.0003088039103	0.0002091378087	1.337517207e-005	1.356580693e-005	
1552.147511	1501.260648	486.8527913	490.4025514	2.880808083
2.928103659	2.965103659	0.7454841034	0.7544236136	2734.207032
2733.707032	383.8599958	555.5656104	2723.026925	171.7056147
2178.641422	385.1949282	384.6399588	377.2173891	372.0115948

End

D.17 TEST #17 - T17_SRV_040GPM_107KW_RESULTS_RCICLAND

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T17_SRV_040GPM_107kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1293.96 s, and ending (KEY POINT #11) at t plus 9270.4892 s, for a time period of 7976.5292 s.
Original Data Record Time: 10608.8688 s
No Bulk Pool to Outlet Thermal Stratification Detected (KEY POINT #3), 0 0 0 0 0 0.
No Bulk Pool to Outlet Destratification Detected (KEY POINT #9), 0 0 0 0 0 0.
No Plume detected, setting t_plume (KEY POINT #2) to the end at 7976.5292 s.
At t = 7976.5292 s, the pool pressure is 39.2167 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 114.1334, 113.6103, 113.9301, 113.9931, and 111.3755 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 0.31976 +/- 0 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were -0.20334 +/- 0 C.
Minimum Steam Quality: 0.54714 at t plus 260.4069 s
Maximum Steam Quality: 0.66868 at t plus 7043.8149 s
Time-Averaged Steam Quality: 0.62281 +/- 0.017019
SRV Alignment, no RCIC Turbine 0 0 0 0 0 0
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 7886.5311 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.68281 degrees/min at t plus 3745.7582 s and 0.4432 degrees/min at t plus 5974.6967 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.95905 degrees/min at t plus 4086.4667 s and 0.22503 degrees/min at t plus 4339.9722 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.3626 degrees/min at t plus 4339.0702 s and -0.37952 degrees/min at t plus 4086.5717 s, respectively
Max and min smoothed lower level changerates: 0.69827 degrees/min at t plus 354.9033 s and 0.43452 degrees/min at t plus 1469.6221 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.46939 degrees/min at t plus 4086.7678 s and -0.33822 degrees/min at t plus 6067.198 s, respectively
Max and min smoothed outlet level changerates: 0.6995 degrees/min at t plus 140.8331 s and 0.43417 degrees/min at t plus 7886.5311 s, respectively

Maximum SP Pressure is 39.2167 psia at t plus 7976.5292 s
 Beginning SP Pressure is 15.2811 psia
 Ending SP Pressure is 39.2167 psia
 Time-Average SP Pressure is 22.9872 +/- 6.8327 psia
 SP Levels are fully corrected and compensated
 Pre-Start SP Level is 74.814 cm (cold) / 74.9452 cm (hot) at 14.9175 psia
 Beginning Smoothed SP Level is 75.2856 cm (cold) / 75.443 cm (hot) at 15.2779 psia
 Ending Smoothed SP Level is 75.0084 cm (cold) / 76.1964 cm (hot) at 39.2105 psia
 Minimum Smoothed Cold SP Level is 74.904 cm at t plus 6507.4032 s and 30.3669 psia
 Minimum Smoothed Hot SP Level is 75.443 cm at t plus 0 s and 15.2779 psia
 Maximum Smoothed Cold SP Level is 75.4621 cm at t plus 1367.2252 s and 16.3113 psia
 Maximum Smoothed Hot SP Level is 76.1964 cm at t plus 7976.5292 s and 39.2105 psia
 SP 12 Temperature at the beginning is 39.9796 C, and at the end is 112.8916 C
 At plume detection, the Mixing Number is 192.4433
 The Mixing Number ranges from a minimum of 33.8083 at (KEY POINT #12) t plus 0 s to a
 maximum of 192.4433 at (KEY POINT #13) t plus 7976.5292 s; it had a mean value of
 83.5955 +/- 44.2463 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 33.8083): 50.12938618 0.040894
 0.00925 0.3937 0.7528563591 0.7544304604 0.6339620523
 0.6339620523 0.9996286857 51.59902969 165337.2121 0.0694713448
 0.05874002223 0.04350587777 0.02233588559 0.06584176336 40.76788089
 100.8907057 100.8907057 40.37117962 40.34389474 41.23095727
 38.5208094 4.178528368 4.217777849 2.081048383 0.6296074045
 0.6781204287 0.6781204287 4.270594197 1.736093478 0.03774613291
 991.9239027 957.7129192 0.6161343253 0.971518001 0.0006434795916
 0.0002791233904 1.229977354e-005 1.239884895e-005 1532.627249
 1544.261926 472.7101615 466.1469446 1.046843153 1.053375998
 1.090375998 0.07692138097 0.07531815379 1854.545453 1851.882993
 170.8397624 422.8578976 2676.975617 252.0181353 1431.687556
 169.1821349 169.0666188 172.7763308 161.4558779

KEY POINT #2 (t plus 7976.5292 s with a Mixing Number of 192.4433): 56.17967301
 0.040894 0.00925 0.3937 0.7500839052 0.7619635972
 0.6426819198 0.6426819198 0.9991270532 24.5843645 170760.9938
 0.05624714134 0.05306480774 0.04797946276 0.02580896789 0.07378843065
 113.6103235 129.3544977 129.3544977 113.9300846 114.1334239
 113.9931474 111.3754945 4.235605435 4.263575278 2.232631942
 0.682321851 0.6847529111 0.6847529111 1.527550863 1.332543209
 0.0432952004 948.2117565 935.378623 1.469926382 2.285178981
 0.0002460761155 0.0002140135407 1.3278729e-005 1.345395981e-005
 1530.131305 1506.118777 485.7400711 475.8881603 2.650827298
 2.703469061 2.740469061 1.616518267 1.633585566 1942.432848
 1941.828457 476.7401793 543.631774 2719.197385 66.89159473
 1398.801074 478.0946386 478.9548174 478.363074 467.2828109

KEY POINT #3 (t plus 7976.5292 s with a Mixing Number of 192.4433): 56.17967301

0.040894	0.00925	0.3937	0.7500839052	0.7619635972
0.6426819198	0.6426819198	0.9991270532	24.5843645	170760.9938
0.05624714134	0.05306480774	0.04797946276	0.02580896789	0.07378843065
113.6103235	129.3544977	129.3544977	113.9300846	114.1334239
113.9931474	111.3754945	4.235605435	4.263575278	2.232631942
0.682321851	0.6847529111	0.6847529111	1.527550863	1.332543209
0.0432952004	948.2117565	935.378623	1.469926382	2.285178981
0.0002460761155	0.0002140135407	1.3278729e-005	1.345395981e-005	
1530.131305	1506.118777	485.7400711	475.8881603	2.650827298
2.703469061	2.740469061	1.616518267	1.633585566	1942.432848
1941.828457	476.7401793	543.631774	2719.197385	66.89159473
1398.801074	478.0946386	478.9548174	478.363074	467.2828109

KEY POINT #4 (t plus 5334.6861 s with a Mixing Number of 99.7083): 54.25240425

0.040894	0.00925	0.3937	0.7507975347	0.7584153876
0.6452652591	0.6452652591	0.999440258	36.30292687	171823.21
0.06043452311	0.05597360292	0.04652234197	0.02473474363	0.0712570856
92.02334606	114.9842772	114.9842772	90.29023173	90.78299163
89.27643107	88.22256387	4.207029458	4.238046482	2.146293592
0.674122184	0.6825862385	0.6825862385	1.917734372	1.508158726
0.04019519401	963.9778607	947.0942344	0.9648477596	1.494436095
0.000307292187	0.0002429063475	1.278328668e-005	1.291209621e-005	
1551.630185	1528.072454	479.5347391	471.6614755	1.69090318
1.737216603	1.774216603	0.7575120101	0.7095953074	1913.760411
1912.442509	385.561477	482.4861135	2698.561402	96.92463656
1431.274298	378.2718437	380.3427943	374.0105883	369.5841092

KEY POINT #5 (t plus 5404.9902 s with a Mixing Number of 102.7697): 53.82059697

0.040894	0.00925	0.3937	0.7507997433	0.7585299234
0.652501607	0.652501607	0.9994519882	36.0445655	170343.5445
0.06025336381	0.05590626541	0.04661718436	0.02407274982	0.07068993418
92.98056635	115.3218799	115.3218799	90.99839499	91.46546546
89.9795097	88.84690616	4.20808621	4.238587832	2.148079972
0.6746071326	0.6826643202	0.6826643202	1.896395927	1.503450183
0.04026060878	963.3232131	946.8291811	0.9748288314	1.493168144
0.0003040152113	0.0002421447515	1.279490591e-005	1.292059232e-005	
1550.975875	1527.617355	479.6895173	472.0180874	1.709603574
1.75589938	1.79289938	0.7851117111	0.7288597209	1930.603042
1929.303831	389.5904706	483.9183177	2699.063075	94.3278471
1446.684724	381.2514915	383.2147565	376.9680979	372.2098665

KEY POINT #6 (t plus 4358.1713 s with a Mixing Number of 75.3645): 54.67402517

0.040894	0.00925	0.3937	0.7514032021	0.7575945704
0.6246071155	0.6246071155	0.9994672338	40.53106705	175205.4572
0.06229657407	0.05684033085	0.04557932702	0.02623153086	0.07181085789
82.0476541	110.6165314	110.6165314	81.83229453	82.00810886
81.00692813	79.26028285	4.197173367	4.231283364	2.124167092
0.6683597806	0.6814556121	0.6814556121	2.169631025	1.571994267
0.03937864681	970.535461	950.4786724	0.8430073815	1.348941174
0.0003454930233	0.0002531724357	1.263309274e-005	1.276124397e-005	
1556.580845	1533.684292	477.4947143	469.4735401	1.463704935
1.509691768	1.546691768	0.514854123	0.5104395239	1857.259679
1855.616912	343.6265806	463.9739644	2692.003253	120.3473838
1393.285715	342.7226995	343.4592576	339.2603781	331.9358983

KEY POINT #7 (t plus 4433.0736 s with a Mixing Number of 75.6308): 54.29467976

0.040894	0.00925	0.3937	0.7512428689	0.7575495421
0.6299302753	0.6299302753	0.9994740156	40.20075329	173872.3543
0.0622580703	0.05677906285	0.04561064281	0.02570196899	0.0713126118
82.25656023	110.9266647	110.9266647	82.32744863	82.52847342
81.59878823	79.88303086	4.197356093	4.231749004	2.125678991
0.6684944412	0.681543306	0.681543306	2.163743021	1.567276474
0.03943483953	970.4036267	950.2411056	0.8512243898	1.350588617
0.0003446098329	0.0002524173311	1.264374867e-005	1.276986582e-005	
1556.515325	1533.302927	477.6418446	469.7590943	1.47896148
1.524973374	1.561973374	0.5191669743	0.5206373239	1869.875133
1868.259032	344.5046241	465.2874057	2692.472987	120.7827816
1404.587727	344.8021703	345.6446305	341.7453385	334.549558

KEY POINT #8 (t plus 35.1 s with a Mixing Number of 33.8362): 50.0357969

0.040894	0.00925	0.3937	0.7529085841	0.754511668
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0.6351511729	0.6351511729	0.9996302092	51.54803113	165020.7774
0.06946402147	0.05873424631	0.04346514513	0.02225369466	0.06571883978
40.81281894	100.9206106	100.9206106	40.66917311	40.69535222
41.77008306	38.8036868	4.178528201	4.217816178	2.08116887
0.6296640236	0.678132444	0.678132444	4.266644952	1.735536719
0.03775078581	991.9065273	957.6913236	0.6167461841	0.9706635889
0.0006429423706	0.000279036285	1.230079548e-005	1.239943182e-005	
1532.701655	1544.233633	472.725366	466.1918895	1.04795473
1.054664677	1.091664677	0.07710483701	0.07651973639	1857.296544
1854.639344	171.0276513	422.9841139	2677.022666	251.9564626
1434.31243	170.4274232	170.5353094	175.0291991	162.6380131
KEY POINT #9 (t plus 7976.5292 s with a Mixing Number of 192.4433): 56.17967301				
0.040894	0.00925	0.3937	0.7500839052	0.7619635972
0.6426819198	0.6426819198	0.9991270532	24.5843645	170760.9938
0.05624714134	0.05306480774	0.04797946276	0.02580896789	0.07378843065
113.6103235	129.3544977	129.3544977	113.9300846	114.1334239
113.9931474	111.3754945	4.235605435	4.263575278	2.232631942
0.682321851	0.6847529111	0.6847529111	1.527550863	1.332543209
0.0432952004	948.2117565	935.378623	1.469926382	2.285178981
0.0002460761155	0.0002140135407	1.3278729e-005	1.345395981e-005	
1530.131305	1506.118777	485.7400711	475.8881603	2.650827298
2.703469061	2.740469061	1.616518267	1.633585566	1942.432848
1941.828457	476.7401793	543.631774	2719.197385	66.89159473
1398.801074	478.0946386	478.9548174	478.363074	467.2828109
KEY POINT #10 (t plus 2193.2344 s with a Mixing Number of 47.0246): 52.17352204				
0.040894	0.00925	0.3937	0.7543079779	0.7579059799
0.6291173029	0.6291173029	0.9995786535	48.06750095	170470.8514
0.066038608	0.05813129421	0.04416979509	0.02435681083	0.06852660592
61.15088819	104.0309321	104.0309321	60.82611083	60.97325424
61.95657075	59.90772076	4.183223487	4.221909128	2.094092748
0.651909271	0.6793223197	0.6793223197	2.941354697	1.679486553
0.03824666627	982.6188598	955.4232321	0.6831455893	1.08542198
0.0004583777086	0.0002702362051	1.240719356e-005	1.251582891e-005	
1554.561164	1541.145563	474.290442	467.2250648	1.169023
1.193455899	1.230455899	0.2103262481	0.2072094273	1851.281689
1848.971204	256.0551051	436.1182111	2681.888573	180.0631059
1415.163478	254.6965131	255.310606	259.4271064	250.860295
KEY POINT #11 (t plus 7976.5292 s with a Mixing Number of 192.4433): 56.17967301				
0.040894	0.00925	0.3937	0.7500839052	0.7619635972
0.6426819198	0.6426819198	0.9991270532	24.5843645	170760.9938
0.05624714134	0.05306480774	0.04797946276	0.02580896789	0.07378843065
113.6103235	129.3544977	129.3544977	113.9300846	114.1334239
113.9931474	111.3754945	4.235605435	4.263575278	2.232631942
0.682321851	0.6847529111	0.6847529111	1.527550863	1.332543209
0.0432952004	948.2117565	935.378623	1.469926382	2.285178981
0.0002460761155	0.0002140135407	1.3278729e-005	1.345395981e-005	
1530.131305	1506.118777	485.7400711	475.8881603	2.650827298
2.703469061	2.740469061	1.616518267	1.633585566	1942.432848
1941.828457	476.7401793	543.631774	2719.197385	66.89159473
1398.801074	478.0946386	478.9548174	478.363074	467.2828109
KEY POINT #12 (t plus 0 s with a Mixing Number of 33.8083): 50.12938618 0.040894				
0.00925	0.3937	0.7528563591	0.7544304604	0.6339620523
0.6339620523	0.9996286857	51.59902969	165337.2121	0.0694713448
0.05874002223	0.04350587777	0.02233588559	0.06584176336	40.76788089
100.8907057	100.8907057	40.37117962	40.34389474	41.23095727
38.5208094	4.178528368	4.217777849	2.081048383	0.6296074045
0.6781204287	0.6781204287	4.270594197	1.736093478	0.03774613291
991.9239027	957.7129192	0.6161343253	0.971518001	0.0006434795916
0.0002791233904	1.229977354e-005	1.239884895e-005	1532.627249	
1544.261926	472.7101615	466.1469446	1.046843153	1.053375998
1.090375998	0.07692138097	0.07531815379	1854.545453	1851.882993
170.8397624	422.8578976	2676.975617	252.0181353	1431.687556
169.1821349	169.0666188	172.7763308	161.4558779	
KEY POINT #13 (t plus 7976.5292 s with a Mixing Number of 192.4433): 56.17967301				
0.040894	0.00925	0.3937	0.7500839052	0.7619635972
0.6426819198	0.6426819198	0.9991270532	24.5843645	170760.9938
0.05624714134	0.05306480774	0.04797946276	0.02580896789	0.07378843065

113.6103235	129.3544977	129.3544977	113.9300846	114.1334239
113.9931474	111.3754945	4.235605435	4.263575278	2.232631942
0.682321851	0.6847529111	0.6847529111	1.527550863	1.332543209
0.0432952004	948.2117565	935.378623	1.469926382	2.285178981
0.0002460761155	0.0002140135407	1.3278729e-005	1.345395981e-005	
1530.131305	1506.118777	485.7400711	475.8881603	2.650827298
2.703469061	2.740469061	1.616518267	1.633585566	1942.432848
1941.828457	476.7401793	543.631774	2719.197385	66.89159473
1398.801074	478.0946386	478.9548174	478.363074	467.2828109
KEY POINT #14 (t plus 3980.4617 s with a Mixing Number of 67.0049): 54.64255574				
0.040894	0.00925	0.3937	0.7518824927	0.7575617031
0.6202431615	0.6202431615	0.9994828597	42.16615786	175839.2358
0.06313603771	0.05713596494	0.04530919487	0.02646032993	0.0717695248
77.46396161	109.1170387	109.1170387	78.44165054	78.24171987
77.61427918	75.86111253	4.193334941	4.229063011	2.116981426
0.6652714964	0.6810155132	0.6810155132	2.306377689	1.595223333
0.03911070479	973.3843067	951.6213538	0.804180629	1.295886524
0.0003659062197	0.0002568823954	1.258159206e-005	1.270792985e-005	
1557.657078	1535.490695	476.7784976	468.804458	1.391752657
1.437490787	1.474490787	0.4275091251	0.4450096653	1843.847072
1842.069087	324.3912386	457.6256205	2689.723534	133.2343819
1386.221452	328.4913988	327.6515221	325.0230215	317.6760301

End

D.18 TEST #18 -

T18_RCIC_040GPM_5PSIG_107KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T18_RCIC_040GPM_5PSIG_107kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 2293.3752 s, and ending (KEY POINT #11) at t plus 12088.8404 s, for a time period of 9795.4652 s.
Original Data Record Time: 12302.8907 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 1982.3314 s, T_bulk = 58.5026 C and T_out = 55.4772 C
Stratification Beginning SP12 Temperature = 58.2541 C
Stratification Beginning Pressure = 22.3129 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 9093.7441 s, T_bulk = 124.2146 C and T_out = 74.0387 C
Stratification Ending SP12 Temperature = 124.0978 C
Stratification Ending Pressure = 56.6903 psia
Plume detected! Setting t_plume (KEY POINT #2) to 1230.3204 s.
At t = 1230.3204 s, the pool pressure is 21.3758 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 51.8606, 51.9174, 53.9194, 51.4822, and 49.1627 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 11.73 +/- 3.3179 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 10.8065 +/- 3.3094 C.
Minimum Steam Quality: 0.5303 at t plus 496.5104 s
Maximum Steam Quality: 0.62165 at t plus 9735.4608 s
Time-Averaged Steam Quality: 0.57748 +/- 0.013594
Minimum Turbine Outlet Steam Quality: 0.55749 at t plus 8845.6419 s
Maximum Turbine Outlet Steam Quality: 0.64313 at t plus 3092.2499 s
Time-Averaged Turbine Outlet Steam Quality: 0.59945 +/- 0.015505
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 9705.5561 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.75388 degrees/min at t plus 3086.1495 s and 0.31817 degrees/min at t plus 7940.7272 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.8232 degrees/min at t plus 3997.0676 s and 0.38956 degrees/min at t plus 8838.7445 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.30759 degrees/min at t plus 3074.5479 s and -0.1367 degrees/min at t plus 3988.6651 s, respectively

Max and min smoothed lower level changerates: 3.8238 degrees/min at t plus 6689.0096 s and -0.18939 degrees/min at t plus 2754.7436 s, respectively
 Max and min smoothed mid-lower level changerate differences: 0.74664 degrees/min at t plus 2754.7436 s and -3.3495 degrees/min at t plus 6689.1076 s, respectively
 Max and min smoothed outlet level changerates: 8.4472 degrees/min at t plus 9544.2519 s and -0.0095086 degrees/min at t plus 4174.2698 s, respectively
 Max and min smoothed lower-outlet level changerate differences: 3.771 degrees/min at t plus 6689.0096 s and -8.0785 degrees/min at t plus 9544.3519 s, respectively
 Max and min smoothed hot (SP8) level changerates: 1.2169 degrees/min at t plus 2102.3343 s and 0.14263 degrees/min at t plus 7715.9323 s, respectively
 Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.64281 degrees/min at t plus 2102.2332 s and -0.46345 degrees/min at t plus 3952.0621 s, respectively
 The mean steam flow rate was 44.354 +/- 0.79696 g/s
 The mean feedwater flow rate was 44.7858 +/- 1.5546 g/s
 The mean water injection to steam flow rate was 25.2901 +/- 0.98695 g/s
 Mean Smoothed Condensing Region SP8-SP9 delta T is 12.5745 +/- 2.1425 C over the Stratification Period, beginning at 5.9419 C and ending at 12.8045 C
 Mean Smoothed SP8-Upper Pool delta T is 11.577 +/- 2.4081 C over the Stratification Period, beginning at 5.3039 C and ending at 11.9126 C
 The stratification period begins and ends with Smoothed SP8 readings of 64.6552 and 137.1192 C, respectively
 The stratification period begins and ends with condensing flows of 0.40796 and 1.0804 kg/s, respectively.
 The stratification period begins and ends with condensing+cooling flows of 4.2936 and 1.6224 kg/s, respectively.
 The stratification period had a mean sparger steam enthalpy of 1845.7967 +/- 14.0432 kJ/kg.
 At plume detection, the condensing and condensing+cooling flows are 0.36153 and 12.8033 kg/s, respectively
 The plume period had a mean steam enthalpy of 1842.4117 +/- 18.0727 kJ/kg.
 Maximum Smoothed Top-Mid delta T is 2.3152 degrees C at t plus 3859.4738 s with T_upper = 78.877 C and T_mid = 76.5617 C
 At t plus 3859.4738 s, Smoothed SP8-SP9 is 11.2703 C and Smoothed SP8-Top is 8.955 C, where Smoothed SP8 is 87.832 C and Pool P = 26.7631 psia
 Maximum Smoothed Top-Lower delta T is 23.601 degrees C at t plus 6321.6076 s with T_upper = 104.6449 C and T_low = 81.0439 C
 At t plus 6321.6076 s, Smoothed SP8-SP9 is 15.589 C and Smoothed SP8-Top is 14.9928 C, where Smoothed SP8 is 119.6377 C and Pool P = 38.7688 psia
 Maximum Smoothed Mid-Lower delta T is 23.2666 degrees C at t plus 6419.1012 s with T_mid = 105.0506 C and T_low = 81.7839 C
 At t plus 6419.1012 s, Smoothed SP8-SP9 is 15.0117 C and Smoothed SP8-Top is 14.689 C, where Smoothed SP8 is 120.0623 C and Pool P = 39.349 psia
 Maximum Smoothed Top-Outlet delta T is 52.1601 degrees C at t plus 8870.0403 s with T_upper = 123.6082 C and T_out = 71.4482 C
 At t plus 8870.0403 s, Smoothed SP8-SP9 is 12.9399 C and Smoothed SP8-Top is 12.064 C, where Smoothed SP8 is 135.6722 C and Pool P = 55.0355 psia
 Maximum Smoothed Mid-Outlet delta T is 51.3068 degrees C at t plus 8854.8674 s with T_mid = 122.695 C and T_out = 71.3882 C
 At t plus 8854.8674 s, Smoothed SP8-SP9 is 12.9333 C and Smoothed SP8-Top is 12.1744 C, where Smoothed SP8 is 135.6283 C and Pool P = 54.9258 psia
 Maximum Smoothed Lower-Outlet delta T is 51.3038 degrees C at t plus 8880.6419 s with T_low = 122.8081 C and T_out = 71.5042 C
 At t plus 8880.6419 s, Smoothed SP8-SP9 is 12.8885 C and Smoothed SP8-Top is 12.0253 C, where Smoothed SP8 is 135.6816 C and Pool P = 55.1138 psia
 Maximum Smoothed Condensing Region SP8-SP9 delta T is 15.8154 degrees C at (KEY POINT #14) t plus 6158.7983 s with T_SP8 = 118.4086 C and T_SP9 = 102.5932 C and Pool P = 37.777 psia
 Maximum Smoothed Condensing Region SP8-Upper delta T is 15.2997 degrees C at t plus 6160.8984 s with T_SP8 = 118.4286 C and T_upper = 103.1289 C and Pool P = 37.7912 psia
 Maximum Top-Mid delta T is 3.686 degrees C at (KEY POINT #4) t plus 3171.4504 s ignoring SP 4, with temperatures of 72.4749 and 68.7889 C, respectively, at Set # 2, where Pool P = 24.7844 psia and T_outlet = 61.4629 C
 Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 5155.9869 s with a Smoothed Mid-Axis Top-Mid Delta T of 1.2287 C and a raw SP12 Reading of 91.7815 C.

Maximum Top-Lower delta T is 26.4864 degrees C at t plus 6562.0293 s, with temperatures of 107.4192 and 80.9328 C, respectively, at Set # 1, where Pool P = 40.2082 psia and T_{outlet} = 67.8515 C

Maximum Mid-Low delta T is 25.5094 degrees C at (KEY POINT #6) t plus 6461.5086 s ignoring SP 4, with temperatures of 105.4071 and 79.8977 C, respectively, at Set # 2, where Pool P = 39.5973 psia and T_{outlet} = 67.7397 C

Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 6842.5854 s with a Smoothed Mid-Axis Mid-Low Delta T of 8.5 C and a raw SP12 Reading of 108.3202 C.

Maximum Top-Outlet delta T is 52.6892 degrees C at t plus 8851.6463 s, with temperatures of 124.0125 and 71.3233 C, respectively, at Set # 1, where Pool P = 54.9046 psia

Maximum Mid-Outlet delta T is 51.3416 degrees C at t plus 8933.5669 s ignoring SP 4, with temperatures of 123.208 and 71.8663 C, respectively, at Set # 2, where Pool P = 55.5032 psia

Maximum Lower-Outlet delta T is 52.5639 degrees C at (KEY POINT #8) t plus 8855.2395 s, with temperatures of 123.9 and 71.336 C, respectively, at Set # 1, where Pool P = 54.9214 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 9598.482 s with a Smoothed Mid-Axis Low-Outlet Delta T of 17.5024 C and a raw SP12 Reading of 127.6277 C.

Minimum SP Pressure is 20.3417 psia at t plus 2.9012 s

Maximum SP Pressure is 62.4423 psia at t plus 9795.4652 s

Beginning SP Pressure is 20.3467 psia

Ending SP Pressure is 62.4423 psia

Time-Average SP Pressure is 34.691 +/- 12.6508 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 74.2544 cm (cold) / 74.3712 cm (hot) at 14.5332 psia

Beginning Smoothed SP Level is 75.1509 cm (cold) / 75.3115 cm (hot) at 20.3517 psia

Ending Smoothed SP Level is 74.1134 cm (cold) / 75.6196 cm (hot) at 62.4487 psia

Minimum Smoothed Cold SP Level is 74.1134 cm at t plus 9795.4652 s and 62.4487 psia

Minimum Smoothed Hot SP Level is 75.2763 cm at t plus 1118.417 s and 21.2624 psia

Maximum Smoothed Cold SP Level is 75.1509 cm at t plus 0 s and 20.3517 psia

Maximum Smoothed Hot SP Level is 76.148 cm at t plus 7518.321 s and 46.0056 psia

SP 12 Temperature at the beginning is 40.213 C, and at the end is 129.2164 C

At plume detection, the Mixing Number is 42.2698

The Mixing Number ranges from a minimum of 36.222 at (KEY POINT #12) t plus 0 s to a maximum of 260.3999 at (KEY POINT #13) t plus 9785.1607 s; it had a mean value of 108.8314 +/- 66.2355 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) gl, Sparger Diameter (m) dl, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_{tp}, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) kl, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_{mid} Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) pl, Pool Airspace P p2, Approx Pool Mid P p3, T_{mid} Vapor Pressure p4, T_{Plume} Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 36.222):

52.76468011	0.040894			
0.00925	0.3937	0.7515091528	0.7531146312	0.6050730556
0.6050730556	0.999415092	37.49292817	168772.7785	0.06954332551
0.05677306544	0.04476071544	0.02454233904	0.06930305448	40.32582647
110.9570116	110.9570116	40.76744926	40.33593478	40.09774496
37.83389418	4.17844343	4.231794686	2.12582741	0.6290673997
0.6815518258	0.6815518258	4.309705995	1.566816402	0.03944035246

992.1141674	950.2178368	0.8520319101	1.407323532	0.0006488290651
0.0002523436648	1.264479144e-005	1.278499322e-005	1531.947297	
1533.265467	477.6562229	468.9109494	1.480461343	1.403200816
1.440200816	0.07513671459	0.07691962071	1814.381662	1812.975943
169.0236034	465.4159357	2692.518919	296.3923323	1348.965727
170.8688989	169.0643351	168.0721724	158.6167365	
KEY POINT #2 (t plus 1230.3204 s with a Mixing Number of 42.2698): 52.0906176				
0.040894	0.00925	0.3937	0.7502096506	0.7528176804
0.5935700442	0.5935700442	0.9993587929	34.78639476	165854.3753
0.06762094672	0.05649997055	0.04302077204	0.02539694416	0.0684177162
51.91741515	112.3367199	112.3367199	53.91938496	51.86059758
51.48217706	49.16265223	4.1798902	4.233894008	2.132665808
0.6426370069	0.6819276816	0.6819276816	3.445107128	1.546190968
0.03969372788	987.1886184	949.1556771	0.8894071631	1.497442261
0.0005296678208	0.0002490356207	1.269221447e-005	1.284375955e-005	
1547.454741	1531.535796	478.3064259	468.9377934	1.5499843
1.47394635	1.51094635	0.135755174	0.1496320673	1792.179094
1790.969001	217.4700042	471.2610506	2694.60093	253.7910464
1320.918044	225.8385542	217.2310547	215.6523279	205.9617419
KEY POINT #3 (t plus 1982.3314 s with a Mixing Number of 46.8624): 52.3264424				
0.040894	0.00925	0.3937	0.7496183736	0.7529292316
0.6064813184	0.6064813184	0.9993688239	34.40522607	166125.6246
0.0664606698	0.05626186163	0.04377747781	0.02494997928	0.06872745709
58.71326721	113.5362686	113.5362686	64.65515013	59.35124136
58.60858789	55.56461088	4.182106714	4.235755069	2.138757025
0.6496013232	0.6822362389	0.6822362389	3.06189967	1.528712691
0.03991841652	983.8914697	948.2254614	0.9229717817	1.520886458
0.000475600986	0.0002462236791	1.273346623e-005	1.288083967e-005	
1553.143295	1529.989963	478.8661225	469.80924	1.612586508
1.538681686	1.575681686	0.1878767461	0.2465735571	1823.951414
1822.767694	245.8883805	476.3454349	2696.401055	230.4570544
1347.605979	270.7457745	248.5551076	245.4521201	232.7276004
KEY POINT #4 (t plus 3171.4504 s with a Mixing Number of 56.2566): 51.69709649				
0.040894	0.00925	0.3937	0.7490999287	0.753929576
0.6294760704	0.6294760704	0.999371713	32.23134998	162900.8037
0.06461201551	0.05567116217	0.04453307062	0.02336778061	0.06790085123
69.26309121	116.4986708	116.4986708	80.53164729	71.27458867
66.9994323	61.56002695	4.187470534	4.24049601	2.154394207
0.6590474917	0.6829261193	0.6829261193	2.592566571	1.487278919
0.04049127446	978.2320887	945.9014187	1.010275517	1.603938294
0.0004080326015	0.0002395242485	1.283541742e-005	1.297784305e-005	
1557.592277	1526.007448	480.2257309	471.6064267	1.776117619
1.708591182	1.745591182	0.3021953466	0.4844470892	1882.285085
1881.246225	290.0492135	488.9121113	2700.805746	198.8628979
1393.372973	337.2804507	298.4722013	280.5732484	257.815013
KEY POINT #5 (t plus 5155.9869 s with a Mixing Number of 92.5799): 53.71804838				
0.040894	0.00925	0.3937	0.749398725	0.7573067173
0.6056770497	0.6056770497	0.9991176132	25.55000728	165272.4517
0.06042067269	0.05408661936	0.04512834816	0.02542689497	0.07055524312
92.0966101	124.3546559	124.3546559	104.9156401	93.07861651
76.058082	65.96201707	4.207002574	4.254099893	2.200138491
0.6741857559	0.6842651881	0.6842651881	1.916103521	1.388269148
0.04214073054	963.9561021	939.555113	1.274540677	2.102467048
0.0003070617805	0.0002233008799	1.310619083e-005	1.329166384e-005	
1551.675079	1514.344071	483.6714355	472.9710335	2.276500021
2.215254601	2.252254601	0.7595954913	1.20549443	1849.324169
1848.671366	385.9064671	522.312907	2712.190267	136.4064399
1327.011262	439.9340188	390.0370008	318.5607054	276.2764204
KEY POINT #6 (t plus 6461.5086 s with a Mixing Number of 131.8983): 53.46216869				
0.040894	0.00925	0.3937	0.7503277041	0.7604731456
0.5994419734	0.5994419734	0.9988987337	20.82077733	161294.5433
0.05787202096	0.05271838963	0.04491676803	0.02530239338	0.0702191614
105.3615128	131.0383788	131.0383788	120.288319	105.8451777
82.79744937	67.63750421	4.223365462	4.266916384	2.244184779
0.6798840588	0.6848543155	0.6848543155	1.656500027	1.31491946
0.04370327611	954.511881	933.948082	1.540903065	2.567731638
0.0002666659971	0.0002110489603	1.333685957e-005	1.355459324e-005	

1540.05907	1503.212647	486.4145154	474.3443489	2.787592236
2.730781236	2.767781236	1.224227959	2.004861527	1852.459414
1852.025909	441.855093	550.8231708	2721.513239	108.9680778
1301.636243	505.06378	443.8966932	346.871704	283.3322265
KEY POINT #7 (t plus 6842.5854 s with a Mixing Number of 143.5885): 53.44464421				
0.040894	0.00925	0.3937	0.7499933898	0.7608223736
0.5967605765	0.5967605765	0.9988256854	19.68338381	160358.2795
0.05727347934	0.05233553777	0.04485873077	0.02533741335	0.07019614412
108.4178295	132.8929693	132.8929693	123.1415126	108.944909
101.788765	68.08001361	4.227676722	4.270686216	2.257268275
0.6808922353	0.6849296639	0.6849296639	1.60621196	1.296135968
0.04416425453	952.2237576	932.3585687	1.622239053	2.715216282
0.000258689896	0.0002078733786	1.340089184e-005	1.362926371e-005	
1536.641433	1499.934013	487.1442281	474.625866	2.944786551
2.889093773	2.926093773	1.359210804	2.192499249	1851.295826
1850.908391	454.7811876	558.7505793	2724.0374	103.9693917
1292.545247	517.1985464	457.008468	426.7879466	285.1977505
KEY POINT #8 (t plus 8855.2395 s with a Mixing Number of 217.4416): 53.59732816				
0.040894	0.00925	0.3937	0.7445837006	0.7581435906
0.5783710604	0.5783710604	0.9983618045	14.92555043	156400.3352
0.05442332735	0.05040869386	0.04435257002	0.02604411476	0.07039668478
122.6959867	142.1296004	142.1296004	135.6014957	123.4574126
122.5108574	71.38917344	4.250687486	4.290934121	2.328088738
0.6841425449	0.6847445423	0.6847445423	1.407882248	1.211544447
0.04664662094	940.9926621	924.2244745	2.080325925	3.590978331
0.0002265967911	0.0001933374935	1.371984606e-005	1.401409489e-005	
1517.303636	1482.418098	490.571421	475.3391738	3.838160135
3.787193691	3.824193691	2.162291771	3.187187558	1835.029108
1834.806336	515.3669704	598.3473839	2736.177295	82.98041348
1236.681724	570.3836764	518.6028835	514.5813315	299.1280342
KEY POINT #9 (t plus 9093.7441 s with a Mixing Number of 227.8435): 52.95697315				
0.040894	0.00925	0.3937	0.7433211508	0.7571459813
0.584638398	0.584638398	0.9983541436	14.47622164	154121.6572
0.05409475097	0.05017292378	0.0442225693	0.02533304986	0.06955561916
124.3146646	143.2491369	143.2491369	137.1192057	125.2065683
124.3554662	73.99019627	4.253608969	4.293562846	2.33731474
0.6843626487	0.6846593865	0.6846593865	1.388670886	1.202223723
0.04696926883	939.6639775	923.2139076	2.142252416	3.658204086
0.0002234230962	0.0001917087943	1.375850254e-005	1.405138316e-005	
1514.778405	1480.163573	490.9631637	475.8910314	3.959842132
3.909265563	3.946265563	2.273689775	3.329912274	1851.244139
1851.034578	522.2582534	603.1604938	2737.597932	80.90224045
1248.083645	576.8841985	526.0516081	522.4330527	310.0342795
KEY POINT #10 (t plus 9598.482 s with a Mixing Number of 252.117): 52.92000917				
0.040894	0.00925	0.3937	0.7416060474	0.7562838915
0.5830641499	0.5830641499	0.9982295185	13.53180363	152912.7757
0.05339200594	0.04965047897	0.04345591392	0.02605115541	0.06950706933
127.7589045	145.7220203	145.7220203	140.0380176	128.7217117
127.5223088	109.9905303	4.260048079	4.299509921	2.358184416
0.6847328886	0.6844237681	0.6844237681	1.349699366	1.18229064
0.04769913948	936.799885	920.9627663	2.284284302	3.910787551
0.0002169420458	0.0001882046628	1.384388115e-005	1.415258368e-005	
1509.191338	1475.084991	491.8101999	476.161607	4.239632945
4.189879246	4.226879246	2.526308966	3.618899425	1854.100837
1853.917727	536.9388971	613.8030318	2740.695408	76.86413462
1240.297805	589.4028385	541.040222	535.9322779	461.5310928
KEY POINT #11 (t plus 9795.4652 s with a Mixing Number of 259.8183): 51.72469055				
0.040894	0.00925	0.3937	0.7411337341	0.756196195
0.6159925389	0.6159925389	0.9984151184	13.62148318	149465.4793
0.05311087228	0.04944211224	0.04361402283	0.02432307145	0.06793709428
129.1301663	146.7052917	146.7052917	140.6548324	130.1935858
129.3593922	122.1926531	4.262698901	4.301929409	2.366670028
0.6848431493	0.6843119708	0.6843119708	1.334872212	1.174607993
0.04799599633	935.6454547	920.0604015	2.342813974	3.797287701
0.0002144599257	0.0001868460018	1.387782599e-005	1.415196008e-005	
1506.886177	1473.028141	492.1399982	478.2670724	4.355202288
4.305684537	4.342684537	2.633025755	3.68248233	1926.51408

1926.328535	542.7901942	618.0390723	2741.911328	75.24887813
1308.475008	592.0543914	547.3231733	543.7685808	513.2682337
KEY POINT #12 (t plus 0 s with a Mixing Number of 36.222):	52.76468011			0.040894
0.00925	0.3937	0.7515091528	0.7531146312	0.6050730556
0.6050730556	0.999415092	37.49292817	168772.7785	0.06954332551
0.05677306544	0.04476071544	0.02454233904	0.06930305448	40.32582647
110.9570116	110.9570116	40.76744926	40.33593478	40.09774496
37.83389418	4.17844343	4.231794686	2.12582741	0.6290673997
0.6815518258	0.6815518258	4.309705995	1.566816402	0.03944035246
992.1141674	950.2178368	0.8520319101	1.407323532	0.0006488290651
0.0002523436648	1.264479144e-005	1.278499322e-005	1531.947297	
1533.265467	477.6562229	468.9109494	1.480461343	1.403200816
1.440200816	0.07513671459	0.07691962071	1814.381662	1812.975943
169.0236034	465.4159357	2692.518919	296.3923323	1348.965727
170.8688989	169.0643351	168.0721724	158.6167365	
KEY POINT #13 (t plus 9785.1607 s with a Mixing Number of 260.3999):	51.74140049			
0.040894	0.00925	0.3937	0.7411436975	0.7561729883
0.6149525009	0.6149525009	0.9984103122	13.62078479	149522.399
0.05311043647	0.0494529417	0.04358562604	0.02437341568	0.06795904172
129.1322892	146.6542296	146.6542296	140.6065885	130.1436053
129.3193349	121.3943417	4.26270482	4.301802985	2.366226743
0.6848429028	0.6843180295	0.6843180295	1.334849921	1.175003628
0.0479804865	935.643341	920.107364	2.339745188	3.798709201
0.0002144559695	0.0001869160838	1.387606326e-005	1.415114288e-005	
1506.881008	1473.135478	492.1229697	478.1997158	4.349139071
4.299345754	4.336345754	2.633193752	3.677477	1924.181732
1923.996207	542.7988128	617.8190292	2741.848406	75.02021643
1306.362703	591.8471471	547.1095911	543.5973839	509.8758441
KEY POINT #14 (t plus 6158.7983 s with a Mixing Number of 122.2445):	53.58642998			
0.040894	0.00925	0.3937	0.7506215003	0.7602838265
0.5989624003	0.5989624003	0.9989441851	21.76334013	162374.7186
0.05841055933	0.05303298505	0.04490998741	0.02547238331	0.07038237071
102.5931548	129.5094145	129.5094145	118.4085544	103.1366084
79.9245741	67.19995392	4.219637216	4.263879449	2.233681876
0.6788739532	0.6847635562	0.6847635562	1.704851597	1.330898646
0.04333233121	956.5488801	935.2475171	1.476344166	2.462233722
0.0002742840875	0.0002137374897	1.328407663e-005	1.349571834e-005	
1542.92399	1505.854244	485.8025911	473.9644874	2.663177461
2.605274472	2.642274472	1.111697425	1.888566995	1847.580827
1847.107184	430.1592052	544.2931338	2719.411387	114.1339286
1303.287693	497.0752165	432.4513127	334.8062553	281.4902488

End

D.19 TEST #19 -

T19_RCIC_060GPM_10PSIG_157KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T19_RCIC_060GPM_10PSIG_157kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1562.9654 s, and ending (KEY POINT #11) at t plus 9930.279 s, for a time period of 8367.3136 s.
Original Data Record Time: 12570.196 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 1817.726 s, T_bulk = 63.5184 C and T_out = 61.0907 C
Stratification Beginning SP12 Temperature = 63.0883 C
Stratification Beginning Pressure = 27.9113 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 8052.6366 s, T_bulk = 143.7795 C and T_out = 100.9486 C
Stratification Ending SP12 Temperature = 143.6292 C
Stratification Ending Pressure = 90.0382 psia
Plume detected! Setting t_plume (KEY POINT #2) to 977.4179 s.

At t = 977.4179 s, the pool pressure is 26.2677 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 52.5632, 52.5913, 54.5922, 52.1931, and 50.1472 C, respectively.

Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 10.3152 +/- 2.4872 C.

Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 9.5672 +/- 2.2434 C.

Minimum Steam Quality: 0.46159 at t plus 24.6014 s
Maximum Steam Quality: 0.62296 at t plus 8312.4384 s
Time-Averaged Steam Quality: 0.57724 +/- 0.024579
Minimum Turbine Outlet Steam Quality: 0.50224 at t plus 24.6014 s
Maximum Turbine Outlet Steam Quality: 0.64181 at t plus 5723.5894 s
Time-Averaged Turbine Outlet Steam Quality: 0.6064 +/- 0.017981

Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 8277.4324 s; using 300 s smoothing

Max and min smoothed upper level changerates: 1.0485 degrees/min at t plus 3744.2612 s and 0.57296 degrees/min at t plus 8071.8257 s, respectively

Max and min smoothed mid (SP9) level changerates: 0.89356 degrees/min at t plus 3566.455 s and 0.6142 degrees/min at t plus 8277.4324 s, respectively

Max and min smoothed upper-mid level changerate differences: 0.18101 degrees/min at t plus 3742.358 s and -0.14213 degrees/min at t plus 4372.6661 s, respectively

Max and min smoothed lower level changerates: 2.1414 degrees/min at t plus 6183.7447 s and 0.36535 degrees/min at t plus 3723.1569 s, respectively

Max and min smoothed mid-lower level changerate differences: 0.51078 degrees/min at t plus 3584.654 s and -1.3795 degrees/min at t plus 6183.7447 s, respectively

Max and min smoothed outlet level changerates: 3.9767 degrees/min at t plus 8277.4324 s and 0.095299 degrees/min at t plus 4771.5739 s, respectively

Max and min smoothed lower-outlet level changerate differences: 1.9678 degrees/min at t plus 6183.7447 s and -3.2617 degrees/min at t plus 8277.4324 s, respectively

Max and min smoothed hot (SP8) level changerates: 1.5222 degrees/min at t plus 1188.518 s and 0.34887 degrees/min at t plus 3078.3591 s, respectively

Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.71814 degrees/min at t plus 1188.416 s and -0.49016 degrees/min at t plus 3078.3591 s, respectively

The mean steam flow rate was 66.4463 +/- 2.7975 g/s
The mean feedwater flow rate was 65.7438 +/- 3.2557 g/s
The mean water injection to steam flow rate was 37.4107 +/- 1.2069 g/s

Mean Smoothed Condensing Region SP8-SP9 delta T is 11.0932 +/- 1.3118 C over the Stratification Period, beginning at 6.6113 C and ending at 9.6765 C

Mean Smoothed SP8-Upper Pool delta T is 10.2638 +/- 1.2045 C over the Stratification Period, beginning at 6.3678 C and ending at 8.7407 C

The stratification period begins and ends with Smoothed SP8 readings of 70.2703 and 153.4088 C, respectively

The stratification period begins and ends with condensing flows of 0.57821 and 1.8257 kg/s, respectively.

The stratification period begins and ends with condensing+cooling flows of 5.7013 and 3.228 kg/s, respectively.

The stratification period had a mean sparger steam enthalpy of 1895.6166 +/- 37.4531 kJ/kg.

At plume detection, the condensing and condensing+cooling flows are 0.4916 and 19.3001 kg/s, respectively

The plume period had a mean steam enthalpy of 1886.6736 +/- 43.499 kJ/kg.

Maximum Smoothed Top-Mid delta T is 1.6842 degrees C at t plus 3878.1568 s with T_upper = 92.3293 C and T_mid = 90.645 C

At t plus 3878.1568 s, Smoothed SP8-SP9 is 11.4917 C and Smoothed SP8-Top is 9.8075 C, where Smoothed SP8 is 102.1368 C and Pool P = 36.7666 psia

Maximum Smoothed Top-Lower delta T is 11.4166 degrees C at t plus 5839.994 s with T_upper = 119.3305 C and T_low = 107.9139 C

At t plus 5839.994 s, Smoothed SP8-SP9 is 12.188 C and Smoothed SP8-Top is 11.3573 C, where Smoothed SP8 is 130.6878 C and Pool P = 55.7996 psia

Maximum Smoothed Mid-Lower delta T is 10.5867 degrees C at t plus 5840.189 s with T_mid = 118.5027 C and T_low = 107.9161 C

At t plus 5840.189 s, Smoothed SP8-SP9 is 12.1911 C and Smoothed SP8-Top is 11.362 C, where Smoothed SP8 is 130.6939 C and Pool P = 55.7988 psia

Maximum Smoothed Top-Outlet delta T is 44.1627 degrees C at t plus 7965.3256 s with T_upper = 143.6504 C and T_out = 99.4877 C

At t plus 7965.3256 s, Smoothed SP8-SP9 is 9.9502 C and Smoothed SP8-Top is 9.1254 C, where Smoothed SP8 is 152.7758 C and Pool P = 88.4678 psia

Maximum Smoothed Mid-Outlet delta T is 43.3991 degrees C at t plus 7946.2255 s with T_mid = 142.6606 C and T_out = 99.2615 C
 At t plus 7946.2255 s, Smoothed SP8-SP9 is 9.9636 C and Smoothed SP8-Top is 9.2904 C, where Smoothed SP8 is 152.6242 C and Pool P = 88.0969 psia
 Maximum Smoothed Lower-Outlet delta T is 43.1981 degrees C at t plus 7902.172 s with T_low = 142.1085 C and T_out = 98.9104 C
 At t plus 7902.172 s, Smoothed SP8-SP9 is 9.8854 C and Smoothed SP8-Top is 9.1188 C, where Smoothed SP8 is 152.0529 C and Pool P = 87.3107 psia
 Maximum Smoothed Condensing Region SP8-SP9 delta T is 12.8996 degrees C at (KEY POINT #14) t plus 5771.8891 s with T_SP8 = 130.4885 C and T_SP9 = 117.589 C and Pool P = 54.9304 psia
 Maximum Smoothed Condensing Region SP8-Upper delta T is 12.2537 degrees C at t plus 5776.9894 s with T_SP8 = 130.5475 C and T_upper = 118.2938 C and Pool P = 54.992 psia
 Maximum Top-Mid delta T is 2.6964 degrees C at (KEY POINT #4) t plus 3722.1679 s ignoring SP 4, with temperatures of 90.0487 and 87.3522 C, respectively, at Set # 2, where Pool P = 35.745 psia and T_outlet = 81.1528 C
 Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 4471.4658 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.99976 C and a raw SP12 Reading of 99.3178 C.
 Maximum Top-Lower delta T is 14.3408 degrees C at t plus 5914.5933 s, with temperatures of 120.7682 and 106.4274 C, respectively, at Set # 1, where Pool P = 56.7833 psia and T_outlet = 90.951 C
 Maximum Mid-Low delta T is 11.9707 degrees C at (KEY POINT #6) t plus 5914.9903 s ignoring SP 4, with temperatures of 119.5086 and 107.5379 C, respectively, at Set # 2, where Pool P = 56.7908 psia and T_outlet = 90.9463 C
 Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 6331.0191 s with a Smoothed Mid-Axis Mid-Low Delta T of 3.9892 C and a raw SP12 Reading of 124.8209 C.
 Maximum Top-Outlet delta T is 44.8581 degrees C at t plus 7986.8248 s, with temperatures of 144.6075 and 99.7494 C, respectively, at Set # 1, where Pool P = 88.8269 psia
 Maximum Mid-Outlet delta T is 43.7058 degrees C at t plus 7963.6295 s ignoring SP 4, with temperatures of 142.9239 and 99.2181 C, respectively, at Set # 2, where Pool P = 88.44 psia
 Maximum Lower-Outlet delta T is 44.398 degrees C at (KEY POINT #8) t plus 7839.3234 s, with temperatures of 142.6222 and 98.2242 C, respectively, at Set # 1, where Pool P = 86.1685 psia
 Low-Outlet Reconvergence NOT Detected, setting t to (KEY POINT #10) t plus 8367.3136 s with a Smoothed Mid-Axis Low-Outlet Delta T of 30.2375 C and a raw SP12 Reading of 146.9219 C.
 Minimum SP Pressure is 25.1354 psia at t plus 2.4041 s
 Maximum SP Pressure is 95.8621 psia at t plus 8367.3136 s
 Beginning SP Pressure is 25.1386 psia
 Ending SP Pressure is 95.8621 psia
 Time-Average SP Pressure is 46.6136 +/- 20.7647 psia
 SP Levels are fully corrected and compensated
 Pre-Start SP Level is 77.4768 cm (cold) / 77.6285 cm (hot) at 24.7303 psia
 Beginning Smoothed SP Level is 77.6315 cm (cold) / 77.805 cm (hot) at 25.1392 psia
 Ending Smoothed SP Level is 76.7495 cm (cold) / 78.9524 cm (hot) at 95.881 psia
 Minimum Smoothed Cold SP Level is 76.7495 cm at t plus 8367.3136 s and 95.881 psia
 Minimum Smoothed Hot SP Level is 77.8038 cm at t plus 7.6994 s and 25.1443 psia
 Maximum Smoothed Cold SP Level is 79.3754 cm at t plus 3681.4596 s and 35.4827 psia
 Maximum Smoothed Hot SP Level is 80.3559 cm at t plus 4141.9669 s and 38.6242 psia
 SP 12 Temperature at the beginning is 39.7868 C, and at the end is 146.9219 C
 At plume detection, the Mixing Number is 44.8991
 The Mixing Number ranges from a minimum of 38.5793 at (KEY POINT #12) t plus 0 s to a maximum of 364.5022 at (KEY POINT #13) t plus 8367.3136 s; it had a mean value of 130.9166 +/- 91.5009 over the test period.
 Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m2-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) kl, Sparger Sat Water Thermal

Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m3) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 38.5793): 72.81053655 0.040894
0.00925 0.3937 0.7763149194 0.7780497256 0.5049946991
0.5049946991 0.9989265291 35.52012539 227191.511 0.06959656899
0.0555025919 0.05389813965 0.04173387349 0.09563201313 39.99842105
117.3406139 117.3406139 40.14561299 40.0124062 39.45363492
37.77736682 4.178365689 4.241881551 2.15899585 0.6286689885
0.68310356 0.68310356 4.338919393 1.475935104 0.04065885631
992.2547945 945.2339703 1.03627021 2.049838951 0.0006528255947
0.0002376814442 1.286441078e-005 1.310574532e-005 1531.44724
1524.8333 480.6062045 466.2487016 1.82499369 1.733286485
1.770286485 0.07383805876 0.07441947837 1609.564356 1608.302676
167.684814 492.486422 2702.046753 324.801608 1117.077934
168.2998356 167.7417424 165.4100932 158.409974

KEY POINT #2 (t plus 977.4179 s with a Mixing Number of 44.8991): 76.95510896
0.040894 0.00925 0.3937 0.7775474692 0.7805787059
0.6009053106 0.6009053106 0.9992360427 42.58789869 240447.618
0.06750697625 0.05518458277 0.06445752253 0.03661812309 0.1010756456
52.59131065 118.9248547 118.9248547 54.59221236 52.56317261
52.19306303 50.14715086 4.179990087 4.244535058 2.167847073
0.6433765599 0.6834152229 0.6834152229 3.403595254 1.455086969
0.04098004163 986.8907583 943.9697768 1.08664878 1.80697126
0.0005238752629 0.0002342844556 1.291898521e-005 1.308809899e-005
1548.180464 1522.573935 481.3149136 471.2479437 1.919944658
1.810692277 1.847692277 0.1402978144 0.1545602529 1826.117384
1824.303655 220.3157138 499.2153945 2704.368581 278.8996807
1326.90199 228.6800282 220.1966411 218.6526081 210.105341

KEY POINT #3 (t plus 1817.726 s with a Mixing Number of 52.4256): 79.29764602
0.040894 0.00925 0.3937 0.7820357705 0.7864915692
0.5913236611 0.5913236611 0.999160226 40.94359691 246344.7843
0.06560113769 0.05482233464 0.06496938297 0.03918303623 0.1041524192
63.6589847 120.7230649 120.7230649 70.27026837 63.90242294
63.287292 61.12937194 4.184262426 4.247621256 2.178202665
0.6542482559 0.6837339879 0.6837339879 2.825385952 1.432184117
0.04135403222 981.3332029 942.5217535 1.146210604 1.93675329
0.0004417753103 0.0002305367873 1.298095803e-005 1.316365575e-005
1555.914819 1519.931088 482.1078405 471.3554594 2.032573468
1.924378055 1.961378055 0.2357675444 0.3156714975 1809.520358
1807.84398 266.609297 506.8586423 2706.982572 240.2493453
1302.661715 294.28469 267.6265082 265.055571 256.0315725

KEY POINT #4 (t plus 3722.1679 s with a Mixing Number of 81.5971): 79.32857287
0.040894 0.00925 0.3937 0.7937336583 0.8027849379
0.6215741868 0.6215741868 0.9990771039 34.73750021 241653.4996
0.06111335493 0.05331198012 0.06720166946 0.0369913702 0.1041930397
88.41597612 128.1496189 128.1496189 100.2171246 89.5115766
85.86422604 81.15772623 4.203043862 4.261231552 2.224555042
0.672232069 0.6846609893 0.6846609893 2.002340813 1.345497669
0.04300923724 966.4499608 936.3948258 1.420774138 2.283658076
0.0003202530717 0.0002161839256 1.323714018e-005 1.342443898e-005
1553.97554 1508.156511 485.2505683 474.6664091 2.556351154
2.464478344 2.501478344 0.6606468727 1.022063181 1894.129411
1892.922717 370.4486701 538.4896775 2717.526497 168.0410075
1355.639733 420.1263531 375.0528285 359.7282265 339.9724888

KEY POINT #5 (t plus 4471.4658 s with a Mixing Number of 103.1226): 81.43349434
0.040894 0.00925 0.3937 0.791611241 0.8026756863

0.6142517558	0.6142517558	0.9989142903	31.02671626	244756.0522
0.05904902476	0.05237398043	0.06839565118	0.03856206907	0.1069577202
99.2877467	132.7070468	132.7070468	110.3717995	100.2375781
93.18814251	86.30720838	4.215318663	4.270303985	2.255939606
0.6775660644	0.6849238225	0.6849238225	1.766341343	1.297990074
0.04411749092	958.9550425	932.5185764	1.613932761	2.624624973
0.0002839199235	0.0002081875966	1.339447228e-005	1.360596107e-005	
1546.123433	1500.266354	487.0716963	475.4445297	2.928711291
2.841160886	2.878160886	0.9886717321	1.451757244	1889.283119
1888.320462	416.2364599	557.9555234	2723.785619	141.7190635
1331.327596	463.0412552	420.239593	390.5485686	361.6220441
KEY POINT #6 (t plus 5914.9903 s with a Mixing Number of 168.7475): 79.68681832				
0.040894	0.00925	0.3937	0.7737611506	0.7884311874
0.6238189869	0.6238189869	0.998592485	23.07503558	232471.5817
0.05507184902	0.05011631875	0.06861987713	0.03604369515	0.1046635723
119.4851953	143.5175886	143.5175886	131.591717	120.4794908
109.6339443	90.82062783	4.24499573	4.294199029	2.339547633
0.6836388345	0.6846369702	0.6846369702	1.447785354	1.200016591
0.04704735345	943.6143225	922.970791	2.157319173	3.453377918
0.000233159785	0.0001913222274	1.376777162e-005	1.401768218e-005	
1522.198802	1479.618812	491.0563338	478.1545984	3.989476493
3.915371094	3.952371094	1.954479689	2.833763118	1935.841339
1935.308881	501.7371396	604.315083	2737.936897	102.5779434
1331.526255	553.2627931	505.957565	459.9996739	380.6753925
KEY POINT #7 (t plus 6331.0191 s with a Mixing Number of 195.5917): 80.0313916				
0.040894	0.00925	0.3937	0.7723095843	0.788290749
0.6148827979	0.6148827979	0.9983994061	20.93343065	231114.4682
0.05398526425	0.0494007913	0.06833378054	0.03678236686	0.1051161474
124.8528483	146.9000832	146.9000832	136.9128705	125.3684585
122.4921146	92.35819441	4.254500969	4.30241248	2.368363704
0.684450813	0.6842886038	0.6842886038	1.382404707	1.173102054
0.04805525768	939.2392543	919.8811469	2.354550393	3.823137876
0.000223969469	0.0001865791275	1.388455039e-005	1.416096427e-005	
1514.007854	1472.618149	492.2048595	478.2347559	4.378394552
4.307237868	4.344237868	2.311746471	3.310210917	1924.880548
1924.44234	524.5752002	618.8785529	2742.151136	94.30335264
1306.001995	576.0273854	526.7679289	514.5378835	387.1725976
KEY POINT #8 (t plus 7839.3234 s with a Mixing Number of 310.7128): 80.08352496				
0.040894	0.00925	0.3937	0.7694573951	0.7898622627
0.599910522	0.599910522	0.9976780292	15.18754201	223359.6711
0.05053929282	0.0468383351	0.06775733249	0.03742728876	0.1051846213
141.5084911	158.856689	158.856689	151.6803286	142.3138903
141.1922651	98.26690132	4.288874988	4.33457939	2.480259683
0.6849273456	0.6820900019	0.6820900019	1.21673436	1.090025568
0.05198796368	924.8873871	908.5651216	3.170675228	5.272974713
0.0001943107779	0.0001715265715	1.429707965e-005	1.466216194e-005	
1484.186655	1445.88451	495.8847928	478.7549843	6.003726082
5.941201364	5.978201364	3.771961959	4.979342109	1921.986218
1921.755557	595.8203968	670.6066048	2756.165877	74.78620792
1251.379613	639.572395	599.2742874	594.4654343	412.1727711
KEY POINT #9 (t plus 8052.6366 s with a Mixing Number of 330.0555): 78.80713126				
0.040894	0.00925	0.3937	0.7688517644	0.7898626279
0.6098309328	0.6098309328	0.9976751016	14.58319735	218986.5199
0.05007103976	0.04646971078	0.06761386833	0.03589429091	0.1035081592
143.7322339	160.5577931	160.5577931	153.4087757	144.668108
143.4586956	101.2222109	4.294074004	4.339582912	2.497440094
0.6847623832	0.6816561858	0.6816561858	1.198196806	1.079581421
0.05259627153	922.8824404	906.9046366	3.303186397	5.403967964
0.0001910726503	0.0001695792818	1.435572926e-005	1.471660825e-005	
1479.723847	1441.834425	496.3598993	479.5779191	6.269577405
6.208367333	6.245367333	4.013299298	5.212211277	1946.686941
1946.474271	605.3805013	677.9999394	2758.042561	72.61943808
1268.687002	647.0497258	609.3991501	604.2071589	424.649904
KEY POINT #10 (t plus 8367.3136 s with a Mixing Number of 364.5022): 79.72467577				
0.040894	0.00925	0.3937	0.7674952806	0.7895238661
0.59314993	0.59314993	0.9973513239	13.53927026	219635.8454
0.04937725751	0.04593659539	0.06631105697	0.03840223868	0.1047132956

147.0109947	163.0100651	163.0100651	155.7523384	147.9401601
146.9383346	116.460199	4.302029248	4.346996735	2.522757896
0.6844218955	0.6809783186	0.6809783186	1.172184666	1.065072664
0.05349549556	919.8871402	904.4884942	3.501981274	5.888402718
0.0001864861453	0.0001668488467	1.44402571e-005	1.484393809e-005	
1472.940711	1435.889656	497.0234113	478.578568	6.669232043
6.610764292	6.647764292	4.391644125	5.541777215	1917.875904
1917.692592	619.4979421	688.6738562	2760.694224	69.17591412
1229.202048	657.2031318	623.4952203	619.1864955	489.1001965
KEY POINT #11 (t plus 8367.3136 s with a Mixing Number of 364.5022): 79.72467577				
0.040894	0.00925	0.3937	0.7674952806	0.7895238661
0.59314993	0.59314993	0.9973513239	13.53927026	219635.8454
0.04937725751	0.04593659539	0.06631105697	0.03840223868	0.1047132956
147.0109947	163.0100651	163.0100651	155.7523384	147.9401601
146.9383346	116.460199	4.302029248	4.346996735	2.522757896
0.6844218955	0.6809783186	0.6809783186	1.172184666	1.065072664
0.05349549556	919.8871402	904.4884942	3.501981274	5.888402718
0.0001864861453	0.0001668488467	1.44402571e-005	1.484393809e-005	
1472.940711	1435.889656	497.0234113	478.578568	6.669232043
6.610764292	6.647764292	4.391644125	5.541777215	1917.875904
1917.692592	619.4979421	688.6738562	2760.694224	69.17591412
1229.202048	657.2031318	623.4952203	619.1864955	489.1001965
KEY POINT #12 (t plus 0 s with a Mixing Number of 38.5793): 72.81053655 0.040894				
0.00925	0.3937	0.7763149194	0.7780497256	0.5049946991
0.5049946991	0.9989265291	35.52012539	227191.511	0.06959656899
0.0555025919	0.05389813965	0.04173387349	0.09563201313	39.99842105
117.3406139	117.3406139	40.14561299	40.0124062	39.45363492
37.77736682	4.178365689	4.241881551	2.15899585	0.6286689885
0.68310356	0.68310356	4.338919393	1.475935104	0.04065885631
992.2547945	945.2339703	1.03627021	2.049838951	0.0006528255947
0.000237681442	1.286441078e-005	1.310574532e-005	1531.44724	
1524.8333	480.6062045	466.2487016	1.82499369	1.733286485
1.770286485	0.07383805876	0.07441947837	1609.564356	1608.302676
167.684814	492.486422	2702.046753	324.801608	1117.077934
168.2998356	167.7417424	165.4100932	158.409974	
KEY POINT #13 (t plus 8367.3136 s with a Mixing Number of 364.5022): 79.72467577				
0.040894	0.00925	0.3937	0.7674952806	0.7895238661
0.59314993	0.59314993	0.9973513239	13.53927026	219635.8454
0.04937725751	0.04593659539	0.06631105697	0.03840223868	0.1047132956
147.0109947	163.0100651	163.0100651	155.7523384	147.9401601
146.9383346	116.460199	4.302029248	4.346996735	2.522757896
0.6844218955	0.6809783186	0.6809783186	1.172184666	1.065072664
0.05349549556	919.8871402	904.4884942	3.501981274	5.888402718
0.0001864861453	0.0001668488467	1.44402571e-005	1.484393809e-005	
1472.940711	1435.889656	497.0234113	478.578568	6.669232043
6.610764292	6.647764292	4.391644125	5.541777215	1917.875904
1917.692592	619.4979421	688.6738562	2760.694224	69.17591412
1229.202048	657.2031318	623.4952203	619.1864955	489.1001965
KEY POINT #14 (t plus 5771.8891 s with a Mixing Number of 160.3724): 79.14939848				
0.040894	0.00925	0.3937	0.7747234185	0.7889714186
0.6307992806	0.6307992806	0.9986762411	23.89015418	231775.9558
0.05545280872	0.05036139336	0.06871958306	0.03523812243	0.1039577055
117.5889727	142.3543834	142.3543834	130.4885297	118.2786811
108.1468163	90.26843581	4.241808375	4.291458782	2.329930027
0.6832730897	0.6847285235	0.6847285235	1.472542469	1.209657853
0.04671101666	945.1303017	924.0219993	2.092642964	3.313055156
0.0002371980423	0.0001930083167	1.372760774e-005	1.396493217e-005	
1524.916967	1481.967676	490.6504887	478.3039009	3.862346893
3.787023739	3.824023739	1.839619628	2.742318628	1947.996893
1947.426154	493.6816808	599.3135225	2736.463441	105.6318417
1348.68337	548.5472712	496.6064785	453.702534	378.3435409

End

D.20 TEST #20 - T20_RCIC_1ATM_57KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T20_RCIC_1ATM_57kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 2078.8719 s, and ending (KEY POINT #11) at t plus 15071.183 s, for a time period of 12992.3111 s.
Original Data Record Time: 16478.1055 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 3224.9565 s, T_bulk = 55.6078 C and T_out = 53.3852 C
Stratification Beginning SP12 Temperature = 55.1982 C
Stratification Beginning Pressure = 15.2659 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 9485.4535 s, T_bulk = 84.6456 C and T_out = 72.0563 C
Stratification Ending SP12 Temperature = 84.473 C
Stratification Ending Pressure = 15.2377 psia
Plume detected! Setting t_plume (KEY POINT #2) to 3609.5595 s.
At t = 3609.5595 s, the pool pressure is 15.2627 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 57.7168, 57.5261, 59.5267, 57.8725, and 54.7286 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 8.806 +/- 3.1575 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 8.3013 +/- 3.0427 C.
Minimum Steam Quality: 0.97248 at t plus 9593.6557 s
Maximum Steam Quality: 1.0121 at t plus 3353.8528 s
Time-Averaged Steam Quality: 1.0071 +/- 0.0016623
Minimum Turbine Outlet Steam Quality: 0.98382 at t plus 9593.6557 s
Maximum Turbine Outlet Steam Quality: 1.0223 at t plus 7911.0285 s
Time-Averaged Turbine Outlet Steam Quality: 1.0174 +/- 0.001815
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 12902.313 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.43333 degrees/min at t plus 6973.0108 s and 0.17699 degrees/min at t plus 10060.8655 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.41556 degrees/min at t plus 7391.1157 s and 0.19428 degrees/min at t plus 9587.5544 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.17726 degrees/min at t plus 6984.6155 s and -0.14667 degrees/min at t plus 10060.2654 s, respectively
Max and min smoothed lower level changerates: 0.97015 degrees/min at t plus 8625.0393 s and 0.015747 degrees/min at t plus 6981.0123 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.32911 degrees/min at t plus 7505.4203 s and -0.74234 degrees/min at t plus 8625.0393 s, respectively
Max and min smoothed outlet level changerates: 2.3129 degrees/min at t plus 9708.6583 s and 0.0086426 degrees/min at t plus 8791.7409 s, respectively
Max and min smoothed lower-outlet level changerate differences: 0.86828 degrees/min at t plus 8625.0393 s and -2.015 degrees/min at t plus 9712.8585 s, respectively
Max and min smoothed hot (SP8) level changerates: 0.91653 degrees/min at t plus 4862.8791 s and 0.01821 degrees/min at t plus 10660.5738 s, respectively
Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.67911 degrees/min at t plus 4862.8791 s and -0.33511 degrees/min at t plus 7275.6182 s, respectively
The mean steam flow rate was 23.8957 +/- 0.78305 g/s
The mean feedwater flow rate was 23.4546 +/- 1.129 g/s
The mean water injection to steam flow rate was 0.0061292 +/- 0.028436 g/s
Mean Smoothed Condensing Region SP8-SP9 delta T is 8.3634 +/- 3.5149 C over the Stratification Period, beginning at 1.4895 C and ending at 11.8254 C
Mean Smoothed SP8-Upper Pool delta T is 7.8799 +/- 3.3771 C over the Stratification Period, beginning at 1.3073 C and ending at 11.237 C
The stratification period begins and ends with Smoothed SP8 readings of 57.1592 and 97.016 C, respectively
The stratification period begins and ends with condensing flows of 0.27341 and 0.79128 kg/s, respectively.
The stratification period begins and ends with condensing+cooling flows of 9.2413 and 1.1347 kg/s, respectively.
The stratification period had a mean sparger steam enthalpy of 2719.8569 +/- 1.0362 kJ/kg.
At plume detection, the condensing and condensing+cooling flows are 0.28485 and 6.8534 kg/s, respectively

The plume period had a mean steam enthalpy of 2720.5284 +/- 0.99922 kJ/kg.

Maximum Smoothed Top-Mid delta T is 1.2573 degrees C at t plus 9710.4554 s with T_upper = 86.967 C and T_mid = 85.7096 C

At t plus 9710.4554 s, Smoothed SP8-SP9 is 12.0289 C and Smoothed SP8-Top is 10.7715 C, where Smoothed SP8 is 97.7385 C and Pool P = 15.2362 psia

Maximum Smoothed Top-Lower delta T is 5.8466 degrees C at t plus 8446.8371 s with T_upper = 81.5142 C and T_low = 75.6676 C

At t plus 8446.8371 s, Smoothed SP8-SP9 is 10.7535 C and Smoothed SP8-Top is 10.2588 C, where Smoothed SP8 is 91.7731 C and Pool P = 15.2527 psia

Maximum Smoothed Mid-Lower delta T is 5.5273 degrees C at t plus 8413.5322 s with T_mid = 80.9039 C and T_low = 75.3766 C

At t plus 8413.5322 s, Smoothed SP8-SP9 is 10.9349 C and Smoothed SP8-Top is 10.6334 C, where Smoothed SP8 is 91.8389 C and Pool P = 15.2511 psia

Maximum Smoothed Top-Outlet delta T is 13.7148 degrees C at t plus 9344.5995 s with T_upper = 85.2301 C and T_out = 71.5153 C

At t plus 9344.5995 s, Smoothed SP8-SP9 is 11.7886 C and Smoothed SP8-Top is 11.0087 C, where Smoothed SP8 is 96.2388 C and Pool P = 15.2535 psia

Maximum Smoothed Mid-Outlet delta T is 13.0456 degrees C at t plus 9490.0518 s with T_mid = 85.2391 C and T_out = 72.1936 C

At t plus 9490.0518 s, Smoothed SP8-SP9 is 11.8117 C and Smoothed SP8-Top is 11.243 C, where Smoothed SP8 is 97.0508 C and Pool P = 15.2373 psia

Maximum Smoothed Lower-Outlet delta T is 13.4754 degrees C at t plus 9517.4554 s with T_low = 85.9246 C and T_out = 72.4492 C

At t plus 9517.4554 s, Smoothed SP8-SP9 is 11.778 C and Smoothed SP8-Top is 10.9618 C, where Smoothed SP8 is 96.9436 C and Pool P = 15.2513 psia

Maximum Smoothed Condensing Region SP8-SP9 delta T is 12.523 degrees C at (KEY POINT #14) t plus 9195.649 s with T_SP8 = 96.2987 C and T_SP9 = 83.7756 C and Pool P = 15.252 psia

Maximum Smoothed Condensing Region SP8-Upper delta T is 11.8167 degrees C at t plus 9195.649 s with T_SP8 = 96.2987 C and T_upper = 84.4819 C and Pool P = 15.252 psia

Maximum Top-Mid delta T is 1.6034 degrees C at (KEY POINT #4) t plus 7125.1135 s ignoring SP 4, with temperatures of 74.8059 and 73.2025 C, respectively, at Set # 2, where Pool P = 15.2521 psia and T_outlet = 67.3946 C

Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 7477.7207 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.99983 C and a raw SP12 Reading of 75.609 C.

Maximum Top-Lower delta T is 7.1289 degrees C at t plus 8778.7421 s, with temperatures of 82.7181 and 75.5892 C, respectively, at Set # 1, where Pool P = 15.2497 psia and T_outlet = 70.9883 C

Maximum Mid-Low delta T is 5.7523 degrees C at (KEY POINT #6) t plus 8537.5383 s ignoring SP 4, with temperatures of 81.3109 and 75.5585 C, respectively, at Set # 2, where Pool P = 15.2508 psia and T_outlet = 70.5233 C

Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 8712.5413 s with a Smoothed Mid-Axis Mid-Low Delta T of 1.9158 C and a raw SP12 Reading of 81.9018 C.

Maximum Top-Outlet delta T is 14.0029 degrees C at t plus 9366.9518 s, with temperatures of 85.5923 and 71.5894 C, respectively, at Set # 1, where Pool P = 15.2516 psia

Maximum Mid-Outlet delta T is 12.7364 degrees C at t plus 9408.5561 s ignoring SP 4, with temperatures of 84.3102 and 71.5738 C, respectively, at Set # 2, where Pool P = 15.2498 psia

Maximum Lower-Outlet delta T is 13.9535 degrees C at (KEY POINT #8) t plus 9344.9515 s, with temperatures of 85.3905 and 71.437 C, respectively, at Set # 1, where Pool P = 15.2459 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 9780.3604 s with a Smoothed Mid-Axis Low-Outlet Delta T of 4.65 C and a raw SP12 Reading of 85.7542 C.

Minimum SP Pressure is 14.783 psia at t plus 0.30002 s

Maximum SP Pressure is 15.4698 psia at t plus 12978.0143 s

Beginning SP Pressure is 14.7935 psia

Ending SP Pressure is 15.4565 psia

Time-Average SP Pressure is 15.2425 +/- 0.089631 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 78.0448 cm (cold) / 78.2002 cm (hot) at 14.562 psia

Beginning Smoothed SP Level is 78.4526 cm (cold) / 78.6366 cm (hot) at 14.7971 psia

Ending Smoothed SP Level is 77.9517 cm (cold) / 79.0159 cm (hot) at 15.4623 psia

Minimum Smoothed Cold SP Level is 77.8984 cm at t plus 12557.7043 s and 15.3311 psia

Minimum Smoothed Hot SP Level is 78.6231 cm at t plus 2607.2411 s and 15.2673 psia

Maximum Smoothed Cold SP Level is 78.4575 cm at t plus 552.1106 s and 14.9821 psia

Maximum Smoothed Hot SP Level is 79.0175 cm at t plus 12983.6136 s and 15.4577 psia

SP 12 Temperature at the beginning is 40.0183 C, and at the end is 99.9748 C
 At plume detection, the Mixing Number is 44.626
 The Mixing Number ranges from a minimum of 33.6287 at (KEY POINT #12) t plus 0 s to a maximum of 648.6732 at (KEY POINT #13) t plus 12992.3111 s; it had a mean value of 102.0038 +/- 103.016 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m3) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 33.6287): 17.2933 0.040894
 0.00925 0.3937 0.784525937 0.786366053 1.01229275
 1 1 28.3878995 55108.5536 0.0695240922 0.0585842657
 0.0227136507 3.16566909e-006 0.0227136507 40.444008 115.132806
 101.696401 40.4559645 40.5916857 40.741424 38.0774187
 4.17853687 4.21881729 2.0843193 0.629197093 0.678440305
 0.678440305 4.29935352 1.72121457 0.0378722462 992.050873
 957.129682 0.632792924 0.609263471 0.000647389461 0.000276793532
 1.23273139e-005 1.28327122e-005 1532.08343 1543.49029 473.118764
 482.37706 1.07713425 1.02022112 1.05722112 0.0756103015
 0.0756583575 2706.73038 2705.92451 169.483515 426.258826
 2678.24146 256.775311 2280.47156 169.533476 170.099088
 170.727871 159.600179

KEY POINT #2 (t plus 3609.5595 s with a Mixing Number of 44.626): 17.6877954
 0.040894 0.00925 0.3937 0.782805323 0.78647775
 1.01680787 1 1 28.5614993 55413.2951
 0.0666651005 0.058408531 0.0232317954 2.82251833e-006 0.0232317954
 57.5261171 120.990061 102.603615 59.5267408 57.7167549
 57.8724946 54.7286332 4.18175496 4.22000463 2.08806454
 0.648411116 0.678790963 0.678790963 3.1237276 1.70475793
 0.0380161442 984.466475 956.469453 0.651987975 0.619363298
 0.000484356381 0.000274211613 1.23583417e-005 1.30532701e-005 1552.23681
 1542.59824 473.576262 486.106589 1.11210592 1.05259368
 1.08959368 0.177705036 0.195129704 2718.28873 2717.47297
 240.88278 430.08934 2679.66244 189.20656 2288.19939
 249.249673 241.67855 242.332788 229.19115

KEY POINT #3 (t plus 3224.9565 s with a Mixing Number of 43.0069): 17.6790675
 0.040894 0.00925 0.3937 0.782900198 0.786370198
 1.01706937 1 1 28.5780136 55338.9464
 0.0669833021 0.0584084091 0.0232203318 1.00468258e-005 0.0232203318
 55.6697176 121.280299 102.604243 57.1592349 55.8518934
 56.1314889 53.3122207 4.181095 4.22000546 2.08806716
 0.646546402 0.678791203 0.678791203 3.22446412 1.70474663
 0.0380162447 985.382803 956.468994 0.652001442 0.618892448
 0.000498617151 0.000274209838 1.23583632e-005 1.30643576e-005 1550.80887
 1542.59762 473.576578 486.296562 1.11213048 1.05263245
 1.08963245 0.162741467 0.174658158 2718.87889 2718.06219

233.120403	430.091995	2679.66342	196.971592	2288.7869
239.348597	233.880659	235.052675	223.269762	
KEY POINT #4 (t plus 7125.1135 s with a Mixing Number of 65.4321):				19.3663978
0.040894	0.00925	0.3937	0.781215775	0.787245886
1.0188561	1	1	31.6163766	60292.8642
0.0638095721	0.0584360899	0.025436533	6.74370361e-006	0.025436533
73.7447575	123.127464	102.461472	85.8643987	74.5248556
72.7134464	67.4676162	4.19061334	4.21981741	2.08747334
0.662538022	0.678736687	0.678736687	2.42910434	1.70731586
0.0379934646	975.607366	956.573142	0.648949546	0.61270564
0.000384042586	0.000274613282	1.23534791e-005	1.31353765e-005	1557.8745
1542.73962	473.504763	487.522866	1.10656537	1.05163231
1.08863231	0.366127476	0.598566082	2722.86501	2721.86541
308.769439	429.489098	2679.44011	120.719659	2293.37591
359.616927	312.037375	304.449451	282.482799	
KEY POINT #5 (t plus 7477.7207 s with a Mixing Number of 70.4269):				19.1265364
0.040894	0.00925	0.3937	0.780976524	0.787300683
1.01891859	1	1	31.2414957	59535.2177
0.0634069343	0.058437558	0.0251214902	9.1296261e-006	0.0251214902
75.9726387	123.189733	102.453898	87.0332637	76.6520416
73.3854076	68.6203986	4.19225972	4.21980745	2.08744189
0.664186042	0.678733788	0.678733788	2.35433221	1.70745236
0.0379922575	974.277464	956.578665	0.648787974	0.612438262
0.00037300041	0.000274634714	1.235322e-005	1.31377798e-005	1557.76743
1542.74714	473.500951	487.564465	1.1062708	1.05160254
1.08860254	0.401931268	0.626370466	2722.97056	2721.99453
318.10744	429.457116	2679.42826	111.349676	2293.51344
364.527783	320.954486	307.265045	287.309332	
KEY POINT #6 (t plus 8537.5383 s with a Mixing Number of 87.2294):				18.6051333
0.040894	0.00925	0.3937	0.780760613	0.787901895
1.01787411	1	1	30.315501	58112.162
0.062415268	0.0584424294	0.0244366603	4.71361171e-006	0.0244366603
81.4029424	122.006838	102.428768	92.4599335	81.7418222
76.6387626	70.4925607	4.19670556	4.21977744	2.08733755
0.667918589	0.678724164	0.678724164	2.18810242	1.70790546
0.0379882535	970.92815	956.596987	0.648252095	0.613835214
0.000348243226	0.000274705849	1.23523603e-005	1.30925833e-005	1556.69593
1542.77207	473.488303	486.797388	1.10529383	1.05157211
1.08857211	0.501733013	0.769998294	2720.52538	2719.60635
340.884479	429.350997	2679.38893	88.4665185	2291.17438
387.345646	342.305362	320.901619	295.149546	
KEY POINT #7 (t plus 8712.5413 s with a Mixing Number of 89.7922):				18.5629217
0.040894	0.00925	0.3937	0.780630368	0.787907184
1.01809908	1	1	30.2751849	57939.9854
0.0622932817	0.0584449325	0.0243812181	8.62616823e-007	0.0243812181
82.0655217	122.244278	102.415854	93.6351462	82.4988418
79.5532496	70.834157	4.19729009	4.21975742	2.08728396
0.668346764	0.678719215	0.678719215	2.16924751	1.70813839
0.0379861965	970.509187	956.606401	0.647976864	0.613161521
0.000345415619	0.000274742415	1.23519186e-005	1.31016968e-005	1556.48895
1542.78487	473.481802	486.954198	1.10479207	1.05154839
1.08854839	0.51522182	0.804462895	2721.00956	2720.09297
343.665321	429.296467	2679.36873	85.6311452	2291.71309
392.291317	345.482832	333.124769	296.580317	
KEY POINT #8 (t plus 9344.9515 s with a Mixing Number of 100.3919):				18.573379
0.040894	0.00925	0.3937	0.780318136	0.787922475
1.01813072	1	1	30.3079737	57967.396
0.0618527943	0.0584458625	0.0243949531	7.35712596e-006	0.0243949531
84.448507	122.27486	102.411055	96.2452032	85.2300862
84.4433639	71.5157276	4.19946818	4.21975111	2.08726404
0.669838341	0.678717376	0.678717376	2.10379267	1.70822495
0.0379854323	968.984313	956.609898	0.647874622	0.613006352
0.000335566536	0.000274756005	1.23517545e-005	1.31028787e-005	1555.61177
1542.78963	473.479387	486.974844	1.10460569	1.05138714
1.08838714	0.566274928	0.88561273	2721.07544	2720.15687
353.669963	429.276205	2679.36122	75.606242	2291.79924
403.28091	356.951136	353.64978	299.435287	

KEY POINT #9 (t plus 9485.4535 s with a Mixing Number of 104.401): 18.5788676

0.040894	0.00925	0.3937	0.780300808	0.788004844
1.01781875	1	1	30.2874864	58044.076
0.0617150586	0.0584470602	0.024402162	1.35312424e-006	0.024402162
85.1906103	121.92292	102.404876	97.0159744	85.7789556
85.5858067	72.1604192	4.20017079	4.21974299	2.08723841
0.670287462	0.678715007	0.678715007	2.08413431	1.70833644
0.0379844483	968.503674	956.614402	0.647742973	0.613451296
0.000332598165	0.000274773507	1.23515431e-005	1.30894359e-005	1555.2967
1542.79575	473.476276	486.746112	1.10436569	1.05107641
1.08807641	0.58301265	0.910836422	2720.36288	2719.44555
356.786639	429.250112	2679.35155	72.463473	2291.11277
406.527738	359.256625	358.448017	302.136051	

KEY POINT #10 (t plus 9780.3604 s with a Mixing Number of 109.4082): 18.5535139

0.040894	0.00925	0.3937	0.779941628	0.787862869
1.01797714	1	1	30.2505769	57932.4189
0.0615494428	0.0584435145	0.0243688616	8.15937577e-006	0.0243688616
86.0810442	122.115872	102.423169	97.9722354	87.2109983
87.1534187	80.9387371	4.20102893	4.21976703	2.08731431
0.670816809	0.678722019	0.678722019	2.06098395	1.70800643
0.0379873617	967.923432	956.601068	0.648132763	0.613532967
0.000329096205	0.0002747217	1.23521688e-005	1.30967671e-005	1554.89293
1542.77762	473.485485	486.869363	1.10507628	1.05131834
1.08831834	0.603640133	0.94295593	2720.7448	2719.8297
360.527014	429.327357	2679.38017	68.8003426	2291.41744
410.556976	365.273286	365.034059	338.94142	

KEY POINT #11 (t plus 12992.3111 s with a Mixing Number of 648.6732): 19.095888

0.040894	0.00925	0.3937	0.77951688	0.790158943
1.01832792	1	1	30.7697635	59499.5336
0.0588219367	0.0583684855	0.0250812354	7.14251177e-006	0.0250812354
100.466365	122.869102	102.810077	102.69256	100.657177
100.547054	98.6217698	4.21722177	4.22027735	2.08892618
0.677953508	0.67886936	0.67886936	1.74403385	1.70105597
0.0380491754	958.022003	956.318682	0.656421927	0.620782346
0.000280367961	0.000273630067	1.23654055e-005	1.31245943e-005	1544.67355
1542.39182	473.679994	487.303887	1.12019438	1.06608652
1.10308652	1.0311751	1.11558454	2722.15188	2721.2051
421.072455	430.961242	2679.98517	9.88878657	2291.19063
2679.96893	421.875903	421.414094	413.300301	

KEY POINT #12 (t plus 0 s with a Mixing Number of 33.6287): 17.2933 0.040894

0.00925	0.3937	0.784525937	0.786366053	1.01229275
1	1	28.3878995	55108.5536	0.0695240922
0.0227136507	3.16566909e-006	0.0227136507	40.444008	115.132806
101.696401	40.4559645	40.5916857	40.741424	38.0774187
4.17853687	4.21881729	2.0843193	0.629197093	0.678440305
0.678440305	4.29935352	1.72121457	0.0378722462	992.050873
957.129682	0.632792924	0.609263471	0.000647389461	0.000276793532
1.23273139e-005	1.28327122e-005	1532.08343	1543.49029	473.118764
482.37706	1.07713425	1.02022112	1.05722112	0.0756103015
0.0756583575	2706.73038	2705.92451	169.483515	426.258826
2678.24146	256.775311	2280.47156	169.533476	170.099088
170.727871	159.600179			

KEY POINT #13 (t plus 12992.3111 s with a Mixing Number of 648.6732): 19.095888

0.040894	0.00925	0.3937	0.77951688	0.790158943
1.01832792	1	1	30.7697635	59499.5336
0.0588219367	0.0583684855	0.0250812354	7.14251177e-006	0.0250812354
100.466365	122.869102	102.810077	102.69256	100.657177
100.547054	98.6217698	4.21722177	4.22027735	2.08892618
0.677953508	0.67886936	0.67886936	1.74403385	1.70105597
0.0380491754	958.022003	956.318682	0.656421927	0.620782346
0.000280367961	0.000273630067	1.23654055e-005	1.31245943e-005	1544.67355
1542.39182	473.679994	487.303887	1.12019438	1.06608652
1.10308652	1.0311751	1.11558454	2722.15188	2721.2051
421.072455	430.961242	2679.98517	9.88878657	2291.19063
2679.96893	421.875903	421.414094	413.300301	

KEY POINT #14 (t plus 9195.649 s with a Mixing Number of 97.207): 18.5672789

0.040894	0.00925	0.3937	0.780290647	0.787829249
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1.01785897		1	1	30.2737279	57999.6893
0.0619774507	0.0584462455		0.024386941	5.95636522e-006	0.024386941
83.7756365	121.971492		102.409079	96.2986751	84.4819381
83.3669485	71.2169212		4.19884112	4.21974851	2.08725585
0.669424818	0.678716619		0.678716619	2.12190976	1.7082606
0.0379851176	969.41774		956.611339	0.64783252	0.613463062
0.00033829788	0.000274761601	1.23516869e-005	1.30912822e-005		1555.88034
1542.79158	473.478392		486.777203	1.10452894	1.05150639
1.08850639	0.5514482		0.887343686	2720.45891	2719.54241
350.844485	429.267861		2679.35813	78.4233755	2291.19105
403.506145	353.80903		349.129965	298.18361	

End

D.21 TEST #21 - T21_RCIC_020GPM_57KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T21_RCIC_020GPM_57kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 2225.0753 s, and ending (KEY POINT #11) at t plus 18140.1606 s, for a time period of 15915.0853 s.
Original Data Record Time: 19780.1504 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 2412.944 s, T_bulk = 51.7363 C and T_out = 49.2512 C
Stratification Beginning SP12 Temperature = 51.6947 C
Stratification Beginning Pressure = 16.284 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 11365.199 s, T_bulk = 93.9202 C and T_out = 71.0933 C
Stratification Ending SP12 Temperature = 93.8152 C
Stratification Ending Pressure = 28.0762 psia
Plume detected! Setting t_plume (KEY POINT #2) to 1776.5286 s.
At t = 1776.5286 s, the pool pressure is 15.9188 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 49.0328, 48.884, 50.8941, 49.1077, and 46.584 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 10.9113 +/- 3.8881 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 10.372 +/- 3.7803 C.
Minimum Steam Quality: 0.57084 at t plus 2299.3415 s
Maximum Steam Quality: 0.68061 at t plus 13275.3323 s
Time-Averaged Steam Quality: 0.62229 +/- 0.018351
Minimum Turbine Outlet Steam Quality: 0.58905 at t plus 2299.5735 s
Maximum Turbine Outlet Steam Quality: 0.68737 at t plus 13275.3323 s
Time-Averaged Turbine Outlet Steam Quality: 0.6345 +/- 0.014589
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 15825.1091 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.456 degrees/min at t plus 6332.7162 s and 0.17192 degrees/min at t plus 11080.3947 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.35745 degrees/min at t plus 8053.8426 s and 0.19229 degrees/min at t plus 11605.7048 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.15261 degrees/min at t plus 6326.8109 s and -0.11865 degrees/min at t plus 5353.4952 s, respectively
Max and min smoothed lower level changerates: 1.4088 degrees/min at t plus 9535.6684 s and 0.027255 degrees/min at t plus 8778.16 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.29941 degrees/min at t plus 8778.064 s and -1.1796 degrees/min at t plus 9535.6684 s, respectively
Max and min smoothed outlet level changerates: 2.9442 degrees/min at t plus 11681.2091 s and -0.0019412 degrees/min at t plus 9423.464 s, respectively
Max and min smoothed lower-outlet level changerate differences: 1.39 degrees/min at t plus 9535.6684 s and -2.5921 degrees/min at t plus 11654.5026 s, respectively
Max and min smoothed hot (SP8) level changerates: 0.81927 degrees/min at t plus 6579.8123 s and -0.14543 degrees/min at t plus 10524.784 s, respectively
Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.4953 degrees/min at t plus 6621.5137 s and -0.36276 degrees/min at t plus 10524.784 s, respectively
The mean steam flow rate was 23.811 +/- 0.75462 g/s

The mean feedwater flow rate was 23.2469 +/- 0.85061 g/s
 The mean water injection to steam flow rate was 12.4674 +/- 0.36292 g/s
 Mean Smoothed Condensing Region SP8-SP9 delta T is 11.4856 +/- 3.348 C over the Stratification Period, beginning at 3.5174 C and ending at 14.8787 C
 Mean Smoothed SP8-Upper Pool delta T is 10.9199 +/- 3.282 C over the Stratification Period, beginning at 3.2995 C and ending at 14.1912 C
 The stratification period begins and ends with Smoothed SP8 readings of 55.4119 and 108.9393 C, respectively
 The stratification period begins and ends with condensing flows of 0.22806 and 0.46943 kg/s, respectively.
 The stratification period begins and ends with condensing+cooling flows of 3.8644 and 0.83918 kg/s, respectively.
 The stratification period had a mean sparger steam enthalpy of 1873.5353 +/- 22.9931 kJ/kg.
 At plume detection, the condensing and condensing+cooling flows are 0.21668 and 6.7977 kg/s, respectively
 The plume period had a mean steam enthalpy of 1870.4632 +/- 25.6547 kJ/kg.
 Maximum Smoothed Top-Mid delta T is 1.2792 degrees C at t plus 15536.0736 s with T_upper = 113.3442 C and T_mid = 112.065 C
 At t plus 15536.0736 s, Smoothed SP8-SP9 is 12.2296 C and Smoothed SP8-Top is 10.9504 C, where Smoothed SP8 is 124.2946 C and Pool P = 39.3564 psia
 Maximum Smoothed Top-Lower delta T is 9.8992 degrees C at t plus 9253.1612 s with T_upper = 86.5543 C and T_low = 76.6552 C
 At t plus 9253.1612 s, Smoothed SP8-SP9 is 13.7849 C and Smoothed SP8-Top is 13.2754 C, where Smoothed SP8 is 99.8297 C and Pool P = 24.425 psia
 Maximum Smoothed Mid-Lower delta T is 9.3944 degrees C at t plus 9254.7623 s with T_mid = 86.0525 C and T_low = 76.6581 C
 At t plus 9254.7623 s, Smoothed SP8-SP9 is 13.8327 C and Smoothed SP8-Top is 13.3337 C, where Smoothed SP8 is 99.8852 C and Pool P = 24.4266 psia
 Maximum Smoothed Top-Outlet delta T is 23.7673 degrees C at t plus 11258.9969 s with T_upper = 94.4223 C and T_out = 70.655 C
 At t plus 11258.9969 s, Smoothed SP8-SP9 is 14.6701 C and Smoothed SP8-Top is 13.8416 C, where Smoothed SP8 is 108.2639 C and Pool P = 27.8734 psia
 Maximum Smoothed Mid-Outlet delta T is 23.0068 degrees C at t plus 11336.3014 s with T_mid = 93.9499 C and T_out = 70.9432 C
 At t plus 11336.3014 s, Smoothed SP8-SP9 is 15.2702 C and Smoothed SP8-Top is 14.5995 C, where Smoothed SP8 is 109.2202 C and Pool P = 28.0234 psia
 Maximum Smoothed Lower-Outlet delta T is 23.1475 degrees C at t plus 11234.7956 s with T_low = 93.7436 C and T_out = 70.5961 C
 At t plus 11234.7956 s, Smoothed SP8-SP9 is 14.9113 C and Smoothed SP8-Top is 14.1792 C, where Smoothed SP8 is 108.4789 C and Pool P = 27.8321 psia
 Maximum Smoothed Condensing Region SP8-SP9 delta T is 16.0051 degrees C at (KEY POINT #14) t plus 11156.0001 s with T_SP8 = 109.282 C and T_SP9 = 93.2768 C and Pool P = 27.6943 psia
 Maximum Smoothed Condensing Region SP8-Upper delta T is 15.3167 degrees C at t plus 11156.0001 s with T_SP8 = 109.282 C and T_upper = 93.9653 C and Pool P = 27.6943 psia
 Maximum Top-Mid delta T is 1.5038 degrees C at (KEY POINT #4) t plus 6632.7164 s ignoring SP 4, with temperatures of 73.1159 and 71.612 C, respectively, at Set # 2, where Pool P = 20.148 psia and T_outlet = 66.1422 C
 Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 7235.2268 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.99935 C and a raw SP12 Reading of 74.899 C.
 Maximum Top-Lower delta T is 11.7104 degrees C at t plus 9445.2662 s, with temperatures of 87.7114 and 76.001 C, respectively, at Set # 1, where Pool P = 24.7752 psia and T_outlet = 69.3374 C
 Maximum Mid-Low delta T is 10.6345 degrees C at (KEY POINT #6) t plus 9368.7628 s ignoring SP 4, with temperatures of 86.3071 and 75.6726 C, respectively, at Set # 2, where Pool P = 24.6282 psia and T_outlet = 69.3547 C
 Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 9607.7795 s with a Smoothed Mid-Axis Mid-Low Delta T of 3.5446 C and a raw SP12 Reading of 87.4097 C.
 Maximum Top-Outlet delta T is 24.0903 degrees C at t plus 11265.2973 s, with temperatures of 94.635 and 70.5447 C, respectively, at Set # 1, where Pool P = 27.8862 psia
 Maximum Mid-Outlet delta T is 23.0215 degrees C at t plus 11323.7977 s ignoring SP 4, with temperatures of 93.8984 and 70.8768 C, respectively, at Set # 2, where Pool P = 27.9945 psia

Maximum Lower-Outlet delta T is 23.9096 degrees C at (KEY POINT #8) t plus 11293.5979 s, with temperatures of 94.6902 and 70.7806 C, respectively, at Set # 1, where Pool P = 27.9383 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 11859.1083 s with a Smoothed Mid-Axis Low-Outlet Delta T of 7.9685 C and a raw SP12 Reading of 95.9483 C.

Minimum SP Pressure is 15.1517 psia at t plus 0.39802 s
Maximum SP Pressure is 40.7132 psia at t plus 15915.0853 s
Beginning SP Pressure is 15.1583 psia
Ending SP Pressure is 40.7132 psia
Time-Average SP Pressure is 23.9081 +/- 7.2782 psia
SP Levels are fully corrected and compensated
Pre-Start SP Level is 77.49 cm (cold) / 77.6269 cm (hot) at 14.6959 psia
Beginning Smoothed SP Level is 77.8778 cm (cold) / 78.059 cm (hot) at 15.1586 psia
Ending Smoothed SP Level is 79.1329 cm (cold) / 80.5747 cm (hot) at 40.7106 psia
Minimum Smoothed Cold SP Level is 77.7337 cm at t plus 2118.6352 s and 16.1046 psia
Minimum Smoothed Hot SP Level is 78.0136 cm at t plus 2118.6352 s and 16.1046 psia
Maximum Smoothed Cold SP Level is 79.1379 cm at t plus 15742.6794 s and 40.0887 psia
Maximum Smoothed Hot SP Level is 80.5749 cm at t plus 15909.6929 s and 40.6906 psia
SP 12 Temperature at the beginning is 39.8595 C, and at the end is 113.5954 C
At plume detection, the Mixing Number is 40.0775
The Mixing Number ranges from a minimum of 34.7871 at (KEY POINT #12) t plus 0 s to a maximum of 220.3551 at (KEY POINT #13) t plus 15866.6805 s; it had a mean value of 93.0894 +/- 51.2867 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 34.7871): 26.4827517 0.040894

0.00925	0.3937	0.778778348	0.780589535	0.609059596
0.609059596	0.999566626	24.9717928	86896.9888	0.0695312694
0.0584611863	0.0223482762	0.0124351353	0.0347834115	40.3999124
102.331989	102.331989	40.7913522	40.5759864	40.8351669
38.6385874	4.17853099	4.21964725	2.08693622	0.629142616
0.67868703	0.67868703	4.30326097	1.70965257	0.0379728482
992.068913	956.667518	0.64619178	1.06050663	0.000647922649
0.0002749801	1.23490499e-005	1.24628674e-005	1532.01364	1542.86789
473.439573	465.974067	1.10153816	1.04514773	1.08214773
0.0754332975	0.0770171539	1800.12978	1799.50619	169.301467
428.94234	2679.23747	259.640873	1371.18744	170.93711
170.035693	171.121783	161.947289		

KEY POINT #2 (t plus 1776.5286 s with a Mixing Number of 40.0775): 26.9434015

0.040894	0.00925	0.3937	0.778670054	0.781309486
0.619600034	0.619600034	0.999566804	24.7562002	88102.3008
0.0681309808	0.0582060829	0.0228819152	0.0125065306	0.0353884458
48.8839859	103.646358	103.646358	50.8940905	49.0328377
49.1076931	46.584048	4.17930397	4.22139158	2.09245199
0.639278148	0.679181593	0.679181593	3.64240454	1.68622227

0.0381840531	988.549362	955.706023	0.674633723	1.08834964
0.000557152493	0.000271297061	1.23940268e-005	1.25061826e-005	1544.07656
1541.54286	474.098692	466.792707	1.15345585	1.09760116
1.13460116	0.116832758	0.129098105	1827.22151	1826.60865
204.759125	434.493519	2681.28992	229.734393	1392.728
213.16037	205.379754	205.695627	195.152927	
KEY POINT #3 (t plus 2412.944 s with a Mixing Number of 42.2955): 26.8372733				
0.040894	0.00925	0.3937	0.777631587	0.780578502
0.62656261	0.62656261	0.999570963	24.4533188	87624.0133
0.0676248291	0.058089461	0.0229767688	0.0122722844	0.0352490532
51.8944337	104.245895	104.245895	55.4118696	52.1123465
52.0415152	49.2560554	4.17996501	4.22219984	2.09501524
0.642594095	0.679400198	0.679400198	3.44662761	1.67574478
0.0382818273	987.182882	955.264874	0.687941363	1.09749002
0.000529856721	0.000269646482	1.24145546e-005	1.25249166e-005	1547.3728
1540.92161	474.397404	467.229816	1.17779977	1.12239987
1.15939987	0.135602507	0.160750778	1844.38051	1843.78255
217.343777	437.026446	2682.22283	219.682669	1407.35407
232.048259	218.253193	217.960119	206.321717	
KEY POINT #4 (t plus 6632.7164 s with a Mixing Number of 64.9032): 27.4071564				
0.040894	0.00925	0.3937	0.777912327	0.78357501
0.638681217	0.638681217	0.999505536	21.0631899	87991.576
0.064121093	0.0569272199	0.0236968303	0.0123007281	0.0359975584
72.0115794	110.17634	110.17634	84.3882082	72.7905912
70.2594315	66.1290259	4.18933005	4.23062624	2.12203637
0.661226027	0.681329186	0.681329186	2.49013068	1.57874103
0.0392993476	976.63859	950.815142	0.831455047	1.30118735
0.000393031629	0.000254251329	1.26179706e-005	1.27374495e-005	1557.87978
1534.22104	477.285292	469.780404	1.44227267	1.38935771
1.42635771	0.340169241	0.564932779	1886.31809	1885.87443
301.534885	462.109976	2691.33548	160.575091	1424.20812
353.443313	304.797251	294.197055	276.907189	
KEY POINT #5 (t plus 7235.2268 s with a Mixing Number of 70.2271): 27.5752125				
0.040894	0.00925	0.3937	0.777615173	0.783720388
0.635955664	0.635955664	0.999481136	20.3666961	88230.3714
0.0635446115	0.0567031278	0.0237596986	0.0124585907	0.0362182894
75.2123747	111.310746	111.310746	87.5969215	75.9157907
72.178864	67.9803421	4.19159994	4.23232873	2.12756373
0.663652178	0.681650332	0.681650332	2.3793299	1.56147418
0.0395048029	974.751586	949.94631	0.861490556	1.35393646
0.000376717122	0.000251487883	1.26569473e-005	1.27808681e-005	1557.89812
1532.82697	477.823578	470.091948	1.49803665	1.44592208
1.48292208	0.389395866	0.640159224	1883.05515	1882.64035
314.95223	466.914233	2693.05388	151.962004	1416.14092
366.927133	317.899487	302.241767	284.661829	
KEY POINT #6 (t plus 9368.7628 s with a Mixing Number of 94.9988): 27.9124289				
0.040894	0.00925	0.3937	0.777456253	0.785345737
0.632885231	0.632885231	0.999390374	17.7627248	88094.4702
0.0614693817	0.0557708888	0.0240701947	0.012591007	0.0366612017
86.510761	115.99986	115.99986	100.585062	87.0197293
78.0469384	69.3844276	4.20130561	4.23968316	2.15170112
0.671103429	0.682817116	0.682817116	2.0499088	1.49408804
0.0403929968	967.671104	946.295404	0.995125465	1.57140468
0.000327446026	0.000240628568	1.28182438e-005	1.29571228e-005	1554.81214
1526.6943	479.999072	471.567851	1.74767006	1.69817822
1.73517822	0.613810958	1.0355381	1887.85848	1887.54296
362.382909	486.795085	2700.06822	124.412176	1401.06339
421.620424	364.520042	326.85829	290.561618	
KEY POINT #7 (t plus 9607.7795 s with a Mixing Number of 97.6445): 27.7532201				
0.040894	0.00925	0.3937	0.777494646	0.785585314
0.635277543	0.635277543	0.999387068	17.4590139	87474.1852
0.061287831	0.0556698888	0.0240199669	0.0124321242	0.0364520911
87.4834569	116.505036	116.505036	102.474516	87.9529185
83.5912579	69.4794092	4.20226417	4.24050642	2.15442873
0.671665942	0.682927492	0.682927492	2.02539011	1.48719245
0.0404925334	967.032098	945.896384	1.01047005	1.58962128
0.000323726805	0.000239510217	1.28356366e-005	1.29745728e-005	1554.33062

1525.99864	480.228617	471.817012	1.77648309	1.72713635
1.76413635	0.637363351	1.10707286	1894.39911	1894.09429
366.472227	488.93913	2700.81515	122.466903	1405.45998
429.593152	368.443817	350.124978	290.961731	
KEY POINT #8 (t plus 11293.5979 s with a Mixing Number of 117.1848):	27.6653481			
0.040894	0.00925	0.3937	0.779783255	0.789110918
0.635875829	0.635875829	0.999323241	15.780444	86376.1375
0.0601155694	0.0550071191	0.0240715373	0.0122651395	0.0363366768
93.7071374	119.806636	119.806636	108.611433	94.4817792
93.7166695	70.7545309	4.20886611	4.24603848	2.17288375
0.674975991	0.683576171	0.683576171	1.88053383	1.44375699
0.0411621693	962.836169	943.261451	1.11553513	1.7531413
0.000301581269	0.000232432626	1.29493711e-005	1.30979085e-005	1550.49016
1521.28832	481.705273	472.882388	1.97451877	1.92616152
1.96316152	0.80661515	1.36815793	1903.8494	1903.60037
392.661273	502.962651	2705.65327	110.301378	1400.88674
455.52933	395.92068	392.70277	296.318174	
KEY POINT #9 (t plus 11365.199 s with a Mixing Number of 118.434):	27.4182218			
0.040894	0.00925	0.3937	0.780102124	0.789486854
0.642920035	0.642920035	0.99934058	15.7422282	85597.0077
0.0600484451	0.0549768866	0.0240875912	0.0119245009	0.0360120921
94.0606042	119.956693	119.956693	108.939324	94.7481172
94.1833218	71.1110333	4.20926613	4.24629623	2.17374877
0.67514899	0.683602671	0.683602671	1.87288862	1.44184804
0.0411934044	962.592246	943.14058	1.12051202	1.74169892
0.000300403639	0.000232120209	1.29545427e-005	1.30990649e-005	1550.23313
1521.06755	481.771409	473.189661	1.98393081	1.93558648
1.97258648	0.817252017	1.38342153	1919.73236	1919.48454
394.149759	503.600478	2705.87134	109.450719	1416.13188
456.916481	397.042658	394.667695	297.812144	
KEY POINT #10 (t plus 11859.1083 s with a Mixing Number of 125.579):	28.037825			
0.040894	0.00925	0.3937	0.782297829	0.792197956
0.633299975	0.633299975	0.999290598	15.3805249	87231.3345
0.059686006	0.0547683443	0.0241895515	0.0126363499	0.0368259015
95.9638834	120.990497	120.990497	110.651357	96.7582503
96.4640592	87.6915344	4.21146255	4.24808706	2.17977113
0.676054156	0.68377823	0.68377823	1.83271396	1.42884518
0.041410521	961.269427	942.305216	1.15528952	1.82294331
0.000294200382	0.000229988984	1.2990177e-005	1.31441164e-005	1548.78294
1519.53099	482.224714	473.145476	2.04977511	2.0015063
2.0385063	0.876552136	1.46541167	1901.0956	1900.85904
402.168272	507.995858	2707.36935	105.827587	1393.09974
464.163049	405.512803	404.276258	367.372923	
KEY POINT #11 (t plus 15915.0853 s with a Mixing Number of 220.2694):	28.616288			
0.040894	0.00925	0.3937	0.791329086	0.805746971
0.659350564	0.659350564	0.999128604	11.986706	86456.9869
0.0562174046	0.0525539395	0.0253003969	0.0122852791	0.037585676
113.759887	131.835814	131.835814	124.97161	115.032522
114.711983	111.916605	4.23581647	4.26852567	2.24976412
0.682364599	0.68489137	0.68489137	1.52543991	1.30676383
0.043899995	948.106165	933.266415	1.57546381	2.38733543
0.00024573921	0.000209672225	1.33643912e-005	1.3535453e-005	1529.95666
1501.81286	486.729965	477.23643	2.8543268	2.80689515
2.84389515	1.62448293	2.32021395	1984.09129	1983.94761
477.381116	554.230888	2722.60201	76.8497716	1429.8604
524.976982	482.771826	481.416019	469.580552	
KEY POINT #12 (t plus 0 s with a Mixing Number of 34.7871):	26.4827517			0.040894
0.00925	0.3937	0.778778348	0.780589535	0.609059596
0.609059596	0.999566626	24.9717928	86896.9888	0.0695312694
0.0584611863	0.0223482762	0.0124351353	0.0347834115	40.3999124
102.331989	102.331989	40.7913522	40.5759864	40.8351669
38.6385874	4.17853099	4.21964725	2.08693622	0.629142616
0.67868703	0.67868703	4.30326097	1.70965257	0.0379728482
992.068913	956.667518	0.64619178	1.06050663	0.000647922649
0.0002749801	1.23490499e-005	1.24628674e-005	1532.01364	1542.86789
473.439573	465.974067	1.10153816	1.04514773	1.08214773
0.0754332975	0.0770171539	1800.12978	1799.50619	169.301467

428.94234	2679.23747	259.640873	1371.18744	170.93711
170.035693	171.121783	161.947289		
KEY POINT #13 (t plus 15866.6805 s with a Mixing Number of 220.3551): 28.7336427				
0.040894	0.00925	0.3937	0.791351451	0.805683184
0.657412587	0.657412587	0.999124669	12.0483431	86836.8985
0.0562319699	0.0525834885	0.025341838	0.0123979759	0.0377398139
113.686636	131.692619	131.692619	125.446765	114.772686
114.47919	111.72551	4.23570356	4.2682354	2.2487571
0.682345934	0.684885234	0.684885234	1.52649108	1.30821947
0.0438645049	948.162834	933.389021	1.56921226	2.38486258
0.000245908375	0.000209918178	1.33594472e-005	1.35315011e-005	1530.05074
1502.06533	486.673507	477.118592	2.84224886	2.79474413
2.83174413	1.62057809	2.35434451	1979.55256	1979.4074
477.06997	553.618864	2722.40688	76.5488948	1425.9337
526.998185	481.669864	480.428774	468.770812	
KEY POINT #14 (t plus 11156.0001 s with a Mixing Number of 115.6884): 27.5105095				
0.040894	0.00925	0.3937	0.779311724	0.788527461
0.639358884	0.639358884	0.999338829	15.9047866	85973.7114
0.060197204	0.0550614585	0.0240423803	0.0120909258	0.0361333061
93.2768468	119.536808	119.536808	109.281956	93.9652996
93.0248698	70.3410475	4.20838397	4.24557641	2.17133409
0.674762954	0.683527869	0.683527869	1.88992103	1.44720354
0.0411061805	963.132062	943.478556	1.10663073	1.7297
0.000303025748	0.000232996385	1.29400722e-005	1.30855671e-005	1550.79651
1521.68384	481.586135	472.928026	1.95768606	1.90929413
1.94629413	0.793822043	1.39952075	1910.86087	1910.6079
390.84905	501.81583	2705.26073	110.96678	1409.04504
458.363524	393.745291	389.79005	294.585033	

End

D.22 TEST #22 - T22_RCIC_5PSIG_57KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T22_RCIC_5PSIG_57kw\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1765.272 s, and ending (KEY POINT #11) at t plus 18019.0696 s, for a time period of 16253.7976 s.
Original Data Record Time: 20227.2079 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 3089.9657 s, T_bulk = 55.3946 C and T_out = 53.443 C
Stratification Beginning SP12 Temperature = 55.0453 C
Stratification Beginning Pressure = 21.9324 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 13171.8404 s, T_bulk = 103.3419 C and T_out = 74.1528 C
Stratification Ending SP12 Temperature = 103.2469 C
Stratification Ending Pressure = 39.1479 psia
Plume detected! Setting t_plume (KEY POINT #2) to 3062.4552 s.
At t = 3062.4552 s, the pool pressure is 21.9116 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 55.6055, 55.3391, 57.3462, 55.7947, and 53.0737 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 11.7856 +/- 4.2743 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 11.1821 +/- 4.1572 C.
Minimum Steam Quality: 0.98863 at t plus 16097.0927 s
Maximum Steam Quality: 1.0091 at t plus 3508.3577 s
Time-Averaged Steam Quality: 1.0007 +/- 0.0037667
Minimum Turbine Outlet Steam Quality: 0.9904 at t plus 16097.0927 s
Maximum Turbine Outlet Steam Quality: 1.0154 at t plus 1602.0286 s
Time-Averaged Turbine Outlet Steam Quality: 1.0045 +/- 0.0050629
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 16163.7965 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.4574 degrees/min at t plus 7092.8267 s and 0.16889 degrees/min at t plus 10312.8888 s, respectively

Max and min smoothed mid (SP9) level changerates: 0.40467 degrees/min at t plus 8256.4482 s and 0.2058 degrees/min at t plus 10363.2367 s, respectively
 Max and min smoothed upper-mid level changerate differences: 0.19153 degrees/min at t plus 7090.4266 s and -0.11469 degrees/min at t plus 6859.2223 s, respectively
 Max and min smoothed lower level changerates: 1.8499 degrees/min at t plus 10345.5887 s and -0.021777 degrees/min at t plus 9934.6002 s, respectively
 Max and min smoothed mid-lower level changerate differences: 0.35861 degrees/min at t plus 9676.3754 s and -1.6425 degrees/min at t plus 10345.5887 s, respectively
 Max and min smoothed outlet level changerates: 2.0683 degrees/min at t plus 13892.6576 s and -0.040146 degrees/min at t plus 8599.7548 s, respectively
 Max and min smoothed lower-outlet level changerate differences: 1.8526 degrees/min at t plus 10345.5887 s and -1.7796 degrees/min at t plus 13922.5533 s, respectively
 Max and min smoothed hot (SP8) level changerates: 0.70033 degrees/min at t plus 9287.0652 s and -0.29324 degrees/min at t plus 10671.0953 s, respectively
 Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.47559 degrees/min at t plus 5101.5888 s and -0.50703 degrees/min at t plus 10671.0953 s, respectively
 The mean steam flow rate was 23.7392 +/- 0.56134 g/s
 The mean feedwater flow rate was 23.4865 +/- 0.8817 g/s
 The mean water injection to steam flow rate was 0.017675 +/- 0.029716 g/s
 Mean Smoothed Condensing Region SP8-SP9 delta T is 11.8119 +/- 4.2502 C over the Stratification Period, beginning at 2.2106 C and ending at 15.0497 C
 Mean Smoothed SP8-Upper Pool delta T is 11.2075 +/- 4.1344 C over the Stratification Period, beginning at 2.0026 C and ending at 14.2081 C
 The stratification period begins and ends with Smoothed SP8 readings of 57.686 and 118.4363 C, respectively
 The stratification period begins and ends with condensing flows of 0.21873 and 0.45742 kg/s, respectively.
 The stratification period begins and ends with condensing+cooling flows of 6.2292 and 0.84267 kg/s, respectively.
 The stratification period had a mean sparger steam enthalpy of 2720.0668 +/- 1.0376 kJ/kg. At plume detection, the condensing and condensing+cooling flows are 0.21792 and 6.852 kg/s, respectively
 The plume period had a mean steam enthalpy of 2720.1395 +/- 1.0015 kJ/kg.
 Maximum Smoothed Top-Mid delta T is 1.0545 degrees C at t plus 8131.5431 s with T_upper = 80.9894 C and T_mid = 79.9349 C
 At t plus 8131.5431 s, Smoothed SP8-SP9 is 12.8938 C and Smoothed SP8-Top is 11.8393 C, where Smoothed SP8 is 92.8286 C and Pool P = 28.0467 psia
 Maximum Smoothed Top-Lower delta T is 12.9009 degrees C at t plus 10102.8818 s with T_upper = 92.0631 C and T_low = 79.1622 C
 At t plus 10102.8818 s, Smoothed SP8-SP9 is 16.2686 C and Smoothed SP8-Top is 15.4549 C, where Smoothed SP8 is 107.518 C and Pool P = 32.3078 psia
 Maximum Smoothed Mid-Lower delta T is 12.0973 degrees C at t plus 10063.6826 s with T_mid = 91.1066 C and T_low = 79.0092 C
 At t plus 10063.6826 s, Smoothed SP8-SP9 is 15.5925 C and Smoothed SP8-Top is 15.0003 C, where Smoothed SP8 is 106.6991 C and Pool P = 32.2268 psia
 Maximum Smoothed Top-Outlet delta T is 30.2653 degrees C at t plus 12949.5336 s with T_upper = 103.2358 C and T_out = 72.9705 C
 At t plus 12949.5336 s, Smoothed SP8-SP9 is 15.2852 C and Smoothed SP8-Top is 14.4968 C, where Smoothed SP8 is 117.7326 C and Pool P = 38.565 psia
 Maximum Smoothed Mid-Outlet delta T is 29.5206 degrees C at t plus 12997.1364 s with T_mid = 102.6842 C and T_out = 73.1637 C
 At t plus 12997.1364 s, Smoothed SP8-SP9 is 15.1479 C and Smoothed SP8-Top is 14.4663 C, where Smoothed SP8 is 117.8321 C and Pool P = 38.6917 psia
 Maximum Smoothed Lower-Outlet delta T is 29.8239 degrees C at t plus 12898.1377 s with T_low = 102.6611 C and T_out = 72.8372 C
 At t plus 12898.1377 s, Smoothed SP8-SP9 is 15.0114 C and Smoothed SP8-Top is 14.3193 C, where Smoothed SP8 is 117.3048 C and Pool P = 38.43 psia
 Maximum Smoothed Condensing Region SP8-SP9 delta T is 18.1021 degrees C at (KEY POINT #14) t plus 10550.2944 s with T_SP8 = 111.0549 C and T_SP9 = 92.9529 C and Pool P = 33.2167 psia
 Maximum Smoothed Condensing Region SP8-Upper delta T is 17.5044 degrees C at t plus 10550.2944 s with T_SP8 = 111.0549 C and T_upper = 93.5506 C and Pool P = 33.2167 psia
 Maximum Top-Mid delta T is 1.6915 degrees C at (KEY POINT #4) t plus 6732.6231 s ignoring SP 4, with temperatures of 74.0878 and 72.3963 C, respectively, at Set # 2, where Pool P = 25.7782 psia and T_outlet = 66.8951 C

Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 8868.2572 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.9994 C and a raw SP12 Reading of 83.9331 C.
Maximum Top-Lower delta T is 14.4675 degrees C at t plus 10301.3862 s, with temperatures of 92.6994 and 78.2319 C, respectively, at Set # 1, where Pool P = 32.7151 psia and T_{outlet} = 71.6388 C
Maximum Mid-Low delta T is 13.2481 degrees C at (KEY POINT #6) t plus 10258.7397 s ignoring SP 4, with temperatures of 91.7788 and 78.5307 C, respectively, at Set # 2, where Pool P = 32.6305 psia and T_{outlet} = 71.6201 C
Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 10458.3922 s with a Smoothed Mid-Axis Mid-Low Delta T of 4.4123 C and a raw SP12 Reading of 92.4085 C.
Maximum Top-Outlet delta T is 30.6625 degrees C at t plus 12924.6352 s, with temperatures of 103.3544 and 72.6918 C, respectively, at Set # 1, where Pool P = 38.4974 psia
Maximum Mid-Outlet delta T is 29.5836 degrees C at t plus 12924.7342 s ignoring SP 4, with temperatures of 102.2785 and 72.6949 C, respectively, at Set # 2, where Pool P = 38.4975 psia
Maximum Lower-Outlet delta T is 30.6689 degrees C at (KEY POINT #8) t plus 12910.5334 s, with temperatures of 103.5366 and 72.8677 C, respectively, at Set # 1, where Pool P = 38.4705 psia
Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 14089.9559 s with a Smoothed Mid-Axis Low-Outlet Delta T of 10.2204 C and a raw SP12 Reading of 107.0718 C.
Minimum SP Pressure is 20.1853 psia at t plus 0.30001 s
Maximum SP Pressure is 49.2923 psia at t plus 16253.0976 s
Beginning SP Pressure is 20.1914 psia
Ending SP Pressure is 49.2886 psia
Time-Average SP Pressure is 30.2835 +/- 8.4019 psia
SP Levels are fully corrected and compensated
Pre-Start SP Level is 77.3645 cm (cold) / 77.5128 cm (hot) at 19.7982 psia
Beginning Smoothed SP Level is 77.3546 cm (cold) / 77.5321 cm (hot) at 20.1957 psia
Ending Smoothed SP Level is 77.8339 cm (cold) / 79.2667 cm (hot) at 49.2959 psia
Minimum Smoothed Cold SP Level is 77.2367 cm at t plus 5942.5379 s and 24.7324 psia
Minimum Smoothed Hot SP Level is 77.5311 cm at t plus 1.1981 s and 20.196 psia
Maximum Smoothed Cold SP Level is 78.6466 cm at t plus 13729.0512 s and 40.6809 psia
Maximum Smoothed Hot SP Level is 79.887 cm at t plus 14137.4596 s and 41.8904 psia
SP 12 Temperature at the beginning is 40.0468 C, and at the end is 116.5126 C
At plume detection, the Mixing Number is 44.594
The Mixing Number ranges from a minimum of 35.5649 at (KEY POINT #12) t plus 0 s to a maximum of 206.2654 at (KEY POINT #13) t plus 16253.7976 s; it had a mean value of 90.5371 +/- 48.283 over the test period.
Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_{tp}, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) kl, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_{mid} Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_{mid} Vapor Pressure p4, T_{Plume} Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11
KEY POINT #1 (t plus 0 s with a Mixing Number of 35.5649): 15.5362169 0.040894
0.00925 0.3937 0.773545542 0.775321363 1.00673936
1 1 19.1096756 49296.4793 0.0695306602 0.0569384095
0.0204058336 8.80188471e-006 0.0204058336 40.403655 117.254516
110.11962 40.7724006 40.5654084 40.7402484 38.2946725

4.17844559	4.23054189	2.12176312	0.629165348	0.681312728
0.681312728	4.30272383	1.5796147	0.0392891688	992.082199
950.858435	0.8299759	0.813353331	0.000647878423	0.000254390958
1.26160223e-005	1.2888102e-005	1532.07613	1534.28981	477.258257
482.282767	1.43952996	1.39244581	1.42944581	0.0754483068
0.0769398152	2706.63913	2706.27395	169.347854	461.869821
2691.24935	292.521967	2244.76931	170.888637	170.022227
170.755882	160.541145			
KEY POINT #2 (t plus 3062.4552 s with a Mixing Number of 44.594): 17.6611485				
0.040894	0.00925	0.3937	0.773118119	0.776409939
1.01082763	1	1	20.3620499	54966.5105
0.0670397749	0.0564491676	0.0231967963	2.30876977e-005	0.0231967963
55.3391484	124.009982	112.592921	57.3462098	55.6054959
55.7946696	53.0737003	4.18088158	4.23428868	2.13395531
0.646232504	0.681995004	0.681995004	3.24282184	1.54242295
0.0397413709	985.56333	948.957527	0.896491504	0.868219394
0.000501238037	0.000248430097	1.27010235e-005	1.31395463e-005	1550.6137
1531.2089	478.426406	486.383132	1.56318451	1.51059265
1.54759265	0.160193116	0.176205327	2719.46673	2719.05212
231.77722	472.34678	2694.98619	240.56956	2247.11995
240.169193	232.889354	233.683263	222.311847	
KEY POINT #3 (t plus 3089.9657 s with a Mixing Number of 44.731): 17.6993602				
0.040894	0.00925	0.3937	0.773122234	0.776436812
1.01051895	1	1	20.3666005	55135.3135
0.0670165095	0.056444374	0.0232469849	1.65191312e-005	0.0232469849
55.4753755	123.704287	112.617087	57.6859916	55.6834218
55.9112573	53.22141	4.18092627	4.23432599	2.13407726
0.646371899	0.682001314	0.682001314	3.23517605	1.54206851
0.0397458746	985.49714	948.938822	0.897162103	0.869656045
0.000500158757	0.000248373119	1.27018544e-005	1.31276597e-005	1550.72694
1531.17798	478.437711	486.17181	1.5644344	1.51203613
1.54903613	0.161239127	0.179046874	2718.81644	2718.40164
232.346895	472.449199	2695.02251	240.102305	2246.36724
241.590163	233.215284	234.170844	222.929426	
KEY POINT #4 (t plus 6732.6231 s with a Mixing Number of 62.667): 18.0632776				
0.040894	0.00925	0.3937	0.772841749	0.77849456
1.00792273	1	1	17.8264043	56032.101
0.0640150299	0.0554931262	0.0237249673	1.80473687e-005	0.0237249673
72.6026116	125.577408	117.387846	84.2000122	73.1515219
72.951167	66.9041623	4.18965035	4.24195978	2.15925609
0.661704639	0.683113271	0.683113271	2.46893949	1.47530422
0.0406683211	976.310811	945.196436	1.03774437	1.01405858
0.000389939154	0.000237578841	1.28660375e-005	1.31831515e-005	1557.98272
1524.76688	480.62747	486.424488	1.82776788	1.77793401
1.81493401	0.348840784	0.560760955	2719.93873	2719.62095
304.042587	492.686976	2702.11623	188.644388	2227.25175
352.683596	306.341056	305.504415	280.183868	
KEY POINT #5 (t plus 8868.2572 s with a Mixing Number of 83.1324): 18.2265247				
0.040894	0.00925	0.3937	0.779113634	0.786778312
1.00567192	1	1	15.8171761	56330.683
0.0618522359	0.0546686425	0.0239393821	1.89491579e-005	0.0239393821
84.4515185	127.241835	121.483962	98.3758947	85.1441977
78.0630957	71.2041901	4.1992538	4.24895123	2.18268469
0.669892993	0.68385772	0.68385772	2.10359929	1.42272896
0.0415153503	969.026433	941.904855	1.17219432	1.15323694
0.000335580198	0.000228984549	1.30071892e-005	1.32317853e-005	1555.79739
1518.78797	482.43965	486.580137	2.08182749	2.03482506
2.07182506	0.56634203	0.956793281	2720.79868	2720.54849
353.759913	510.094597	2708.08169	156.334684	2210.70408
412.332369	356.667542	326.952984	298.210432	
KEY POINT #6 (t plus 10258.7397 s with a Mixing Number of 101.5478): 18.4068117				
0.040894	0.00925	0.3937	0.78491513	0.794050909
1.00333299	1	1	14.4770728	56825.7555
0.060451645	0.0540311824	0.0241761776	2.00072339e-005	0.0241761776
91.9327585	127.956862	124.627208	108.807427	92.5452571
81.2441369	71.6275595	4.20681493	4.25459962	2.20184076
0.674103782	0.684299018	0.684299018	1.91978327	1.38509416

0.0422015034	964.068608	939.33019	1.28462056	1.27249789
0.000307627785	0.000222775034	1.31155931e-005	1.32462499e-005	1551.79183
1513.91147	483.786726	486.222718	2.29572811	2.24991264
2.28691264	0.754942464	1.37726484	2720.08301	2719.87342
385.219824	523.47377	2712.57717	138.253945	2196.60924
456.381701	387.795394	340.314499	300.001342	
KEY POINT #7 (t plus 10458.3922 s with a Mixing Number of 103.1962):				18.4547648
0.040894	0.00925	0.3937	0.785215657	0.794520335
1.00390168	1	1	14.3720279	56820.3784
0.0603225561	0.0539519417	0.0242391609	1.40079163e-005	0.0242391609
92.6152321	128.912195	125.016529	108.557704	93.1373029
87.7114832	71.6298906	4.2075616	4.25531675	2.204286
0.67445236	0.684345887	0.684345887	1.9044923	1.38058727
0.0422887386	963.60331	939.008354	1.29913031	1.28481729
0.00030528117	0.000222027941	1.31290242e-005	1.32820156e-005	1551.33362
1513.29035	483.950908	486.796373	2.32342317	2.27763689
2.31463689	0.774480885	1.36567007	2721.87227	2721.66572
388.09325	525.132225	2713.12886	137.038975	2196.74005
455.327848	390.288744	367.474757	300.013364	
KEY POINT #8 (t plus 12910.5334 s with a Mixing Number of 135.8328):				18.3937277
0.040894	0.00925	0.3937	0.78587739	0.797201171
1.00065312	1	1	12.3393039	56454.32
0.0584675691	0.0529457052	0.0241589926	1.11574052e-005	0.0241589926
102.299051	130.56458	129.934062	117.343098	103.048675
102.670969	72.8630667	4.21923713	4.26471654	2.2365733
0.678764507	0.684791367	0.684791367	1.71014295	1.32641496
0.0434345384	956.76531	934.887615	1.49405187	1.49135014
0.000275117113	0.000212984264	1.32987356e-005	1.33239246e-005	1543.22748
1505.12618	485.973478	486.448438	2.69727054	2.65207695
2.68907695	1.10026235	1.8251395	2721.56908	2721.41683
428.921742	546.106264	2719.99702	117.184521	2175.46282
492.558259	432.083691	430.492383	305.209873	
KEY POINT #9 (t plus 13171.8404 s with a Mixing Number of 140.4129):				18.378512
0.040894	0.00925	0.3937	0.786234044	0.797803544
0.999808366	0.999808366	0.999999689	12.1099615	56429.6636
0.0582565672	0.0528269771	0.0241390076	1.66145248e-005	0.0241390076
103.386567	130.511149	130.511149	118.436298	104.22818
103.292591	74.0833013	4.22067478	4.26586198	2.24053423
0.67917628	0.68482595	0.68482595	1.69070022	1.32037827
0.0435744419	955.970619	934.397286	1.51838988	1.51868044
0.000272061588	0.00021196872	1.33186578e-005	1.33187196e-005	1542.13808
1504.12984	486.204559	486.201029	2.74416924	2.69904811
2.73604811	1.14303696	1.89024234	2720.52096	2720.3743
433.514501	548.570878	2720.79058	115.056376	2171.95008
497.199572	437.065892	433.119204	310.326525	
KEY POINT #10 (t plus 14089.9559 s with a Mixing Number of 156.9678):				18.3808507
0.040894	0.00925	0.3937	0.786346974	0.798851486
0.998193548	0.998193548	0.999996873	11.398155	56123.3808
0.0575094243	0.0523857964	0.0241420794	2.51625127e-005	0.0241420794
107.215564	132.649887	132.649887	121.168013	107.815474
107.358053	96.7357501	4.22594317	4.27018667	2.25553189
0.68051207	0.68492195	0.68492195	1.62561317	1.29856138
0.0441031388	953.13066	932.567739	1.61138597	1.61429708
0.000261775736	0.000208284382	1.33924987e-005	1.33931081e-005	1538.02886
1500.36836	487.049369	487.015017	2.92378344	2.87878023
2.91578023	1.30472146	2.06125872	2719.9253	2719.79538
449.698693	557.711108	2723.70815	108.012414	2162.21419
508.810584	452.23289	450.30218	405.490639	
KEY POINT #11 (t plus 16253.7976 s with a Mixing Number of 206.2654):				18.9328689
0.040894	0.00925	0.3937	0.778339103	0.79266675
0.995718401	0.995718401	0.999991291	10.0417966	56975.9509
0.0556325613	0.0512135006	0.0248671203	1.92110075e-005	0.0248671203
116.691601	138.290861	138.290861	128.603318	117.591941
117.095469	112.761731	4.2404128	4.2822131	2.29750815
0.683066177	0.684934065	0.684934065	1.48458437	1.24497819
0.0455765122	945.824058	927.649044	1.87880066	1.88686309
0.000239144021	0.000199132541	1.35872884e-005	1.35889042e-005	1526.09707

1489.93466	489.189216	489.100957	3.44358836	3.39883349
3.43583349	1.78722174	2.59159975	2722.11948	2722.01865
489.84828	581.866956	2731.22132	92.0186762	2140.25253
540.483006	493.665548	491.562255	473.201117	
KEY POINT #12 (t plus 0 s with a Mixing Number of 35.5649): 15.5362169 0.040894				
0.00925	0.3937	0.773545542	0.775321363	1.00673936
1	1	19.1096756	49296.4793	0.0695306602 0.0569384095
0.0204058336	8.80188471e-006	0.0204058336	40.403655	117.254516
110.11962	40.7724006	40.5654084	40.7402484	38.2946725
4.17844559	4.23054189	2.12176312	0.629165348	0.681312728
0.681312728	4.30272383	1.5796147	0.0392891688	992.082199
950.858435	0.8299759	0.813353331	0.000647878423	0.000254390958
1.26160223e-005	1.2888102e-005	1532.07613	1534.28981	477.258257
482.282767	1.43952996	1.39244581	1.42944581	0.0754483068
0.0769398152	2706.63913	2706.27395	169.347854	461.869821
2691.24935	292.521967	2244.76931	170.888637	170.022227
170.755882	160.541145			
KEY POINT #13 (t plus 16253.7976 s with a Mixing Number of 206.2654): 18.9328689				
0.040894	0.00925	0.3937	0.778339103	0.79266675
0.995718401	0.995718401	0.999991291	10.0417966	56975.9509
0.0556325613	0.0512135006	0.0248671203	1.92110075e-005	0.0248671203
116.691601	138.290861	138.290861	128.603318	117.591941
117.095469	112.761731	4.2404128	4.2822131	2.29750815
0.683066177	0.684934065	0.684934065	1.48458437	1.24497819
0.0455765122	945.824058	927.649044	1.87880066	1.88686309
0.000239144021	0.000199132541	1.35872884e-005	1.35889042e-005	1526.09707
1489.93466	489.189216	489.100957	3.44358836	3.39883349
3.43583349	1.78722174	2.59159975	2722.11948	2722.01865
489.84828	581.866956	2731.22132	92.0186762	2140.25253
540.483006	493.665548	491.562255	473.201117	
KEY POINT #14 (t plus 10550.2944 s with a Mixing Number of 104.2972): 18.4105783				
0.040894	0.00925	0.3937	0.785292561	0.794692623
1.00328923	1	1	14.2435787	56762.1132
0.0602586153	0.0539165035	0.0241811247	1.8178264e-005	0.0241811247
92.9528502	128.468738	125.190543	111.054946	93.5505635
89.4839913	71.6738573	4.20793489	4.25563855	2.20538417
0.674622537	0.684366282	0.684366282	1.89701226	1.37858354
0.0423278922	963.372255	938.864295	1.30565825	1.29352453
0.000304131898	0.000221695542	1.31350277e-005	1.32638153e-005	1551.10106
1513.01152	484.024101	486.426387	2.33588959	2.29015998
2.32715998	0.784300971	1.48531018	2720.77315	2720.57027
389.514823	525.873595	2713.37507	136.358772	2194.89955
465.891762	392.028861	374.92606	300.198555	

End

D.23 TEST #23 -

T23_RCIC_020GPM_5PSIG_57KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T23_RCIC_020GPM_5PSIG_57kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 2193.2825 s, and ending (KEY POINT #11) at t
plus 18315.3556 s, for a time period of 16122.0731 s.
Original Data Record Time: 20155.7398 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus
2371.0316 s, T_bulk = 51.6511 C and T_out = 49.4885 C
Stratification Beginning SP12 Temperature = 51.4379 C
Stratification Beginning Pressure = 21.5501 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus
13104.5215 s, T_bulk = 102.7497 C and T_out = 70.8931 C
Stratification Ending SP12 Temperature = 102.6447 C
Stratification Ending Pressure = 38.8963 psia
Plume detected! Setting t_plume (KEY POINT #2) to 1871.525 s.

At t = 1871.525 s, the pool pressure is 21.2267 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 49.7758, 49.5888, 51.59, 49.8948, and 47.4724 C, respectively.

Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 12.087 +/- 4.246 C.

Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 11.4914 +/- 4.1702 C.

Minimum Steam Quality: 0.54962 at t plus 1669.0205 s
Maximum Steam Quality: 0.6619 at t plus 15438.4621 s
Time-Averaged Steam Quality: 0.60989 +/- 0.014907
Minimum Turbine Outlet Steam Quality: 0.56166 at t plus 1669.2245 s
Maximum Turbine Outlet Steam Quality: 0.66577 at t plus 15438.4621 s
Time-Averaged Turbine Outlet Steam Quality: 0.61822 +/- 0.013391

Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 16032.073 s; using 300 s smoothing

Max and min smoothed upper level changerates: 0.43635 degrees/min at t plus 6218.6017 s and 0.1574 degrees/min at t plus 12511.9107 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.41786 degrees/min at t plus 7380.2201 s and 0.21319 degrees/min at t plus 10301.5732 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.1456 degrees/min at t plus 6106.5993 s and -0.13983 degrees/min at t plus 5732.4919 s, respectively
Max and min smoothed lower level changerates: 1.8459 degrees/min at t plus 10064.7767 s and -0.048452 degrees/min at t plus 6238.9168 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.35597 degrees/min at t plus 6218.6017 s and -1.6097 degrees/min at t plus 10123.071 s, respectively
Max and min smoothed outlet level changerates: 2.5215 degrees/min at t plus 13883.235 s and -0.041776 degrees/min at t plus 7842.2296 s, respectively
Max and min smoothed lower-outlet level changerate differences: 1.844 degrees/min at t plus 10122.983 s and -2.3407 degrees/min at t plus 13883.3361 s, respectively
Max and min smoothed hot (SP8) level changerates: 0.83671 degrees/min at t plus 3905.9584 s and -0.16118 degrees/min at t plus 11941.3181 s, respectively
Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.56439 degrees/min at t plus 3905.9584 s and -0.39221 degrees/min at t plus 11941.3181 s, respectively

The mean steam flow rate was 23.2608 +/- 0.52474 g/s
The mean feedwater flow rate was 22.9218 +/- 1.2274 g/s
The mean water injection to steam flow rate was 12.4637 +/- 0.42445 g/s
Mean Smoothed Condensing Region SP8-SP9 delta T is 12.5343 +/- 3.7904 C over the Stratification Period, beginning at 3.2487 C and ending at 14.7817 C
Mean Smoothed SP8-Upper Pool delta T is 11.9227 +/- 3.7434 C over the Stratification Period, beginning at 3.0067 C and ending at 14.1501 C
The stratification period begins and ends with Smoothed SP8 readings of 55.2347 and 117.5495 C, respectively
The stratification period begins and ends with condensing flows of 0.18985 and 0.41195 kg/s, respectively.
The stratification period begins and ends with condensing+cooling flows of 4.1263 and 0.79736 kg/s, respectively.
The stratification period had a mean sparger steam enthalpy of 1868.491 +/- 22.527 kJ/kg.
At plume detection, the condensing and condensing+cooling flows are 0.18285 and 6.7411 kg/s, respectively
The plume period had a mean steam enthalpy of 1866.0177 +/- 25.0028 kJ/kg.
Maximum Smoothed Top-Mid delta T is 1.2445 degrees C at t plus 7231.6206 s with T_upper = 76.5145 C and T_mid = 75.27 C
At t plus 7231.6206 s, Smoothed SP8-SP9 is 12.9052 C and Smoothed SP8-Top is 11.6607 C, where Smoothed SP8 is 88.1752 C and Pool P = 26.7746 psia
Maximum Smoothed Top-Lower delta T is 13.901 degrees C at t plus 9722.6611 s with T_upper = 90.0903 C and T_low = 76.1893 C
At t plus 9722.6611 s, Smoothed SP8-SP9 is 16.1154 C and Smoothed SP8-Top is 15.6275 C, where Smoothed SP8 is 105.7178 C and Pool P = 31.6763 psia
Maximum Smoothed Mid-Lower delta T is 13.4151 degrees C at t plus 9723.4621 s with T_mid = 89.6059 C and T_low = 76.1908 C
At t plus 9723.4621 s, Smoothed SP8-SP9 is 16.1626 C and Smoothed SP8-Top is 15.6772 C, where Smoothed SP8 is 105.7685 C and Pool P = 31.6772 psia
Maximum Smoothed Top-Outlet delta T is 32.7578 degrees C at t plus 12986.4187 s with T_upper = 103.0909 C and T_out = 70.3331 C
At t plus 12986.4187 s, Smoothed SP8-SP9 is 14.8252 C and Smoothed SP8-Top is 14.0135 C, where Smoothed SP8 is 117.1044 C and Pool P = 38.5985 psia

Maximum Smoothed Mid-Outlet delta T is 31.9519 degrees C at t plus 12989.422 s with T_mid = 102.2956 C and T_out = 70.3437 C
 At t plus 12989.422 s, Smoothed SP8-SP9 is 14.8039 C and Smoothed SP8-Top is 14.0135 C, where Smoothed SP8 is 117.0995 C and Pool P = 38.6139 psia
 Maximum Smoothed Lower-Outlet delta T is 32.0958 degrees C at t plus 13080.8431 s with T_low = 102.8859 C and T_out = 70.7902 C
 At t plus 13080.8431 s, Smoothed SP8-SP9 is 14.9258 C and Smoothed SP8-Top is 14.2353 C, where Smoothed SP8 is 117.5729 C and Pool P = 38.8444 psia
 Maximum Smoothed Condensing Region SP8-SP9 delta T is 17.1342 degrees C at (KEY POINT #14) t plus 10412.3736 s with T_SP8 = 109.337 C and T_SP9 = 92.2028 C and Pool P = 33.0453 psia
 Maximum Smoothed Condensing Region SP8-Upper delta T is 16.6294 degrees C at t plus 10412.3736 s with T_SP8 = 109.337 C and T_upper = 92.7076 C and Pool P = 33.0453 psia
 Maximum Top-Mid delta T is 1.7768 degrees C at (KEY POINT #4) t plus 6703.2074 s ignoring SP 4, with temperatures of 73.8722 and 72.0954 C, respectively, at Set # 2, where Pool P = 25.9467 psia and T_outlet = 66.2571 C
 Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 8262.9376 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.99937 C and a raw SP12 Reading of 81.2771 C.
 Maximum Top-Lower delta T is 15.7337 degrees C at t plus 9958.4655 s, with temperatures of 91.2724 and 75.5386 C, respectively, at Set # 1, where Pool P = 32.1355 psia and T_outlet = 68.0813 C
 Maximum Mid-Low delta T is 14.4379 degrees C at (KEY POINT #6) t plus 9889.5637 s ignoring SP 4, with temperatures of 90.1271 and 75.6893 C, respectively, at Set # 2, where Pool P = 32.0156 psia and T_outlet = 68.0212 C
 Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 10134.2677 s with a Smoothed Mid-Axis Mid-Low Delta T of 4.8114 C and a raw SP12 Reading of 91.0473 C.
 Maximum Top-Outlet delta T is 33.0979 degrees C at t plus 13052.2216 s, with temperatures of 103.6805 and 70.5826 C, respectively, at Set # 1, where Pool P = 38.7598 psia
 Maximum Mid-Outlet delta T is 31.9227 degrees C at t plus 12992.4212 s ignoring SP 4, with temperatures of 102.1219 and 70.1992 C, respectively, at Set # 2, where Pool P = 38.6142 psia
 Maximum Lower-Outlet delta T is 32.906 degrees C at (KEY POINT #8) t plus 13093.5229 s, with temperatures of 103.8949 and 70.9889 C, respectively, at Set # 1, where Pool P = 38.8707 psia
 Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 14154.1406 s with a Smoothed Mid-Axis Low-Outlet Delta T of 10.9677 C and a raw SP12 Reading of 106.7449 C.
 Minimum SP Pressure is 20.3078 psia at t plus 3.4932 s
 Maximum SP Pressure is 48.1581 psia at t plus 16121.9701 s
 Beginning SP Pressure is 20.3167 psia
 Ending SP Pressure is 48.1577 psia
 Time-Average SP Pressure is 30.1934 +/- 8.0838 psia
 SP Levels are fully corrected and compensated
 Pre-Start SP Level is 76.5669 cm (cold) / 76.7094 cm (hot) at 14.6231 psia
 Beginning Smoothed SP Level is 77.01 cm (cold) / 77.184 cm (hot) at 20.3101 psia
 Ending Smoothed SP Level is 77.6691 cm (cold) / 79.0604 cm (hot) at 48.1646 psia
 Minimum Smoothed Cold SP Level is 76.9818 cm at t plus 4118.7736 s and 22.9369 psia
 Minimum Smoothed Hot SP Level is 77.1784 cm at t plus 151.6947 s and 20.3688 psia
 Maximum Smoothed Cold SP Level is 78.5494 cm at t plus 13221.9253 s and 39.1895 psia
 Maximum Smoothed Hot SP Level is 79.7381 cm at t plus 13896.6348 s and 40.9547 psia
 SP 12 Temperature at the beginning is 39.9661 C, and at the end is 115.0955 C
 At plume detection, the Mixing Number is 41.8031
 The Mixing Number ranges from a minimum of 36.3202 at (KEY POINT #12) t plus 0 s to a maximum of 202.1715 at (KEY POINT #13) t plus 16122.0061 s; it had a mean value of 91.9771 +/- 47.5729 over the test period.
 Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction v1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1,

Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m3) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 36.3202): 26.308562 0.040894
0.00925 0.3937 0.770100391 0.771839768 0.58851607
0.58851607 0.999385637 18.5347816 84236.325 0.0695141745
0.0568939649 0.0218860127 0.0126686117 0.0345546245 40.5049298
110.344865 110.344865 41.0017771 40.5985197 40.6665476
38.4391222 4.17844323 4.23087729 2.12285 0.629293784
0.681377859 0.681377859 4.29372813 1.57615103 0.0393296436
992.043687 950.686426 0.835862537 1.41941581 0.000646656247
0.000253837287 1.26237597e-005 1.27719524e-005 1532.24675 1534.01618
477.36555 468.10107 1.45044723 1.40033402 1.43733402
0.0758554371 0.0778803816 1774.83272 1774.48918 169.771723
462.82356 2691.59128 293.051837 1312.00916 171.847771
170.161278 170.448626 161.145428

KEY POINT #2 (t plus 1871.525 s with a Mixing Number of 41.8031): 27.141099
0.040894 0.00925 0.3937 0.770078465 0.772679246
0.597373881 0.597373881 0.999382283 18.6278943 86603.5629
0.0680129069 0.0566339696 0.0226153118 0.0130327971 0.0356481089
49.5888288 111.660266 111.660266 51.5900366 49.7757825
49.8948196 47.4724465 4.1793573 4.23285925 2.12929079
0.640086043 0.681746212 0.681746212 3.59482886 1.55623251
0.0395688304 988.250247 949.677481 0.870919971 1.4570138
0.000550563069 0.000250647508 1.26689602e-005 1.28159635e-005 1544.95242
1532.39033 477.988497 468.861943 1.51557058 1.46383853
1.50083853 0.121014493 0.13359421 1798.01035 1797.66335
207.736547 468.394878 2693.58167 260.658331 1329.61547
216.100744 208.51643 209.016954 198.897327

KEY POINT #3 (t plus 2371.0316 s with a Mixing Number of 43.4983): 26.7220172
0.040894 0.00925 0.3937 0.770151872 0.773014512
0.610444997 0.610444997 0.999407085 18.4935624 85211.864
0.0676093521 0.0565492324 0.0226362192 0.0124614523 0.0350976715
51.9860382 112.088153 112.088153 55.2347363 52.2280338
52.1420255 49.610811 4.17990506 4.23351255 2.13142065
0.642711479 0.681861626 0.681861626 3.44081378 1.54986509
0.039647683 987.15596 949.347649 0.882577345 1.44493616
0.000529067164 0.000249625699 1.26836688e-005 1.28241552e-005 1547.52598
1531.85124 478.189794 469.48049 1.53726501 1.48574045
1.52274045 0.136211917 0.159395324 1828.19104 1827.84903
217.757853 470.207774 2694.22674 252.449921 1357.98326
231.338574 218.767921 218.411412 207.835749

KEY POINT #4 (t plus 6703.2074 s with a Mixing Number of 64.6401): 27.1378071
0.040894 0.00925 0.3937 0.770505684 0.776107994
0.627708353 0.627708353 0.999345678 16.3383899 85243.0875
0.0640351105 0.0554575656 0.0233722763 0.0122715088 0.0356437851
72.4907882 117.565247 117.565247 85.2877958 73.4560268
70.2326117 66.2139635 4.18957071 4.2422541 2.16023553
0.661618894 0.683149515 0.683149515 2.4729103 1.47293984
0.0407039306 976.376644 945.055376 1.04329629 1.66098417
0.000390523109 0.000237194217 1.28721475e-005 1.30189264e-005 1557.97953
1524.5169 480.707268 471.88052 1.83821828 1.78881647
1.82581647 0.347185968 0.585234945 1880.27527 1880.00833
303.574975 493.440269 2702.37703 189.865294 1386.835
357.252692 307.617857 294.117374 277.29571

KEY POINT #5 (t plus 8262.9376 s with a Mixing Number of 80.1941): 27.2012958
0.040894 0.00925 0.3937 0.775465444 0.782526682
0.630125646 0.630125646 0.999290566 15.044343 84723.8867

0.0623645951	0.0548587126	0.0235810452	0.0121461284	0.0357271736
81.6783177	120.542789	120.542789	95.5214502	82.3982641
74.5341802	67.5277581	4.19674462	4.24730826	2.17714953
0.668146483	0.683703703	0.683703703	2.18011548	1.43444459
0.0413160808	970.795364	942.667549	1.14012307	1.80807469
0.000347087236	0.000230907441	1.29747438e-005	1.31293527e-005	1556.78481
1520.19977	482.028902	472.888835	2.02104446	1.97333119
2.01033119	0.507302689	0.862458255	1892.99149	1892.76516
342.113199	506.092119	2706.72155	163.978919	1386.89938
400.302951	345.133517	312.153739	282.810456	
KEY POINT #6 (t plus 9889.5637 s with a Mixing Number of 100.4121): 27.2093551				
0.040894	0.00925	0.3937	0.783588296	0.792348312
0.626777498	0.626777498	0.999200842	13.5208762	83893.5631
0.0607716186	0.0541541911	0.0235987737	0.0121389852	0.0357377589
90.2360814	124.022239	124.022239	106.504567	90.6450922
78.2107943	67.978147	4.20499559	4.25349299	2.198073
0.673212741	0.684222791	0.684222791	1.95880867	1.39216377
0.0420669403	965.216971	939.829009	1.26233323	2.01239584
0.000313601983	0.000223945399	1.3094724e-005	1.32632269e-005	1552.86903
1514.86919	483.530431	473.771435	2.25322636	2.20691149
2.24391149	0.708139875	1.27335335	1894.23699	1894.05417
378.080452	520.897263	2711.71763	142.816811	1373.33972
446.644984	379.799117	327.586157	284.715205	
KEY POINT #7 (t plus 10134.2677 s with a Mixing Number of 102.99): 27.289104				
0.040894	0.00925	0.3937	0.784186906	0.793161704
0.623505332	0.623505332	0.999178087	13.3061976	84010.3377
0.0605955329	0.0540578086	0.023569421	0.012273083	0.035842504
91.1706759	124.496321	124.496321	107.98639	91.7109154
84.8440833	68.160269	4.20598806	4.2543594	2.2010223
0.67370866	0.684282877	0.684282877	1.93713008	1.38661683
0.042172288	964.586563	939.438244	1.27977193	2.05085666
0.000310286498	0.000223027269	1.31110778e-005	1.32836107e-005	1552.28944
1514.11945	483.731396	473.769478	2.2864778	2.24024666
2.27724666	0.733611649	1.33944558	1888.24277	1888.06571
382.013455	522.916272	2712.39144	140.902818	1365.32649
452.909822	384.284545	355.426008	285.48042	
KEY POINT #8 (t plus 13093.5229 s with a Mixing Number of 142.4475): 27.3611726				
0.040894	0.00925	0.3937	0.785443237	0.796820066
0.613151408	0.613151408	0.998982543	11.1310965	82800.4767
0.0583881361	0.0528740159	0.0234650109	0.0124721507	0.0359371616
102.708777	130.282591	130.282591	117.7352	103.377356
102.878931	70.8944166	4.21977327	4.26540724	2.23896113
0.678921934	0.684812695	0.684812695	1.70276555	1.32276138
0.0435188936	956.467041	934.591652	1.50871285	2.45808422
0.000273959004	0.000212369824	1.33107674e-005	1.35133013e-005	1542.82335
1504.52539	486.113197	474.819662	2.72551634	2.68021009
2.71721009	1.11621977	1.84827575	1880.02419	1879.90029
430.65268	547.594674	2720.4766	116.941994	1332.42952
494.223547	433.472963	431.372049	296.965585	
KEY POINT #9 (t plus 13104.5215 s with a Mixing Number of 142.6853): 27.3421464				
0.040894	0.00925	0.3937	0.785439459	0.796825277
0.614035668	0.614035668	0.998985703	11.1327212	82742.4841
0.0583766752	0.0528696315	0.0234768931	0.0124352787	0.0359121718
102.767861	130.303899	130.303899	117.549536	103.39944
102.806357	70.9907438	4.21985142	4.26544957	2.23910754
0.678944335	0.684813956	0.684813956	1.70170703	1.32253878
0.0435240645	956.423855	934.573542	1.5096129	2.45601645
0.00027379266	0.000212332369	1.3311503e-005	1.35133692e-005	1542.76418
1504.48857	486.121723	474.865838	2.72725092	2.68195375
2.71895375	1.11853658	1.83729082	1881.99873	1881.87479
430.902133	547.685677	2720.50589	116.783543	1334.31305
493.436056	433.566304	431.065921	297.369177	
KEY POINT #10 (t plus 14154.1406 s with a Mixing Number of 160.884): 27.4499979				
0.040894	0.00925	0.3937	0.78488748	0.797235013
0.616147102	0.616147102	0.99892701	10.5293299	82544.9048
0.0575678844	0.0524014205	0.0234012083	0.0126526197	0.036053828
106.917171	132.574296	132.574296	120.85804	107.676545

107.174391	95.6703989	4.22551902	4.27003166	2.25499325
0.680414777	0.684919418	0.684919418	1.63050374	1.29931783
0.0440841766	953.354715	932.632734	1.60802293	2.60700331
0.000262552087	0.000208412509	1.33898887e-005	1.3599146e-005	1538.36591
1500.50315	487.019823	475.504102	2.91727693	2.87207067
2.90907067	1.29148018	2.04124047	1892.20756	1892.0967
448.437275	557.38789	2723.60567	108.950616	1334.81967
507.493378	451.645187	449.525533	401.003367	
KEY POINT #11 (t plus 16122.0731 s with a Mixing Number of 202.1714):	28.0703691			
0.040894	0.00925	0.3937	0.776690973	0.790604041
0.645069705	0.645069705	0.998911171	9.85643487	83403.9352
0.0559186614	0.0513793987	0.0245396181	0.012329028	0.0368686461
115.25975	137.496193	137.496193	128.050623	116.103226
115.674719	112.926921	4.23809011	4.28046307	2.29138166
0.682748419	0.684953376	0.684953376	1.50423324	1.25219582
0.0453618952	946.953678	928.350143	1.83911143	2.84792315
0.000242329171	0.000200374526	1.35598464e-005	1.37632555e-005	1528.05743
1491.44892	488.895569	477.989244	3.36615251	3.32083419
3.35783419	1.70614942	2.548712	1966.56593	1966.46878
483.772767	578.459653	2730.17926	94.6868854	1388.10628
538.122469	487.346849	485.532864	473.894945	
KEY POINT #12 (t plus 0 s with a Mixing Number of 36.3202):	26.308562			0.040894
0.00925	0.3937	0.770100391	0.771839768	0.58851607
0.58851607	0.999385637	18.5347816	84236.325	0.0695141745
0.0568939649	0.0218860127	0.0126686117	0.0345546245	40.5049298
110.344865	110.344865	41.0017771	40.5985197	40.6665476
38.4391222	4.17844323	4.23087729	2.12285	0.629293784
0.681377859	0.681377859	4.29372813	1.57615103	0.0393296436
992.043687	950.686426	0.835862537	1.41941581	0.000646656247
0.000253837287	1.26237597e-005	1.27719524e-005	1532.24675	1534.01618
477.36555	468.10107	1.45044723	1.40033402	1.43733402
0.0758554371	0.0778803816	1774.83272	1774.48918	169.771723
462.82356	2691.59128	293.051837	1312.00916	171.847771
170.161278	170.448626	161.145428		
KEY POINT #13 (t plus 16122.0061 s with a Mixing Number of 202.1715):	28.0701445			
0.040894	0.00925	0.3937	0.776691788	0.79060484
0.645050733	0.645050733	0.998911086	9.85610597	83403.2001
0.0559187195	0.0513794294	0.0245387461	0.012329605	0.0368683511
115.259459	137.496047	137.496047	128.052906	116.102927
115.673957	112.927195	4.23808965	4.28046274	2.29138053
0.682748352	0.684953379	0.684953379	1.50423729	1.25219717
0.0453618557	946.953907	928.350272	1.83910415	2.8479954
0.000242329828	0.000200374757	1.35598413e-005	1.37632667e-005	1528.05783
1491.44919	488.895515	477.988328	3.36613832	3.32081751
3.35781751	1.70613324	2.54888797	1966.52475	1966.42761
483.771531	578.459023	2730.17906	94.6874913	1388.06573
538.132196	487.345582	485.529631	473.896105	
KEY POINT #14 (t plus 10412.3736 s with a Mixing Number of 105.859):	27.2675288			
0.040894	0.00925	0.3937	0.784663069	0.793880175
0.623803718	0.623803718	0.999166092	13.1001514	83818.0369
0.060400598	0.0539498751	0.0235749046	0.0122392618	0.0358141664
92.2027747	125.026679	125.026679	109.337009	92.7075816
90.0583152	68.1777648	4.20710531	4.2553355	2.20434997
0.674243343	0.684347086	0.684347086	1.91370471	1.38047022
0.0422910195	963.885587	938.999955	1.29951033	2.08146669
0.000306696069	0.000222008528	1.31293744e-005	1.33035605e-005	1551.61576
1513.27411	483.955181	473.928617	2.3241488	2.27803068
2.31503068	0.762623062	1.40212185	1890.2095	1890.03789
386.357935	525.175464	2713.14322	138.81753	1365.03404
458.623242	388.480546	377.339857	285.556774	

End

D.24 TEST #24 -

T24_RCIC_15PSIG_VENT86C_107KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T24_RCIC_15PSIG_VENT86C_107kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 3038.2918 s, and ending (KEY POINT #11) at t
plus 11246.9323 s, for a time period of 8208.6405 s.
Original Data Record Time: 12983.6576 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus
540.1059 s, T_bulk = 45.2374 C and T_out = 41.1117 C
Stratification Beginning SP12 Temperature = 44.8367 C
Stratification Beginning Pressure = 31.0244 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus
6115.5028 s, T_bulk = 96.2799 C and T_out = 61.2771 C
Stratification Ending SP12 Temperature = 95.9282 C
Stratification Ending Pressure = 20.8446 psia
Plume detected! Setting t_plume (KEY POINT #2) to 530.2053 s.
At t = 530.2053 s, the pool pressure is 31.0141 psia while the Smoothed Upper, Mid, SP8,
Lower, and Outlet Temperatures are 45.9483, 46.0653, 48.0662, 45.8911, and
40.9845 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9
temperatures were 11.4238 +/- 4.6645 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper
temperatures were 9.8795 +/- 3.7847 C.
Minimum Steam Quality: 0.99474 at t plus 120.5009 s
Maximum Steam Quality: 1.0027 at t plus 4592.0817 s
Time-Averaged Steam Quality: 0.99919 +/- 0.0012281
Minimum Turbine Outlet Steam Quality: 1.0021 at t plus 4413.6845 s
Maximum Turbine Outlet Steam Quality: 1.0252 at t plus 4845.4821 s
Time-Averaged Turbine Outlet Steam Quality: 1.0111 +/- 0.0054923
Smoothed Changerates may not fully include test beginning and end periods, analysis
ending at t plus 8118.6343 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.86495 degrees/min at t plus 2631.9425 s
and 0.2698 degrees/min at t plus 5749.4029 s, respectively
Max and min smoothed mid (SP9) level changerates: 1.0301 degrees/min at t plus 4668.48 s
and 0.31509 degrees/min at t plus 5424.6943 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.38676 degrees/min at t
plus 2735.3424 s and -0.63035 degrees/min at t plus 4697.9357 s, respectively
Max and min smoothed lower level changerates: 2.643 degrees/min at t plus 5064.7837 s
and -0.11384 degrees/min at t plus 1988.6327 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.74034 degrees/min at t
plus 4702.377 s and -2.1252 degrees/min at t plus 5064.7837 s, respectively
Max and min smoothed outlet level changerates: 5.9618 degrees/min at t plus 6372.4075 s
and -0.027165 degrees/min at t plus 2850.047 s, respectively
Max and min smoothed lower-outlet level changerate differences: 2.5547 degrees/min at t
plus 5076.3834 s and -5.3039 degrees/min at t plus 6378.8049 s, respectively
Max and min smoothed hot (SP8) level changerates: 1.4102 degrees/min at t plus 1680.3261
s and -1.7822 degrees/min at t plus 4564.1741 s, respectively
Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.91742 degrees/min
at t plus 1680.3261 s and -2.5409 degrees/min at t plus 4564.2731 s, respectively
The mean steam flow rate was 44.7852 +/- 1.2886 g/s
The mean feedwater flow rate was 44.0008 +/- 1.8175 g/s
The mean water injection to steam flow rate was 0.0098182 +/- 0.026025 g/s
Mean Smoothed Condensing Region SP8-SP9 delta T is 11.4402 +/- 4.6524 C over the
Stratification Period, beginning at 2.3276 C and ending at 11.2607 C
Mean Smoothed SP8-Upper Pool delta T is 9.8928 +/- 3.7748 C over the Stratification
Period, beginning at 2.5375 C and ending at 10.8079 C
The stratification period begins and ends with Smoothed SP8 readings of 48.5645 and
108.3207 C, respectively
The stratification period begins and ends with condensing flows of 0.29505 and 1.7593
kg/s, respectively.
The stratification period begins and ends with condensing+cooling flows of 11.1616 and
2.1617 kg/s, respectively.
The stratification period had a mean sparger steam enthalpy of 2730.6608 +/- 1.4045 kJ/kg.

At plume detection, the condensing and condensing+cooling flows are 0.29447 and 12.9958 kg/s, respectively

The plume period had a mean steam enthalpy of 2731.4411 +/- 1.6834 kJ/kg.

Maximum Smoothed Top-Mid delta T is 3.6719 degrees C at t plus 3174.9596 s with T_upper = 72.2899 C and T_mid = 68.618 C

At t plus 3174.9596 s, Smoothed SP8-SP9 is 16.2705 C and Smoothed SP8-Top is 12.5986 C, where Smoothed SP8 is 84.8885 C and Pool P = 36.1724 psia

Maximum Smoothed Top-Lower delta T is 14.0896 degrees C at t plus 4619.2752 s with T_upper = 87.6787 C and T_low = 73.5891 C

At t plus 4619.2752 s, Smoothed SP8-SP9 is 9.1824 C and Smoothed SP8-Top is 6.4506 C, where Smoothed SP8 is 94.1294 C and Pool P = 20.6372 psia

Maximum Smoothed Mid-Lower delta T is 13.4675 degrees C at t plus 4836.9777 s with T_mid = 88.2075 C and T_low = 74.74 C

At t plus 4836.9777 s, Smoothed SP8-SP9 is 7.2291 C and Smoothed SP8-Top is 6.7113 C, where Smoothed SP8 is 95.4366 C and Pool P = 15.3434 psia

Maximum Smoothed Top-Outlet delta T is 36.3436 degrees C at t plus 6088.1052 s with T_upper = 97.3828 C and T_out = 61.0392 C

At t plus 6088.1052 s, Smoothed SP8-SP9 is 11.5878 C and Smoothed SP8-Top is 11.0456 C, where Smoothed SP8 is 108.4284 C and Pool P = 20.7639 psia

Maximum Smoothed Mid-Outlet delta T is 35.8449 degrees C at t plus 6109.7005 s with T_mid = 97.0338 C and T_out = 61.1889 C

At t plus 6109.7005 s, Smoothed SP8-SP9 is 11.1972 C and Smoothed SP8-Top is 10.7631 C, where Smoothed SP8 is 108.231 C and Pool P = 20.821 psia

Maximum Smoothed Lower-Outlet delta T is 35.6495 degrees C at t plus 6080.8028 s with T_low = 96.6377 C and T_out = 60.9881 C

At t plus 6080.8028 s, Smoothed SP8-SP9 is 11.4958 C and Smoothed SP8-Top is 10.961 C, where Smoothed SP8 is 108.281 C and Pool P = 20.7348 psia

Maximum Smoothed Condensing Region SP8-SP9 delta T is 19.0892 degrees C at (KEY POINT #14) t plus 3737.2608 s with T_SP8 = 94.2638 C and T_SP9 = 75.1746 C and Pool P = 37.9781 psia

Maximum Smoothed Condensing Region SP8-Upper delta T is 16.1741 degrees C at t plus 3737.2608 s with T_SP8 = 94.2638 C and T_upper = 78.0896 C and Pool P = 37.9781 psia

Maximum Top-Mid delta T is 5.0724 degrees C at (KEY POINT #4) t plus 3187.2523 s ignoring SP 4, with temperatures of 73.6726 and 68.6002 C, respectively, at Set # 2, where Pool P = 36.1998 psia and T_outlet = 56.1338 C

Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 4654.2762 s with a Smoothed Mid-Axis Top-Mid Delta T of 1.6885 C and a raw SP12 Reading of 86.1157 C.

Maximum Top-Lower delta T is 18.8355 degrees C at t plus 4613.1759 s, with temperatures of 87.7763 and 68.9407 C, respectively, at Set # 1, where Pool P = 21.0516 psia and T_outlet = 58.5542 C

Maximum Mid-Low delta T is 14.5565 degrees C at (KEY POINT #6) t plus 4990.9805 s ignoring SP 4, with temperatures of 89.3747 and 74.8182 C, respectively, at Set # 2, where Pool P = 16.4433 psia and T_outlet = 59.0766 C

Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 5241.1868 s with a Smoothed Mid-Axis Mid-Low Delta T of 4.8447 C and a raw SP12 Reading of 91.5377 C.

Maximum Top-Outlet delta T is 36.7412 degrees C at t plus 6096.0037 s, with temperatures of 97.7389 and 60.9977 C, respectively, at Set # 1, where Pool P = 20.7742 psia

Maximum Mid-Outlet delta T is 35.4601 degrees C at t plus 6105.5022 s ignoring SP 4, with temperatures of 96.6135 and 61.1534 C, respectively, at Set # 2, where Pool P = 20.8038 psia

Maximum Lower-Outlet delta T is 36.5721 degrees C at (KEY POINT #8) t plus 6103.0011 s, with temperatures of 97.6688 and 61.0967 C, respectively, at Set # 1, where Pool P = 20.8016 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 6459.1074 s with a Smoothed Mid-Axis Low-Outlet Delta T of 12.188 C and a raw SP12 Reading of 98.6875 C.

Minimum SP Pressure is 15.343 psia at t plus 4836.1856 s

Maximum SP Pressure is 40.8567 psia at t plus 4470.4747 s

Beginning SP Pressure is 30.5239 psia

Ending SP Pressure is 32.3111 psia

Time-Average SP Pressure is 29.1865 +/- 6.9157 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 76.363 cm (cold) / 76.4948 cm (hot) at 14.6281 psia

Beginning Smoothed SP Level is 78.3622 cm (cold) / 78.5503 cm (hot) at 30.5234 psia

Ending Smoothed SP Level is 77.938 cm (cold) / 79.3065 cm (hot) at 32.3224 psia

Minimum Smoothed Cold SP Level is 76.3791 cm at t plus 6840.6193 s and 23.9818 psia

Minimum Smoothed Hot SP Level is 77.1817 cm at t plus 4814.1794 s and 15.4067 psia

Maximum Smoothed Cold SP Level is 78.7871 cm at t plus 3281.6527 s and 36.482 psia
 Maximum Smoothed Hot SP Level is 79.5186 cm at t plus 4420.0748 s and 40.6367 psia
 SP 12 Temperature at the beginning is 39.9438 C, and at the end is 113.4903 C
 At plume detection, the Mixing Number is 42.0753

The Mixing Number ranges from a minimum of 39.6359 at (KEY POINT #12) t plus 0 s to a maximum of 254.8528 at (KEY POINT #13) t plus 8208.6405 s; it had a mean value of 97.4678 +/- 58.8632 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 39.6359): 33.08521587 0.040894
 0.00925 0.3937 0.7836220492 0.7855031549 1.006313715
 1 1 27.75982624 101743.5513 0.06948876859
 0.05442750174 0.0434553287 1.006187186e-005 0.0434553287 40.66093633
 129.0613714 122.6753877 41.66791232 40.71885552 40.23158929
 36.87472868 4.17827036 4.251062793 2.189823602 0.6295271393
 0.6840381966 0.6840381966 4.279562952 1.40819784 0.04177166183
 992.0145929 940.9339203 1.213833482 1.192113967 0.0006447885825
 0.0002265930092 1.30482712e-005 1.329801054e-005 1532.620416
 1516.968672 482.9547405 487.5467971 2.160903368 2.1045156
 2.1415156 0.07648630269 0.08066835385 2724.421126 2723.650518
 170.4858849 515.163675 2709.794247 344.6777901 2209.257451
 174.6933078 170.7263833 168.6935511 154.6715116

KEY POINT #2 (t plus 530.2053 s with a Mixing Number of 42.0753): 32.76904188
 0.040894 0.00925 0.3937 0.784424842 0.7867699226
 1.00710534 1 1 27.14747972 100399.857
 0.06860051293 0.05432300786 0.04304005426 1.491588007e-005 0.04304005426
 46.0652565 130.3710527 123.1907633 48.06618006 45.94829043
 45.89105069 40.98448666 4.178614866 4.251987273 2.192957696
 0.6360967796 0.6841112625 0.6841112625 3.842214204 1.402013778
 0.04188395326 989.8205754 940.5120399 1.232211157 1.20749324
 0.0005848876148 0.0002255729743 1.306604509e-005 1.334720227e-005
 1540.709288 1516.170651 483.1758588 488.3290108 2.195859544
 2.138609516 2.175609516 0.1013250578 0.1121368043 2726.85206
 2726.115074 193.0702119 517.3572369 2710.531822 324.287025
 2209.494823 201.4315817 192.5799745 192.3438448 171.8463477

KEY POINT #3 (t plus 540.1059 s with a Mixing Number of 42.16): 32.76622413
 0.040894 0.00925 0.3937 0.7844483409 0.7868052427
 1.007095247 1 1 27.1353368 100391.7342
 0.0685720452 0.05432099934 0.04303635331 1.302954618e-005 0.04303635331
 46.23688756 130.3703826 123.2006642 48.56446787 46.02692685
 46.31460925 41.06472298 4.178636836 4.252005099 2.193018179
 0.6362974863 0.6841126367 0.6841126367 3.82951838 1.40189557
 0.04188611893 989.7475114 940.5039241 1.232566395 1.20787682
 0.0005831358442 0.000225553463 1.306638656e-005 1.334713441e-005
 1540.937848 1516.155256 483.1800966 488.3259703 2.196535571

2.139328415	2.176328415	0.1022158838	0.1149783375	2726.843217
2726.10689	193.7874563	517.3993823	2710.545973	323.611926
2209.443834	203.5139666	192.9086279	194.1137952	172.1816586
KEY POINT #4 (t plus 3187.2523 s with a Mixing Number of 57.8576): 33.83776389				
0.040894	0.00925	0.3937	0.787796125	0.7937242272
1.006595513	1	1	24.34436369	102565.825
0.06471000507	0.05333542332	0.0444437527	9.437640397e-006	0.0444437527
68.71191805	134.5691723	128.0351923	85.59562172	72.37365253
65.33644069	56.29154615	4.186957893	4.261010985	2.223796172
0.6586355417	0.6846514171	0.6846514171	2.613834399	1.346743194
0.0429823386	978.577462	936.4910128	1.416175869	1.390258122
0.0004111730472	0.0002163922223	1.323319079e-005	1.349144821e-005	
1557.624262	1508.348213	485.2037818	489.9576215	2.547522951
2.495793287	2.532793287	0.2950289164	0.5923206736	2732.333904
2731.741256	287.8058811	538.0014902	2717.367222	250.1956091
2194.332414	358.6010315	303.1402947	273.6777407	235.848131
KEY POINT #5 (t plus 4654.2762 s with a Mixing Number of 82.0582): 35.04082734				
0.040894	0.00925	0.3937	0.7655041431	0.7731254214
1.019482522	1	1	47.41772052	107287.276
0.06159698407	0.05729966426	0.0460239001	7.921878714e-006	0.0460239001
85.8256479	129.2738055	108.2845642	93.68446909	87.84261223
74.42372091	58.50612623	4.20028703	4.227852395	2.113080015
0.6706787897	0.6807596282	0.6807596282	2.067558	1.608425454
0.03896460042	968.1016437	952.2514683	0.7832600012	0.7391088895
0.0003301016073	0.0002589851802	1.255301584e-005	1.335628647e-005	
1555.056855	1536.466528	476.3774335	490.6359105	1.353080157
1.287819746	1.324819746	0.5976622715	0.8059369408	2734.231049
2731.982608	359.4726364	454.1027132	2688.451851	94.63007678
2280.128335	392.5170029	367.946032	311.635418	245.0062643
KEY POINT #6 (t plus 4990.9805 s with a Mixing Number of 102.5165): 34.77070922				
0.040894	0.00925	0.3937	0.7650457809	0.7729939096
1.021298947	1	1	52.9192652	106768.8167
0.06092460601	0.05797959147	0.04566911711	5.655252398e-006	0.04566911711
89.42229738	128.0303828	104.80996	97.78135382	89.8340324
76.83265374	59.16034487	4.204379328	4.222967512	2.097454261
0.6727150874	0.6796018868	0.6796018868	1.978167456	1.666004793
0.03837464772	965.7160045	954.8483604	0.7006559393	0.6571333667
0.0003165135658	0.0002681100429	1.243387447e-005	1.331768419e-005	
1553.146725	1540.327546	474.6773256	490.3603293	1.201089095
1.134076085	1.171076085	0.6865652219	0.9364705679	2733.687284
2730.886835	374.575695	439.4099829	2683.098629	64.83428788
2294.277301	409.758862	376.3055583	321.7211974	247.7293941
KEY POINT #7 (t plus 5241.1868 s with a Mixing Number of 109.1277): 34.57936056				
0.040894	0.00925	0.3937	0.7653078691	0.7736505596
1.01997673	1	1	49.11594585	106095.456
0.06052835661	0.05758663741	0.0454177928	9.113729752e-006	0.0454177928
91.52664635	128.4483202	106.821409	100.8075141	92.34479714
85.82742646	59.49387495	4.206602115	4.22576248	2.106372121
0.6738383643	0.6802897987	0.6802897987	1.929093819	1.632175826
0.03871230899	964.2991395	953.3515431	0.7475619559	0.7041765929
0.0003090136381	0.0002627579211	1.250281877e-005	1.332845368e-005	
1551.858524	1538.134366	475.6666271	490.3292666	1.287254269
1.222421777	1.259421777	0.7435119656	1.043756028	2733.332604
2730.920228	383.4323262	447.9134164	2686.206454	64.48109024
2285.419188	422.5229446	386.873021	359.4763964	249.1317901
KEY POINT #8 (t plus 6103.0011 s with a Mixing Number of 130.4794): 34.33773188				
0.040894	0.00925	0.3937	0.7646154523	0.7738265626
1.017219329	1	1	41.99244426	105098.8921
0.05949665081	0.05671017522	0.04510042889	9.251259416e-006	0.04510042889
96.95475008	129.6181101	111.2751135	108.2586808	97.41882553
96.67845021	61.13211779	4.21277406	4.232274806	2.127388299
0.676474041	0.6816404762	0.6816404762	1.812496353	1.5620106
0.03949829487	960.5468563	949.9736863	0.860533935	0.8178798839
0.0002910449777	0.0002515738457	1.265572276e-005	1.336081837e-005	
1547.860852	1532.871294	477.8067404	490.3609109	1.496258537
1.434330227	1.471330227	0.9088112939	1.351892081	2733.097692

2731.334326	406.2988582	466.7632988	2693.000025	60.46444059
2266.334393	454.0019345	408.2527459	405.136281	256.0020276
KEY POINT #9 (t plus 6115.5028 s with a Mixing Number of 131.0746): 34.34906302				
0.040894	0.00925	0.3937	0.7646102611	0.7738309495
1.017172925	1	1	41.92851755	105134.8677
0.0594765048	0.05669964055	0.04511531162	7.077462995e-006	0.04511531162
97.06003132	129.6180808	111.3283765	108.3207045	97.5128098
96.80048694	61.24096777	4.212900338	4.232355425	2.127650573
0.6765214033	0.6816552029	0.6816552029	1.810367608	1.561208896
0.03950802445	960.472648	949.9327624	0.8619642141	0.819357648
0.0002907147894	0.0002514453678	1.265755325e-005	1.336065393e-005	
1547.773699	1532.805022	477.8319075	490.3515712	1.498917105
1.437020204	1.474020204	0.9122960158	1.354740478	2733.067023
2731.309022	406.7425947	466.9889171	2693.080518	60.2463224
2266.078106	454.2643569	408.6489423	405.650566	256.4575907
KEY POINT #10 (t plus 6459.1074 s with a Mixing Number of 145.302): 34.38755972				
0.040894	0.00925	0.3937	0.7643698195	0.7741047966
1.016127401	1	1	39.64067204	105137.3033
0.05896793912	0.05635372949	0.04516587459	1.829882892e-005	0.04516587459
99.70897084	130.1368523	113.0738284	110.4497117	100.4649535
100.4437162	86.40375151	4.216151427	4.235033637	2.136392584
0.6776687292	0.6821192887	0.6821192887	1.758347409	1.535401612
0.03983130715	958.5896413	948.5848129	0.9099128031	0.8678332121
0.0002826219776	0.0002473007643	1.271756095e-005	1.337531801e-005	
1545.471657	1530.590502	478.6509734	490.3800875	1.588211466
1.527441608	1.564441608	1.003692059	1.45555215	2733.103752
2731.532369	417.9134062	474.385065	2695.7082	56.47165879
2258.718687	463.2754417	421.0998296	421.012895	361.9249126
KEY POINT #11 (t plus 8208.6405 s with a Mixing Number of 254.8528): 36.53177854				
0.040894	0.00925	0.3937	0.7793797652	0.7930647225
1.010234481	1	1	29.40895034	110527.8788
0.0560604913	0.05406252905	0.04798216976	8.245342853e-006	0.04798216976
114.5482901	134.8067154	124.473113	123.0968613	114.6922455
114.8406192	111.4767501	4.237215211	4.25431685	2.200877364
0.6825201329	0.6842799945	0.6842799945	1.514262784	1.386887216
0.04216711365	947.4604905	939.4573956	1.278913746	1.242412796
0.0002439136993	0.0002230720489	1.311027719e-005	1.351632338e-005	
1528.777987	1514.15628	483.7215788	491.0746608	2.28484078
2.228547864	2.265547864	1.667001461	2.189456391	2735.632193
2734.767306	480.6796993	522.817425	2712.358491	42.13772569
2212.814768	516.9628161	481.2884671	481.9197139	467.676962
KEY POINT #12 (t plus 0 s with a Mixing Number of 39.6359): 33.08521587 0.040894				
0.00925	0.3937	0.7836220492	0.7855031549	1.006313715
1	1	27.75982624	101743.5513	0.06948876859
0.05442750174	0.0434553287	1.006187186e-005	0.0434553287	40.66093633
129.0613714	122.6753877	41.66791232	40.71885552	40.23158929
36.87472868	4.17827036	4.251062793	2.189823602	0.6295271393
0.6840381966	0.6840381966	4.279562952	1.40819784	0.04177166183
992.0145929	940.9339203	1.213833482	1.192113967	0.0006447885825
0.0002265930092	1.30482712e-005	1.329801054e-005	1532.620416	
1516.968672	482.9547405	487.5467971	2.160903368	2.1045156
2.1415156	0.07648630269	0.08066835385	2724.421126	2723.650518
170.4858849	515.163675	2709.794247	344.6777901	2209.257451
174.6933078	170.7263833	168.6935511	154.6715116	
KEY POINT #13 (t plus 8208.6405 s with a Mixing Number of 254.8528): 36.53177854				
0.040894	0.00925	0.3937	0.7793797652	0.7930647225
1.010234481	1	1	29.40895034	110527.8788
0.0560604913	0.05406252905	0.04798216976	8.245342853e-006	0.04798216976
114.5482901	134.8067154	124.473113	123.0968613	114.6922455
114.8406192	111.4767501	4.237215211	4.25431685	2.200877364
0.6825201329	0.6842799945	0.6842799945	1.514262784	1.386887216
0.04216711365	947.4604905	939.4573956	1.278913746	1.242412796
0.0002439136993	0.0002230720489	1.311027719e-005	1.351632338e-005	
1528.777987	1514.15628	483.7215788	491.0746608	2.28484078
2.228547864	2.265547864	1.667001461	2.189456391	2735.632193
2734.767306	480.6796993	522.817425	2712.358491	42.13772569
2212.814768	516.9628161	481.2884671	481.9197139	467.676962

KEY POINT #14 (t plus 3737.2608 s with a Mixing Number of 64.4178): 33.83158113

0.040894	0.00925	0.3937	0.7877283078	0.7945388724
1.005722397	1	1	23.234677	102407.731
0.06355144889	0.05301664135	0.04443563204	5.065536873e-006	0.04443563204
75.17457701	135.2141941	129.5889592	94.26377105	78.0896482
68.42178886	57.00288861	4.191315097	4.264035882	2.234222
0.6636862837	0.6847689184	0.6847689184	2.380413198	1.33005606
0.043351429	974.8262096	935.1801587	1.479648245	1.456247394
0.000376933624	0.0002135960097	1.32868225e-005	1.350980698e-005	
1558.114163	1505.718191	485.8346561	489.9603839	2.669536997
2.618538282	2.655538282	0.3887813445	0.8234185076	2732.506623
2731.966773	314.8883591	544.6327402	2719.521197	229.7443811
2187.873883	395.0571551	327.1082361	286.6027061	238.8327099

End

D.25 TEST #25 - T25_SRV_STD_57KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T25_SRV_STD_57kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1691.7668 s, and ending (KEY POINT #11) at t plus 18621.6661 s, for a time period of 16929.8993 s.
Original Data Record Time: 20030.7427 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 6603.4197 s, T_bulk = 70.0701 C and T_out = 67.761 C
Stratification Beginning SP12 Temperature = 69.956 C
Stratification Beginning Pressure = 19.2421 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 16900.1006 s, T_bulk = 116.2053 C and T_out = 114.0093 C
Stratification Ending SP12 Temperature = 116.1249 C
Stratification Ending Pressure = 42.1972 psia
No Plume detected, setting t_plume (KEY POINT #2) to the end at 16929.8993 s.
At t = 16929.8993 s, the pool pressure is 42.3063 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 117.3251, 116.9493, 116.9278, 117.224, and 114.4262 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 0 +/- 0 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 0 +/- 0 C.
Minimum Steam Quality: 0.9936 at t plus 16855.603 s
Maximum Steam Quality: 1.0174 at t plus 2627.9463 s
Time-Averaged Steam Quality: 1.0076 +/- 0.0049616
SRV Alignment, no RCIC Turbine 0 0 0 0 0
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 16839.8972 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.33739 degrees/min at t plus 10745.4896 s and 0.22283 degrees/min at t plus 8309.9443 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.3961 degrees/min at t plus 7018.6475 s and 0.14012 degrees/min at t plus 339.4064 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.13307 degrees/min at t plus 10333.789 s and -0.14591 degrees/min at t plus 8349.6475 s, respectively
Max and min smoothed lower level changerates: 0.41737 degrees/min at t plus 10729.8977 s and 0.15482 degrees/min at t plus 10143.6781 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.20819 degrees/min at t plus 10145.8783 s and -0.19929 degrees/min at t plus 10731.4878 s, respectively
Max and min smoothed outlet level changerates: 0.49568 degrees/min at t plus 7996.9414 s and 0.061126 degrees/min at t plus 12571.92 s, respectively
Max and min smoothed lower-outlet level changerate differences: 0.21599 degrees/min at t plus 10730.6387 s and -0.18239 degrees/min at t plus 8076.743 s, respectively
Max and min smoothed hot (SP8) level changerates: 0.37154 degrees/min at t plus 5909.405 s and 0.17485 degrees/min at t plus 10163.4803 s, respectively
Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.16484 degrees/min at t plus 10333.883 s and -0.18319 degrees/min at t plus 7069.7224 s, respectively
The mean steam flow rate was 23.9164 +/- 0.92242 g/s

The mean feedwater flow rate was 23.7145 +/- 1.0977 g/s
 The mean water injection to steam flow rate was 0.0096928 +/- 0.026798 g/s
 Mean Smoothed Condensing Region SP8-SP9 delta T is -0.14091 +/- 0.205 C over the Stratification Period, beginning at 0.3469 C and ending at -0.11539 C
 Mean Smoothed SP8-Upper Pool delta T is -0.22317 +/- 0.19547 C over the Stratification Period, beginning at 0.10825 C and ending at -0.35347 C
 The stratification period begins and ends with Smoothed SP8 readings of 70.9899 and 116.798 C, respectively
 The stratification period begins and ends with condensing flows of 0.33727 and 0.80483 kg/s, respectively.
 The stratification period begins and ends with condensing+cooling flows of 39.5461 and -115.5447 kg/s, respectively.
 The stratification period had a mean sparger steam enthalpy of 2718.4167 +/- 1.0752 kJ/kg. At plume detection, the condensing and condensing+cooling flows are 0.80306 and -620.5149 kg/s, respectively
 The plume period had a mean steam enthalpy of 0 +/- 0 kJ/kg.
 Maximum Smoothed Top-Mid delta T is 0.64757 degrees C at t plus 6368.9103 s with T_upper = 69.8538 C and T_mid = 69.2063 C
 At t plus 6368.9103 s, Smoothed SP8-SP9 is 0.55351 C and Smoothed SP8-Top is -0.094059 C, where Smoothed SP8 is 69.7598 C and Pool P = 18.9846 psia
 Maximum Smoothed Top-Lower delta T is 1.2709 degrees C at t plus 6509.7133 s with T_upper = 70.4505 C and T_low = 69.1796 C
 At t plus 6509.7133 s, Smoothed SP8-SP9 is 0.076161 C and Smoothed SP8-Top is -0.097364 C, where Smoothed SP8 is 70.3531 C and Pool P = 19.133 psia
 Maximum Smoothed Mid-Lower delta T is 1.4952 degrees C at t plus 7482.133 s with T_mid = 75.3094 C and T_low = 73.8142 C
 At t plus 7482.133 s, Smoothed SP8-SP9 is -0.30494 C and Smoothed SP8-Top is 0.11512 C, where Smoothed SP8 is 75.0045 C and Pool P = 20.2598 psia
 Maximum Smoothed Top-Outlet delta T is 4.1028 degrees C at t plus 7659.7361 s with T_upper = 75.7184 C and T_out = 71.6156 C
 At t plus 7659.7361 s, Smoothed SP8-SP9 is -0.21127 C and Smoothed SP8-Top is 0.092383 C, where Smoothed SP8 is 75.8108 C and Pool P = 20.4894 psia
 Maximum Smoothed Mid-Outlet delta T is 4.4689 degrees C at t plus 7482.332 s with T_mid = 75.3099 C and T_out = 70.8411 C
 At t plus 7482.332 s, Smoothed SP8-SP9 is -0.30353 C and Smoothed SP8-Top is 0.11678 C, where Smoothed SP8 is 75.0064 C and Pool P = 20.2601 psia
 Maximum Smoothed Lower-Outlet delta T is 3.9891 degrees C at t plus 13684.4407 s with T_low = 102.9397 C and T_out = 98.9506 C
 At t plus 13684.4407 s, Smoothed SP8-SP9 is -0.18986 C and Smoothed SP8-Top is -0.31091 C, where Smoothed SP8 is 102.6498 C and Pool P = 31.8778 psia
 Maximum Smoothed Condensing Region SP8-SP9 delta T is 0.56935 degrees C at (KEY POINT #14) t plus 6386.6133 s with T_SP8 = 69.8783 C and T_SP9 = 69.309 C and Pool P = 19.0114 psia
 Maximum Smoothed Condensing Region SP8-Upper delta T is 0.41262 degrees C at t plus 8325.5472 s with T_SP8 = 78.855 C and T_upper = 78.4424 C and Pool P = 21.3724 psia
 Maximum Top-Mid delta T is 1.8778 degrees C at (KEY POINT #4) t plus 5238.1636 s ignoring SP 4, with temperatures of 65.3151 and 63.4373 C, respectively, at Set # 2, where Pool P = 17.884 psia and T_outlet = 61.3759 C
 Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 5238.1636 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.50499 C and a raw SP12 Reading of 63.4373 C.
 Maximum Top-Lower delta T is 1.994 degrees C at t plus 5428.5975 s, with temperatures of 66.1962 and 64.2022 C, respectively, at Set # 2, where Pool P = 18.0618 psia and T_outlet = 62.3223 C
 Maximum Mid-Low delta T is 2.2984 degrees C at (KEY POINT #6) t plus 4913.6861 s ignoring SP 4, with temperatures of 64.107 and 61.8087 C, respectively, at Set # 2, where Pool P = 17.5857 psia and T_outlet = 59.9851 C
 Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 4913.6861 s with a Smoothed Mid-Axis Mid-Low Delta T of 0.77012 C and a raw SP12 Reading of 64.107 C.
 Maximum Top-Outlet delta T is 4.8176 degrees C at t plus 7684.8366 s, with temperatures of 76.3598 and 71.5422 C, respectively, at Set # 1, where Pool P = 20.5177 psia
 Maximum Mid-Outlet delta T is 4.1598 degrees C at t plus 5667.8462 s ignoring SP 4, with temperatures of 67.141 and 62.9812 C, respectively, at Set # 2, where Pool P = 18.2755 psia
 Maximum Lower-Outlet delta T is 4.4134 degrees C at (KEY POINT #8) t plus 312.9049 s, with temperatures of 42.7376 and 38.3242 C, respectively, at Set # 1, where Pool P = 14.9519 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 9730.9715 s with a Smoothed Mid-Axis Low-Outlet Delta T of 1.4708 C and a raw SP12 Reading of 84.2147 C.

Minimum SP Pressure is 14.8651 psia at t plus 53.035 s
 Maximum SP Pressure is 42.3064 psia at t plus 16929.1423 s
 Beginning SP Pressure is 14.8724 psia
 Ending SP Pressure is 42.3063 psia

Time-Average SP Pressure is 23.8366 +/- 7.793 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 77.5315 cm (cold) / 77.6764 cm (hot) at 14.5453 psia
 Beginning Smoothed SP Level is 77.8835 cm (cold) / 78.0552 cm (hot) at 14.8659 psia
 Ending Smoothed SP Level is 78.8656 cm (cold) / 80.3502 cm (hot) at 42.312 psia
 Minimum Smoothed Cold SP Level is 77.6424 cm at t plus 10599.3842 s and 25.0142 psia
 Minimum Smoothed Hot SP Level is 78.0535 cm at t plus 32.1008 s and 14.8741 psia
 Maximum Smoothed Cold SP Level is 78.8909 cm at t plus 16654.6976 s and 41.2695 psia
 Maximum Smoothed Hot SP Level is 80.3533 cm at t plus 16823.9192 s and 41.9066 psia

SP 12 Temperature at the beginning is 39.7858 C, and at the end is 116.2199 C

At plume detection, the Mixing Number is 257.6212

The Mixing Number ranges from a minimum of 32.9355 at (KEY POINT #12) t plus 0 s to a maximum of 258.5348 at (KEY POINT #13) t plus 16885.1507 s; it had a mean value of 97.5297 +/- 61.7823 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) gl, Sparger Diameter (m) dl, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) mdl, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m3) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 32.9355): 15.7813689 0.040894
 0.00925 0.3937 0.778835164 0.780551912 1.00830913
 1 1 26.9054711 51154.2295 0.0697067273 0.0588738685
 0.0207278253 5.08205061e-006 0.0207278253 39.3198886 109.289089
 100.197122 39.1941363 39.4943748 40.0334569 37.1190151
 4.17855667 4.21689432 2.07827362 0.627765276 0.677838671
 0.677838671 4.40103552 1.74910493 0.0376388204 992.476182
 958.212648 0.602081769 0.586692503 0.000661189375 0.00028115738
 1.22760775e-005 1.26160301e-005 1530.16435 1544.91056 472.356696
 478.692918 1.02133481 1.02496454 1.06196454 0.0712082334
 0.0707298422 2695.35193 2694.62802 164.786753 419.93091
 2675.88303 255.144157 2275.42102 164.261289 165.514344
 167.770027 155.595783

KEY POINT #2 (t plus 16929.8993 s with a Mixing Number of 257.6212): 19.3316694
 0.040894 0.00925 0.3937 0.788656314 0.803502014
 0.99864144 0.99864144 0.999997695 12.2208543 59132.5479
 0.0555809724 0.0525284558 0.0253909194 1.85852259e-005 0.0253909194
 116.949322 131.959277 131.959277 116.927815 117.325128
 117.224021 114.426164 4.24096055 4.26877639 2.25063417
 0.683091683 0.684896479 0.684896479 1.48109233 1.30551188
 0.0439306527 945.589105 933.160635 1.58086996 1.58301694
 0.0002385596 0.000209460606 1.33686539e-005 1.33691058e-005 1525.62735
 1501.59479 486.778577 486.753004 2.86477374 2.91730979

2.95430979	1.8021435	1.80089439	2719.97409	2719.82474
490.906964	554.758609	2722.77011	63.8516447	2165.21548
490.815755	492.499647	492.07329	480.216118	
KEY POINT #3 (t plus 6603.4197 s with a Mixing Number of 60.1263):	18.0812751			
0.040894	0.00925	0.3937	0.778250598	0.783628121
1.01368497	1	1	25.2296215	56603.6886
0.0643660181	0.0575897134	0.0237486058	9.98159096e-006	0.0237486058
70.6429975	121.548735	106.8057	70.9899009	70.8816522
69.7482559	67.8179327	4.1884331	4.2257403	2.10630112
0.660142955	0.680284615	0.680284615	2.54020261	1.63243468
0.038709631	977.421869	953.363303	0.747185981	0.716969719
0.000400363767	0.00026279897	1.250228e-005	1.30630296e-005	1557.73678
1538.15194	475.658955	485.803537	1.28656211	1.32644324
1.36344324	0.32078578	0.325608445	2717.45035	2716.81382
295.796936	447.846981	2686.18227	152.050045	2269.60337
297.249957	296.795157	292.051102	283.972044	
KEY POINT #4 (t plus 5238.1636 s with a Mixing Number of 51.4485):	17.9032882			
0.040894	0.00925	0.3937	0.778592206	0.783063068
1.01453689	1	1	26.6200308	56165.8949
0.0655320051	0.0579583981	0.0235148314	7.93220637e-006	0.0235148314
64.0536452	120.682541	104.918682	64.0574091	64.4201702
63.6102757	61.3060709	4.18461626	4.22311629	2.09792745
0.654565944	0.679640319	0.679640319	2.80786308	1.66414041
0.0383926318	981.083783	954.767916	0.703128465	0.672776362
0.000439211492	0.000267815717	1.2437599e-005	1.30352605e-005	1555.9611
1540.21198	474.731155	485.543444	1.20562142	1.23286355
1.26986355	0.239999544	0.240040213	2716.58788	2715.87925
268.203247	439.869454	2683.26722	171.666207	2276.71842
268.218997	269.735637	266.349464	256.712845	
KEY POINT #5 (t plus 5238.1636 s with a Mixing Number of 51.4485):	17.9032882			
0.040894	0.00925	0.3937	0.778592206	0.783063068
1.01453689	1	1	26.6200308	56165.8949
0.0655320051	0.0579583981	0.0235148314	7.93220637e-006	0.0235148314
64.0536452	120.682541	104.918682	64.0574091	64.4201702
63.6102757	61.3060709	4.18461626	4.22311629	2.09792745
0.654565944	0.679640319	0.679640319	2.80786308	1.66414041
0.0383926318	981.083783	954.767916	0.703128465	0.672776362
0.000439211492	0.000267815717	1.2437599e-005	1.30352605e-005	1555.9611
1540.21198	474.731155	485.543444	1.20562142	1.23286355
1.26986355	0.239999544	0.240040213	2716.58788	2715.87925
268.203247	439.869454	2683.26722	171.666207	2276.71842
268.218997	269.735637	266.349464	256.712845	
KEY POINT #6 (t plus 4913.6861 s with a Mixing Number of 50.0134):	17.8426597			
0.040894	0.00925	0.3937	0.778365421	0.782600182
1.01463723	1	1	26.9070903	56017.5468
0.0657516725	0.0580393034	0.0234351997	1.45265227e-005	0.0234351997
62.7980351	120.397607	104.503493	62.377167	62.8564792
62.3033172	59.9430052	4.18399269	4.22254955	2.09612578
0.653431848	0.679492784	0.679492784	2.86433109	1.67128267
0.0383241162	981.753735	955.074836	0.693724372	0.663532157
0.000447334711	0.00026894285	1.24233768e-005	1.30255209e-005	1555.40294
1540.65146	474.525374	485.422134	1.18838889	1.21280922
1.24980922	0.226754935	0.222456844	2716.20038	2715.47639
262.947729	438.114906	2682.62302	175.167178	2278.08548
261.186863	263.190842	260.879395	251.009504	
KEY POINT #7 (t plus 4913.6861 s with a Mixing Number of 50.0134):	17.8426597			
0.040894	0.00925	0.3937	0.778365421	0.782600182
1.01463723	1	1	26.9070903	56017.5468
0.0657516725	0.0580393034	0.0234351997	1.45265227e-005	0.0234351997
62.7980351	120.397607	104.503493	62.377167	62.8564792
62.3033172	59.9430052	4.18399269	4.22254955	2.09612578
0.653431848	0.679492784	0.679492784	2.86433109	1.67128267
0.0383241162	981.753735	955.074836	0.693724372	0.663532157
0.000447334711	0.00026894285	1.24233768e-005	1.30255209e-005	1555.40294
1540.65146	474.525374	485.422134	1.18838889	1.21280922
1.24980922	0.226754935	0.222456844	2716.20038	2715.47639
262.947729	438.114906	2682.62302	175.167178	2278.08548
261.186863	263.190842	260.879395	251.009504	

262.947729	438.114906	2682.62302	175.167178	2278.08548
261.186863	263.190842	260.879395	251.009504	
KEY POINT #8 (t plus 312.9049 s with a Mixing Number of 33.4559):	16.1225646			
0.040894	0.00925	0.3937	0.779006603	0.780860017
1.01154193	1	1	27.641193	51687.3966
0.0694673549	0.05884461	0.0211759641	2.07576937e-005	0.0211759641
40.7923652	113.007466	100.348835	40.6359698	40.8312894
41.3021971	38.3490232	4.17853395	4.21708669	2.07887735
0.629637057	0.677900808	0.677900808	4.26845857	1.7462426
0.0376621953	991.913558	958.103525	0.605133029	0.583852102
0.000643187234	0.000280710205	1.22812597e-005	1.27558399e-005	1532.66405
1544.76992	472.434148	481.171726	1.02687001	1.03091571
1.06791571	0.0770212894	0.0763850388	2702.91969	2702.15566
170.940084	420.571097	2676.12225	249.631012	2282.3486
170.286581	171.101227	173.072025	160.736057	
KEY POINT #9 (t plus 16900.1006 s with a Mixing Number of 258.1257):	19.3104902			
0.040894	0.00925	0.3937	0.788707239	0.803514088
0.99853481	0.99853481	0.999997521	12.2345044	59081.3989
0.0555881629	0.0525471085	0.0253631019	1.37946999e-005	0.0253631019
116.913409	131.868911	131.868911	116.798022	117.151494
117.099644	114.244856	4.24090286	4.26859284	2.24999719
0.683083783	0.684892756	0.684892756	1.4815763	1.30642794
0.0439082082	945.617309	933.238065	1.5769116	1.57922155
0.000238638039	0.000209615455	1.33655339e-005	1.33660205e-005	1525.67618
1501.75444	486.743002	486.715455	2.85712432	2.90965992
2.94665992	1.80005809	1.79337112	2719.61983	2719.47015
490.754117	554.372353	2722.64708	63.6182361	2165.24748
490.264786	491.762648	491.545224	479.447425	
KEY POINT #10 (t plus 9730.9715 s with a Mixing Number of 88.3552):	18.4067834			
0.040894	0.00925	0.3937	0.776704849	0.784245298
1.01002367	1	1	20.9736149	57390.3415
0.0617740682	0.0563938154	0.0241761404	5.92674364e-006	0.0241761404
84.8728485	123.422585	112.871899	84.5621553	84.8870366
84.5566344	82.645315	4.19974253	4.23472018	2.13536652
0.670126681	0.682067434	0.682067434	2.09238684	1.53834166
0.039793463	968.730034	948.741435	0.904257622	0.877831307
0.000333869098	0.000247773809	1.27106166e-005	1.31159178e-005	1555.54254
1530.85092	478.556782	485.929674	1.57766311	1.62118796
1.65818796	0.575795749	0.568811807	2718.11646	2717.67657
355.496793	473.52916	2695.40522	118.032367	2244.5873
354.192007	355.555045	354.170236	346.149013	
KEY POINT #11 (t plus 16929.8993 s with a Mixing Number of 257.6212):	19.3316694			
0.040894	0.00925	0.3937	0.788656314	0.803502014
0.99864144	0.99864144	0.999997695	12.2208543	59132.5479
0.0555809724	0.0525284558	0.0253909194	1.85852259e-005	0.0253909194
116.949322	131.959277	131.959277	116.927815	117.325128
117.224021	114.426164	4.24096055	4.26877639	2.25063417
0.683091683	0.684896479	0.684896479	1.48109233	1.30551188
0.0439306527	945.589105	933.160635	1.58086996	1.58301694
0.0002385596	0.000209460606	1.33686539e-005	1.33691058e-005	1525.62735
1501.59479	486.778577	486.753004	2.86477374	2.91730979
2.95430979	1.8021435	1.80089439	2719.97409	2719.82474
490.906964	554.758609	2722.77011	63.8516447	2165.21548
490.815755	492.499647	492.07329	480.216118	
KEY POINT #12 (t plus 0 s with a Mixing Number of 32.9355):	15.7813689			0.040894
0.00925	0.3937	0.778835164	0.780551912	1.00830913
1	1	26.9054711	51154.2295	0.0697067273
0.0207278253	5.08205061e-006	0.0207278253	39.3198886	109.289089
100.197122	39.1941363	39.4943748	40.0334569	37.1190151
4.17855667	4.21689432	2.07827362	0.627765276	0.677838671
0.677838671	4.40103552	1.74910493	0.0376388204	992.476182
958.212648	0.602081769	0.586692503	0.000661189375	0.00028115738
1.22760775e-005	1.26160301e-005	1530.16435	1544.91056	472.356696
478.692918	1.02133481	1.02496454	1.06196454	0.0712082334
0.0707298422	2695.35193	2694.62802	164.786753	419.93091
2675.88303	255.144157	2275.42102	164.261289	165.514344
167.770027	155.595783			

KEY POINT #13 (t plus 16885.1507 s with a Mixing Number of 258.5348): 19.338571

0.040894	0.00925	0.3937	0.788707509	0.803498179
0.998435983	0.998435983	0.999997357	12.2645023	59174.25
0.0555885827	0.0525566683	0.0253999841	8.96296035e-006	0.0253999841
116.911312	131.822592	131.822592	116.727251	117.072935
117.038411	114.131704	4.24090037	4.26849884	2.24967104
0.683083118	0.684890813	0.684890813	1.48160473	1.30689808
0.0438967149	945.618784	933.27774	1.57488573	1.57734856
0.000238642527	0.000209694912	1.33639347e-005	1.33644536e-005	1525.67825
1501.83619	486.724755	486.695367	2.85320982	2.90574654
2.94274654	1.7999364	1.7892798	2719.34298	2719.19257
490.744947	554.174374	2722.58399	63.4294267	2165.16861
489.964392	491.429186	491.285252	478.967782	

KEY POINT #14 (t plus 6386.6133 s with a Mixing Number of 58.1547): 18.0654861

0.040894	0.00925	0.3937	0.77835866	0.783585897
1.01390526	1	1	25.4922163	56560.4796
0.0646038538	0.0576516648	0.0237278681	1.89340726e-005	0.0237278681
69.3089606	121.487187	106.489185	69.8783126	69.9241998
68.7114288	66.700166	4.18758647	4.22529463	2.10487518
0.659064162	0.680179541	0.680179541	2.59077834	1.63766774
0.038655813	978.182746	953.600006	0.739643527	0.709232245
0.000407750185	0.000263628502	1.24914263e-005	1.30615934e-005	1557.52982
1538.5046	475.504192	485.816388	1.27268167	1.31033905
1.34733905	0.302798327	0.310367925	2717.48112	2716.83127
290.208664	446.508524	2685.69481	156.299861	2270.9726
292.592976	292.783759	287.708036	279.29137	

End

D.26 TEST #26 -

T26_RCIC_1ATM_VENT82C_107KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T26_RCIC_1ATM_VENT82C_107kW\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1509.1673 s, and ending (KEY POINT #11) at t plus 10111.6164 s, for a time period of 8602.4491 s.
Original Data Record Time: 11495.6395 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 2640.345 s, T_{bulk} = 63.6021 C and T_{out} = 61.4211 C
Stratification Beginning SP12 Temperature = 63.4172 C
Stratification Beginning Pressure = 15.2914 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 6323.8097 s, T_{bulk} = 97.0206 C and T_{out} = 70.8237 C
Stratification Ending SP12 Temperature = 96.9722 C
Stratification Ending Pressure = 22.0599 psia
Plume detected! Setting t_{plume} (KEY POINT #2) to 2082.5331 s.
At t = 2082.5331 s, the pool pressure is 15.2922 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 59.1194, 59.1647, 61.1649, 58.9958, and 56.2378 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 8.5801 +/- 2.1794 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 7.9115 +/- 1.9317 C.
Minimum Steam Quality: 0.99202 at t plus 25.8015 s
Maximum Steam Quality: 1.0028 at t plus 2775.4548 s
Time-Averaged Steam Quality: 0.99993 +/- 0.0012993
Minimum Turbine Outlet Steam Quality: 1.0072 at t plus 8593.6485 s
Maximum Turbine Outlet Steam Quality: 1.0254 at t plus 4198.5711 s
Time-Averaged Turbine Outlet Steam Quality: 1.0191 +/- 0.0043041
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 8512.4489 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.84043 degrees/min at t plus 3772.8678 s and 0.41471 degrees/min at t plus 3417.2585 s, respectively

Max and min smoothed mid (SP9) level changerates: 0.7516 degrees/min at t plus 3835.6664 s and 0.36488 degrees/min at t plus 6562.7144 s, respectively
 Max and min smoothed upper-mid level changerate differences: 0.20378 degrees/min at t plus 6562.7144 s and -0.27064 degrees/min at t plus 7050.6223 s, respectively
 Max and min smoothed lower level changerates: 1.2781 degrees/min at t plus 4573.3776 s and 0.044961 degrees/min at t plus 3701.0637 s, respectively
 Max and min smoothed mid-lower level changerate differences: 0.59245 degrees/min at t plus 3701.0637 s and -0.70995 degrees/min at t plus 4573.3776 s, respectively
 Max and min smoothed outlet level changerates: 5.7403 degrees/min at t plus 6529.0134 s and -0.048199 degrees/min at t plus 5084.6958 s, respectively
 Max and min smoothed lower-outlet level changerate differences: 1.2426 degrees/min at t plus 4573.3776 s and -5.0585 degrees/min at t plus 6532.9357 s, respectively
 Max and min smoothed hot (SP8) level changerates: 1.2131 degrees/min at t plus 2512.6417 s and 0.24144 degrees/min at t plus 3461.656 s, respectively
 Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.6746 degrees/min at t plus 2516.873 s and -0.32688 degrees/min at t plus 3843.8649 s, respectively
 The mean steam flow rate was 45.565 +/- 1.3016 g/s
 The mean feedwater flow rate was 44.6838 +/- 1.5754 g/s
 The mean water injection to steam flow rate was 0.0097884 +/- 0.028318 g/s
 Mean Smoothed Condensing Region SP8-SP9 delta T is 9.2768 +/- 1.2571 C over the Stratification Period, beginning at 6.465 C and ending at 11.7715 C
 Mean Smoothed SP8-Upper Pool delta T is 8.5209 +/- 1.1511 C over the Stratification Period, beginning at 5.8939 C and ending at 10.8756 C
 The stratification period begins and ends with Smoothed SP8 readings of 70.6423 and 109.2254 C, respectively
 The stratification period begins and ends with condensing flows of 0.64802 and 1.6396 kg/s, respectively.
 The stratification period begins and ends with condensing+cooling flows of 4.0282 and 2.1077 kg/s, respectively.
 The stratification period had a mean sparger steam enthalpy of 2730.8514 +/- 1.1326 kJ/kg. At plume detection, the condensing and condensing+cooling flows are 0.56834 and 13.146 kg/s, respectively
 The plume period had a mean steam enthalpy of 2732.9937 +/- 0.91994 kJ/kg.
 Maximum Smoothed Top-Mid delta T is 1.7985 degrees C at t plus 6653.4135 s with T_upper = 101.3939 C and T_mid = 99.5954 C
 At t plus 6653.4135 s, Smoothed SP8-SP9 is 11.94 C and Smoothed SP8-Top is 10.1415 C, where Smoothed SP8 is 111.5354 C and Pool P = 23.4219 psia
 Maximum Smoothed Top-Lower delta T is 6.5168 degrees C at t plus 4451.0766 s with T_upper = 82.1349 C and T_low = 75.6181 C
 At t plus 4451.0766 s, Smoothed SP8-SP9 is 8.1524 C and Smoothed SP8-Top is 7.2914 C, where Smoothed SP8 is 89.4263 C and Pool P = 15.2931 psia
 Maximum Smoothed Mid-Lower delta T is 5.6576 degrees C at t plus 4451.8766 s with T_mid = 81.2811 C and T_low = 75.6236 C
 At t plus 4451.8766 s, Smoothed SP8-SP9 is 8.2045 C and Smoothed SP8-Top is 7.3481 C, where Smoothed SP8 is 89.4856 C and Pool P = 15.2923 psia
 Maximum Smoothed Top-Outlet delta T is 27.4555 degrees C at t plus 6341.9107 s with T_upper = 98.5772 C and T_out = 71.1217 C
 At t plus 6341.9107 s, Smoothed SP8-SP9 is 11.6858 C and Smoothed SP8-Top is 10.6089 C, where Smoothed SP8 is 109.1861 C and Pool P = 22.1177 psia
 Maximum Smoothed Mid-Outlet delta T is 26.5262 degrees C at t plus 6324.6097 s with T_mid = 97.4617 C and T_out = 70.9355 C
 At t plus 6324.6097 s, Smoothed SP8-SP9 is 11.7431 C and Smoothed SP8-Top is 10.8452 C, where Smoothed SP8 is 109.2048 C and Pool P = 22.062 psia
 Maximum Smoothed Lower-Outlet delta T is 26.8493 degrees C at t plus 6326.0088 s with T_low = 97.797 C and T_out = 70.9477 C
 At t plus 6326.0088 s, Smoothed SP8-SP9 is 11.7032 C and Smoothed SP8-Top is 10.7966 C, where Smoothed SP8 is 109.1745 C and Pool P = 22.0628 psia
 Maximum Smoothed Condensing Region SP8-SP9 delta T is 12.5882 degrees C at (KEY POINT #14) t plus 6199.7076 s with T_SP8 = 108.848 C and T_SP9 = 96.2597 C and Pool P = 21.5888 psia
 Maximum Smoothed Condensing Region SP8-Upper delta T is 11.351 degrees C at t plus 6199.6096 s with T_SP8 = 108.8474 C and T_upper = 97.4964 C and Pool P = 21.5897 psia
 Maximum Top-Mid delta T is 2.2039 degrees C at (KEY POINT #4) t plus 3775.2629 s ignoring SP 4, with temperatures of 75.7427 and 73.5389 C, respectively, at Set # 2, where Pool P = 15.2903 psia and T_outlet = 67.2342 C

Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 3996.1786 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.99997 C and a raw SP12 Reading of 76.7294 C.

Maximum Top-Lower delta T is 8.9909 degrees C at t plus 4725.7823 s, with temperatures of 85.4287 and 76.4379 C, respectively, at Set # 1, where Pool P = 16.0928 psia and T_{outlet} = 69.7055 C

Maximum Mid-Low delta T is 5.8443 degrees C at (KEY POINT #6) t plus 4453.9778 s ignoring SP 4, with temperatures of 81.2265 and 75.3822 C, respectively, at Set # 2, where Pool P = 15.2906 psia and T_{outlet} = 69.5136 C

Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 4729.3845 s with a Smoothed Mid-Axis Mid-Low Delta T of 1.9481 C and a raw SP12 Reading of 83.9083 C.

Maximum Top-Outlet delta T is 27.769 degrees C at t plus 6317.5123 s, with temperatures of 98.5289 and 70.7599 C, respectively, at Set # 1, where Pool P = 22.0199 psia

Maximum Mid-Outlet delta T is 26.4062 degrees C at t plus 6338.6125 s ignoring SP 4, with temperatures of 97.4816 and 71.0754 C, respectively, at Set # 2, where Pool P = 22.1052 psia

Maximum Lower-Outlet delta T is 27.6752 degrees C at (KEY POINT #8) t plus 6300.4094 s, with temperatures of 98.4029 and 70.7277 C, respectively, at Set # 1, where Pool P = 21.9649 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 6569.4147 s with a Smoothed Mid-Axis Low-Outlet Delta T of 9.222 C and a raw SP12 Reading of 98.8064 C.

Minimum SP Pressure is 15.0019 psia at t plus 5.8023 s

Maximum SP Pressure is 35.42 psia at t plus 8602.4491 s

Beginning SP Pressure is 15.0056 psia

Ending SP Pressure is 35.42 psia

Time-Average SP Pressure is 19.3841 +/- 5.807 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 77.0053 cm (cold) / 77.1471 cm (hot) at 14.6275 psia

Beginning Smoothed SP Level is 77.5295 cm (cold) / 77.7042 cm (hot) at 15.0073 psia

Ending Smoothed SP Level is 78.3837 cm (cold) / 79.8394 cm (hot) at 35.4126 psia

Minimum Smoothed Cold SP Level is 77.0556 cm at t plus 6859.8234 s and 24.4406 psia

Minimum Smoothed Hot SP Level is 77.667 cm at t plus 1136.419 s and 15.2928 psia

Maximum Smoothed Cold SP Level is 78.3881 cm at t plus 8563.2508 s and 35.1228 psia

Maximum Smoothed Hot SP Level is 79.8402 cm at t plus 8601.45 s and 35.4055 psia

SP 12 Temperature at the beginning is 40.0993 C, and at the end is 116.1783 C

At plume detection, the Mixing Number is 43.1113

The Mixing Number ranges from a minimum of 33.092 at (KEY POINT #12) t plus 0 s to a maximum of 265.6553 at (KEY POINT #13) t plus 8594.2756 s; it had a mean value of 95.099 +/- 63.2521 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) vl, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) kl, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_{mid} Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_{mid} Vapor Pressure p4, T_{Plume} Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 33.092): 32.12299817 0.040894
0.00925 0.3937 0.7752947668 0.7770417406 1.01508366
1 1 51.98562368 101259.0949 0.0695913551
0.05845146077 0.04219151689 7.518137368e-006 0.04219151689 40.03049824
118.8719371 102.3821718 40.38905902 39.99034888 40.14875671

37.10384371	4.178537448	4.219713153	2.08714423	0.6286735691
0.6787062992	0.6787062992	4.336370381	1.708746198	0.03798083344
992.2107477	956.6309505	0.6472594501	0.6180309077	0.0006524200102
0.0002748378306	1.235076643e-005	1.297303603e-005	1531.388781	
1542.818238	473.4648448	484.7481391	1.103484274	1.034718392
1.071718392	0.07396443077	0.07538978576	2715.959198	2713.256693
167.7569336	429.15424	2679.316018	261.3973065	2286.804958
169.2551925	167.5876612	168.2526757	155.5332582	
KEY POINT #2 (t plus 2082.5331 s with a Mixing Number of 43.1113): 33.86741642				
0.040894	0.00925	0.3937	0.7732251275	0.776964192
1.021292233	1	1	54.11118369	104383.2621
0.06638273419	0.0582673855	0.04448269941	9.781019026e-006	0.04448269941
59.16472889	126.645787	103.3308756	61.16492946	59.11940016
58.99575949	56.23781761	4.182398101	4.220969441	2.091115143
0.6500137008	0.6790648055	0.6790648055	3.039100596	1.69178802
0.03813296622	983.641766	955.9375131	0.6677157224	0.6260233283
0.0004723263968	0.0002721729496	1.238322786e-005	1.326816291e-005	
1553.355625	1541.865541	473.9410179	489.6786587	1.140813636
1.05426262	1.09126262	0.1918730746	0.2104618939	2731.583419
2728.655399	247.7357094	433.1608712	2680.798181	185.4251618
2298.422548	256.1021893	247.5446961	247.0305339	235.5012192
KEY POINT #3 (t plus 2640.345 s with a Mixing Number of 47.136): 34.10870152				
0.040894	0.00925	0.3937	0.7725502866	0.7769150951
1.021774835	1	1	54.95701958	105019.9145
0.06551032867	0.05830878328	0.04479961206	8.118896114e-006	0.04479961206
64.17729651	126.9835477	103.1176986	70.64231007	64.74842759
64.01254673	61.45689986	4.184719343	4.220685431	2.090216455
0.6546669858	0.6789852041	0.6789852041	2.802544188	1.69556954
0.03809858674	981.0151614	956.0936828	0.6630738951	0.620755696
0.0004384363695	0.0002727676936	1.237593199e-005	1.328168326e-005	
1555.9807	1542.081928	473.8342841	489.926578	1.132336044
1.054293348	1.091293348	0.2413386716	0.3207762832	2732.440151
2729.419877	268.705853	432.2604575	2680.465582	163.5546045
2300.179693	295.7718399	271.0945505	268.0179243	257.3288695
KEY POINT #4 (t plus 3775.2629 s with a Mixing Number of 58.9357): 34.62123231				
0.040894	0.00925	0.3937	0.7719950154	0.777907966
1.022266776	1	1	56.24754711	106484.2289
0.06375767287	0.05834876664	0.04547278869	1.037108454e-005	0.04547278869
74.03269581	127.3392114	102.9117047	83.19025321	75.25512996
72.54072764	67.10429218	4.190819732	4.220411938	2.08935159
0.6627550209	0.6789077587	0.6789077587	2.419219798	1.699239559
0.03806547323	975.4379115	956.2443966	0.6586134746	0.6156557972
0.0003825862649	0.0002733446255	1.236888288e-005	1.329587196e-005	
1557.872338	1542.289752	473.7310012	490.1843528	1.124193621
1.054267396	1.091267396	0.3705977286	0.5388149937	2733.380219
2730.216432	309.9763199	431.3904446	2680.143942	121.4141247
2301.989774	348.3869287	315.0984965	303.7260039	280.9619924
KEY POINT #5 (t plus 3996.1786 s with a Mixing Number of 63.5247): 34.72902357				
0.040894	0.00925	0.3937	0.7718946322	0.7781193432
1.022348221	1	1	56.44152672	106787.3312
0.06327717839	0.05834845266	0.04561436565	1.716074362e-005	0.04561436565
76.68771792	127.4313434	102.9133227	85.38951066	77.38768641
73.29709537	68.44577368	4.192809473	4.220414082	2.089358369
0.6647006467	0.6789083691	0.6789083691	2.331194218	1.699210671
0.03806573291	973.8460813	956.2432135	0.6586484141	0.6155412711
0.0003695723152	0.0002733400853	1.236893825e-005	1.329941177e-005	
1557.691797	1542.288125	473.731813	490.243419	1.124257388
1.054253106	1.091253106	0.4140300275	0.5875683949	2733.58766
2730.402014	321.1056478	431.397278	2680.146469	110.2916302
2302.190382	357.6223225	324.0393117	306.8952027	286.5783691
KEY POINT #6 (t plus 4453.9778 s with a Mixing Number of 74.0127): 34.94783353				
0.040894	0.00925	0.3937	0.7717118507	0.7786073981
1.022516618	1	1	56.80404153	107400.9865
0.06243399257	0.05834777565	0.04590175864	5.415621659e-006	0.04590175864
81.30113521	127.6219873	102.9168115	89.49232223	82.14475012
75.66373279	69.55944445	4.196615969	4.220418707	2.089372989
0.66785242	0.6789096849	0.6789096849	2.191036383	1.699148386

0.03806629286	970.9933774	956.2406626	0.658723756	0.6153075702
0.0003486830726	0.0002733302963	1.236905762e-005	1.330673722e-005	
1556.726789	1542.284615	473.7335634	490.3655761	1.124394892
1.054239956	1.091239956	0.4996869135	0.6883998627	2734.012635
2730.785936	340.4574403	431.4120123	2680.151919	90.95457198
2302.600623	374.8639225	343.9967368	316.814125	291.2417968
KEY POINT #7 (t plus 4729.3845 s with a Mixing Number of 80.6335): 35.04036703				
0.040894	0.00925	0.3937	0.7732379057	0.7806248165
1.021812666	1	1	54.3521079	107562.7182
0.06195026974	0.05808315764	0.04602329551	9.986768363e-006	0.04602329551
83.92245459	128.1045956	104.2782761	92.33644629	84.79209298
81.32700224	69.72257908	4.198964131	4.222243717	2.095154531
0.6695187189	0.6794118808	0.6794118808	2.117936138	1.675182567
0.03828713394	969.3269137	955.2410021	0.6886661495	0.6448318553
0.0003377018344	0.00026955785	1.241566352e-005	1.332190923e-005	
1555.834295	1540.887754	474.4135029	490.4850004	1.179126576
1.11038952	1.14738952	0.5546553001	0.7664493458	2734.199136
2731.244984	351.4655965	437.1632654	2682.273153	85.69766895
2297.03587	386.8305818	355.116196	340.5718741	291.929573
KEY POINT #8 (t plus 6300.4094 s with a Mixing Number of 125.5324): 35.06509258				
0.040894	0.00925	0.3937	0.7710103267	0.780610561
1.016530622	1	1	40.72944722	107131.1167
0.05946538753	0.05639600116	0.04605577094	9.885778489e-006	0.04605577094
97.11811774	130.3690049	112.860886	109.2643423	98.10580254
97.36978089	70.73272397	4.21295266	4.234703113	2.135310669
0.6765517048	0.6820645917	0.6820645917	1.809189405	1.538502351
0.03979140233	960.4352594	948.7499724	0.9039500134	0.8611120853
0.0002905349941	0.0002477996567	1.271023789e-005	1.338501772e-005	
1547.740903	1530.865096	478.5516403	490.5722022	1.577089466
1.514926185	1.551926185	0.9142233685	1.398689391	2733.777065
2732.118177	406.9932116	473.482481	2695.388685	66.48926936
2260.294584	458.2602733	411.1535882	408.0548574	296.193276
KEY POINT #9 (t plus 6323.8097 s with a Mixing Number of 127.4873): 35.06380873				
0.040894	0.00925	0.3937	0.7710007765	0.7806442933
1.016425685	1	1	40.57949676	107133.0952
0.05940108778	0.05637437911	0.0460540847	1.149065311e-005	0.0460540847
97.45391681	130.3589539	112.9698189	109.2254455	98.34987487
97.74376425	70.92869353	4.213358078	4.234872064	2.135863596
0.6767014426	0.6820926391	0.6820926391	1.802440309	1.536914501
0.0398117998	960.1980068	948.6655081	0.9069963721	0.8642925633
0.000289487372	0.000247544212	1.2713984e-005	1.338428047e-005	
1547.459435	1530.724778	478.6024758	490.5457205	1.582771027
1.520672755	1.557672755	0.9254317688	1.396854929	2733.690301
2732.043605	408.40842	473.9441979	2695.552173	65.53577788
2259.746103	458.0961896	412.1826181	409.6310631	297.0145634
KEY POINT #10 (t plus 6569.4147 s with a Mixing Number of 132.9717): 35.1046525				
0.040894	0.00925	0.3937	0.7708691994	0.7809034876
1.016008564	1	1	39.01661424	107058.3972
0.05912469307	0.05612282508	0.04610773039	7.584911267e-006	0.04610773039
98.89428294	131.1053721	114.2352586	110.6320402	100.5417726
100.2028889	89.47545659	4.215114846	4.236855034	2.142369836
0.6773301342	0.6824082541	0.6824082541	1.774029383	1.518717534
0.04005125968	959.1764024	947.6805268	0.9429985564	0.8998840121
0.000285070183	0.000244611952	1.275751261e-005	1.340922055e-005	
1546.22097	1529.071329	479.1898418	490.804152	1.65001182
1.588671251	1.625671251	0.9748099623	1.464464783	2734.477122
2732.954826	414.4835919	479.3092566	2697.445648	64.8256647
2255.167865	464.0513447	421.4283795	420.0019402	374.8393064
KEY POINT #11 (t plus 8602.4491 s with a Mixing Number of 265.116): 36.55809967				
0.040894	0.00925	0.3937	0.7838366873	0.79839433
1.008815198	1	1	26.95952323	110271.3178
0.0555672	0.05346942301	0.04801674089	5.364221568e-006	0.04801674089
117.0181003	136.1645972	127.3806378	125.8031651	117.2859049
117.3566581	114.2175139	4.241194308	4.259755956	2.219482431
0.6830779249	0.6845938473	0.6845938473	1.480233455	1.353919546
0.04282932882	945.5175837	937.0401595	1.390102184	1.35618807
0.0002384033184	0.0002175911015	1.321060018e-005	1.355753208e-005	

1525.423773	1509.438711	484.9351553	491.2592809	2.497497851
2.441609699	2.478609699	1.80614289	2.380212137	2736.409074
2735.682258	491.1648663	535.2094238	2716.454155	44.04455751
2201.19965	528.4908585	492.2995269	492.6021231	479.2980209
KEY POINT #12 (t plus 0 s with a Mixing Number of 33.092): 32.12299817 0.040894				
0.00925	0.3937	0.7752947668	0.7770417406	1.01508366
1	1	51.98562368	101259.0949	0.0695913551
0.05845146077	0.04219151689	7.518137368e-006	0.04219151689	40.03049824
118.8719371	102.3821718	40.38905902	39.99034888	40.14875671
37.10384371	4.178537448	4.219713153	2.08714423	0.6286735691
0.6787062992	0.6787062992	4.336370381	1.708746198	0.03798083344
992.2107477	956.6309505	0.6472594501	0.6180309077	0.0006524200102
0.0002748378306	1.235076643e-005	1.297303603e-005	1531.388781	
1542.818238	473.4648448	484.7481391	1.103484274	1.034718392
1.071718392	0.07396443077	0.07538978576	2715.959198	2713.256693
167.7569336	429.15424	2679.316018	261.3973065	2286.804958
169.2551925	167.5876612	168.2526757	155.5332582	
KEY POINT #13 (t plus 8594.2756 s with a Mixing Number of 265.6553): 36.56168624				
0.040894	0.00925	0.3937	0.7838495292	0.7983978601
1.008852294	1	1	27.00435989	110283.7667
0.05556944362	0.05347960215	0.04802145163	7.308479108e-006	0.04802145163
117.0068965	136.1539958	127.3308804	125.7751127	117.205089
117.2787581	114.1686252	4.241176698	4.259661015	2.219156405
0.6830753747	0.6845892748	0.6845892748	1.480384402	1.354468684
0.04281775706	945.5263224	937.0818295	1.388136061	1.354123956
0.0002384277293	0.0002176827524	1.320888298e-005	1.355733162e-005	
1525.438665	1509.521183	484.914666	491.2653217	2.493727981
2.437565029	2.474565029	1.805490906	2.378167741	2736.424128
2735.694893	491.1170617	534.9972142	2716.38461	43.88015252
2201.426914	528.3711692	491.9564543	492.2714095	479.0906102
KEY POINT #14 (t plus 6199.7076 s with a Mixing Number of 121.4863): 35.03039498				
0.040894	0.00925	0.3937	0.7710885616	0.7805528358
1.017010832	1	1	41.38673382	106998.3653
0.05962951791	0.05649521993	0.04601019786	1.196679185e-005	0.04601019786
96.25972611	130.4144973	112.3606834	108.847975	97.49772143
96.25589236	70.34167064	4.211929986	4.233930859	2.132786158
0.6761618699	0.6819340113	0.6819340113	1.826665123	1.545837715
0.03969817622	961.0388256	949.1371554	0.890067863	0.8466361756
0.0002932435509	0.0002489788684	1.269303837e-005	1.338836317e-005	
1548.44195	1531.505295	478.3176582	490.6924114	1.551215081
1.488786928	1.525786928	0.8860825787	1.379155142	2734.169591
2732.456729	403.375306	471.3625991	2694.636983	67.98729315
2262.806992	456.4975745	408.5892861	403.3605259	294.5532883

End

D.27 TEST #27 - T27_RCIC_080GPM_107KW_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T27_RCIC_080GPM_107kw\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1819.4701 s, and ending (KEY POINT #11) at t plus 10524.1239 s, for a time period of 8704.6538 s.
Original Data Record Time: 11618.0575 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 2592.5453 s, T_bulk = 63.7245 C and T_out = 61.6323 C
Stratification Beginning SP12 Temperature = 63.8034 C
Stratification Beginning Pressure = 17.5567 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 7301.1276 s, T_bulk = 105.037 C and T_out = 90.9014 C
Stratification Ending SP12 Temperature = 104.899 C
Stratification Ending Pressure = 33.7117 psia
Plume detected! Setting t_plume (KEY POINT #2) to 1694.1349 s.
At t = 1694.1349 s, the pool pressure is 16.3486 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 55.6644, 55.6855, 57.6886, 55.4453, and 53.8309 C, respectively.

Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 9.9742 +/- 3.4134 C.

Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 9.5579 +/- 3.2697 C.

Minimum Steam Quality: 0.319 at t plus 2.0721 s
Maximum Steam Quality: 0.47964 at t plus 8520.6813 s
Time-Averaged Steam Quality: 0.3986 +/- 0.029085

Minimum Turbine Outlet Steam Quality: 0.37276 at t plus 2.1151 s
Maximum Turbine Outlet Steam Quality: 0.50272 at t plus 8520.6813 s
Time-Averaged Turbine Outlet Steam Quality: 0.44072 +/- 0.020375

Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 8614.6517 s; using 300 s smoothing

Max and min smoothed upper level changerates: 0.7136 degrees/min at t plus 3219.3091 s and 0.37045 degrees/min at t plus 3891.0695 s, respectively

Max and min smoothed mid (SP9) level changerates: 0.62455 degrees/min at t plus 3016.7535 s and 0.45099 degrees/min at t plus 3865.8691 s, respectively

Max and min smoothed upper-mid level changerate differences: 0.20347 degrees/min at t plus 3217.355 s and -0.13313 degrees/min at t plus 3587.9652 s, respectively

Max and min smoothed lower level changerates: 1.0469 degrees/min at t plus 6386.6133 s and 0.28042 degrees/min at t plus 5700.421 s, respectively

Max and min smoothed mid-lower level changerate differences: 0.2666 degrees/min at t plus 5700.421 s and -0.52418 degrees/min at t plus 6408.5185 s, respectively

Max and min smoothed outlet level changerates: 3.7081 degrees/min at t plus 7448.234 s and 0.061381 degrees/min at t plus 6443.3145 s, respectively

Max and min smoothed lower-outlet level changerate differences: 0.92768 degrees/min at t plus 6386.6133 s and -3.2257 degrees/min at t plus 7447.733 s, respectively

Max and min smoothed hot (SP8) level changerates: 1.0327 degrees/min at t plus 5829.7994 s and 0.23054 degrees/min at t plus 4652.9801 s, respectively

Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.5005 degrees/min at t plus 5829.7994 s and -0.32327 degrees/min at t plus 4671.8802 s, respectively

The mean steam flow rate was 44.8416 +/- 1.4812 g/s
The mean feedwater flow rate was 44.3968 +/- 1.5511 g/s
The mean water injection to steam flow rate was 49.8607 +/- 1.5562 g/s
Mean Smoothed Condensing Region SP8-SP9 delta T is 11.081 +/- 2.43 C over the Stratification Period, beginning at 6.5808 C and ending at 14.712 C
Mean Smoothed SP8-Upper Pool delta T is 10.6101 +/- 2.3551 C over the Stratification Period, beginning at 6.2803 C and ending at 13.6607 C
The stratification period begins and ends with Smoothed SP8 readings of 70.0916 and 119.7275 C, respectively
The stratification period begins and ends with condensing flows of 0.51407 and 1.0994 kg/s, respectively.
The stratification period begins and ends with condensing+cooling flows of 3.8337 and 1.5724 kg/s, respectively.
The stratification period had a mean sparger steam enthalpy of 1469.3177 +/- 34.6479 kJ/kg.
At plume detection, the condensing and condensing+cooling flows are 0.44817 and 13.0125 kg/s, respectively
The plume period had a mean steam enthalpy of 1460.0121 +/- 39.3415 kJ/kg.
Maximum Smoothed Top-Mid delta T is 1.5147 degrees C at t plus 8555.1483 s with T_upper = 116.7845 C and T_mid = 115.2699 C
At t plus 8555.1483 s, Smoothed SP8-SP9 is 13.0526 C and Smoothed SP8-Top is 11.5379 C, where Smoothed SP8 is 128.3224 C and Pool P = 41.5899 psia
Maximum Smoothed Top-Lower delta T is 3.8845 degrees C at t plus 5991.2167 s with T_upper = 94.7735 C and T_low = 90.889 C
At t plus 5991.2167 s, Smoothed SP8-SP9 is 13.5854 C and Smoothed SP8-Top is 13.0411 C, where Smoothed SP8 is 107.8146 C and Pool P = 27.4142 psia
Maximum Smoothed Mid-Lower delta T is 3.3669 degrees C at t plus 5975.4048 s with T_mid = 94.0911 C and T_low = 90.7241 C
At t plus 5975.4048 s, Smoothed SP8-SP9 is 13.83 C and Smoothed SP8-Top is 13.3543 C, where Smoothed SP8 is 107.9211 C and Pool P = 27.3317 psia
Maximum Smoothed Top-Outlet delta T is 15.1842 degrees C at t plus 7156.2453 s with T_upper = 104.8889 C and T_out = 89.7047 C
At t plus 7156.2453 s, Smoothed SP8-SP9 is 14.1991 C and Smoothed SP8-Top is 13.2767 C, where Smoothed SP8 is 118.1656 C and Pool P = 32.9107 psia
Maximum Smoothed Mid-Outlet delta T is 14.3678 degrees C at t plus 7138.5253 s with T_mid = 103.8074 C and T_out = 89.4397 C

At t plus 7138.5253 s, Smoothed SP8-SP9 is 14.2212 C and Smoothed SP8-Top is 13.4111 C, where Smoothed SP8 is 118.0287 C and Pool P = 32.8437 psia
Maximum Smoothed Lower-Outlet delta T is 14.5683 degrees C at t plus 7140.7544 s with T_low = 104.0319 C and T_out = 89.4637 C
At t plus 7140.7544 s, Smoothed SP8-SP9 is 14.1817 C and Smoothed SP8-Top is 13.3771 C, where Smoothed SP8 is 118.0102 C and Pool P = 32.8588 psia
Maximum Smoothed Condensing Region SP8-SP9 delta T is 15.0499 degrees C at (KEY POINT #14) t plus 7229.9255 s with T_SP8 = 119.5729 C and T_SP9 = 104.5229 C and Pool P = 33.3209 psia
Maximum Smoothed Condensing Region SP8-Upper delta T is 14.5503 degrees C at t plus 6525.0152 s with T_SP8 = 113.8269 C and T_upper = 99.2767 C and Pool P = 29.7621 psia
Maximum Top-Mid delta T is 1.6971 degrees C at (KEY POINT #4) t plus 1010.5198 s ignoring SP 4, with temperatures of 50.2184 and 48.5213 C, respectively, at Set # 2, where Pool P = 15.6983 psia and T_outlet = 47.4385 C
Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 1010.5198 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.72402 C and a raw SP12 Reading of 48.5213 C.
Maximum Top-Lower delta T is 6.0919 degrees C at t plus 6212.7203 s, with temperatures of 96.5204 and 90.4285 C, respectively, at Set # 1, where Pool P = 28.3515 psia and T_outlet = 87.2296 C
Maximum Mid-Low delta T is 3.6553 degrees C at (KEY POINT #6) t plus 5973.1176 s ignoring SP 4, with temperatures of 94.0895 and 90.4342 C, respectively, at Set # 2, where Pool P = 27.3214 psia and T_outlet = 86.3097 C
Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 6452.215 s with a Smoothed Mid-Axis Mid-Low Delta T of 1.2177 C and a raw SP12 Reading of 98.202 C.
Maximum Top-Outlet delta T is 15.7868 degrees C at t plus 7307.925 s, with temperatures of 106.7238 and 90.937 C, respectively, at Set # 1, where Pool P = 33.7402 psia
Maximum Mid-Outlet delta T is 14.5652 degrees C at t plus 7128.0227 s ignoring SP 4, with temperatures of 103.7279 and 89.1627 C, respectively, at Set # 2, where Pool P = 32.7853 psia
Maximum Lower-Outlet delta T is 15.6986 degrees C at (KEY POINT #8) t plus 7170.0251 s, with temperatures of 105.5135 and 89.8148 C, respectively, at Set # 1, where Pool P = 32.9939 psia
Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 7477.3327 s with a Smoothed Mid-Axis Low-Outlet Delta T of 5.2281 C and a raw SP12 Reading of 106.5597 C.
Minimum SP Pressure is 15.0115 psia at t plus 11.1976 s
Maximum SP Pressure is 42.7139 psia at t plus 8704.6538 s
Beginning SP Pressure is 15.0199 psia
Ending SP Pressure is 42.7139 psia
Time-Average SP Pressure is 23.9627 +/- 7.9515 psia
SP Levels are fully corrected and compensated
Pre-Start SP Level is 76.7617 cm (cold) / 76.9032 cm (hot) at 14.6411 psia
Beginning Smoothed SP Level is 77.1506 cm (cold) / 77.3257 cm (hot) at 15.0134 psia
Ending Smoothed SP Level is 78.1684 cm (cold) / 79.6268 cm (hot) at 42.7224 psia
Minimum Smoothed Cold SP Level is 76.8548 cm at t plus 5354.4412 s and 24.852 psia
Minimum Smoothed Hot SP Level is 77.324 cm at t plus 12.4987 s and 15.02 psia
Maximum Smoothed Cold SP Level is 78.2187 cm at t plus 8375.149 s and 40.3156 psia
Maximum Smoothed Hot SP Level is 79.6415 cm at t plus 8596.4497 s and 41.8829 psia
SP 12 Temperature at the beginning is 39.8782 C, and at the end is 116.5265 C
At plume detection, the Mixing Number is 44.2139
The Mixing Number ranges from a minimum of 34.9051 at (KEY POINT #12) t plus 0 s to a maximum of 207.4643 at (KEY POINT #13) t plus 8704.6538 s; it had a mean value of 88.3259 +/- 48.1948 over the test period.
Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m2-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m3) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam

Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 34.9051): 72.38472375 0.040894
0.00925 0.3937 0.7715058191 0.7732573834 0.3789396626
0.3789396626 0.9988639358 41.38887283 233587.7032 0.06954819604
0.05830516357 0.04175272278 0.05332001229 0.09507273507 40.29589145
103.1363424 103.1363424 40.3976587 40.25619674 40.47728475
38.25276641 4.178534214 4.22071023 2.090294903 0.6290104092
0.6789921879 0.6789921879 4.312614423 1.695238152 0.03810158895
992.1106211 956.0800328 0.6634788041 1.748893333 0.0006491940053
0.0002727155856 1.237657003e-005 1.267233186e-005 1531.837411
1542.063057 473.8436248 455.0073867 1.133075386 1.035136769
1.072136769 0.07501716378 0.07542426039 1285.967519 1284.254481
168.8659257 432.3392025 2680.49468 263.4732768 853.6283169
169.2911636 168.6985543 169.625477 160.3342155

KEY POINT #2 (t plus 1694.1349 s with a Mixing Number of 44.2139): 71.5942382
0.040894 0.00925 0.3937 0.7716700471 0.7749681899
0.4265937528 0.4265937528 0.9989876732 42.49725249 230199.3467
0.0669805974 0.05782027244 0.04406775194 0.04996673059 0.09403448253
55.68554134 105.6265975 105.6265975 57.68863303 55.66440626
55.44527848 53.83091602 4.181083372 4.224091406 2.101033055
0.646566396 0.6798870617 0.6798870617 3.223617539 1.652102188
0.03851047249 985.3809365 954.2428296 0.7194019006 1.68467922
0.0004985030407 0.0002659134934 1.246185629e-005 1.271843217e-005
1550.834439 1539.451151 475.0806583 458.8677045 1.235478968
1.127587454 1.164587454 0.1628643149 0.1790691158 1400.878241
1399.072225 233.1929313 442.8616153 2684.363286 209.668684
958.0166258 241.5687231 233.1031196 232.1899124 225.4445258

KEY POINT #3 (t plus 2592.5453 s with a Mixing Number of 50.9955): 70.96032712
0.040894 0.00925 0.3937 0.7702322694 0.7744926058
0.4358556812 0.4358556812 0.9989671539 40.67338695 227077.0639
0.06562707942 0.05747585568 0.04397430294 0.04922757767 0.09320188061
63.51077206 107.3868132 107.3868132 70.09155791 63.81125299
63.47939345 61.56438452 4.184345574 4.22656438 2.108941886
0.6540777413 0.6804743961 0.6804743961 2.832172626 1.62291426
0.0388091269 981.3809107 952.9275656 0.7611964825 1.74463777
0.0004427122573 0.0002612882477 1.252221191e-005 1.277914893e-005
1555.726299 1537.497049 475.9421898 459.8580185 1.312371085
1.210671457 1.247671457 0.2341946949 0.313243933 1426.868393
1425.214069 265.9297608 450.3047513 2687.075681 184.3749905
976.5636418 293.4779016 267.1856858 265.7999599 257.7915996

KEY POINT #4 (t plus 1010.5198 s with a Mixing Number of 39.9014): 69.80558008
0.040894 0.00925 0.3937 0.7718682175 0.7744954294
0.4177346517 0.4177346517 0.9989913034 42.1877068 225136.0388
0.06804508629 0.05805509738 0.04265658399 0.04902860976 0.09168519375
49.39689047 104.4223952 104.4223952 49.95159124 49.38424214
49.15637218 47.46783232 4.179407167 4.222439293 2.095775555
0.639852255 0.6794637227 0.6794637227 3.6078582 1.672684886
0.03831078455 988.3223913 955.1346967 0.6918994986 1.654642676
0.000552350157 0.0002691640117 1.242059925e-005 1.267957545e-005
1544.669849 1540.736715 474.4851104 458.0210714 1.185046753
1.081916249 1.118916249 0.1198632253 0.1232163025 1377.251379
1375.471576 206.9013789 437.7722241 2682.497071 230.8708452
939.4791546 209.2197295 206.8470477 205.8977172 198.8448792

KEY POINT #5 (t plus 1010.5198 s with a Mixing Number of 39.9014): 69.80558008
0.040894 0.00925 0.3937 0.7718682175 0.7744954294
0.4177346517 0.4177346517 0.9989913034 42.1877068 225136.0388
0.06804508629 0.05805509738 0.04265658399 0.04902860976 0.09168519375
49.39689047 104.4223952 104.4223952 49.95159124 49.38424214

49.15637218	47.46783232	4.179407167	4.222439293	2.095775555
0.639852255	0.6794637227	0.6794637227	3.6078582	1.672684886
0.03831078455	988.3223913	955.1346967	0.6918994986	1.654642676
0.000552350157	0.0002691640117	1.242059925e-005	1.267957545e-005	
1544.669849	1540.736715	474.4851104	458.0210714	1.185046753
1.081916249	1.118916249	0.1198632253	0.1232163025	1377.251379
1375.471576	206.9013789	437.7722241	2682.497071	230.8708452
939.4791546	209.2197295	206.8470477	205.8977172	198.8448792
KEY POINT #6 (t plus 5973.1176 s with a Mixing Number of 105.5813): 73.72536939				
0.040894	0.00925	0.3937	0.7698469542	0.7789155884
0.4477116739	0.4477116739	0.9985495911	29.75824235	227314.7072
0.06004652938	0.05503593498	0.04597649723	0.0508570907	0.09683358793
94.07068739	119.6635668	119.6635668	107.91297	94.55546099
90.77406136	86.33890701	4.209289256	4.245793256	2.172061155
0.6751510653	0.6835506638	0.6835506638	1.872693729	1.445582203
0.04113245438	962.5848346	943.3766046	1.110806625	2.477477282
0.0003003716516	0.0002327312271	1.294444055e-005	1.326322125e-005	
1550.215464	1521.498264	481.6421377	463.0894759	1.965579002
1.884203827	1.921203827	0.8175571537	1.336105712	1489.589513
1488.70396	394.1882734	502.3545624	2705.445202	108.166289
987.2349509	452.5733829	396.2276623	380.3192859	361.6803826
KEY POINT #7 (t plus 6452.215 s with a Mixing Number of 119.6125): 73.8167486				
0.040894	0.00925	0.3937	0.7744297915	0.7844841279
0.4470140955	0.4470140955	0.9984441407	27.86390108	226019.5536
0.0592538884	0.05458759277	0.04607451586	0.05087909286	0.09695360872
98.2216309	121.8847389	121.8847389	112.6878802	98.5711825
97.10985614	87.82559232	4.214180534	4.24965755	2.185069588
0.6770659849	0.6839202343	0.6839202343	1.787162136	1.417803929
0.04160106093	959.6777734	941.5789263	1.186070317	2.6491893
0.0002871321439	0.000228174808	1.302100743e-005	1.335575648e-005	
1546.903326	1518.179978	482.6135274	463.3963093	2.108159343
2.029390781	2.066390781	0.9514854172	1.56810049	1494.603002
1493.826605	411.6818491	511.7994588	2708.658922	100.1176098
982.8035429	472.7851524	413.1537151	406.9987504	367.9384676
KEY POINT #8 (t plus 7170.0251 s with a Mixing Number of 143.3749): 73.1003084				
0.040894	0.00925	0.3937	0.7810004279	0.7925446119
0.451705466	0.451705466	0.9983056439	25.19972088	221530.9732
0.0581163177	0.05387924063	0.04630769415	0.04970491588	0.09601261003
104.1079022	125.37345	125.37345	118.4393628	105.0399639
104.1668174	89.89440916	4.221749743	4.255977633	2.206541932
0.6794157073	0.6843873521	0.6843873521	1.678087095	1.37648451
0.04236915531	955.4206761	938.7127339	1.312548313	2.900838019
0.0002700583407	0.0002213471664	1.31413383e-005	1.349411312e-005	
1541.300812	1512.717636	484.1009077	464.2614903	2.349051777
2.274671655	2.311671655	1.172159407	1.890427505	1515.159085
1514.524059	436.5279041	526.6529194	2713.633626	90.12501536
988.5061652	497.1825892	440.4621683	436.7779657	376.6539036
KEY POINT #9 (t plus 7301.1276 s with a Mixing Number of 146.7069): 70.99360254				
0.040894	0.00925	0.3937	0.7815013969	0.7933019822
0.4682405445	0.4682405445	0.9983831791	24.88829082	215071.6004
0.0579395155	0.05374381516	0.04639272971	0.04685285605	0.09324558576
105.0155258	126.0376268	126.0376268	119.7274862	106.0667649
105.1617552	90.974623	4.222982344	4.25721623	2.210776092
0.6797407924	0.6844606932	0.6844606932	1.662425605	1.368923122
0.04251992864	954.7507266	938.1611817	1.337814512	2.852490075
0.0002675877866	0.0002200907867	1.316425483e-005	1.349881796e-005	
1540.347182	1511.643556	484.3787087	465.5889764	2.397355188
2.32391979	2.36091979	1.209670473	1.96956895	1553.249118
1552.629691	440.3638642	529.4833741	2714.570353	89.11950989
1023.765744	502.6537616	444.802738	440.982733	381.2001959
KEY POINT #10 (t plus 7477.3327 s with a Mixing Number of 152.8768): 70.9261623				
0.040894	0.00925	0.3937	0.7819201686	0.7940763129
0.4706506009	0.4706506009	0.9983566177	24.3710017	214340.5018
0.05766904282	0.05356367987	0.0463375885	0.04681941878	0.09315700729
106.4003588	126.919705	126.919705	120.9964548	107.6135128
106.7186523	100.9416601	4.224900692	4.258878965	2.216472473
0.6802170017	0.6845504285	0.6845504285	1.63908597	1.359026244

0.04272245385	953.7209695	937.4257701	1.371974369	2.910268654
0.0002638959411	0.0002184429295	1.319469312e-005	1.353199445e-005	
1538.844026	1510.20039	484.7449771	465.8958699	2.462751961
2.390255593	2.427255593	1.268808525	2.050159706	1561.063449
1560.469503	446.2182002	533.2437883	2715.809184	87.02558815
1027.819661	508.0475975	451.3434476	447.564352	423.1809089
KEY POINT #11 (t plus 8704.6538 s with a Mixing Number of 207.4643): 73.0539754				
0.040894	0.00925	0.3937	0.7816843232	0.796268037
0.4755433619	0.4755433619	0.9980418077	21.00047377	216388.3025
0.05566649909	0.05217389107	0.0471746867	0.0487770679	0.09595175459
116.5219815	133.6740265	133.6740265	129.1851853	117.6855719
117.1014808	115.33043	4.24024623	4.272302544	2.262891593
0.6830037205	0.6849500464	0.6849500464	1.486914672	1.288416039
0.04436205792	945.9378004	931.6847753	1.657509977	3.478682252
0.0002395069055	0.0002065632329	1.342786094e-005	1.380605715e-005	
1526.232874	1498.528999	487.447415	467.1520328	3.013101056
2.945602819	2.982602819	1.77745626	2.637382709	1591.133014
1590.691994	489.0968006	562.0914171	2725.092017	72.99461641
1029.041597	542.9324366	494.0306125	491.555568	484.0500103
KEY POINT #12 (t plus 0 s with a Mixing Number of 34.9051): 72.38472375 0.040894				
0.00925	0.3937	0.7715058191	0.7732573834	0.3789396626
0.3789396626	0.9988639358	41.38887283	233587.7032	0.06954819604
0.05830516357	0.04175272278	0.05332001229	0.09507273507	40.29589145
103.1363424	103.1363424	40.3976587	40.25619674	40.47728475
38.25276641	4.178534214	4.22071023	2.090294903	0.6290104092
0.6789921879	0.6789921879	4.312614423	1.695238152	0.03810158895
992.1106211	956.0800328	0.6634788041	1.748893333	0.0006491940053
0.0002727155856	1.237657003e-005	1.267233186e-005	1531.837411	
1542.063057	473.8436248	455.0073867	1.133075386	1.035136769
1.072136769	0.07501716378	0.07542426039	1285.967519	1284.254481
168.8659257	432.3392025	2680.49468	263.4732768	853.6283169
169.2911636	168.6985543	169.625477	160.3342155	
KEY POINT #13 (t plus 8704.6538 s with a Mixing Number of 207.4643): 73.0539754				
0.040894	0.00925	0.3937	0.7816843232	0.796268037
0.4755433619	0.4755433619	0.9980418077	21.00047377	216388.3025
0.05566649909	0.05217389107	0.0471746867	0.0487770679	0.09595175459
116.5219815	133.6740265	133.6740265	129.1851853	117.6855719
117.1014808	115.33043	4.24024623	4.272302544	2.262891593
0.6830037205	0.6849500464	0.6849500464	1.486914672	1.288416039
0.04436205792	945.9378004	931.6847753	1.657509977	3.478682252
0.0002395069055	0.0002065632329	1.342786094e-005	1.380605715e-005	
1526.232874	1498.528999	487.447415	467.1520328	3.013101056
2.945602819	2.982602819	1.77745626	2.637382709	1591.133014
1590.691994	489.0968006	562.0914171	2725.092017	72.99461641
1029.041597	542.9324366	494.0306125	491.555568	484.0500103
KEY POINT #14 (t plus 7229.9255 s with a Mixing Number of 145.0114): 72.63314203				
0.040894	0.00925	0.3937	0.781292134	0.7929693141
0.455251165	0.455251165	0.998314732	25.01756564	219992.6711
0.05803552189	0.05381786368	0.04632705556	0.04907196115	0.0953990167
104.5229076	125.6745755	125.6745755	119.5728558	105.4731304
104.8336481	90.52956651	4.222311133	4.256537771	2.208455778
0.6795655785	0.684421219	0.684421219	1.670889656	1.373044568
0.04243733066	955.1147952	938.4629034	1.323955443	2.903285758
0.0002689235966	0.0002207758717	1.315172795e-005	1.350163028e-005	
1540.867701	1512.232011	484.2270714	464.5737906	2.370852541
2.296880224	2.333880224	1.189190144	1.95992802	1523.796849
1523.170971	438.2817134	527.9360878	2714.058737	89.65437445
995.8607615	501.9953494	442.2932117	439.5951529	379.3264192

End

D.28 TEST #28 -

T28_RCIC_2ATM_107KW_COOLSTART_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T28_RCIC_2ATM_107kW_coolstart\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 3597.7018 s, and ending (KEY POINT #11) at t
plus 13818.2734 s, for a time period of 10220.5716 s.
Original Data Record Time: 14771.3649 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus
988.9186 s, $T_{bulk} = 39.3671$ C and $T_{out} = 36.6186$ C
Stratification Beginning SP12 Temperature = 39.2288 C
Stratification Beginning Pressure = 30.2005 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus
8556.5464 s, $T_{bulk} = 107.5201$ C and $T_{out} = 69.4124$ C
Stratification Ending SP12 Temperature = 107.4768 C
Stratification Ending Pressure = 30.1989 psia
Plume detected! Setting t_plume (KEY POINT #2) to 2149.3419 s.
At t = 2149.3419 s, the pool pressure is 30.292 psia while the Smoothed Upper, Mid, SP8,
Lower, and Outlet Temperatures are 50.3658, 50.2292, 52.237, 50.1444, and 45.916
C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9
temperatures were 11.2061 +/- 3.3388 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper
temperatures were 9.949 +/- 2.8621 C.
Minimum Steam Quality: 0.99388 at t plus 9.7956 s
Maximum Steam Quality: 1.0039 at t plus 8015.8345 s
Time-Averaged Steam Quality: 1.0008 +/- 0.0011507
Minimum Turbine Outlet Steam Quality: 1.0031 at t plus 9.7956 s
Maximum Turbine Outlet Steam Quality: 1.0144 at t plus 8015.8345 s
Time-Averaged Turbine Outlet Steam Quality: 1.011 +/- 0.0014241
Smoothed Changerates may not fully include test beginning and end periods, analysis
ending at t plus 10130.5724 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.84304 degrees/min at t plus 4342.7714 s
and 0.25094 degrees/min at t plus 8229.4657 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.83866 degrees/min at t plus
6041.0035 s and 0.28984 degrees/min at t plus 7939.6361 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.30693 degrees/min at t
plus 4342.7714 s and -0.21965 degrees/min at t plus 6041.1985 s, respectively
Max and min smoothed lower level changerates: 3.5154 degrees/min at t plus 7620.0298 s
and -0.1275 degrees/min at t plus 3923.8674 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.7054 degrees/min at t
plus 6677.1169 s and -3.1628 degrees/min at t plus 7620.0298 s, respectively
Max and min smoothed outlet level changerates: 6.6312 degrees/min at t plus 8815.8502 s
and -0.035251 degrees/min at t plus 4640.2784 s, respectively
Max and min smoothed lower-outlet level changerate differences: 3.4684 degrees/min at t
plus 7620.1308 s and -6.0936 degrees/min at t plus 8822.5106 s, respectively
Max and min smoothed hot (SP8) level changerates: 1.4076 degrees/min at t plus 3198.852
s and 0.038434 degrees/min at t plus 9621.9683 s, respectively
Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.90167 degrees/min
at t plus 3198.852 s and -0.42404 degrees/min at t plus 9049.9566 s, respectively
The mean steam flow rate was 44.5795 +/- 1.549 g/s
The mean feedwater flow rate was 43.8989 +/- 1.5794 g/s
The mean water injection to steam flow rate was 0.0074086 +/- 0.030317 g/s
Mean Smoothed Condensing Region SP8-SP9 delta T is 9.6494 +/- 4.7812 C over the
Stratification Period, beginning at 0.41912 C and ending at 11.3544 C
Mean Smoothed SP8-Upper Pool delta T is 8.5702 +/- 4.1794 C over the Stratification
Period, beginning at 0.27803 C and ending at 11.0314 C
The stratification period begins and ends with Smoothed SP8 readings of 40.0335 and
119.7256 C, respectively
The stratification period begins and ends with condensing flows of 0.27037 and 1.7594
kg/s, respectively.
The stratification period begins and ends with condensing+cooling flows of 61.7957 and
2.1312 kg/s, respectively.
The stratification period had a mean sparger steam enthalpy of 2733.7677 +/- 1.3241 kJ/kg.

At plume detection, the condensing and condensing+cooling flows are 0.31515 and 12.8641 kg/s, respectively

The plume period had a mean steam enthalpy of 2734.7211 +/- 0.88685 kJ/kg.

Maximum Smoothed Top-Mid delta T is 3.3234 degrees C at t plus 4804.1788 s with T_upper = 76.155 C and T_mid = 72.8316 C

At t plus 4804.1788 s, Smoothed SP8-SP9 is 15.2149 C and Smoothed SP8-Top is 11.8915 C, where Smoothed SP8 is 88.0465 C and Pool P = 30.1878 psia

Maximum Smoothed Top-Lower delta T is 20.5266 degrees C at t plus 7369.7245 s with T_upper = 102.1131 C and T_low = 81.5864 C

At t plus 7369.7245 s, Smoothed SP8-SP9 is 12.1172 C and Smoothed SP8-Top is 11.1705 C, where Smoothed SP8 is 113.2836 C and Pool P = 30.0455 psia

Maximum Smoothed Mid-Lower delta T is 19.58 degrees C at t plus 7369.6245 s with T_mid = 101.1654 C and T_low = 81.5855 C

At t plus 7369.6245 s, Smoothed SP8-SP9 is 12.1169 C and Smoothed SP8-Top is 11.1703 C, where Smoothed SP8 is 113.2823 C and Pool P = 30.0437 psia

Maximum Smoothed Top-Outlet delta T is 39.4123 degrees C at t plus 8521.0434 s with T_upper = 108.5898 C and T_out = 69.1775 C

At t plus 8521.0434 s, Smoothed SP8-SP9 is 11.4161 C and Smoothed SP8-Top is 11.0152 C, where Smoothed SP8 is 119.605 C and Pool P = 30.1743 psia

Maximum Smoothed Mid-Outlet delta T is 39.0214 degrees C at t plus 8530.3459 s with T_mid = 108.2429 C and T_out = 69.2215 C

At t plus 8530.3459 s, Smoothed SP8-SP9 is 11.2503 C and Smoothed SP8-Top is 10.8761 C, where Smoothed SP8 is 119.4932 C and Pool P = 30.1718 psia

Maximum Smoothed Lower-Outlet delta T is 39.1379 degrees C at t plus 8582.3509 s with T_low = 108.7916 C and T_out = 69.6537 C

At t plus 8582.3509 s, Smoothed SP8-SP9 is 11.4031 C and Smoothed SP8-Top is 11.0166 C, where Smoothed SP8 is 119.8361 C and Pool P = 30.2269 psia

Maximum Smoothed Condensing Region SP8-SP9 delta T is 15.5863 degrees C at (KEY POINT #14) t plus 4761.7814 s with T_SP8 = 88.0391 C and T_SP9 = 72.4528 C and Pool P = 30.1852 psia

Maximum Smoothed Condensing Region SP8-Upper delta T is 13.3846 degrees C at t plus 4176.5719 s with T_SP8 = 81.9147 C and T_upper = 68.5301 C and Pool P = 30.2939 psia

Maximum Top-Mid delta T is 4.5201 degrees C at (KEY POINT #4) t plus 4741.3802 s ignoring SP 4, with temperatures of 76.1137 and 71.5936 C, respectively, at Set # 2, where Pool P = 30.1821 psia and T_outlet = 61.8557 C

Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 6331.4071 s with a Smoothed Mid-Axis Top-Mid Delta T of 1.5067 C and a raw SP12 Reading of 89.78 C.

Maximum Top-Lower delta T is 23.2917 degrees C at t plus 7481.1269 s, with temperatures of 103.5597 and 80.2679 C, respectively, at Set # 1, where Pool P = 30.089 psia and T_outlet = 67.3451 C

Maximum Mid-Low delta T is 20.963 degrees C at (KEY POINT #6) t plus 7512.7287 s ignoring SP 4, with temperatures of 101.9496 and 80.9867 C, respectively, at Set # 2, where Pool P = 30.0895 psia and T_outlet = 67.4549 C

Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 7622.491 s with a Smoothed Mid-Axis Mid-Low Delta T of 6.9675 C and a raw SP12 Reading of 102.8631 C.

Maximum Top-Outlet delta T is 39.8142 degrees C at t plus 8521.9444 s, with temperatures of 108.9019 and 69.0877 C, respectively, at Set # 1, where Pool P = 30.1697 psia

Maximum Mid-Outlet delta T is 38.3183 degrees C at t plus 8550.145 s ignoring SP 4, with temperatures of 107.5931 and 69.2748 C, respectively, at Set # 2, where Pool P = 30.2107 psia

Maximum Lower-Outlet delta T is 39.5557 degrees C at (KEY POINT #8) t plus 8459.9459 s, with temperatures of 108.4633 and 68.9076 C, respectively, at Set # 1, where Pool P = 30.1467 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 8906.7504 s with a Smoothed Mid-Axis Low-Outlet Delta T of 13.1801 C and a raw SP12 Reading of 109.8526 C.

Minimum SP Pressure is 30.0287 psia at t plus 7405.8236 s

Maximum SP Pressure is 30.7579 psia at t plus 3677.8614 s

Beginning SP Pressure is 30.1169 psia

Ending SP Pressure is 30.6733 psia

Time-Average SP Pressure is 30.2926 +/- 0.14944 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 76.9272 cm (cold) / 76.9919 cm (hot) at 14.5072 psia

Beginning Smoothed SP Level is 78.7456 cm (cold) / 78.8526 cm (hot) at 30.1167 psia

Ending Smoothed SP Level is 78.0288 cm (cold) / 79.5634 cm (hot) at 30.655 psia

Minimum Smoothed Cold SP Level is 77.9996 cm at t plus 9856.5667 s and 30.3833 psia

Minimum Smoothed Hot SP Level is 78.85 cm at t plus 72.3011 s and 30.117 psia

Maximum Smoothed Cold SP Level is 78.7458 cm at t plus 6.4984 s and 30.1169 psia
 Maximum Smoothed Hot SP Level is 79.5638 cm at t plus 10220.0725 s and 30.6541 psia
 SP 12 Temperature at the beginning is 29.8523 C, and at the end is 120.1484 C
 At plume detection, the Mixing Number is 43.7322
 The Mixing Number ranges from a minimum of 35.9845 at (KEY POINT #12) t plus 0 s to a
 maximum of 1007.9707 at (KEY POINT #13) t plus 10220.5716 s; it had a mean value
 of 121.5386 +/- 143.845 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 35.9845): 31.6446924 0.040894
 0.00925 0.3937 0.787455978 0.788526287 1.00542564
 1 1 26.769384 97664.8441 0.0710780916 0.0545009661
 0.0415632926 1.33689853e-005 0.0415632926 30.7382055 127.801173
 122.312726 30.8779137 30.7843063 31.2783873 27.991711
 4.17951364 4.25041627 2.18763488 0.616157246 0.683984972
 0.683984972 5.32235029 1.41258604 0.0416931593 995.470697
 941.23011 1.20103447 1.18250278 0.000784637875 0.000227315999
 1.30357651e-005 1.32501932e-005 1512.94113 1517.52624 482.798529
 486.75611 2.1365783 2.07647465 2.11347465 0.0442998975
 0.0446544322 2721.90347 2721.18687 129.019485 513.620401
 2709.27405 384.600916 2208.28307 129.603396 129.210617
 131.278784 117.545138

KEY POINT #2 (t plus 2149.3419 s with a Mixing Number of 43.7322): 32.697841
 0.040894 0.00925 0.3937 0.786829762 0.789722033
 1.0105031 1 1 27.9118811 99339.4162
 0.0679054099 0.054464681 0.0429465364 9.99824197e-006 0.0429465364
 50.2291624 133.18003 122.491884 52.2370218 50.365793
 50.1444409 45.9159789 4.17934812 4.25073524 2.18871441
 0.640828231 0.684011452 0.684011452 3.55238967 1.41041444
 0.0417318871 987.989004 941.08386 1.2073436 1.17173949
 0.000544695374 0.000226958296 1.30419431e-005 1.34603721e-005 1545.77325
 1517.25121 482.875762 490.443865 2.14856701 2.08904351
 2.12604351 0.124924155 0.137893645 2733.36608 2732.58701
 210.466661 514.38276 2709.53115 303.916099 2218.98332
 218.858671 211.036224 210.114133 192.447611

KEY POINT #3 (t plus 988.9186 s with a Mixing Number of 38.9776): 32.1591952
 0.040894 0.00925 0.3937 0.787150606 0.788961015
 1.00932002 1 1 27.4402661 98076.4858
 0.0696589419 0.0544853078 0.0422390593 6.51506704e-006 0.0422390593
 39.6144184 131.864271 122.390047 40.0335347 39.7555084
 39.6102922 36.5769755 4.17828673 4.25055384 2.18810037
 0.628197406 0.683996445 0.683996445 4.37351909 1.41164791
 0.0417098608 992.414501 941.167008 1.2037541 1.17215173
 0.000657550216 0.000227161492 1.30384314e-005 1.34091073e-005 1530.84591
 1517.40764 482.831876 489.565843 2.14174569 2.08231864

2.11931864	0.0723396474	0.0739764028	2730.59951	2729.84654
166.111277	513.949413	2709.38504	347.838136	2216.6501
167.862463	166.699284	166.095634	153.425382	
KEY POINT #4 (t plus 4741.3802 s with a Mixing Number of 59.7026): 34.0677977				
0.040894	0.00925	0.3937	0.7844888949	0.7907880513
1.011197812	1	1	29.28787036	103331.4765
0.06403625486	0.05450082459	0.04474588749	5.042827596e-006	0.04474588749
72.48441432	133.725464	122.3134248	87.21517734	75.45274308
70.20394924	61.75105165	4.189502271	4.250417515	2.187639084
0.6616293469	0.6839850759	0.6839850759	2.473094419	1.412577556
0.0416933101	976.3936286	941.2295394	1.201059021	1.163336108
0.0003905647352	0.0002273146022	1.303578916e-005	1.348251826e-005	
1558.031936	1517.525164	482.7988302	490.8585728	2.136624945
2.081380299	2.118380299	0.3470918445	0.6307932334	2734.719332
2733.861553	303.5720358	513.6233745	2709.275058	210.0513387
2221.095958	365.3725099	316.0096155	294.0212456	258.6452929
KEY POINT #5 (t plus 6331.4071 s with a Mixing Number of 87.404): 34.52540051				
0.040894	0.00925	0.3937	0.7844225027	0.793362633
1.011488945	1	1	29.40302914	104537.845
0.06073591251	0.05443097573	0.04534691971	-1.481818066e-007	
0.04534691971	90.42577265	134.3559044	122.6582442	102.4743314
91.5162474	80.21679446	65.62081656	4.20521993	4.251032157
2.189719828	0.6733083686	0.6840357143	0.6840357143	1.954387456
1.408404592	0.04176794135	965.0848794	940.9479342	1.213225989
1.174208532	0.0003129219046	0.0002266270886	1.304767999e-005	1.350593873e-005
1552.732443	1516.995103	482.9473676	491.2065657	2.159748429
2.104593662	2.141593662	0.7132492597	1.107065677	2735.848762
2734.984224	378.870215	515.0907169	2709.769678	136.2205019
2220.758046	429.6205055	383.4552295	335.9923596	274.8392354
KEY POINT #6 (t plus 7512.7287 s with a Mixing Number of 130.6208): 34.71641681				
0.040894	0.00925	0.3937	0.782159809	0.793207967
1.01153386	1	1	29.95024108	105215.0321
0.0584952498	0.05451831595	0.04559780748	5.989831328e-006	0.04559780748
102.1561782	133.9899081	122.2270377	115.0341724	103.1690178
85.7987784	67.38697037	4.219183083	4.250263998	2.187119746
0.6786772919	0.6839721776	0.6839721776	1.712774124	1.413627312
0.04167467288	956.8429876	941.3000098	1.198026326	1.15928874
0.0002755085241	0.0002274874576	1.30328103e-005	1.349325397e-005	
1543.249686	1517.657492	482.7615456	491.0588545	2.130863595
2.074962834	2.111962834	1.094742489	1.693656357	2735.375169
2734.478152	428.2758845	513.2557984	2709.151005	84.97991388
2222.119371	482.7276868	432.5486522	359.4228136	282.2294441
KEY POINT #7 (t plus 7622.491 s with a Mixing Number of 134.3487): 34.75361592				
0.040894	0.00925	0.3937	0.7821283567	0.7933971144
1.011872606	1	1	29.99053981	105213.5812
0.05836577579	0.0545130284	0.04564666615	1.002202388e-005	0.04564666615
102.8240438	134.3650243	122.2531537	115.3671382	104.0084493
93.23483558	67.53569708	4.22006749	4.250310388	2.187276667
0.6789314683	0.6839760859	0.6839760859	1.700747476	1.413309774
0.04168030464	956.3546938	941.278709	1.1989425	1.159073712
0.0002736190793	0.000227435175	1.303371085e-005	1.350789844e-005	
1542.581619	1517.617507	482.7728202	491.3076518	2.132603993
2.076603265	2.113603265	1.120743308	1.712123342	2736.158071
2735.258639	431.0941466	513.3669203	2709.188513	82.27277372
2222.791151	484.1390103	436.092093	390.6864547	282.8521919
KEY POINT #8 (t plus 8459.9459 s with a Mixing Number of 173.1395): 34.94934702				
0.040894	0.00925	0.3937	0.7811717748	0.7933878768
1.01181609	1	1	30.11763294	105814.2055
0.05741096395	0.05450539346	0.04590374652	4.569947347e-006	0.04590374652
107.7176691	134.342612	122.2908613	119.3003745	108.262016
107.5028049	68.97373807	4.22685524	4.2503774	2.187503363
0.6806270464	0.6839817152	0.6839817152	1.617504459	1.412851575
0.04168843992	952.7144802	941.2479487	1.200266314	1.160543608
0.0002604577682	0.0002273597266	1.303501111e-005	1.350686885e-005	
1537.282823	1517.559745	482.7890946	491.2836549	2.135118914
2.078380619	2.115380619	1.327254893	1.943033128	2736.094502

2735.18743	451.7620714	513.5273659	2709.242662	61.76529452
2222.567136	500.8231895	454.061914	450.8552264	288.8730701
KEY POINT #9 (t plus 8556.5464 s with a Mixing Number of 179.8752): 34.95865339				
0.040894	0.00925	0.3937	0.7813213283	0.7936178006
1.011862028	1	1	30.07500685	105810.8909
0.05728264852	0.05449242955	0.04591596984	7.763053386e-006	0.04591596984
108.3711685	134.4512468	122.3548811	119.7256084	108.6941654
108.3229453	69.40459768	4.227801883	4.250491252	2.187888587
0.6808317192	0.6839912355	0.6839912355	1.607004433	1.412074402
0.04170226245	952.2203593	941.19571	1.202516581	1.16257875
0.000258786864	0.0002272317381	1.303721871e-005	1.351088872e-005	
1536.523527	1517.461595	482.8167125	491.3425124	2.139394269
2.082592361	2.119592361	1.357061646	1.969451644	2736.282572
2735.378066	454.5249315	513.7997757	2709.33457	59.2748442
2222.482797	502.6288145	455.8893302	454.3223724	290.6775661
KEY POINT #10 (t plus 8906.7504 s with a Mixing Number of 211.9435): 34.86332991				
0.040894	0.00925	0.3937	0.7815464539	0.7944454065
1.011737016	1	1	29.76698776	105498.6852
0.0567922359	0.05444355647	0.04579076851	1.844107905e-006	0.04579076851
110.8600019	134.5525896	122.5961555	120.7099794	111.1966996
111.2520209	96.50463179	4.231497357	4.250921262	2.189344248
0.6815642509	0.6840266961	0.6840266961	1.56825889	1.409153956
0.04175447481	950.320957	940.998678	1.211027879	1.171255024
0.000252598337	0.0002267505949	1.304553885e-005	1.35139221e-005	
1533.521071	1517.090767	482.9206555	491.3549496	2.15556979
2.099010519	2.136010519	1.475671127	2.031734819	2736.327794
2735.44172	465.0529716	514.8264887	2709.680681	49.77351704
2221.501305	506.8103095	466.4765584	466.7132163	404.4579698
KEY POINT #11 (t plus 10220.5716 s with a Mixing Number of 1007.9707): 36.75326781				
0.040894	0.00925	0.3937	0.7802883115	0.7956340204
1.012138596	1	1	31.20530889	111019.5717
0.05482057778	0.05439647514	0.04827308184	5.863811308e-006	0.04827308184
120.7317695	135.1889862	122.8284713	122.8370324	120.917936
120.8604594	116.7488664	4.247624677	4.251336693	2.190751621
0.6837441611	0.6840602146	0.6840602146	1.432080027	1.406354623
0.04180492623	942.5133635	940.8087265	1.219269016	1.177932012
0.0002305232762	0.0002262891214	1.305355045e-005	1.353804659e-005	
1519.929093	1516.732328	483.020527	491.7327475	2.171238803
2.113586827	2.150586827	2.033131503	2.171817992	2737.621795
2736.648023	506.9038867	515.8151831	2710.013536	8.911296413
2221.806612	2710.26356	507.6934884	507.4517858	490.0042161
KEY POINT #12 (t plus 0 s with a Mixing Number of 35.9845): 31.6446924				
0.00925	0.3937	0.787455978	0.788526287	1.00542564
1	1	26.769384	97664.8441	0.0710780916
0.0415632926	1.33689853e-005	0.0415632926	30.7382055	127.801173
122.312726	30.8779137	30.7843063	31.2783873	27.991711
4.17951364	4.25041627	2.18763488	0.616157246	0.683984972
0.683984972	5.32235029	1.41258604	0.0416931593	995.470697
941.23011	1.20103447	1.18250278	0.000784637875	0.000227315999
1.30357651e-005	1.32501932e-005	1512.94113	1517.52624	482.798529
486.75611	2.1365783	2.07647465	2.11347465	0.0442998975
0.0446544322	2721.90347	2721.18687	129.019485	513.620401
2709.27405	384.600916	2208.28307	129.603396	129.210617
131.278784	117.545138			
KEY POINT #13 (t plus 10220.5716 s with a Mixing Number of 1007.9707): 36.75326781				
0.040894	0.00925	0.3937	0.7802883115	0.7956340204
1.012138596	1	1	31.20530889	111019.5717
0.05482057778	0.05439647514	0.04827308184	5.863811308e-006	0.04827308184
120.7317695	135.1889862	122.8284713	122.8370324	120.917936
120.8604594	116.7488664	4.247624677	4.251336693	2.190751621
0.6837441611	0.6840602146	0.6840602146	1.432080027	1.406354623
0.04180492623	942.5133635	940.8087265	1.219269016	1.177932012
0.0002305232762	0.0002262891214	1.305355045e-005	1.353804659e-005	
1519.929093	1516.732328	483.020527	491.7327475	2.171238803
2.113586827	2.150586827	2.033131503	2.171817992	2737.621795
2736.648023	506.9038867	515.8151831	2710.013536	8.911296413
2221.806612	2710.26356	507.6934884	507.4517858	490.0042161

KEY POINT #14 (t plus 4761.7814 s with a Mixing Number of 59.6698): 34.07064259

0.040894	0.00925	0.3937	0.7844765921	0.7908128175
1.011203794	1	1	29.29222799	103338.5904
0.0640419317	0.05450109571	0.04474962407	5.449893174e-006	0.04474962407
72.45279463	133.7303582	122.3120859	88.03908103	75.72519598
70.34500822	61.88135511	4.189480506	4.250415134	2.187631029
0.6616048973	0.6839848766	0.6839848766	2.474220019	1.412593812
0.04169302106	976.4120973	941.2306319	1.201011972	1.163270747
0.0003907300868	0.0002273172794	1.303574299e-005	1.348271592e-005	
1558.030346	1517.527217	482.7982525	490.8622226	2.136535556
2.081245916	2.118245916	0.3466252317	0.6511523615	2734.730842
2733.872807	303.4395545	513.6176775	2709.273136	210.178123
2221.113165	368.8348157	317.1516585	294.6119932	259.1903823

End

D.29 TEST #29 -

T29_RCIC_040GPM_2ATM_107KW_COOLSTART_RESULTS_RCICLAND

.TXT

Output Saved to C:\Local
Files\RCICLAND_NOTITLES\Export\T29_RCIC_040GPM_2ATM_107kW_coolstart\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 2421.3895 s, and ending (KEY POINT #11) at t plus 11903.9429 s, for a time period of 9482.5534 s.
Original Data Record Time: 12783.2642 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 686.2982 s, T_bulk = 41.237 C and T_out = 38.2616 C
Stratification Beginning SP12 Temperature = 41.1185 C
Stratification Beginning Pressure = 30.4162 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 7919.0259 s, T_bulk = 106.5178 C and T_out = 67.3287 C
Stratification Ending SP12 Temperature = 106.3929 C
Stratification Ending Pressure = 30.1945 psia
Plume detected! Setting t_plume (KEY POINT #2) to 542.398 s.
At t = 542.398 s, the pool pressure is 30.47 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 40.594, 40.7242, 42.7248, 40.7346, and 37.0169 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 11.1358 +/- 3.1852 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 9.7558 +/- 2.9322 C.
Minimum Steam Quality: 0.5427 at t plus 1266.8364 s
Maximum Steam Quality: 0.69186 at t plus 9342.5534 s
Time-Averaged Steam Quality: 0.58277 +/- 0.024407
Minimum Turbine Outlet Steam Quality: 0.56487 at t plus 1266.8364 s
Maximum Turbine Outlet Steam Quality: 0.71497 at t plus 9342.5534 s
Time-Averaged Turbine Outlet Steam Quality: 0.60572 +/- 0.025005
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 9392.5532 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.71102 degrees/min at t plus 3165.8401 s and 0.23849 degrees/min at t plus 7474.5195 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.8017 degrees/min at t plus 4929.674 s and 0.30623 degrees/min at t plus 7376.5179 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.30098 degrees/min at t plus 3331.3465 s and -0.24691 degrees/min at t plus 4698.7737 s, respectively
Max and min smoothed lower level changerates: 3.6305 degrees/min at t plus 6834.4069 s and -0.22265 degrees/min at t plus 2371.5286 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.73399 degrees/min at t plus 2371.5286 s and -3.2396 degrees/min at t plus 6834.5029 s, respectively

Max and min smoothed outlet level changerates: 7.3879 degrees/min at t plus 8150.8062 s and 0.062581 degrees/min at t plus 3286.646 s, respectively
 Max and min smoothed lower-outlet level changerate differences: 3.4692 degrees/min at t plus 6834.5029 s and -6.7515 degrees/min at t plus 8148.7341 s, respectively
 Max and min smoothed hot (SP8) level changerates: 1.2922 degrees/min at t plus 1628.7421 s and 0.031968 degrees/min at t plus 8797.9542 s, respectively
 Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.74072 degrees/min at t plus 1628.7421 s and -0.49716 degrees/min at t plus 4584.9672 s, respectively
 The mean steam flow rate was 44.4372 +/- 1.3231 g/s
 The mean feedwater flow rate was 43.8014 +/- 1.3563 g/s
 The mean water injection to steam flow rate was 24.967 +/- 0.98627 g/s
 Mean Smoothed Condensing Region SP8-SP9 delta T is 11.3136 +/- 2.9542 C over the Stratification Period, beginning at 2.0677 C and ending at 12.0317 C
 Mean Smoothed SP8-Upper Pool delta T is 9.9079 +/- 2.7536 C over the Stratification Period, beginning at 2.043 C and ending at 11.5869 C
 The stratification period begins and ends with Smoothed SP8 readings of 44.0852 and 119.1462 C, respectively
 The stratification period begins and ends with condensing flows of 0.25209 and 1.4972 kg/s, respectively.
 The stratification period begins and ends with condensing+cooling flows of 12.3975 and 1.8759 kg/s, respectively.
 The stratification period had a mean sparger steam enthalpy of 1832.8194 +/- 29.4297 kJ/kg.
 At plume detection, the condensing and condensing+cooling flows are 0.24798 and 12.8708 kg/s, respectively
 The plume period had a mean steam enthalpy of 1832.1684 +/- 30.1413 kJ/kg.
 Maximum Smoothed Top-Mid delta T is 3.475 degrees C at t plus 3790.0518 s with T_upper = 72.0414 C and T_mid = 68.5664 C
 At t plus 3790.0518 s, Smoothed SP8-SP9 is 13.1252 C and Smoothed SP8-Top is 9.6502 C, where Smoothed SP8 is 81.6916 C and Pool P = 30.0906 psia
 Maximum Smoothed Top-Lower delta T is 20.9753 degrees C at t plus 6689.3046 s with T_upper = 100.4795 C and T_low = 79.5042 C
 At t plus 6689.3046 s, Smoothed SP8-SP9 is 13.5815 C and Smoothed SP8-Top is 12.8731 C, where Smoothed SP8 is 113.3527 C and Pool P = 30.3847 psia
 Maximum Smoothed Mid-Lower delta T is 20.2768 degrees C at t plus 6649.2033 s with T_mid = 99.471 C and T_low = 79.1943 C
 At t plus 6649.2033 s, Smoothed SP8-SP9 is 13.7733 C and Smoothed SP8-Top is 13.1036 C, where Smoothed SP8 is 113.2444 C and Pool P = 30.3735 psia
 Maximum Smoothed Top-Outlet delta T is 40.2664 degrees C at t plus 7868.225 s with T_upper = 107.3852 C and T_out = 67.1188 C
 At t plus 7868.225 s, Smoothed SP8-SP9 is 12.1177 C and Smoothed SP8-Top is 11.624 C, where Smoothed SP8 is 119.0091 C and Pool P = 30.158 psia
 Maximum Smoothed Mid-Outlet delta T is 39.8618 degrees C at t plus 7890.5253 s with T_mid = 107.0386 C and T_out = 67.1769 C
 At t plus 7890.5253 s, Smoothed SP8-SP9 is 12.023 C and Smoothed SP8-Top is 11.646 C, where Smoothed SP8 is 119.0616 C and Pool P = 30.1835 psia
 Maximum Smoothed Lower-Outlet delta T is 39.7363 degrees C at t plus 7876.3265 s with T_low = 106.8678 C and T_out = 67.1315 C
 At t plus 7876.3265 s, Smoothed SP8-SP9 is 12.1113 C and Smoothed SP8-Top is 11.6469 C, where Smoothed SP8 is 119.0276 C and Pool P = 30.1566 psia
 Maximum Smoothed Condensing Region SP8-SP9 delta T is 15.2782 degrees C at (KEY POINT #14) t plus 3452.1455 s with T_SP8 = 80.6975 C and T_SP9 = 65.4193 C and Pool P = 30.144 psia
 Maximum Smoothed Condensing Region SP8-Upper delta T is 13.6966 degrees C at t plus 6438.9993 s with T_SP8 = 112.007 C and T_upper = 98.3103 C and Pool P = 30.3471 psia
 Maximum Top-Mid delta T is 4.5032 degrees C at (KEY POINT #4) t plus 3779.2502 s ignoring SP 4, with temperatures of 72.887 and 68.3839 C, respectively, at Set # 2, where Pool P = 30.0883 psia and T_outlet = 55.1907 C
 Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 5512.7823 s with a Smoothed Mid-Axis Top-Mid Delta T of 1.5009 C and a raw SP12 Reading of 88.1274 C.
 Maximum Top-Lower delta T is 24.6725 degrees C at t plus 6864.2076 s, with temperatures of 101.6049 and 76.9323 C, respectively, at Set # 1, where Pool P = 30.2516 psia and T_outlet = 64.4505 C

Maximum Mid-Low delta T is 22.9288 degrees C at (KEY POINT #6) t plus 6779.0087 s ignoring SP 4, with temperatures of 100.3888 and 77.46 C, respectively, at Set # 2, where Pool P = 30.2924 psia and T_outlet = 64.306 C
 Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 6907.4091 s with a Smoothed Mid-Axis Mid-Low Delta T of 7.6348 C and a raw SP12 Reading of 101.2453 C.
 Maximum Top-Outlet delta T is 40.589 degrees C at t plus 7885.227 s, with temperatures of 107.6631 and 67.0741 C, respectively, at Set # 1, where Pool P = 30.1835 psia
 Maximum Mid-Outlet delta T is 39.2762 degrees C at t plus 7879.6287 s ignoring SP 4, with temperatures of 106.3925 and 67.1163 C, respectively, at Set # 2, where Pool P = 30.171 psia
 Maximum Lower-Outlet delta T is 40.5239 degrees C at (KEY POINT #8) t plus 7897.6257 s, with temperatures of 107.66 and 67.1361 C, respectively, at Set # 1, where Pool P = 30.1844 psia
 Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 8227.6366 s with a Smoothed Mid-Axis Low-Outlet Delta T of 13.5078 C and a raw SP12 Reading of 108.2521 C.
 Minimum SP Pressure is 30.0661 psia at t plus 3906.3534 s
 Maximum SP Pressure is 30.7716 psia at t plus 0.095 s
 Beginning SP Pressure is 30.7714 psia
 Ending SP Pressure is 30.6327 psia
 Time-Average SP Pressure is 30.3084 +/- 0.1357 psia
 SP Levels are fully corrected and compensated
 Pre-Start SP Level is 77.6254 cm (cold) / 77.7354 cm (hot) at 14.9529 psia
 Beginning Smoothed SP Level is 79.3256 cm (cold) / 79.4734 cm (hot) at 30.7753 psia
 Ending Smoothed SP Level is 78.4509 cm (cold) / 79.9593 cm (hot) at 30.6398 psia
 Minimum Smoothed Cold SP Level is 78.4361 cm at t plus 8964.7437 s and 30.2278 psia
 Minimum Smoothed Hot SP Level is 79.3541 cm at t plus 1164.0076 s and 30.2738 psia
 Maximum Smoothed Cold SP Level is 79.3261 cm at t plus 1.5891 s and 30.7742 psia
 Maximum Smoothed Hot SP Level is 79.963 cm at t plus 9422.855 s and 30.6347 psia
 SP 12 Temperature at the beginning is 34.8532 C, and at the end is 118.5262 C
 At plume detection, the Mixing Number is 40.4185
 The Mixing Number ranges from a minimum of 38.3773 at (KEY POINT #12) t plus 0 s to a maximum of 583.4237 at (KEY POINT #13) t plus 9482.5534 s; it had a mean value of 113.3299 +/- 99.1442 over the test period.
 Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m2-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m3) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11
 KEY POINT #1 (t plus 0 s with a Mixing Number of 38.3773): 51.61938384 0.040894
 0.00925 0.3937 0.7932564766 0.7947342414 0.5868551578
 0.5868551578 0.9990816679 24.68923522 159225.3684 0.07034558419
 0.05434626122 0.04366747656 0.02413130405 0.06779878061 35.35368584
 123.0761222 123.0761222 36.22099008 35.39245315 35.58442203
 33.33701237 4.178601485 4.251781049 2.19225813 0.6225949036
 0.6840952704 0.6840952704 4.792192796 1.403384126 0.04185890043
 993.9621641 940.605982 1.228103912 2.090764796 0.0007140175541
 0.0002257991256 1.306209128e-005 1.325745453e-005 1522.918193
 1516.348739 483.1267616 471.7915116 2.188044249 2.121881199

2.158881199	0.0573965824	0.0602000977	1804.74482	1804.135262
148.3117326	516.8692535	2710.367924	368.5575209	1287.875567
151.935807	148.4721994	149.2774996	139.8902388	
KEY POINT #2 (t plus 542.398 s with a Mixing Number of 40.4185): 51.28695416				
0.040894	0.00925	0.3937	0.7920800712	0.793987005
0.5744083845	0.5744083845	0.9990430608	24.24283087	158230.0388
0.06947846325	0.05441309924	0.04238613268	0.02497602266	0.06736215534
40.72419355	122.7464548	122.7464548	42.7248134	40.59399978
40.73459913	37.01691815	4.178271373	4.251189874	2.190254118
0.6296066732	0.6840484513	0.6840484513	4.274004634	1.40734148
0.04178709498	991.9903877	940.8758131	1.216354424	2.115551374
0.0006440323279	0.0002264518378	1.3050722e-005	1.325493389e-005	
1532.724721	1516.859025	482.9852923	471.128454	2.165696465
2.101140773	2.138140773	0.07674339216	0.08526843347	1776.552799
1775.965084	170.7498922	515.466124	2709.89607	344.7162318
1261.086675	179.109063	170.2044031	170.7949616	155.2653368
KEY POINT #3 (t plus 686.2982 s with a Mixing Number of 40.9697): 51.14460326				
0.040894	0.00925	0.3937	0.7917913134	0.7938306137
0.575828478	0.575828478	0.9990501853	24.27443902	157830.4865
0.06926728228	0.05442434812	0.04229689891	0.02487828756	0.06717518648
42.01755417	122.6909496	122.6909496	44.0852386	42.04225952
42.42583275	38.276308	4.178296981	4.25109061	2.189917829
0.6312213286	0.6840404471	0.6840404471	4.162534591	1.408010218
0.04177503992	991.4832383	940.9211981	1.214385146	2.106932449
0.0006288400817	0.000226562082	1.304880786e-005	1.32516059e-005	
1534.813687	1516.944673	482.9854322	471.181127	2.1619522
2.096978914	2.133978914	0.08216585225	0.09152103728	1779.524638
1778.93539	176.1535483	515.2299031	2709.816547	339.0763548
1264.294735	184.7930538	176.2552764	177.861045	160.527153
KEY POINT #4 (t plus 3779.2502 s with a Mixing Number of 58.2357): 52.91184064				
0.040894	0.00925	0.3937	0.7891938375	0.7950549434
0.601095449	0.601095449	0.9991528273	26.47098274	163690.7537
0.06475212379	0.05449237775	0.04443841982	0.02505792066	0.06949634049
68.47474203	122.3551369	122.3551369	82.18995367	71.87441763
65.13728686	54.93148523	4.186905951	4.250491707	2.187890127
0.6584171999	0.6839912734	0.6839912734	2.623236294	1.412071299
0.04170231771	978.6932233	941.1955012	1.202525579	1.998861968
0.0004125203468	0.000227231227	1.303722753e-005	1.321868684e-005	
1557.499127	1517.461203	482.8168228	472.2292458	2.139411366
2.074579069	2.111579069	0.2919896802	0.5177886107	1834.227117
1833.526404	286.7782673	513.8008642	2709.334937	227.0225968
1320.426253	344.2685301	301.0146443	272.8093969	230.1262248
KEY POINT #5 (t plus 5512.7823 s with a Mixing Number of 87.4956): 53.07010672				
0.040894	0.00925	0.3937	0.7883994802	0.7970683337
0.606009545	0.606009545	0.9991649094	26.60721043	164129.1807
0.06114123039	0.05445092153	0.04464206782	0.0250621451	0.06970421293
88.26713918	122.5598037	122.5598037	100.1653134	89.3271145
74.93662202	60.84324562	4.202975751	4.250856381	2.18912454
0.6721284592	0.6840213958	0.6840213958	2.006000555	1.409593108
0.04174659617	966.5302044	941.02838	1.209742416	1.994576127
0.0003207941568	0.0002268229643	1.304428527e-005	1.322280983e-005	
1553.984128	1517.146732	482.9050092	472.4963984	2.15312633
2.088224968	2.125224968	0.6568837521	1.020177418	1845.544488
1844.836544	369.7938555	514.671791	2709.628561	144.8779355
1330.872697	419.8796437	374.2481655	313.8496954	254.8484434
KEY POINT #6 (t plus 6779.0087 s with a Mixing Number of 129.16): 52.80108413				
0.040894	0.00925	0.3937	0.7872182389	0.7981209898
0.6173351977	0.6173351977	0.9992032713	26.94982351	163390.1536
0.05882997271	0.05444675092	0.04495793161	0.02439293723	0.06935086884
100.4247128	122.580389	122.580389	114.1007998	101.3567555
84.06056191	64.32434071	4.216932083	4.250893118	2.189248939
0.6779937123	0.6840243991	0.6840243991	1.744749959	1.409344388
0.04175105716	958.1008501	941.0115611	1.210470211	1.959236731
0.0002805189836	0.0002267819777	1.304499515e-005	1.321528554e-005	
1544.922675	1517.115044	482.91387	472.9763724	2.154509733
2.08833131	2.12533131	1.029647699	1.642757849	1870.473899

1869.747606	420.9734778	514.7593928	2709.658077	93.78591498
1355.714506	478.7736918	424.9031234	352.1238848	269.4122751
KEY POINT #7 (t plus 6907.4091 s with a Mixing Number of 133.6578): 52.87329607				
0.040894	0.00925	0.3937	0.7869133958	0.79804722
0.6163495364	0.6163495364	0.9992008082	26.97196513	163621.7151
0.05867343587	0.05445403177	0.04494099579	0.02450471884	0.06944571463
101.2353299	122.5444516	122.5444516	114.8876533	101.9853803
92.31076105	64.55557651	4.217976827	4.25082899	2.189031794
0.678318562	0.6840191528	0.6840191528	1.72963767	1.409778661
0.04174327015	957.5141445	941.040922	1.209199871	1.960305666
0.0002781535758	0.0002268535403	1.304375586e-005	1.321463088e-005	
1544.151519	1517.170357	482.8984	472.9255679	2.15209509
2.085808582	2.122808582	1.05971228	1.685581983	1868.221233
1867.493746	424.3920264	514.60646	2709.606547	90.2144336
1353.614773	482.107529	427.5548171	386.7988607	270.3796979
KEY POINT #8 (t plus 7897.6257 s with a Mixing Number of 177.7726): 53.48734038				
0.040894	0.00925	0.3937	0.7855636453	0.7978241553
0.613797252	0.613797252	0.9991935521	27.21822585	165526.2206
0.05754835964	0.05446570826	0.04518883044	0.02506339237	0.07025222281
107.0168519	122.4868124	122.4868124	119.1186582	107.4672096
106.8028952	67.20661634	4.225849245	4.250726205	2.188683802
0.6804022275	0.6840107077	0.6840107077	1.628924908	1.410475806
0.04173078943	953.2432305	941.0880018	1.207164643	1.965129567
0.0002622725212	0.0002269684068	1.30417682e-005	1.321428889e-005	
1538.085003	1517.259004	482.8735774	472.8036064	2.148226898
2.080895024	2.117895024	1.29589119	1.93183231	1862.486845
1861.746013	448.8003606	514.3611792	2709.52388	65.56081866
1348.125665	500.0519859	450.7023997	447.8975688	281.4749362
KEY POINT #9 (t plus 7919.0259 s with a Mixing Number of 178.8376): 53.82352507				
0.040894	0.00925	0.3937	0.7855951359	0.7978771977
0.6092714002	0.6092714002	0.9991777497	27.17801401	166518.9246
0.05752923197	0.05446321964	0.04518751595	0.0255062641	0.07069378005
107.1144836	122.4990977	122.4990977	119.1462322	107.5593338
107.0005947	67.36716224	4.225988454	4.250748105	2.188757945
0.6804339666	0.6840125109	0.6840125109	1.627324759	1.410327152
0.04173344868	953.1698498	941.0779683	1.207598201	1.980406848
0.0002620184728	0.000226943915	1.304219185e-005	1.321807259e-005	
1537.974334	1517.240116	482.8788692	472.6177024	2.149050892
2.081656951	2.118656951	1.300223534	1.93352854	1852.580839
1851.842195	449.2129997	514.413458	2709.541502	65.20045832
1338.167381	500.1690868	451.0918235	448.7330389	282.1470738
KEY POINT #10 (t plus 8227.6366 s with a Mixing Number of 203.3194): 54.69693197				
0.040894	0.00925	0.3937	0.78582987	0.7986176845
0.606751811	0.606751811	0.9991642209	27.35173209	169103.6924
0.05709810698	0.05442441375	0.04520691391	0.02663403061	0.07184094452
109.3093397	122.6906258	122.6906258	120.2053698	109.6702226
109.6687926	94.6569311	4.229176821	4.251090031	2.189915868
0.6811168625	0.6840404003	0.6840404003	1.592175534	1.408014122
0.04177496962	951.5085784	940.9214629	1.214373664	1.999761178
0.0002564228573	0.0002265627255	1.304879669e-005	1.322724716e-005	
1535.413353	1516.945172	482.961293	472.5642494	2.16193037
2.093847077	2.130847077	1.400814048	1.999609326	1847.546617
1846.7985	458.4927922	515.2285249	2709.816083	56.73573275
1332.318092	504.6668045	460.0178852	460.014386	396.6769497
KEY POINT #11 (t plus 9482.5534 s with a Mixing Number of 583.4237): 53.7204065				
0.040894	0.00925	0.3937	0.7845087997	0.7995926354
0.6947403698	0.6947403698	0.9994281523	30.48507654	166669.6897
0.0551810531	0.05436408253	0.04874604206	0.0218122983	0.07055834036
118.9424089	122.9882434	122.9882434	122.4884303	119.176448
119.1291505	116.2077451	4.244523212	4.251623192	2.191722809
0.6834338266	0.6840829106	0.6840829106	1.454862826	1.404436601
0.04183972494	943.9614	940.6779558	1.224962961	1.76218703
0.0002342553966	0.000225972772	1.305906052e-005	1.318081475e-005	
1522.586218	1516.485031	483.0890914	475.9570751	2.182068751
2.112538085	2.149538085	1.92101894	2.148335395	2041.509158
2040.579818	499.3060988	516.4952038	2710.242221	17.18910502
1525.013954	514.3681475	500.2983279	500.1000233	487.7095958

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KEY POINT #12 (t plus 0 s with a Mixing Number of 38.3773): 51.61938384      0.040894
0.00925      0.3937      0.7932564766      0.7947342414      0.5868551578
0.5868551578      0.9990816679      24.68923522      159225.3684      0.07034558419
0.05434626122      0.04366747656      0.02413130405      0.06779878061      35.35368584
123.0761222      123.0761222      36.22099008      35.39245315      35.58442203
33.33701237      4.178601485      4.251781049      2.19225813      0.6225949036
0.6840952704      0.6840952704      4.792192796      1.403384126      0.04185890043
993.9621641      940.605982      1.228103912      2.090764796      0.0007140175541
0.0002257991256      1.306209128e-005      1.325745453e-005      1522.918193
1516.348739      483.1267616      471.7915116      2.188044249      2.121881199
2.158881199      0.0573965824      0.0602000977      1804.74482      1804.135262
148.3117326      516.8692535      2710.367924      368.5575209      1287.875567
151.935807      148.4721994      149.2774996      139.8902388
KEY POINT #13 (t plus 9482.5534 s with a Mixing Number of 583.4237): 53.7204065
0.040894      0.00925      0.3937      0.7845087997      0.7995926354
0.6947403698      0.6947403698      0.9994281523      30.48507654      166669.6897
0.0551810531      0.05436408253      0.04874604206      0.0218122983      0.07055834036
118.9424089      122.9882434      122.9882434      122.9884303      119.176448
119.1291505      116.2077451      4.244523212      4.251623192      2.191722809
0.6834338266      0.6840829106      0.6840829106      1.454862826      1.404436601
0.04183972494      943.9614      940.6779558      1.224962961      1.76218703
0.0002342553966      0.000225972772      1.305906052e-005      1.318081475e-005
1522.586218      1516.485031      483.0890914      475.9570751      2.182068751
2.112538085      2.149538085      1.92101894      2.148335395      2041.509158
2040.579818      499.3060988      516.4952038      2710.242221      17.18910502
1525.013954      514.3681475      500.2983279      500.1000233      487.7095958
KEY POINT #14 (t plus 3452.1455 s with a Mixing Number of 55.4679): 52.91740319
0.040894      0.00925      0.3937      0.7894573864      0.7948432033
0.5992279607      0.5992279607      0.9991446419      26.34457172      163661.4614
0.06529216246      0.05447999258      0.04437189128      0.02513175526      0.06950364654
65.41933003      122.4162908      122.4162908      80.6975432      68.65102938
63.48493482      53.77164539      4.18515054      4.25060056      2.188258507
0.6558162391      0.6840003238      0.6840003238      2.748467845      1.411329808
0.04171553383      980.3861871      941.1455847      1.2046783      2.008664394
0.0004306869796      0.0002271090948      1.303933633e-005      1.322244264e-005
1556.631008      1517.36735      482.8431896      472.1652043      2.143501874
2.078614769      2.115614769      0.2551453655      0.4876992607      1830.277188
1829.583151      273.9886114      514.0610864      2709.422704      240.072475
1316.216101      338.0059213      287.5153112      265.8953657      225.2779473

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End

D.30 TEST #30 -

T30_RCIC_080GPM_57KW_COOLSTART_RESULTS_RCICLAND.TXT

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Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T30_RCIC_080GPM_57kW_coolstart\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 2203.474 s, and ending (KEY POINT #11) at t
plus 20182.1884 s, for a time period of 17978.7144 s.
Original Data Record Time: 22790.5595 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus
5335.5922 s, T_bulk = 55.5341 C and T_out = 53.0125 C
Stratification Beginning SP12 Temperature = 55.3239 C
Stratification Beginning Pressure = 17.4069 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus
13152.6443 s, T_bulk = 92.4014 C and T_out = 69.3727 C
Stratification Ending SP12 Temperature = 92.3024 C
Stratification Ending Pressure = 27.9687 psia
Plume detected! Setting t_plume (KEY POINT #2) to 3516.9612 s.
At t = 3516.9612 s, the pool pressure is 16.2641 psia while the Smoothed Upper, Mid, SP8,
Lower, and Outlet Temperatures are 47.5369, 47.2643, 49.2782, 47.5057, and
45.3062 C, respectively.

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Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 11.3906 +/- 4.409 C.

Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 10.8656 +/- 4.3628 C.

Minimum Steam Quality: 0.17554 at t plus 45.5286 s
Maximum Steam Quality: 0.30659 at t plus 17511.5326 s
Time-Averaged Steam Quality: 0.2401 +/- 0.029898
Minimum Turbine Outlet Steam Quality: 0.20004 at t plus 46.4067 s
Maximum Turbine Outlet Steam Quality: 0.31816 at t plus 17511.5326 s
Time-Averaged Turbine Outlet Steam Quality: 0.26127 +/- 0.025091
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 17888.8122 s; using 300 s smoothing

Max and min smoothed upper level changerates: 0.41347 degrees/min at t plus 7413.231 s and 0.15204 degrees/min at t plus 12456.6285 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.35502 degrees/min at t plus 7484.4301 s and 0.20614 degrees/min at t plus 12964.3235 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.1197 degrees/min at t plus 5012.1877 s and -0.10849 degrees/min at t plus 6272.4088 s, respectively
Max and min smoothed lower level changerates: 1.5163 degrees/min at t plus 10824.8982 s and -0.0086167 degrees/min at t plus 7619.7588 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.31882 degrees/min at t plus 7541.0333 s and -1.2499 degrees/min at t plus 10824.8982 s, respectively
Max and min smoothed outlet level changerates: 2.3593 degrees/min at t plus 13515.3351 s and -0.071645 degrees/min at t plus 8405.6438 s, respectively
Max and min smoothed lower-outlet level changerate differences: 1.4504 degrees/min at t plus 10824.9892 s and -2.084 degrees/min at t plus 13518.0372 s, respectively
Max and min smoothed hot (SP8) level changerates: 0.93189 degrees/min at t plus 7355.6277 s and -0.10359 degrees/min at t plus 14853.6576 s, respectively
Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.61636 degrees/min at t plus 7355.6277 s and -0.40199 degrees/min at t plus 8603.5471 s, respectively

The mean steam flow rate was 23.2712 +/- 0.79276 g/s
The mean feedwater flow rate was 23.0286 +/- 0.8109 g/s
The mean water injection to steam flow rate was 49.8132 +/- 0.91985 g/s
Mean Smoothed Condensing Region SP8-SP9 delta T is 13.1511 +/- 2.6857 C over the Stratification Period, beginning at 5.6683 C and ending at 15.1888 C
Mean Smoothed SP8-Upper Pool delta T is 12.5868 +/- 2.7378 C over the Stratification Period, beginning at 5.078 C and ending at 14.6728 C
The stratification period begins and ends with Smoothed SP8 readings of 61.4696 and 107.6154 C, respectively
The stratification period begins and ends with condensing flows of 0.19641 and 0.36325 kg/s, respectively.
The stratification period begins and ends with condensing+cooling flows of 2.2983 and 0.71181 kg/s, respectively.
The stratification period had a mean sparger steam enthalpy of 1049.0672 +/- 15.0896 kJ/kg.

At plume detection, the condensing and condensing+cooling flows are 0.16529 and 6.6239 kg/s, respectively
The plume period had a mean steam enthalpy of 1037.8013 +/- 27.4779 kJ/kg.
Maximum Smoothed Top-Mid delta T is 1.1354 degrees C at t plus 16775.2245 s with T_upper = 108.9385 C and T_mid = 107.8032 C
At t plus 16775.2245 s, Smoothed SP8-SP9 is 13.1269 C and Smoothed SP8-Top is 11.9916 C, where Smoothed SP8 is 120.9301 C and Pool P = 36.8361 psia
Maximum Smoothed Top-Lower delta T is 9.4607 degrees C at t plus 10442.7803 s with T_upper = 81.9627 C and T_low = 72.502 C
At t plus 10442.7803 s, Smoothed SP8-SP9 is 15.0273 C and Smoothed SP8-Top is 14.6305 C, where Smoothed SP8 is 96.5932 C and Pool P = 23.4475 psia
Maximum Smoothed Mid-Lower delta T is 9.0729 degrees C at t plus 10444.2864 s with T_mid = 81.5728 C and T_low = 72.4999 C
At t plus 10444.2864 s, Smoothed SP8-SP9 is 15.0588 C and Smoothed SP8-Top is 14.6842 C, where Smoothed SP8 is 96.6316 C and Pool P = 23.4519 psia
Maximum Smoothed Top-Outlet delta T is 24.0711 degrees C at t plus 12943.7224 s with T_upper = 92.1655 C and T_out = 68.0944 C
At t plus 12943.7224 s, Smoothed SP8-SP9 is 15.3027 C and Smoothed SP8-Top is 14.7665 C, where Smoothed SP8 is 106.932 C and Pool P = 27.6062 psia
Maximum Smoothed Mid-Outlet delta T is 23.5371 degrees C at t plus 12941.9273 s with T_mid = 91.6242 C and T_out = 68.0871 C

At t plus 12941.9273 s, Smoothed SP8-SP9 is 15.2672 C and Smoothed SP8-Top is 14.7385 C, where Smoothed SP8 is 106.8914 C and Pool P = 27.605 psia
Maximum Smoothed Lower-Outlet delta T is 23.2967 degrees C at t plus 12950.1247 s with T_low = 91.4378 C and T_out = 68.1412 C
At t plus 12950.1247 s, Smoothed SP8-SP9 is 15.2654 C and Smoothed SP8-Top is 14.7128 C, where Smoothed SP8 is 106.9165 C and Pool P = 27.618 psia
Maximum Smoothed Condensing Region SP8-SP9 delta T is 16.1228 degrees C at (KEY POINT #14) t plus 12191.4123 s with T_SP8 = 104.892 C and T_SP9 = 88.7692 C and Pool P = 26.3161 psia
Maximum Smoothed Condensing Region SP8-Upper delta T is 15.6608 degrees C at t plus 12191.4123 s with T_SP8 = 104.892 C and T_upper = 89.2312 C and Pool P = 26.3161 psia
Maximum Top-Mid delta T is 1.3333 degrees C at (KEY POINT #4) t plus 2083.2402 s ignoring SP 4, with temperatures of 41.2251 and 39.8918 C, respectively, at Set # 2, where Pool P = 15.5929 psia and T_outlet = 38.845 C
Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 2083.2402 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.87451 C and a raw SP12 Reading of 39.8918 C.
Maximum Top-Lower delta T is 11.2421 degrees C at t plus 10759.8935 s, with temperatures of 83.766 and 72.5239 C, respectively, at Set # 1, where Pool P = 23.967 psia and T_outlet = 65.4585 C
Maximum Mid-Low delta T is 10.1362 degrees C at (KEY POINT #6) t plus 10686.0862 s ignoring SP 4, with temperatures of 82.4498 and 72.3136 C, respectively, at Set # 2, where Pool P = 23.8429 psia and T_outlet = 65.4195 C
Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 11029.4949 s with a Smoothed Mid-Axis Mid-Low Delta T of 3.377 C and a raw SP12 Reading of 84.01 C.
Maximum Top-Outlet delta T is 24.4647 degrees C at t plus 12881.3238 s, with temperatures of 92.3755 and 67.9109 C, respectively, at Set # 1, where Pool P = 27.4961 psia
Maximum Mid-Outlet delta T is 23.5644 degrees C at t plus 12922.2261 s ignoring SP 4, with temperatures of 91.4505 and 67.8861 C, respectively, at Set # 2, where Pool P = 27.5643 psia
Maximum Lower-Outlet delta T is 24.1744 degrees C at (KEY POINT #8) t plus 12900.1239 s, with temperatures of 92.2558 and 68.0814 C, respectively, at Set # 1, where Pool P = 27.5365 psia
Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 13699.6426 s with a Smoothed Mid-Axis Low-Outlet Delta T of 8.0547 C and a raw SP12 Reading of 94.352 C.
Minimum SP Pressure is 14.925 psia at t plus 10.7026 s
Maximum SP Pressure is 40.8153 psia at t plus 17976.9253 s
Beginning SP Pressure is 14.9295 psia
Ending SP Pressure is 40.8146 psia
Time-Average SP Pressure is 23.3253 +/- 7.3439 psia
SP Levels are fully corrected and compensated
Pre-Start SP Level is 77.1382 cm (cold) / 77.2197 cm (hot) at 14.6029 psia
Beginning Smoothed SP Level is 77.6995 cm (cold) / 77.8002 cm (hot) at 14.9309 psia
Ending Smoothed SP Level is 78.9924 cm (cold) / 80.4052 cm (hot) at 40.8193 psia
Minimum Smoothed Cold SP Level is 77.3953 cm at t plus 10615.4882 s and 23.729 psia
Minimum Smoothed Hot SP Level is 77.7365 cm at t plus 3076.854 s and 16.0403 psia
Maximum Smoothed Cold SP Level is 79.0062 cm at t plus 17225.5983 s and 38.2605 psia
Maximum Smoothed Hot SP Level is 80.4069 cm at t plus 17949.9147 s and 40.7204 psia
SP 12 Temperature at the beginning is 29.8168 C, and at the end is 112.9885 C
At plume detection, the Mixing Number is 39.8935
The Mixing Number ranges from a minimum of 30.2892 at (KEY POINT #12) t plus 0 s to a maximum of 222.6332 at (KEY POINT #13) t plus 17978.7144 s; it had a mean value of 88.3793 +/- 52.6148 over the test period.
Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m2-s) g1, Sparger Diameter (m) d1, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vf1, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) md1, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m3) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam

Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 30.2892): 56.95591238 0.040894
0.00925 0.3937 0.7769951224 0.7780023228 0.2049962995
0.2049962995 0.9974288322 18.40175324 179006.6465 0.07112475445
0.05855346127 0.02215293418 0.05265503756 0.07480797173 30.44163519
101.8555658 101.8555658 30.73900902 30.60077491 30.78287799
28.69206289 4.179875241 4.219024305 2.084971587 0.6156755065
0.678502554 0.678502554 5.360423464 1.7183048 0.03789734629
995.5148047 957.014117 0.6361268311 3.095135101 0.000789564578
0.0002763373973 1.233275619e-005 1.301155642e-005 1512.082966
1543.335556 473.1992278 431.8513333 1.083203125 1.029447646
1.066447646 0.04355539483 0.04430192944 888.8309391 888.4923146
127.6845771 426.9307822 2678.491096 299.2462051 461.9001569
128.9275523 128.3482109 129.1125536 120.3768921

KEY POINT #2 (t plus 3516.9612 s with a Mixing Number of 39.8935): 55.19298357
0.040894 0.00925 0.3937 0.7752555653 0.7776907489
0.2397336965 0.2397336965 0.9977206111 19.27128767 173604.5635
0.06840129971 0.05808750599 0.0224592477 0.05003322907 0.07249247677
47.26431198 104.2559384 104.2559384 49.27821725 47.53692459
47.50572445 45.3062175 4.17902222 4.222213445 2.095058431
0.6374361397 0.679403823 0.679403823 3.755333451 1.67557036
0.03828347294 989.2613594 955.2574705 0.6881661001 2.864000814
0.0005728098901 0.0002696189861 1.241489855e-005 1.30011667e-005
1542.102424 1540.91111 474.4023978 438.6885783 1.178211169
1.121453697 1.158453697 0.1076906648 0.119156121 975.6830616
975.3116791 197.9923229 437.0688828 2682.238436 239.0765599
538.6141789 206.4088135 199.1301063 199.0027579 189.815173

KEY POINT #3 (t plus 5335.5922 s with a Mixing Number of 46.9918): 54.82921649
0.040894 0.00925 0.3937 0.7754163643 0.7788044915
0.2539324454 0.2539324454 0.9977537515 19.09152109 171879.7106
0.06696079705 0.05772395357 0.02279875002 0.0492159418 0.07201469182
55.80135967 106.119568 106.119568 61.46963658 56.39164762
55.87077062 53.00367442 4.181106078 4.224777023 2.103220986
0.6466879905 0.6800553118 0.6800553118 3.217098108 1.643821721
0.03859329769 985.3247898 953.8758594 0.7309140899 2.871914513
0.0004975857277 0.000264603241 1.247875391e-005 1.304508817e-005
1550.940752 1538.912808 475.3230232 441.0580751 1.25662891
1.200006437 1.237006437 0.1637658888 0.2134239057 1014.164339
1013.799853 233.6833294 444.9456959 2685.124796 211.2623665
569.2186433 257.3890714 236.150003 233.975073 221.9925539

KEY POINT #4 (t plus 2083.2402 s with a Mixing Number of 35.4803): 55.86745454
0.040894 0.00925 0.3937 0.7766152805 0.7784227918
0.2266843735 0.2266843735 0.9976414423 19.15849104 175884.3354
0.06951492442 0.05831311387 0.02231691075 0.05106144077 0.07337835152
40.50032392 103.0953923 103.0953923 41.20744002 40.95573348
40.88005788 38.80015699 4.178523081 4.22065577 2.090122634
0.6292711254 0.6789768428 0.6789768428 4.294322014 1.695966196
0.0380949959 992.0315436 956.1100123 0.6625897077 2.916067577
0.0006467100443 0.0002728300615 1.237516863e-005 1.298946652e-005
1532.186448 1542.104493 473.8231069 436.3203098 1.131451985
1.075352216 1.112352216 0.07583688012 0.07873212918 942.179726
941.8126782 169.7237132 432.1662441 2680.430764 262.4425309
510.0134819 172.6784146 171.6251497 171.3120318 162.6251034

KEY POINT #5 (t plus 2083.2402 s with a Mixing Number of 35.4803): 55.86745454
0.040894 0.00925 0.3937 0.7766152805 0.7784227918
0.2266843735 0.2266843735 0.9976414423 19.15849104 175884.3354
0.06951492442 0.05831311387 0.02231691075 0.05106144077 0.07337835152
40.50032392 103.0953923 103.0953923 41.20744002 40.95573348

40.88005788	38.80015699	4.178523081	4.22065577	2.090122634
0.6292711254	0.6789768428	0.6789768428	4.294322014	1.695966196
0.0380949959	992.0315436	956.1100123	0.6625897077	2.916067577
0.0006467100443	0.0002728300615	1.237516863e-005	1.298946652e-005	
1532.186448	1542.104493	473.8231069	436.3203098	1.131451985
1.075352216	1.112352216	0.07583688012	0.07873212918	942.179726
941.8126782	169.7237132	432.1662441	2680.430764	262.4425309
510.0134819	172.6784146	171.6251497	171.3120318	162.6251034
KEY POINT #6 (t plus 10686.0862 s with a Mixing Number of 89.7776): 55.9626866				
0.040894	0.00925	0.3937	0.7739801112	0.7811046688
0.2585312297	0.2585312297	0.9970789935	15.00017441	170052.4764
0.06218037776	0.0559566424	0.02341527953	0.05008815326	0.07350343279
82.67773936	115.0693335	115.0693335	98.10316741	83.09160971
74.96262041	65.38045016	4.197707797	4.238182616	2.146742609
0.6687688906	0.6826060358	0.6826060358	2.152013393	1.506969503
0.04021164302	970.1467049	947.0275029	0.96735458	3.730802395
0.0003428536904	0.0002427140526	1.278621392e-005	1.345783463e-005	
1556.395022	1527.95808	479.5737739	441.2377324	1.695598722
1.644117303	1.681117303	0.527954306	0.9474259494	1055.936016
1055.711011	346.2819547	482.8469277	2698.687867	136.564973
573.0890881	411.1535268	348.0179981	313.9228275	273.7951381
KEY POINT #7 (t plus 11029.4949 s with a Mixing Number of 93.5363): 56.30264141				
0.040894	0.00925	0.3937	0.7740220113	0.7814137458
0.2577510938	0.2577510938	0.9970022245	14.72888212	170616.2536
0.06190561403	0.05581656944	0.02355366766	0.05039627417	0.07394994183
84.16354061	115.7711973	115.7711973	99.25793142	84.53114482
81.54718217	65.81600161	4.199061894	4.239312513	2.150474769
0.6696978711	0.6827661799	0.6827661799	2.111359169	1.497231732
0.04034819334	969.1965722	946.4756541	0.9882421502	3.822601129
0.000336735389	0.0002411379645	1.281037203e-005	1.349484688e-005	
1555.847455	1527.006979	479.8948587	441.022747	1.734754543
1.683571141	1.720571141	0.5599554652	0.9876156513	1056.678075
1056.461135	352.5230264	485.8247471	2699.729562	133.3017208
570.8533277	416.0236377	354.0653468	341.5413288	275.6213266
KEY POINT #8 (t plus 12900.1239 s with a Mixing Number of 115.7613): 55.65684625				
0.040894	0.00925	0.3937	0.7766321077	0.7854125707
0.2600221681	0.2600221681	0.9966893073	13.18339808	166568.4601
0.06054310975	0.05509358056	0.02362844675	0.04947328418	0.07310173093
91.44849588	119.3772306	119.3772306	105.986528	92.01565467
91.2333894	67.98508439	4.206365626	4.245303972	2.170421112
0.6738346996	0.6834989092	0.6834989092	1.930805773	1.449250314
0.04107317533	964.3824116	943.6068059	1.101391712	4.221737516
0.0003093035755	0.000233330997	1.29345731e-005	1.366423793e-005	
1552.042347	1521.916875	481.515546	441.03629	1.947786407
1.897931794	1.934931794	0.7413289525	1.250891899	1074.371893
1074.198091	383.1556288	501.1376558	2705.028345	117.982027
573.2342374	444.4336399	385.540174	382.252225	284.7188458
KEY POINT #9 (t plus 13152.6443 s with a Mixing Number of 119.494): 56.54583692				
0.040894	0.00925	0.3937	0.7776949126	0.7866962506
0.2551285464	0.2551285464	0.996552995	12.95476221	168694.8508
0.06035825522	0.05499544804	0.02363321724	0.05063614644	0.07426936368
92.42661194	119.8645701	119.8645701	107.6153837	92.9425614
92.5187384	69.38536616	4.207431052	4.246137928	2.173217443
0.6743379389	0.6835864323	0.6835864323	1.908727674	1.443019324
0.04117422027	963.7166478	943.2147966	1.117454495	4.364868766
0.0003059176656	0.0002323119145	1.295136777e-005	1.370750467e-005	
1551.39439	1521.20315	481.7308172	440.014325	1.978148258
1.92841095	1.96541095	0.7690393072	1.322638735	1065.304641
1065.136815	387.2728075	503.2088997	2705.737481	115.9360921
562.0957412	451.3187379	389.4424732	387.6618106	290.5844062
KEY POINT #10 (t plus 13699.6426 s with a Mixing Number of 125.9496): 56.2006634				
0.040894	0.00925	0.3937	0.780510294	0.7900521412
0.2722201049	0.2722201049	0.9967357761	13.29716992	167784.9397
0.0599607914	0.05477415557	0.02367830071	0.05013769948	0.07381600019
94.52171363	120.9617188	120.9617188	109.1611881	95.25928609
94.60524108	86.16711783	4.209780703	4.248036848	2.179601995
0.6753750274	0.6837735083	0.6837735083	1.863000053	1.429203655

0.04140443145	962.2755718	942.3285317	1.154309776	4.22651314
0.0002988810582	0.0002300478155	1.298918491e-005	1.369771288e-005	
1549.901677	1519.574132	482.2121503	443.1197692	2.047918392
1.997704557	2.034704557	0.8313032162	1.393828739	1106.785968
1106.609153	396.0955563	507.8734781	2707.327757	111.7779218
598.9124894	457.8592362	399.1995939	396.4485667	360.9675751
KEY POINT #11 (t plus 17978.7144 s with a Mixing Number of 222.6332):				56.62461293
0.040894	0.00925	0.3937	0.7899237898	0.8040518497
0.3082379359	0.3082379359	0.9962135263	11.08578704	164101.0007
0.05634888756	0.05253057691	0.02491916468	0.04945366628	0.07437283096
113.0982131	131.9490016	131.9490016	124.9167751	114.1361116
113.8531733	112.1344495	4.234772387	4.268755511	2.250561699
0.6822005151	0.6848960599	0.6848960599	1.534984846	1.305615967
0.04392809906	948.6230236	933.169441	1.580419459	5.107856818
0.000247278332	0.0002094782025	1.336829911e-005	1.411086411e-005	
1530.827029	1501.612954	486.7745333	448.1608166	2.8639031
2.814390816	2.851390816	1.58948918	2.316301191	1223.1102
1222.987305	474.5792804	554.7146869	2722.756126	80.13540656
668.3955129	524.7441738	478.9741617	477.7780975	470.5032459
KEY POINT #12 (t plus 0 s with a Mixing Number of 30.2892):				56.95591238
0.00925	0.3937	0.7769951224	0.7780023228	0.2049962995
0.2049962995	0.9974288322	18.40175324	179006.6465	0.07112475445
0.05855346127	0.02215293418	0.05265503756	0.07480797173	30.44163519
101.8555658	101.8555658	30.73900902	30.60077491	30.78287799
28.69206289	4.179875241	4.219024305	2.084971587	0.6156755065
0.678502554	0.678502554	5.360423464	1.7183048	0.03789734629
995.5148047	957.014117	0.6361268311	3.095135101	0.000789564578
0.0002763373973	1.233275619e-005	1.301155642e-005	1512.082966	
1543.335556	473.1992278	431.8513333	1.083203125	1.029447646
1.066447646	0.04355539483	0.04430192944	888.8309391	888.4923146
127.6845771	426.9307822	2678.491096	299.2462051	461.9001569
128.9275523	128.3482109	129.1125536	120.3768921	
KEY POINT #13 (t plus 17978.7144 s with a Mixing Number of 222.6332):				56.62461293
0.040894	0.00925	0.3937	0.7899237898	0.8040518497
0.3082379359	0.3082379359	0.9962135263	11.08578704	164101.0007
0.05634888756	0.05253057691	0.02491916468	0.04945366628	0.07437283096
113.0982131	131.9490016	131.9490016	124.9167751	114.1361116
113.8531733	112.1344495	4.234772387	4.268755511	2.250561699
0.6822005151	0.6848960599	0.6848960599	1.534984846	1.305615967
0.04392809906	948.6230236	933.169441	1.580419459	5.107856818
0.000247278332	0.0002094782025	1.336829911e-005	1.411086411e-005	
1530.827029	1501.612954	486.7745333	448.1608166	2.8639031
2.814390816	2.851390816	1.58948918	2.316301191	1223.1102
1222.987305	474.5792804	554.7146869	2722.756126	80.13540656
668.3955129	524.7441738	478.9741617	477.7780975	470.5032459
KEY POINT #14 (t plus 12191.4123 s with a Mixing Number of 106.859):				56.47477422
0.040894	0.00925	0.3937	0.7745828627	0.7827992936
0.2558202449	0.2558202449	0.9967539814	13.7053415	169656.5151
0.06104715772	0.05536674004	0.02362994431	0.05054608303	0.07417602733
88.76920108	118.0180441	118.0180441	104.8920043	89.23117024
88.16798741	67.09580228	4.203550702	4.243008758	2.162749752
0.6723932429	0.6832403736	0.6832403736	1.993792399	1.466941841
0.04079525532	966.182699	944.6947178	1.057575967	4.120639694
0.0003189238412	0.0002362177287	1.288774416e-005	1.361267745e-005	
1553.653428	1523.875148	480.910408	440.3969687	1.865113666
1.814780668	1.851780668	0.6696497137	1.204508005	1060.319914
1060.132078	371.8829063	495.3632247	2703.04172	123.4803184
564.9566897	439.8045866	373.8236095	369.3572589	280.9891261

End

D.31 TEST #31 -

T31_RCIC_STD_32KW_COOLSTART_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T31_RCIC_STD_32kW_coolstart\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 2098.074 s, and ending (KEY POINT #11) at t
plus 33496.2229 s, for a time period of 31398.1489 s.
Original Data Record Time: 33936.8281 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus
1785.2331 s, T_bulk = 39.6457 C and T_out = 37.5095 C
Stratification Beginning SP12 Temperature = 39.4586 C
Stratification Beginning Pressure = 14.8741 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus
24369.6199 s, T_bulk = 96.8123 C and T_out = 70.2051 C
Stratification Ending SP12 Temperature = 96.6826 C
Stratification Ending Pressure = 29.3707 psia
Plume detected! Setting t_plume (KEY POINT #2) to 8700.9447 s.
At t = 8700.9447 s, the pool pressure is 17.0445 psia while the Smoothed Upper, Mid, SP8,
Lower, and Outlet Temperatures are 57.8431, 57.647, 59.6496, 57.826, and 54.8411
C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9
temperatures were 9.1649 +/- 3.2151 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper
temperatures were 8.7328 +/- 3.1822 C.
Minimum Steam Quality: 0.97819 at t plus 30952.3414 s
Maximum Steam Quality: 1.0121 at t plus 4513.2741 s
Time-Averaged Steam Quality: 0.9978 +/- 0.0052489
Minimum Turbine Outlet Steam Quality: 0.97902 at t plus 30952.3414 s
Maximum Turbine Outlet Steam Quality: 1.0149 at t plus 4896.7931 s
Time-Averaged Turbine Outlet Steam Quality: 0.99981 +/- 0.005897
Smoothed Changerates may not fully include test beginning and end periods, analysis
ending at t plus 31308.1447 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.25507 degrees/min at t plus 20567.4534 s
and 0.045959 degrees/min at t plus 20785.0578 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.19846 degrees/min at t plus
11272.1907 s and 0.096896 degrees/min at t plus 11455.6932 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.11527 degrees/min at t
plus 20568.5555 s and -0.082531 degrees/min at t plus 20807.3551 s, respectively
Max and min smoothed lower level changerates: 0.77139 degrees/min at t plus 18260.1144 s
and -0.10524 degrees/min at t plus 14062.8384 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.26889 degrees/min at t
plus 14062.9404 s and -0.62679 degrees/min at t plus 18260.1144 s, respectively
Max and min smoothed outlet level changerates: 1.0021 degrees/min at t plus 26303.4505 s
and -0.051996 degrees/min at t plus 16183.2856 s, respectively
Max and min smoothed lower-outlet level changerate differences: 0.76157 degrees/min at t
plus 18260.0134 s and -0.82459 degrees/min at t plus 26309.7528 s, respectively
Max and min smoothed hot (SP8) level changerates: 0.71492 degrees/min at t plus
14038.342 s and -0.18381 degrees/min at t plus 20538.3537 s, respectively
Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.55299 degrees/min
at t plus 14038.342 s and -0.35225 degrees/min at t plus 14272.1433 s,
respectively
The mean steam flow rate was 13.0481 +/- 1.678 g/s
The mean feedwater flow rate was 12.9251 +/- 1.0638 g/s
The mean water injection to steam flow rate was 0.0080696 +/- 0.028074 g/s
Mean Smoothed Condensing Region SP8-SP9 delta T is 6.5608 +/- 4.7612 C over the
Stratification Period, beginning at -0.17248 C and ending at 10.5221 C
Mean Smoothed SP8-Upper Pool delta T is 6.2063 +/- 4.6492 C over the Stratification
Period, beginning at -0.39035 C and ending at 9.9383 C
The stratification period begins and ends with Smoothed SP8 readings of 39.6888 and
107.4244 C, respectively
The stratification period begins and ends with condensing flows of 0.10439 and 0.28054
kg/s, respectively.
The stratification period begins and ends with condensing+cooling flows of -41.56 and
0.66621 kg/s, respectively.

The stratification period had a mean sparger steam enthalpy of 2696.2221 +/- 1.5699 kJ/kg. At plume detection, the condensing and condensing+cooling flows are 0.14268 and 3.6798 kg/s, respectively

The plume period had a mean steam enthalpy of 2696.8901 +/- 0.87338 kJ/kg.

Maximum Smoothed Top-Mid delta T is 0.75585 degrees C at t plus 29905.9155 s with T_upper = 110.0453 C and T_mid = 109.2894 C

At t plus 29905.9155 s, Smoothed SP8-SP9 is 8.8729 C and Smoothed SP8-Top is 8.117 C, where Smoothed SP8 is 118.1623 C and Pool P = 36.9998 psia

Maximum Smoothed Top-Lower delta T is 7.9672 degrees C at t plus 17544.2995 s with T_upper = 81.594 C and T_low = 73.6268 C

At t plus 17544.2995 s, Smoothed SP8-SP9 is 11.7292 C and Smoothed SP8-Top is 11.2546 C, where Smoothed SP8 is 92.8486 C and Pool P = 22.6633 psia

Maximum Smoothed Mid-Lower delta T is 7.4926 degrees C at t plus 17544.2005 s with T_mid = 81.1191 C and T_low = 73.6265 C

At t plus 17544.2005 s, Smoothed SP8-SP9 is 11.7328 C and Smoothed SP8-Top is 11.2582 C, where Smoothed SP8 is 92.8519 C and Pool P = 22.6623 psia

Maximum Smoothed Top-Outlet delta T is 27.7072 degrees C at t plus 23726.3071 s with T_upper = 96.1003 C and T_out = 68.3931 C

At t plus 23726.3071 s, Smoothed SP8-SP9 is 10.212 C and Smoothed SP8-Top is 9.5637 C, where Smoothed SP8 is 105.664 C and Pool P = 28.6505 psia

Maximum Smoothed Mid-Outlet delta T is 27.0832 degrees C at t plus 23893.1126 s with T_mid = 95.7958 C and T_out = 68.7126 C

At t plus 23893.1126 s, Smoothed SP8-SP9 is 10.9947 C and Smoothed SP8-Top is 10.4773 C, where Smoothed SP8 is 106.7905 C and Pool P = 28.8354 psia

Maximum Smoothed Lower-Outlet delta T is 27.2708 degrees C at t plus 24069.6127 s with T_low = 96.5325 C and T_out = 69.2617 C

At t plus 24069.6127 s, Smoothed SP8-SP9 is 10.2955 C and Smoothed SP8-Top is 9.7132 C, where Smoothed SP8 is 106.48 C and Pool P = 29.0298 psia

Maximum Smoothed Condensing Region SP8-SP9 delta T is 12.9435 degrees C at (KEY POINT #14) t plus 20075.5453 s with T_SP8 = 100.2562 C and T_SP9 = 87.3127 C and Pool P = 24.9855 psia

Maximum Smoothed Condensing Region SP8-Upper delta T is 12.51 degrees C at t plus 20075.5453 s with T_SP8 = 100.2562 C and T_upper = 87.7462 C and Pool P = 24.9855 psia

Maximum Top-Mid delta T is 1.0492 degrees C at (KEY POINT #4) t plus 4918.4833 s ignoring SP 4, with temperatures of 48.2987 and 47.2495 C, respectively, at Set # 2, where Pool P = 15.686 psia and T_outlet = 45.5399 C

Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 4918.4833 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.62768 C and a raw SP12 Reading of 47.2495 C.

Maximum Top-Lower delta T is 9.2105 degrees C at t plus 18013.7083 s, with temperatures of 82.4772 and 73.2667 C, respectively, at Set # 1, where Pool P = 23.0954 psia and T_outlet = 67.6531 C

Maximum Mid-Low delta T is 8.3812 degrees C at (KEY POINT #6) t plus 17588.201 s ignoring SP 4, with temperatures of 81.0458 and 72.6646 C, respectively, at Set # 2, where Pool P = 22.7017 psia and T_outlet = 67.6774 C

Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 18411.8171 s with a Smoothed Mid-Axis Mid-Low Delta T of 2.7924 C and a raw SP12 Reading of 83.1785 C.

Maximum Top-Outlet delta T is 28.0253 degrees C at t plus 23966.8098 s, with temperatures of 96.672 and 68.6467 C, respectively, at Set # 1, where Pool P = 28.9211 psia

Maximum Mid-Outlet delta T is 27.1363 degrees C at t plus 23561.7057 s ignoring SP 4, with temperatures of 94.9386 and 67.8023 C, respectively, at Set # 2, where Pool P = 28.4729 psia

Maximum Lower-Outlet delta T is 27.9004 degrees C at (KEY POINT #8) t plus 23750.5085 s, with temperatures of 96.2528 and 68.3524 C, respectively, at Set # 1, where Pool P = 28.6776 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 26532.8566 s with a Smoothed Mid-Axis Low-Outlet Delta T of 9.2992 C and a raw SP12 Reading of 101.4608 C.

Minimum SP Pressure is 14.5772 psia at t plus 23.4023 s

Maximum SP Pressure is 39.5948 psia at t plus 31397.6508 s

Beginning SP Pressure is 14.6026 psia

Ending SP Pressure is 39.5933 psia

Time-Average SP Pressure is 23.0621 +/- 7.1829 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 77.3013 cm (cold) / 77.4171 cm (hot) at 14.5352 psia

Beginning Smoothed SP Level is 77.4816 cm (cold) / 77.6167 cm (hot) at 14.5987 psia

Ending Smoothed SP Level is 78.8823 cm (cold) / 80.2758 cm (hot) at 39.5891 psia

Minimum Smoothed Cold SP Level is 77.4169 cm at t plus 19138.8277 s and 24.1219 psia

Minimum Smoothed Hot SP Level is 77.6122 cm at t plus 42.1054 s and 14.5954 psia
 Maximum Smoothed Cold SP Level is 78.9679 cm at t plus 29185.9113 s and 35.8581 psia
 Maximum Smoothed Hot SP Level is 80.2794 cm at t plus 30826.2392 s and 38.567 psia
 SP 12 Temperature at the beginning is 35.0053 C, and at the end is 112.4948 C
 At plume detection, the Mixing Number is 47.8841

The Mixing Number ranges from a minimum of 31.346 at (KEY POINT #12) t plus 16.6109 s to a maximum of 245.9829 at (KEY POINT #13) t plus 31373.4515 s; it had a mean value of 95.1452 +/- 58.2319 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) gl, Sparger Diameter (m) dl, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality xl, Bounded Quality x2, Sparger Void Fraction vfl, Sparger fluid velocity (m/s) vl, Two phase Re re_tp, Pool Mid T T_{sat} Surface Tension (N/m) sigl, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) mdl, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) tl, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_{mid} Viscosity (Pa-s) mul, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) pl, Pool Airspace P p2, Approx Pool Mid P p3, T_{mid} Vapor Pressure p4, T_{Plume} Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) el, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 31.3518): 8.85144695 0.040894
 0.00925 0.3937 0.774815585 0.776167201 1.00379484
 1 1 14.6478339 29084.7682 0.0703301793 0.0587874192
 0.0116258131 -7.01938007e-006 0.0116258131 35.4499599 104.774786
 100.645227 35.2669174 35.5482218 35.7910568 33.1457519
 4.17887484 4.21746395 2.08006201 0.622666977 0.678021384
 0.678021384 4.78271276 1.74067693 0.0377080203 993.877852
 957.890036 0.611130484 0.603918825 0.00071264094 0.000279840253
 1.22913855e-005 1.24453827e-005 1522.93188 1544.49315 472.585242
 475.509961 1.03775545 1.00654739 1.04354739 0.0577020963
 0.0571224349 2685.36027 2685.14571 148.613894 421.821881
 2676.58922 273.207987 2263.53839 147.84898 149.022992
 150.040903 138.990181

KEY POINT #2 (t plus 8700.9447 s with a Mixing Number of 47.8841): 9.59622503
 0.040894 0.00925 0.3937 0.774903865 0.778467507
 1.00502958 1 1 13.75486 31022.2345
 0.0666443233 0.0579091928 0.0126040318 6.88554843e-006 0.0126040318
 57.6469674 110.573179 105.170999 59.6495713 57.8431002
 57.8259622 54.8411216 4.18177292 4.22346257 2.09902947
 0.64853704 0.679728958 0.679728958 3.11729659 1.65982964
 0.038434485 984.410443 954.581019 0.708893967 0.698041811
 0.000483451002 0.000267134905 1.24462437e-005 1.26498955e-005 1552.34468
 1539.94246 474.855923 478.669415 1.21619426 1.17529091
 1.21229091 0.178718546 0.196245321 2695.12737 2694.93817
 241.398518 440.935843 2683.65822 199.537325 2254.19153
 249.773735 242.217271 242.148559 229.671887

KEY POINT #3 (t plus 1785.2331 s with a Mixing Number of 33.6881): 9.03814845
 0.040894 0.00925 0.3937 0.776756462 0.778486913
 1.0053576 1 1 14.7706352 29500.3238
 0.0696188514 0.0586767087 0.0118710337 1.27706999e-005 0.0118710337
 39.8612946 107.046741 101.218398 39.6888117 40.0791628
 40.2118187 37.4793476 4.17854265 4.21819891 2.08237251
 0.628457714 0.67825149 0.67825149 4.35160121 1.73001164
 0.037797236 992.273059 957.476059 0.622866015 0.612558056
 0.000654485924 0.000278171561 1.23109729e-005 1.25288809e-005 1531.09898

1543.95043	472.876608	476.98027	1.05907695	1.0253472
1.0623472	0.0732999321	0.0726278674	2689.78109	2689.56292
167.049079	424.241014	2677.4909	257.191936	2265.54007
166.328351	167.957943	168.515352	157.101524	
KEY POINT #4 (t plus 4918.4833 s with a Mixing Number of 38.9251):				9.57763488
0.040894	0.00925	0.3937	0.776088908	0.778586356
1.00698612	1	1	14.9255859	30963.942
0.068297711	0.0583728038	0.0125796148	4.81467796e-006	0.0125796148
47.8859808	110.362779	102.787818	48.1407893	48.1827555
48.1938079	45.4779868	4.17913074	4.2202479	2.08883312
0.638146545	0.678860933	0.678860933	3.71131102	1.70145432
0.0380456092	988.987846	956.334946	0.65594272	0.641937987
0.000566711225	0.000273692658	1.23646439e-005	1.26491582e-005	1542.87246
1542.41414	473.668817	478.974057	1.11932002	1.08131913
1.11831913	0.111124156	0.112558392	2695.88552	2695.66274
200.586839	430.867239	2679.95039	230.2804	2265.01828
201.651721	201.825632	201.874856	190.529451	
KEY POINT #5 (t plus 4918.4833 s with a Mixing Number of 38.9251):				9.57763488
0.040894	0.00925	0.3937	0.776088908	0.778586356
1.00698612	1	1	14.9255859	30963.942
0.068297711	0.0583728038	0.0125796148	4.81467796e-006	0.0125796148
47.8859808	110.362779	102.787818	48.1407893	48.1827555
48.1938079	45.4779868	4.17913074	4.2202479	2.08883312
0.638146545	0.678860933	0.678860933	3.71131102	1.70145432
0.0380456092	988.987846	956.334946	0.65594272	0.641937987
0.000566711225	0.000273692658	1.23646439e-005	1.26491582e-005	1542.87246
1542.41414	473.668817	478.974057	1.11932002	1.08131913
1.11831913	0.111124156	0.112558392	2695.88552	2695.66274
200.586839	430.867239	2679.95039	230.2804	2265.01828
201.651721	201.825632	201.874856	190.529451	
KEY POINT #6 (t plus 17588.201 s with a Mixing Number of 88.2999):				9.80910747
0.040894	0.00925	0.3937	0.774361468	0.781256269
1.0002555	1	1	10.6704742	31483.0714
0.0624428489	0.0562755357	0.0128836394	1.46232866e-005	0.0128836394
81.2529731	113.732155	113.467466	93.4469246	81.7136946
74.0897712	67.6714783	4.19646154	4.23564742	2.13840395
0.667848281	0.682218998	0.682218998	2.19234108	1.52970401
0.0399054172	971.045148	948.278985	0.921019291	0.92031909
0.000348901381	0.000246383382	1.27310996e-005	1.27412487e-005	1556.83674
1530.07968	478.834162	479.02629	1.60894064	1.56544897
1.60244897	0.498721403	0.798858357	2696.97918	2696.86532
340.295867	476.053746	2696.29806	135.757879	2220.92544
391.53848	342.228014	310.258313	283.378562	
KEY POINT #7 (t plus 18411.8171 s with a Mixing Number of 93.7839):				9.85101667
0.040894	0.00925	0.3937	0.774224989	0.78147161
0.999702767	0.999702767	0.999999702	10.3894415	31560.0854
0.0620585625	0.0560830159	0.0129386844	1.22453158e-005	0.0129386844
83.3371755	114.435199	114.435199	95.6063229	83.7503854
80.283618	67.5503733	4.19831284	4.23717178	2.14341191
0.669182445	0.682456406	0.682456406	2.13379688	1.51588375
0.0400895202	969.723923	947.524262	0.948791317	0.949073131
0.000340112675	0.000244154504	1.2764392e-005	1.27644609e-005	1556.15352
1528.80616	479.28211	479.277814	1.66084705	1.61744429
1.65444429	0.541962716	0.86514722	2697.19265	2697.08471
349.048169	480.157185	2697.74385	131.109016	2217.03546
400.633263	350.781694	336.233977	282.875838	
KEY POINT #8 (t plus 23750.5085 s with a Mixing Number of 137.1581):				9.88862396
0.040894	0.00925	0.3937	0.780535556	0.790204112
0.995491771	0.995491771	0.999994525	8.64212589	31165.4502
0.0597760795	0.05486163	0.0129880792	6.30573355e-006	0.0129880792
95.491705	120.528329	120.528329	106.119915	96.1288229
95.4756223	68.4405822	4.21091225	4.24728319	2.1770652
0.675833418	0.683701257	0.683701257	1.84252492	1.43462625
0.041313041	961.598501	942.679237	1.13963591	1.14479065
0.000295717375	0.00023093722	1.29742454e-005	1.29754387e-005	1549.15191
1520.22128	482.022565	481.950635	2.02012201	1.97705753
2.01405753	0.861517503	1.25664388	2696.85417	2696.77948

400.17798	506.030636	2706.70061	105.852656	2190.82353
445.002964	402.859774	400.111628	286.632409	
KEY POINT #9 (t plus 24369.6199 s with a Mixing Number of 143.538):				10.0217448
0.040894	0.00925	0.3937	0.782676899	0.792717471
0.995317388	0.995317388	0.999994182	8.56444696	31522.1769
0.059506685	0.054710556	0.0131629249	4.31311638e-006	0.0131629249
96.9023023	121.276576	121.276576	107.42436	97.4860728
96.7486498	70.2603898	4.21257612	4.24858731	2.18145715
0.676483155	0.683824652	0.683824652	1.81350268	1.42529234
0.0414712	960.610253	942.073239	1.1650657	1.1705401
0.000291224177	0.000229405674	1.30000394e-005	1.30012985e-005	1548.02364
1519.10099	482.349434	482.273852	2.06830759	2.02523753
2.06223753	0.907079439	1.31405322	2697.56083	2697.48748
406.12271	509.212518	2707.78253	103.089809	2188.34832
450.518462	408.580806	405.476817	294.256708	
KEY POINT #10 (t plus 26532.8566 s with a Mixing Number of 164.0653):				11.3174859
0.040894	0.00925	0.3937	0.787617306	0.798917043
0.995103175	0.995103175	0.9999934	8.93464731	35344.4563
0.0585965787	0.0541638315	0.0148647986	1.14019925e-006	0.0148647986
101.632764	123.974795	123.974795	111.248308	102.177157
101.796277	92.0614742	4.21846589	4.2534066	2.19777915
0.678481729	0.684216638	0.684216638	1.72230173	1.39272164
0.0420564382	957.229755	939.868063	1.26059865	1.2667936
0.000277008346	0.000224037673	1.30930875e-005	1.30944798e-005	1543.79146
1514.94392	483.510271	483.427935	2.2499205	2.20708224
2.24408224	1.07471568	1.49492206	2701.00121	2700.92139
426.07756	520.695234	2711.65011	94.6176736	2180.30598
466.70403	428.372987	426.768694	385.762868	
KEY POINT #11 (t plus 31398.1489 s with a Mixing Number of 245.9767):				10.1130884
0.040894	0.00925	0.3937	0.788822594	0.80275799
0.988658526	0.988658526	0.999981175	6.52592889	31015.4346
0.0564340074	0.0527567729	0.013282899	6.81528223e-006	0.013282899
112.669346	130.852077	130.852077	120.548441	113.33915
113.010355	108.970263	4.2341232	4.26654293	2.24289134
0.682086194	0.684844644	0.684844644	1.54124	1.31684228
0.0436576399	948.952096	934.106948	1.53291733	1.55047312
0.00024828246	0.000211373095	1.33304277e-005	1.33341559e-005	1531.36511
1503.5375	486.340452	486.128275	2.77218507	2.72957406
2.76657406	1.56713998	2.0214051	2696.67576	2696.63318
472.757157	550.027232	2721.25813	77.2700752	2146.64853
506.168407	475.592312	474.202416	457.109873	
KEY POINT #12 (t plus 16.6109 s with a Mixing Number of 31.346):				8.85705877
0.040894	0.00925	0.3937	0.774783855	0.776135639
1.00388439	1	1	14.6722676	29095.3093
0.0703270624	0.0587890113	0.0116331839	-1.44666333e-006	0.0116331839
35.4694354	104.864429	100.636979	35.3818169	35.5988143
35.8139952	33.1663456	4.17887235	4.21745343	2.08002895
0.622693276	0.678018043	0.678018043	4.78066194	1.74083134
0.0377067422	993.871082	957.895983	0.610962934	0.603584776
0.000712365873	0.000279864397	1.22911037e-005	1.24487613e-005	1522.9707
1544.50089	472.581041	475.574022	1.03745125	1.00634236
1.04334236	0.0577640704	0.0574857076	2685.54998	2685.33471
148.695262	421.787072	2676.57624	273.091811	2263.76291
148.329114	149.234393	150.13674	139.076228	
KEY POINT #13 (t plus 31373.4515 s with a Mixing Number of 245.9829):				10.1333046
0.040894	0.00925	0.3937	0.788850767	0.802776094
0.988721298	0.988721298	0.999981302	6.55052237	31080.7767
0.0564356283	0.0527651844	0.0133094517	1.43077903e-005	0.0133094517
112.661175	130.81124	130.81124	120.541022	113.285114
112.887068	108.908946	4.23411131	4.2664612	2.24260834
0.682083893	0.684842473	0.684842473	1.54135984	1.31726464
0.0436476529	948.958281	934.141751	1.53117135	1.54860902
0.000248301625	0.000211444271	1.33290179e-005	1.33327222e-005	1531.37493
1503.6086	486.324199	486.113332	2.76881715	2.72620253
2.76320253	1.56671671	2.02093174	2696.75508	2696.71218
472.722319	549.852777	2721.20218	77.1304579	2146.90231
506.136662	475.363218	473.680107	456.850348	

KEY POINT #14 (t plus 20075.5453 s with a Mixing Number of 105.3569): 9.98248593

0.040894	0.00925	0.3937	0.774331328	0.782263829
0.999100848	0.999100848	0.999999044	9.92930058	31818.5801
0.0613197362	0.055705462	0.013111361	7.73225155e-006	0.013111361
87.3126934	116.327171	116.327171	100.256207	87.746219
86.6714653	67.2133022	4.20209428	4.24021587	2.1534655
0.671568125	0.682888968	0.682888968	2.02965183	1.48961253
0.0404574007	967.144308	946.036999	1.00504576	1.0059493
0.000324373844	0.000239902872	1.28295125e-005	1.28297296e-005	1554.41768
1526.24434	480.147906	480.134511	1.76629439	1.72282587
1.75982587	0.633174809	1.02348758	2698.6617	2698.56311
365.754312	488.184192	2700.55236	122.429879	2210.47751
420.23549	367.574798	363.061421	281.473425	

End

D.32 TEST #32 - T32_RCIC_STD_107KW_A_RESULTS_RCICLAND.TXT

Output Saved to C:\Local Files\RCICLAND_NOTITLES\Export\T32_RCIC_STD_107kW_A\
Using 20-second SP 12 averages for beginning detection
Beginning (KEY POINT #1) detected at t plus 1954.1718 s, and ending (KEY POINT #11) at t plus 11629.1311 s, for a time period of 9674.9593 s.
Original Data Record Time: 12941.0732 s
Bulk Pool to Outlet Thermal Stratification Detected beginning (KEY POINT #3) at t plus 2701.3515 s, T_bulk = 63.6862 C and T_out = 61.262 C
Stratification Beginning SP12 Temperature = 63.4018 C
Stratification Beginning Pressure = 17.8864 psia
Bulk Pool to Outlet Thermal Destratification Detected beginning (KEY POINT #9) at t plus 8695.3573 s, T_bulk = 116.0703 C and T_out = 73.9835 C
Stratification Ending SP12 Temperature = 115.8425 C
Stratification Ending Pressure = 42.6547 psia
Plume detected! Setting t_plume (KEY POINT #2) to 2213.4416 s.
At t = 2213.4416 s, the pool pressure is 17.1663 psia while the Smoothed Upper, Mid, SP8, Lower, and Outlet Temperatures are 59.8221, 59.8394, 61.8401, 59.7449, and 57.0339 C, respectively.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-SP9 temperatures were 10.9686 +/- 2.5661 C.
Over the Plume Period (Plume Detected to Destratification), the mean Smoothed SP8-Upper temperatures were 10.07 +/- 2.3683 C.
Minimum Steam Quality: 0.99525 at t plus 9513.5751 s
Maximum Steam Quality: 1.0039 at t plus 5638.2005 s
Time-Averaged Steam Quality: 1.0004 +/- 0.0013441
Minimum Turbine Outlet Steam Quality: 1.0001 at t plus 9513.5751 s
Maximum Turbine Outlet Steam Quality: 1.024 at t plus 934.4185 s
Time-Averaged Turbine Outlet Steam Quality: 1.0145 +/- 0.0066662
Smoothed Changerates may not fully include test beginning and end periods, analysis ending at t plus 9584.9852 s; using 300 s smoothing
Max and min smoothed upper level changerates: 0.77924 degrees/min at t plus 3928.0687 s and 0.3485 degrees/min at t plus 7716.6404 s, respectively
Max and min smoothed mid (SP9) level changerates: 0.71413 degrees/min at t plus 4253.5753 s and 0.34052 degrees/min at t plus 8787.1576 s, respectively
Max and min smoothed upper-mid level changerate differences: 0.32523 degrees/min at t plus 3885.8693 s and -0.13587 degrees/min at t plus 4478.0831 s, respectively
Max and min smoothed lower level changerates: 3.0133 degrees/min at t plus 6822.2252 s and 0.036062 degrees/min at t plus 3830.1681 s, respectively
Max and min smoothed mid-lower level changerate differences: 0.58748 degrees/min at t plus 5868.4057 s and -2.5671 degrees/min at t plus 6822.2252 s, respectively
Max and min smoothed outlet level changerates: 7.1719 degrees/min at t plus 9023.0791 s and -0.023147 degrees/min at t plus 5083.9898 s, respectively
Max and min smoothed lower-outlet level changerate differences: 2.979 degrees/min at t plus 6822.1242 s and -6.6032 degrees/min at t plus 9019.0658 s, respectively
Max and min smoothed hot (SP8) level changerates: 1.206 degrees/min at t plus 2633.9497 s and 0.17506 degrees/min at t plus 8093.2499 s, respectively

Max and min smoothed hot-mid (SP8-SP9) level changerate differences: 0.70373 degrees/min at t plus 2635.3487 s and -0.27746 degrees/min at t plus 4438.0849 s, respectively

The mean steam flow rate was 44.6769 +/- 0.96462 g/s
The mean feedwater flow rate was 44.2747 +/- 1.3646 g/s
The mean water injection to steam flow rate was 0.012706 +/- 0.026273 g/s
Mean Smoothed Condensing Region SP8-SP9 delta T is 11.5424 +/- 1.6214 C over the Stratification Period, beginning at 5.8519 C and ending at 12.4361 C
Mean Smoothed SP8-Upper Pool delta T is 10.5838 +/- 1.5711 C over the Stratification Period, beginning at 5.7071 C and ending at 11.3279 C
The stratification period begins and ends with Smoothed SP8 readings of 69.8175 and 128.4867 C, respectively
The stratification period begins and ends with condensing flows of 0.56653 and 1.3444 kg/s, respectively.
The stratification period begins and ends with condensing+cooling flows of 4.4037 and 1.8817 kg/s, respectively.
The stratification period had a mean sparger steam enthalpy of 2734.0399 +/- 0.84684 kJ/kg.
At plume detection, the condensing and condensing+cooling flows are 0.53105 and 13.0722 kg/s, respectively
The plume period had a mean steam enthalpy of 2734.8343 +/- 0.5093 kJ/kg.
Maximum Smoothed Top-Mid delta T is 2.1961 degrees C at t plus 4011.4715 s with T_upper = 76.7591 C and T_mid = 74.563 C
At t plus 4011.4715 s, Smoothed SP8-SP9 is 10.9754 C and Smoothed SP8-Top is 8.7793 C, where Smoothed SP8 is 85.5384 C and Pool P = 20.8173 psia
Maximum Smoothed Top-Lower delta T is 20.1396 degrees C at t plus 6540.0151 s with T_upper = 101.9118 C and T_low = 81.7722 C
At t plus 6540.0151 s, Smoothed SP8-SP9 is 12.6153 C and Smoothed SP8-Top is 11.8422 C, where Smoothed SP8 is 113.754 C and Pool P = 31.2785 psia
Maximum Smoothed Mid-Lower delta T is 19.3683 degrees C at t plus 6540.3181 s with T_mid = 101.141 C and T_low = 81.7728 C
At t plus 6540.3181 s, Smoothed SP8-SP9 is 12.6263 C and Smoothed SP8-Top is 11.8574 C, where Smoothed SP8 is 113.7673 C and Pool P = 31.2788 psia
Maximum Smoothed Top-Outlet delta T is 43.1546 degrees C at t plus 8676.7573 s with T_upper = 117.0273 C and T_out = 73.8726 C
At t plus 8676.7573 s, Smoothed SP8-SP9 is 12.5786 C and Smoothed SP8-Top is 11.4574 C, where Smoothed SP8 is 128.4847 C and Pool P = 42.5499 psia
Maximum Smoothed Mid-Outlet delta T is 42.1452 degrees C at t plus 8667.1607 s with T_mid = 115.9591 C and T_out = 73.8139 C
At t plus 8667.1607 s, Smoothed SP8-SP9 is 12.4101 C and Smoothed SP8-Top is 11.4321 C, where Smoothed SP8 is 128.3692 C and Pool P = 42.5049 psia
Maximum Smoothed Lower-Outlet delta T is 42.1033 degrees C at t plus 8699.7596 s with T_low = 116.1975 C and T_out = 74.0945 C
At t plus 8699.7596 s, Smoothed SP8-SP9 is 12.4388 C and Smoothed SP8-Top is 11.3697 C, where Smoothed SP8 is 128.5735 C and Pool P = 42.6806 psia
Maximum Smoothed Condensing Region SP8-SP9 delta T is 13.8692 degrees C at (KEY POINT #14) t plus 7691.6389 s with T_SP8 = 123.2067 C and T_SP9 = 109.3375 C and Pool P = 37.1837 psia
Maximum Smoothed Condensing Region SP8-Upper delta T is 12.9936 degrees C at t plus 7315.9625 s with T_SP8 = 120.711 C and T_upper = 107.7175 C and Pool P = 35.2766 psia
Maximum Top-Mid delta T is 2.8241 degrees C at (KEY POINT #4) t plus 4013.1715 s ignoring SP 4, with temperatures of 76.9067 and 74.0826 C, respectively, at Set # 2, where Pool P = 20.8168 psia and T_outlet = 67.9043 C
Top-Mid Reconvergence Detected at (KEY POINT #5) t plus 5122.393 s with a Smoothed Mid-Axis Top-Mid Delta T of 0.9996 C and a raw SP12 Reading of 86.5765 C.
Maximum Top-Lower delta T is 22.5262 degrees C at t plus 6644.6211 s, with temperatures of 103.088 and 80.5618 C, respectively, at Set # 1, where Pool P = 31.8519 psia and T_outlet = 71.947 C
Maximum Mid-Low delta T is 20.6545 degrees C at (KEY POINT #6) t plus 6616.0364 s ignoring SP 4, with temperatures of 101.7052 and 81.0507 C, respectively, at Set # 2, where Pool P = 31.6993 psia and T_outlet = 71.8616 C
Mid-Low Reconvergence Detected at (KEY POINT #7) t plus 6961.3292 s with a Smoothed Mid-Axis Mid-Low Delta T of 6.8836 C and a raw SP12 Reading of 104.308 C.
Maximum Top-Outlet delta T is 43.5673 degrees C at t plus 8683.4596 s, with temperatures of 117.4591 and 73.8918 C, respectively, at Set # 1, where Pool P = 42.5899 psia

Maximum Mid-Outlet delta T is 42.0022 degrees C at t plus 8686.1768 s ignoring SP 4, with temperatures of 115.9094 and 73.9072 C, respectively, at Set # 2, where Pool P = 42.6129 psia

Maximum Lower-Outlet delta T is 43.4992 degrees C at (KEY POINT #8) t plus 8670.9689 s, with temperatures of 117.3156 and 73.8164 C, respectively, at Set # 1, where Pool P = 42.5111 psia

Low-Outlet Reconvergence Detected at (KEY POINT #10) t plus 9079.9673 s with a Smoothed Mid-Axis Low-Outlet Delta T of 14.4908 C and a raw SP12 Reading of 118.3743 C.

Minimum SP Pressure is 15.1382 psia at t plus 6.4004 s

Maximum SP Pressure is 49.5608 psia at t plus 9674.9593 s

Beginning SP Pressure is 15.142 psia

Ending SP Pressure is 49.5608 psia

Time-Average SP Pressure is 26.6507 +/- 10.201 psia

SP Levels are fully corrected and compensated

Pre-Start SP Level is 78.6067 cm (cold) / 78.7386 cm (hot) at 14.5982 psia

Beginning Smoothed SP Level is 78.806 cm (cold) / 78.9919 cm (hot) at 15.1426 psia

Ending Smoothed SP Level is 77.9987 cm (cold) / 79.6061 cm (hot) at 49.5514 psia

Minimum Smoothed Cold SP Level is 77.9987 cm at t plus 9674.9593 s and 49.5514 psia

Minimum Smoothed Hot SP Level is 78.9359 cm at t plus 264.1111 s and 15.2993 psia

Maximum Smoothed Cold SP Level is 78.8063 cm at t plus 3.1012 s and 15.1442 psia

Maximum Smoothed Hot SP Level is 79.6803 cm at t plus 7491.5355 s and 36.1836 psia

SP 12 Temperature at the beginning is 40.8764 C, and at the end is 122.8031 C

At plume detection, the Mixing Number is 44.7729

The Mixing Number ranges from a minimum of 33.1644 at (KEY POINT #12) t plus 0 s to a maximum of 243.5675 at (KEY POINT #13) t plus 9674.9593 s; it had a mean value of 98.2305 +/- 60.6178 over the test period.

Key Points have Data Dumps of the following for each Key Point: Sparger Massflux (kg/m²-s) gl, Sparger Diameter (m) dl, Water Injection Pipe Diameter d2, Sparger Outlet Elevation d3, Pool Cold Level d4, Pool Hot Level d5, Sparger Steam Quality x1, Bounded Quality x2, Sparger Void Fraction vfl, Sparger fluid velocity (m/s) v1, Two phase Re re_tp, Pool Mid T Tsat Surface Tension (N/m) sig1, Sparger P Psat Surface Tension sig2, Steam at Flowmeter mdot (kg/s) mdl, Water mdot to Steam md2, Sparger mdot md3, Pool Mid T (C) t1, Estimated Sparger Steam T t2, Sparger Saturation T t3, Smoothed Plume T t4, Upper-Level Pool Rear Smoothed T t5, Lower-Level Pool Rear Smoothed T t6, Pool Outlet Smoothed T t7, Pool Mid Heat Capacity (kJ/kg-K) cp1, Sparger Sat Water Heat Capacity cp2, Sparger Sat Steam Heat Capacity cp3, Pool Mid Thermal Conductivity (W/m-K) k1, Sparger Sat Water Thermal Conductivity k2, Sparger Sat Steam Thermal Conductivity k3, Pool Mid Water Pr pr1, Sparger Sat Water Pr pr2, Sparger Sat Steam Pr pr3, Pool Mid Density (kg/m³) rho1, Sparger Sat Water Density rho2, Sparger Sat Steam Density rho3, Sparger Steam Density rho4, Sparger Subcooled T_mid Viscosity (Pa-s) mu1, Sparger Sat Water Viscosity mu2, Sparger Sat Steam Viscosity mu3, Sparger Steam Viscosity mu4, Pool Mid Sonic Velocity (m/s) cs1, Sparger Sat Water Sonic Velocity cs2, Sparger Sat Steam Sonic Velocity cs3, Sparger Sonic Velocity cs4, Sparger P (bar) p1, Pool Airspace P p2, Approx Pool Mid P p3, T_mid Vapor Pressure p4, T_Plume Vapor Pressure p5, Sparger Total Stagnation h (kJ/kg) e1, Sparger Steam Flowing h e2, Pool Mid h e3, Sparger Water Sat h e4, Sparger Steam Sat h e5, Pool Mid Subcooling delta h e6, Steam Condensation delta h e7, Smooth Plume Enthalpy e8, Pool Rear Upper Smoothed Enthalpy e9, Pool Rear Lower Smoothed Enthalpy e10, Pool Outlet Smoothed Enthalpy e11

KEY POINT #1 (t plus 0 s with a Mixing Number of 33.1644): 32.80995373 0.040894

0.00925	0.3937	0.7880599336	0.7899191954	1.020410194
1	1	53.24343762	101551.1707	0.06956965481
0.0583732639	0.04309378937	1.63106753e-005	0.04309378937	40.16396699
125.1571847	102.7854462	40.43445979	40.11370202	39.89608901
37.65113799	4.178533363	4.220244767	2.088823208	0.6288435919
0.6788600348	0.6788600348	4.324377485	1.701496771	0.03804522926
992.160429	956.3366785	0.6558916774	0.6164585443	0.0006507922358
0.0002736993281	1.236456276e-005	1.321235628e-005	1531.616427	
1542.416514	473.6676261	488.7936379	1.119226894	1.04404443
1.08104443	0.07449225453	0.07557194351	2728.685897	2725.851033
168.3154639	430.8572225	2679.946682	262.5417586	2297.828674
169.4457268	168.1039237	167.1977222	157.8210413	

KEY POINT #2 (t plus 2213.4416 s with a Mixing Number of 44.7729): 33.68821498

0.040894	0.00925	0.3937	0.7868786938	0.7909158031
1.020487821	1	1	48.63508038	103311.2465
0.0662660613	0.05767614921	0.0442473297	9.184716526e-006	0.0442473297

59.83944234	128.5833492	106.3640298	61.84008672	59.82205134
59.74490196	57.03394964	4.1826508	4.225119024	2.10431373
0.6506685008	0.6801376599	0.6801376599	3.005310885	1.639746332
0.03863460483	983.3023639	953.6934801	0.7366782287	0.6928169461
0.000467517185	0.0002639578262	1.248713504e-005	1.333490699e-005	
1553.800379	1538.643262	475.4428994	490.4868707	1.267227256
1.183545357	1.220545357	0.197980526	0.2170726895	2733.750197
2731.384826	250.5685847	445.979315	2685.501889	195.4107302
2287.770882	258.9374557	250.494416	250.1746701	238.8411193
KEY POINT #3 (t plus 2701.3515 s with a Mixing Number of 48.3268): 33.66537618				
0.040894	0.00925	0.3937	0.7868468087	0.7914691163
1.020176924	1	1	47.15887766	103108.0879
0.06554744288	0.05749735234	0.0442173324	1.862756065e-005	0.0442173324
63.96555427	129.0934705	107.277156	69.81747139	64.11033093
63.70506808	61.29138746	4.184571106	4.226408296	2.108441303
0.6544872075	0.6804388942	0.6804388942	2.811861085	1.624702177
0.03879028348	981.1366769	953.0099044	0.7585364665	0.7141721805
0.0004397887055	0.000261572114	1.251845027e-005	1.33521232e-005	
1555.924549	1537.621363	475.8888329	490.6774283	1.307468513
1.232918172	1.269918172	0.2390493838	0.3095514747	2734.268327
2732.044367	267.834627	449.8409267	2686.90725	182.0062997
2284.4274	292.3318434	268.4390482	266.7461185	256.6514246
KEY POINT #4 (t plus 4013.1715 s with a Mixing Number of 60.4446): 34.13431466				
0.040894	0.00925	0.3937	0.7858982686	0.7923887331
1.017928652	1	1	41.74750414	104229.5827
0.06365817109	0.05669904614	0.0448332533	6.098129919e-007	0.0448332533
74.58409468	130.4377023	111.3313816	85.47440632	76.77608419
73.02341779	67.94185115	4.191137404	4.232359976	2.127665379
0.6631872073	0.6816560328	0.6816560328	2.400401725	1.561163688
0.03950857364	975.126918	949.9304531	0.862044969	0.8176483758
0.0003798290447	0.0002514381226	1.265765653e-005	1.339244222e-005	
1557.927289	1532.801281	477.8333272	490.8888218	1.499067219
1.435576879	1.472576879	0.3792867226	0.5895219472	2734.738588
2732.995733	312.3180423	467.0016468	2693.085059	154.6836045
2267.736941	358.0088059	321.5054057	305.7793705	284.4998272
KEY POINT #5 (t plus 5122.393 s with a Mixing Number of 80.9034): 34.91678199				
0.040894	0.00925	0.3937	0.7855352791	0.7938135772
1.015598562	1	1	36.73264136	106157.2549
0.06144810532	0.05577411016	0.04586097442	1.738503914e-007	0.04586097442
86.62487943	132.3186498	115.9837388	97.21876077	87.60747789
79.25172467	70.74187287	4.201420567	4.239656983	2.151614491
0.6711692073	0.6828135443	0.6828135443	2.047012932	1.494309221
0.04038983287	967.5963203	946.30812	0.9946388987	0.9505691142
0.0003270065504	0.0002406644169	1.281768879e-005	1.34506764e-005	
1554.754306	1526.716394	479.9917309	491.2724657	1.746756897
1.68568188	1.72268188	0.6165359273	0.9175707788	2735.918217
2734.56893	362.8613854	486.7266695	2700.044357	123.8652841
2249.191547	407.4301557	366.9888499	331.910445	296.2455313
KEY POINT #6 (t plus 6616.0364 s with a Mixing Number of 125.1763): 34.42187643				
0.040894	0.00925	0.3937	0.7847472083	0.7958652135
1.010628369	1	1	28.24675616	104182.5689
0.05857940942	0.05418832042	0.0452109474	1.124056638e-005	0.0452109474
101.7214975	134.6161052	123.854255	114.419825	102.5485956
83.00310555	71.92953599	4.21858694	4.253187365	2.197033663
0.6785151447	0.6842008899	0.6842008899	1.720684699	1.394141255
0.04202978903	957.1649804	939.967241	1.256200273	1.218916408
0.0002767539567	0.000224272435	1.308892965e-005	1.35113602e-005	
1543.700292	1515.133516	483.4590125	491.0968078	2.241539153
2.185092089	2.222092089	1.078089283	1.660011809	2735.566264
2734.768385	426.4502399	520.181961	2711.478477	93.73172113
2215.384303	480.1322652	429.9386055	347.6919118	301.2610395
KEY POINT #7 (t plus 6961.3292 s with a Mixing Number of 136.1769): 34.1864965				
0.040894	0.00925	0.3937	0.7846293809	0.7963934631
1.009318937	1	1	26.58783071	103426.6198
0.05805226366	0.05383598476	0.04490179083	1.869802967e-005	0.04490179083
104.4369467	134.9436638	125.5856895	117.8535403	105.3776217
96.24332838	72.14233982	4.222190709	4.256372185	2.207889843

0.6795356273	0.6844113284	0.6844113284	1.672365901	1.374057933
0.04241717527	955.1778884	938.5366884	1.320580017	1.286330308
0.0002691570064	0.000220944216	1.314866109e-005	1.351704803e-005	
1540.96124	1512.375589	484.1898674	490.8864131	2.364400354
2.308555994	2.345555994	1.185645866	1.855305442	2735.014937
2734.308024	437.9196299	527.5573047	2713.933325	89.63767478
2207.457632	494.6992776	441.8906875	403.369883	302.1625467
KEY POINT #8 (t plus 8670.9689 s with a Mixing Number of 194.3171): 34.47857482				
0.040894	0.00925	0.3937	0.7818464342	0.7960722388
1.004994035	1	1	21.28030361	103599.9227
0.05578340656	0.05223875871	0.04528541714	1.922033254e-005	0.04528541714
115.9372115	138.1859942	133.3607342	128.4682863	116.9645074
115.892045	73.83548443	4.239289146	4.271652155	2.26062793
0.6828768032	0.6849426769	0.6849426769	1.494893055	1.29149925
0.04428245389	946.3998493	931.955354	1.64328906	1.620898323
0.0002408016428	0.0002070868416	1.341704316e-005	1.360972868e-005	
1527.041818	1499.094285	487.3260974	490.9182626	2.985546773
2.93187807	2.96887807	1.74412367	2.581067935	2735.929137
2735.476285	486.6165423	560.7512031	2724.669601	74.13466078
2175.177933	539.8757616	490.9711924	486.4263543	309.3069184
KEY POINT #9 (t plus 8695.3573 s with a Mixing Number of 194.861): 34.48959795				
0.040894	0.00925	0.3937	0.7818262266	0.7960988348
1.004971116	1	1	21.22203964	103612.4531
0.05576075138	0.05221690525	0.04529989533	1.52418031e-005	0.04529989533
116.0505898	138.2670156	133.4663012	128.4866616	117.1587208
116.0673718	74.04391359	4.239472405	4.271871002	2.261389485
0.6829021125	0.6849452807	0.6849452807	1.493337614	1.290458341
0.04430923793	946.3105402	931.8642264	1.648069941	1.625725098
0.0002405496048	0.0002069101221	1.34206883e-005	1.361243341e-005	
1526.887169	1498.904063	487.3670207	490.9425437	2.994808579
2.941167329	2.978167329	1.750546039	2.582499072	2736.017957
2735.567582	487.0978568	561.2027777	2724.812029	74.10492091
2174.815179	539.9547046	491.7955367	487.1702864	310.1810564
KEY POINT #10 (t plus 9079.9673 s with a Mixing Number of 212.7324): 34.27586652				
0.040894	0.00925	0.3937	0.7813015169	0.7963316473
1.003753362	1	1	19.98253608	102850.5202
0.05523229313	0.05183365248	0.04501917267	1.661252027e-005	0.04501917267
118.6875121	138.9007005	135.3142291	130.3924866	120.0039415
119.2420592	103.8079016	4.243835314	4.27575297	2.274919564
0.6834454802	0.684971042	0.684971042	1.458117496	1.272561335
0.0447845923	944.2150227	930.2613895	1.733585511	1.715924071
0.0002348215091	0.0002038629616	1.348449824e-005	1.362829553e-005	
1523.183172	1495.532147	488.0760997	490.780938	3.160738423
3.107642131	3.144642131	1.905467888	2.734472158	2735.78992
2735.390619	498.2945023	569.1114772	2727.290193	70.81697492
2166.678443	548.0917329	503.8814801	500.6494305	435.3279421
KEY POINT #11 (t plus 9674.9593 s with a Mixing Number of 243.5675): 35.05771019				
0.040894	0.00925	0.3937	0.7799869868	0.7960607647
1.002134922	1	1	18.64131533	104821.6095
0.05434288241	0.05115963256	0.04604607465	8.060347328e-006	0.04604607465
123.0927817	140.5495616	138.5486426	134.2357791	124.7627974
124.4340637	119.1459569	4.251501994	4.282784812	2.299510559
0.684175195	0.6849263276	0.6849263276	1.403136772	1.242659245
0.04564663633	940.6478101	927.4210386	1.891822092	1.880974943
0.0002258005232	0.0001987328503	1.359619023e-005	1.367704624e-005	
1516.597833	1489.440358	489.2839192	490.8255199	3.469014281
3.416445369	3.453445369	2.189178547	3.063022949	2736.492739
2736.14524	517.027997	582.9725646	2731.558178	65.94456754
2153.520175	564.5209875	524.1294122	522.733318	500.2664478
KEY POINT #12 (t plus 0 s with a Mixing Number of 33.1644): 32.80995373 0.040894				
0.00925	0.3937	0.7880599336	0.7899191954	1.020410194
1	1	53.24343762	101551.1707	0.06956965481
0.0583732639	0.04309378937	1.63106753e-005	0.04309378937	40.16396699
125.1571847	102.7854462	40.43445979	40.11370202	39.89608901
37.65113799	4.178533363	4.220244767	2.088823208	0.6288435919
0.6788600348	0.6788600348	4.324377485	1.701496771	0.03804522926
992.160429	956.3366785	0.6558916774	0.6164585443	0.0006507922358

0.0002736993281	1.236456276e-005	1.321235628e-005	1531.616427	
1542.416514	473.6676261	488.7936379	1.119226894	1.04404443
1.08104443	0.07449225453	0.07557194351	2728.685897	2725.851033
168.3154639	430.8572225	2679.946682	262.5417586	2297.828674
169.4457268	168.1039237	167.1977222	157.8210413	
KEY POINT #13 (t plus 9674.9593 s with a Mixing Number of 243.5675): 35.05771019				
0.040894	0.00925	0.3937	0.7799869868	0.7960607647
1.002134922	1	1	18.64131533	104821.6095
0.05434288241	0.05115963256	0.04604607465	8.060347328e-006	0.04604607465
123.0927817	140.5495616	138.5486426	134.2357791	124.7627974
124.4340637	119.1459569	4.251501994	4.282784812	2.299510559
0.684175195	0.6849263276	0.6849263276	1.403136772	1.242659245
0.04564663633	940.6478101	927.4210386	1.891822092	1.880974943
0.0002258005232	0.0001987328503	1.359619023e-005	1.367704624e-005	
1516.597833	1489.440358	489.2839192	490.8255199	3.469014281
3.416445369	3.453445369	2.189178547	3.063022949	2736.492739
2736.14524	517.027997	582.9725646	2731.558178	65.94456754
2153.520175	564.5209875	524.1294122	522.733318	500.2664478
KEY POINT #14 (t plus 7691.6389 s with a Mixing Number of 157.617): 34.35908956				
0.040894	0.00925	0.3937	0.7836062695	0.7964596392
1.007348434	1	1	24.13439553	103676.6953
0.05709255659	0.05314662014	0.04512848084	1.20489133e-005	0.04512848084
109.3375261	136.2169209	128.9560082	123.2067284	110.3770482
108.5171097	72.5539576	4.229105265	4.262795833	2.229943215
0.6811522316	0.6847243012	0.6847243012	1.591701253	1.336795397
0.04320007067	951.5090112	935.7153953	1.453521147	1.424036624
0.0002563641225	0.0002147267498	1.326497375e-005	1.355252117e-005	
1535.480771	1506.796584	485.5788145	490.8579704	2.619272675
2.564393276	2.601393276	1.402146285	2.196949718	2735.223954
2734.641485	458.646306	541.9307981	2718.646038	83.28449212
2193.293156	517.4532808	463.0421142	455.1784961	303.9077334

End